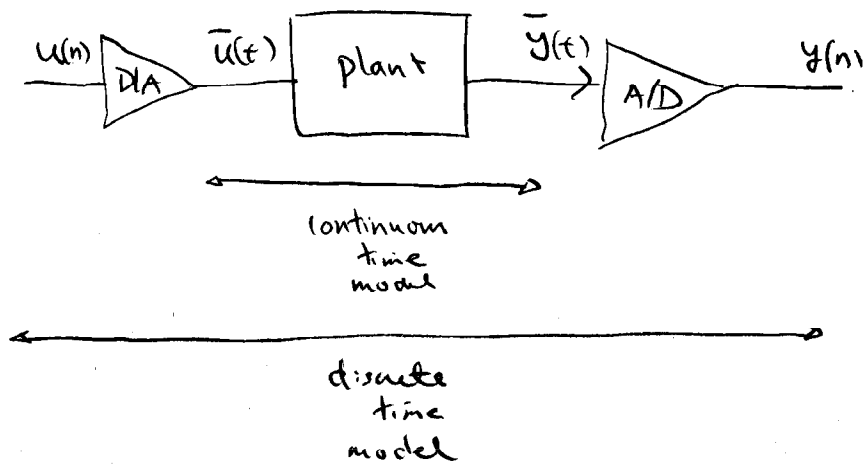
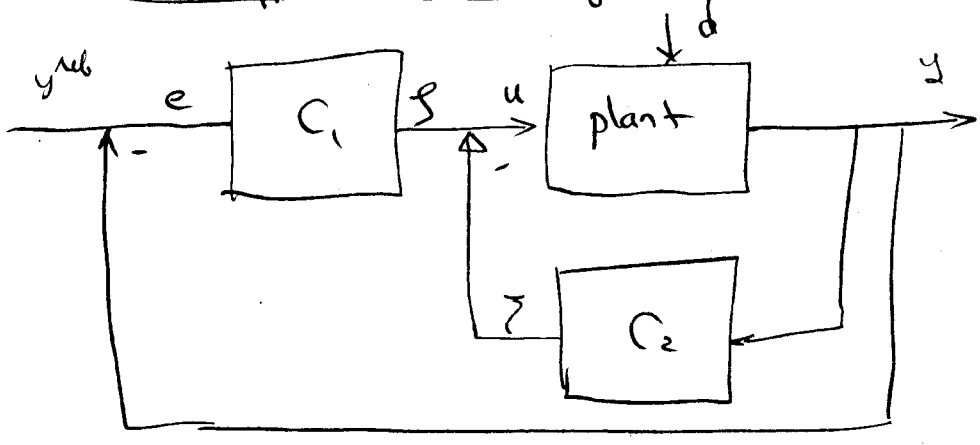


Real-time process =



A typical control system:



