Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B−V	U−B	R−I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Sun						G2 V	-26.72	0.65	0.10						4.85	0	0	0		
NN	00 00 06	-34 29.7	0.758	168.6		DC9	14.90	0.46	-0.44		75.2	7.0	75.2	7.0	14.28					
GJ 1001	00 02 05	-40 57.8	1.618	154.5	-3	M3.5	12.84	1.63	1.30	