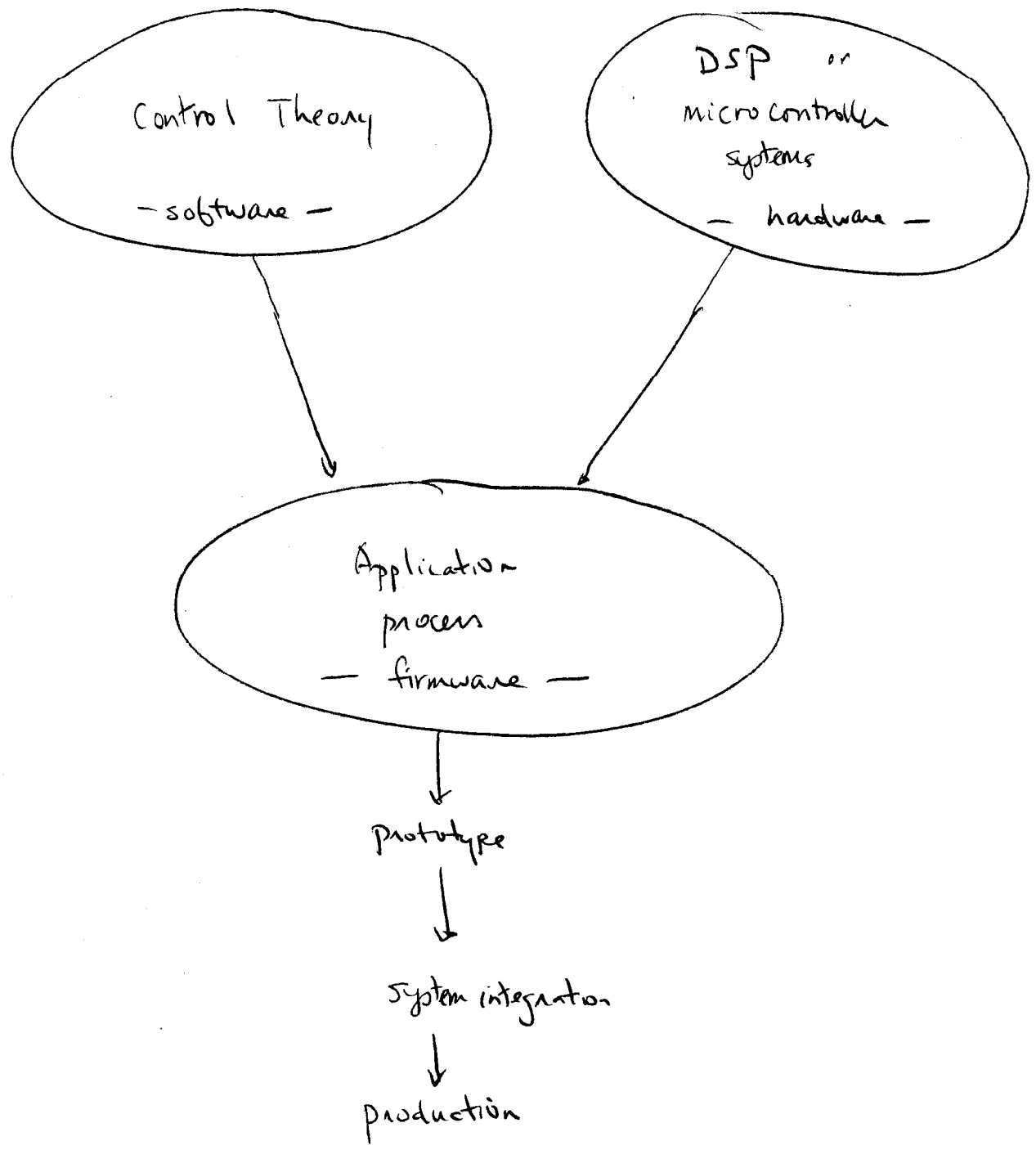
Design C_1 , C_2 so that one or more of the following conditions are met:

- a) closed loop stability
- b) reduce steady state error ($|e| \rightarrow 0$)
- c) disturbance rejection ($|e| \rightarrow 0$ despite presence of d)
- d) good transient characteristics
- e) robust wrt plant parameter variations

Why discrete time

- a) Can implement complex algorithms (& get better results)
- b) Performance is consistent and less susceptible to environment
- c) Low cost (in large quantity)
- d) Flexible
- e)

The Elements



The gateway = sampling } Poisson's theorem
 reconstruction }

zero order
hold
approx

Shannon's theorems

- sampling = $2 \times W_c$

- reconstruction =

$$\bar{y}(t) = \sum_{n=-\infty}^{\infty} y(nT_s) \text{sinc}\left(\frac{t-nT_s}{T_s}\right)$$

$$\bar{Y}(s) = G_{ho}(s) Y^*(s)$$

$$Y^*(s) = \sum_{n=0}^{\infty} y(nT_s) e^{-s n T_s}$$

$$G_{ho} = \frac{1 - e^{-s T_s}}{s}$$

↓ on letting $z = e^{s T_s}$

$$Y(z) = \sum_{n=0}^{\infty} y(n) z^{-n}$$

↑ to mean $y(nT_s)$

$$\dot{\bar{x}} = \bar{A}\bar{x} + \bar{B}u$$

$$\bar{y} = \bar{C}\bar{x} + \bar{D}u$$

$\xrightarrow{\frac{1}{T_s}}$

$$x(n+1) = A x(n) + B u(n)$$

$$y(n) = C x(n) + D u(n)$$

$$A = e^{\bar{A} T_s}, \quad B = \int_0^{T_s} e^{\bar{A} \tau} \bar{B} d\tau$$

↓

↕

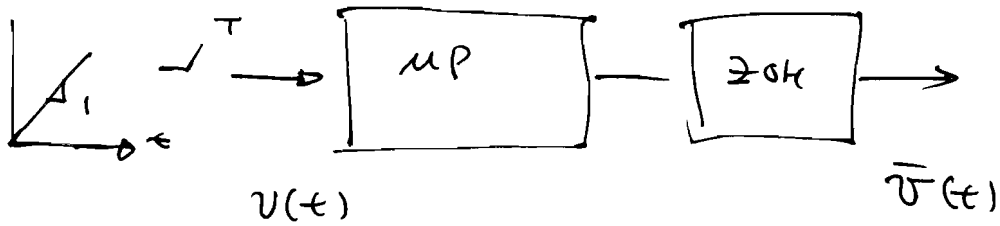
$$\bar{G}(s) = \bar{D} + \bar{C} (sI - \bar{A})^{-1} \bar{B}$$

$\xrightarrow{\frac{1}{T_s}}$

$$G(z) = C (zI - A)^{-1} B + D$$

$$G(z) = Z\left(\frac{\bar{G}(s)}{s}\right) (1 - z^{-1})$$

Example : ramp input with ZOH (The DeBella problem)



$$v(t) = t$$

$$\bar{v}(t) = nT$$

$$n = 0, 1, 2, \dots$$

Frequency domain

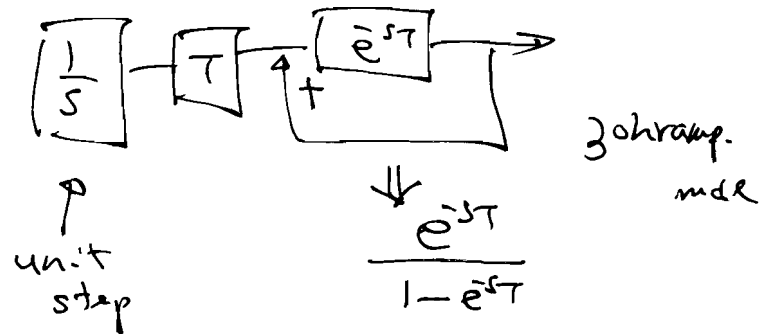
$$Z(t) = \frac{Tz}{(z-1)^2} \quad \leftarrow \text{from table, for signals}$$

but $z = e^{sT}$

\therefore overall:

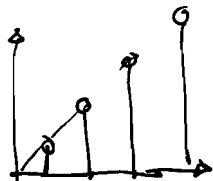
$$\underbrace{\frac{T e^{sT}}{(1 - e^{-sT})^2}}_{\text{ramp}} \cdot \underbrace{\frac{1 - e^{-sT}}{s}}_{\text{ZOH}} = \frac{T e^{-sT}}{s(1 - e^{-sT})}$$

simulation realization:

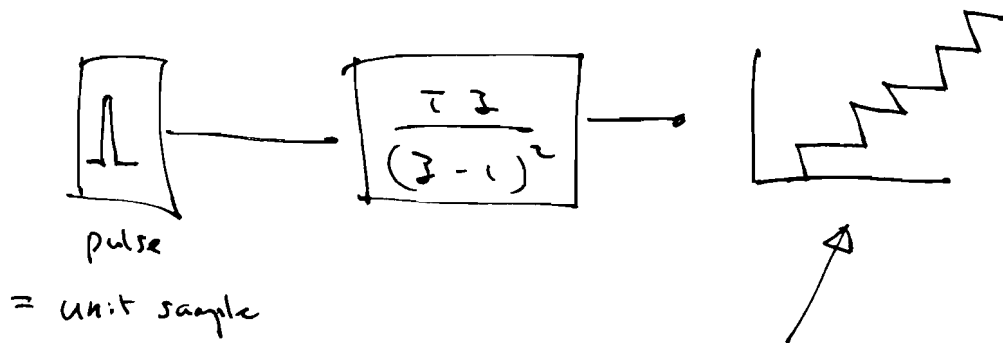


Discrete time approach

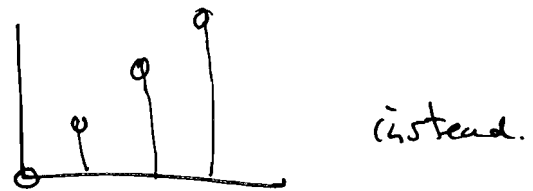
$$\left[\frac{Tz}{(z-1)^2} \right] \longrightarrow \left[\frac{1 - e^{-sT}}{s} \right]$$



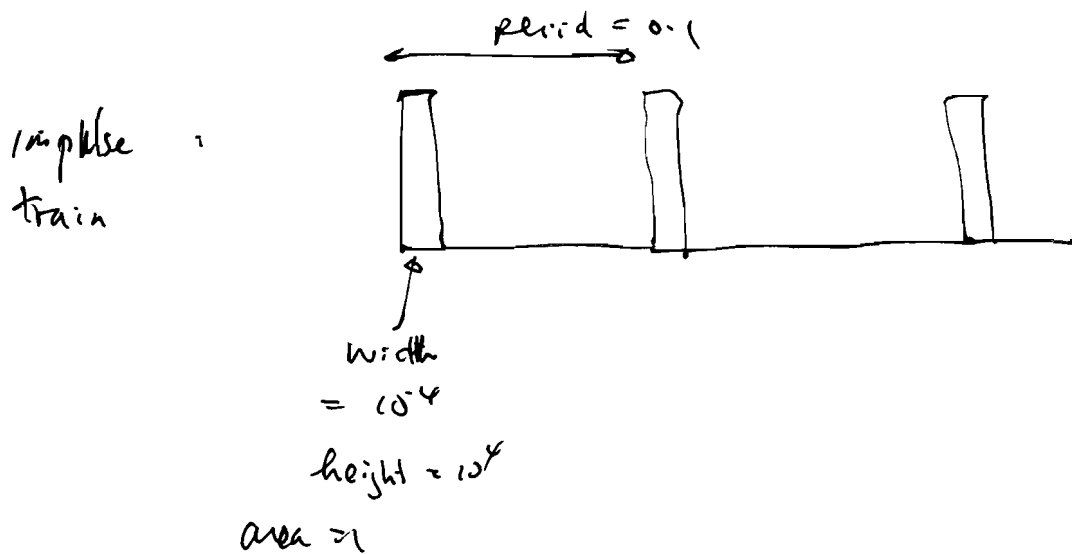
Matlab/Simulink



This is not a correct interpretation of the discrete time signal, which should



zoh ramp. mdl : $T = 0.15$



Basic Properties

- o Model conversion / coordinate transformation
- o Frequency response
- o Stability / speed of response
- o Time / Frequency Domain Solutions

Intermediate Properties

- o System with delay
- o Controllability / Observability
- o Pole placement / observer design
- o Selection of sampling rate
- o Implementation Issue

Control Properties

- o Parameter optimized : eg PID
- o State - observer based
Industrial regulator
LQR
- o Feedforward / deadbeat / Smith predictor / Shaping

$$\dot{x} = \overbrace{\begin{pmatrix} 0 & 1 \\ -2 & 0 \end{pmatrix}}^{A_c} x + \overbrace{\begin{pmatrix} 0 \\ 1 \end{pmatrix}}^{B_c} u$$

$$y = (1 \quad 0) x$$

continuous time eigenvalues: $\pm j\sqrt{2}$ undamped

(I) Convert to discrete time with $T_s = 0.15$

$$A = e^{A_c T_s}$$

$$= \left(\begin{array}{c|c} s & -1 \\ \hline 2 & s \end{array} \right) \Big|_{t=0.1} = \left(\begin{array}{cc} \cos \sqrt{2} t & \frac{1}{\sqrt{2}} \sin \sqrt{2} t \\ \sqrt{2} \sin \sqrt{2} t & \cos \sqrt{2} t \end{array} \right) \Big|_{t=0.1}$$

$$= \begin{pmatrix} 0.9900 & 0.0997 \\ -0.1993 & 0.9900 \end{pmatrix}$$

$$B = \int_0^{T_s} e^{A t} dt B_c = \begin{pmatrix} 0.00499 \\ 0.09967 \end{pmatrix}$$

(II) Pole placement

$$\text{eig}(A) = 0.99 \pm j 0.14$$

Desired: $\frac{1}{2}, \frac{1}{2} \rightarrow$ continuous time: -6.93 U-da

controllability $M_c = [B \quad AB] = \begin{bmatrix} 0.0050 & 0.0149 \\ 0.0997 & 0.0977 \end{bmatrix}$

rank $M_c = 2$

controllable

$$W_c^{-1} = \begin{bmatrix} -98.1668 & 14.9499 \\ 100.1668 & -5.0167 \end{bmatrix} \leftarrow e_i'$$

$$P = \begin{bmatrix} 100.1668 & -5.0167 \\ 100.1688 & +5.0167 \end{bmatrix}$$

Old characteristic poly = $z^2 - 1.98z + 1$

New " " " " " $z^2 - z + 0.25$

$$\therefore K = \begin{bmatrix} +0.25 & -1 & -1+1.98 \end{bmatrix} P$$

$$= \begin{bmatrix} 23.038 & 8.6789 \end{bmatrix}$$

check eig(A-BK) = 0.5041, 0.4959 \approx 0.5, 0.5 OK

U-do Find K so that eig(A-BK) = 0, 0
 ans: [98.17 14.95]
 deadbeat response

(II) Industrial Regulator

$$\left. \begin{aligned} x(n+1) &= Ax(n) + Bu(n) \\ y(n) &= Cx(n) \\ e(n) &= y^{\text{ref}} - y(n) \\ y(n+1) &= y(n) + e(n) \end{aligned} \right\} \begin{bmatrix} x(n+1) \\ y(n+1) \end{bmatrix} = A \begin{bmatrix} x(n) \\ y(n) \end{bmatrix} + B u(n)$$

$$A = \begin{pmatrix} A & 0 \\ -C & 1 \end{pmatrix} \quad B = \begin{pmatrix} B \\ 0 \end{pmatrix}$$

eigenvalue = $0.99 \pm j0.14$, 1
to shift to 0.5, 0.5, 0.5

$$M_c = [B \quad AB \quad A^2B] = \begin{bmatrix} 0.005 & 0.0149 & 0.0245 \\ 0.0997 & 0.0977 & 0.0937 \\ 0 & -0.005 & -0.0199 \end{bmatrix}$$

rank = 3 OK

$$M_c^{-1} = \begin{bmatrix} \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot \\ -50.08 & 2.508 & -100.17 \end{bmatrix}$$

← e_3'

↖ u-do

$$P = \begin{bmatrix} e_3' \\ e_3'A \\ e_3'A^2 \end{bmatrix} = \begin{bmatrix} -50.08 & 2.508 & -100.17 \\ 50.08 & -2.508 & -100.17 \\ 150.25 & 2.508 & -100.17 \end{bmatrix}$$

u-d. $PAP^T = ?$

Old C.P. = $z^3 - 2.98z^2 + 2.98z - 1$

New C.P. = $z^3 - 1.5z^2 + 0.75z - 0.125$

$$\therefore K = \begin{bmatrix} -0.125 + 1 & 0.75 - 2.98 & -1.5 + 2.98 \end{bmatrix} P \\ = \begin{bmatrix} 66.86 & 11.50 & -12.52 \end{bmatrix}$$

Check $\text{eig}(A - BK) = 0.51 \pm j0.02, 0.48 \approx 0.5, 0.5, 0.5$

$$\therefore u(n) = -66.86 x_1(n) - 11.5 x_2(n) + 12.52 z(n)$$

U-do

ans

place all poles to 0, 0, 0

$$K = [248.42 \quad 17.46 \quad -100.17]$$

(IV) Observer design

$$\hat{x}(n+1) = A\hat{x}(n) + Bu(n) + L[y(n) - C\hat{x}(n)]$$

Design L so that $(A-LC)$ has eigenvalues twice as fast as closed loop plant (0.5, 0.5)

$$0.5 \rightarrow -6.93$$

$$\text{twice as fast} = -13.86 \rightarrow \lambda = \frac{1}{4}$$

U-do

twice as fast

$$\lambda = \frac{1}{8} \quad \underline{\text{not}} \quad \frac{1}{6}$$

Using duality

$$\text{let } B_{\text{dual}} = C' = \begin{pmatrix} 1 \\ 0 \end{pmatrix}$$

$$A_{\text{dual}} = A' = \begin{pmatrix} 0.99 & -0.1993 \\ 0.0997 & 0.9900 \end{pmatrix}$$

Find K_{dual} so that $(A_{\text{dual}} - B_{\text{dual}} K_{\text{dual}})$ has eigenvalues at 0.25, 0.25

U-d.

$$K_{\text{dual}} = [1.4800 \quad 5.2952]$$

then $L = K_{\text{desired}} = \begin{bmatrix} 1.48 \\ 5.30 \end{bmatrix}$

check $\text{eig}(A-LC) = 0.25, 0.25$ checks

U-ds Find L to shift ^{observed} eigenvalues to 0,0
ans $L = \begin{bmatrix} 1.9800 \\ 9.6347 \end{bmatrix}$

(V) Combined control and estimation

(A) State feedback only

$$x(n+1) = Ax(n) + Bu(n)$$

$$y(n) = Cx(n)$$

$$\hat{x}(n+1) = A\hat{x}(n) + Bu(n) + L(y(n) - C\hat{x}(n))$$

$$u(n) = -K\hat{x}(n)$$

$$\left[\begin{array}{l} \hat{x}(n+1) = (A - BK - LC)\hat{x} + Ly(n) \\ u(n) = -K\hat{x}(n) \end{array} \right] \text{controller}$$

(B) Industrial regulator

$$\text{add } \zeta(n+1) = \zeta(n) + e(n)$$

$$e(n) = y_{\text{sub}} - y(n)$$

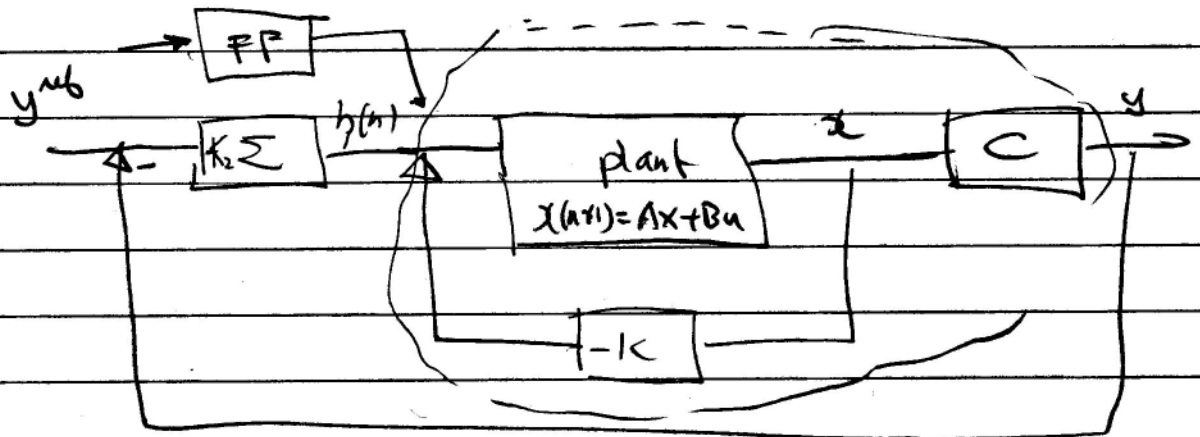
$$\hat{x}(n+1) = (A - BK_1 - LC)\hat{x}(n) - BK_2\zeta(n) + Ly(n)$$

$$u(n) = -K_1\hat{x}(n) - K_2\zeta(n)$$

where $K = [K_1 \quad | \quad K_2]$

controller

(8) Feedforward control



$$\begin{aligned} \eta(n) \text{ seen } \quad & x(n+1) = (A - BK)x(n) + Bv(n) \\ & y(n) = Cx(n) \\ & v(n) = -K_f \eta(n) \end{aligned}$$

$$\begin{aligned} \therefore \text{DC gain } & C(zI - A + BK)^{-1}B \Big|_{z=1} \\ & = 0.0399 \end{aligned}$$

$$\therefore \text{ set } \boxed{\text{FF}} \text{ to } \frac{1}{0.0399} = 25.04$$

to help $\eta(n)$ to reach the "right" steady state =

$$y(\infty) = 1$$

$$\Rightarrow \eta(\infty) = 25.04 \quad ! \quad (U-d0)$$

(XV) Input shaping

continuous time $\frac{1}{s^2 + 2}$

must put into

$$\frac{1}{s^2 + 2\zeta\omega_0 s + \omega_0^2}$$

$$\therefore G(s) = \frac{1}{2} \left(\frac{2}{s^2 + 2} \right)$$

$$\zeta = 0$$

$$\omega_0 = \sqrt{2}$$

$$\therefore M_p = 1$$

$$\Delta T = \frac{\pi}{\sqrt{2}}$$

Shape

$$A_1 = 2 \cdot \frac{1}{2} = 1 = A_2, \quad \Delta T = \frac{\pi}{\sqrt{2}}$$

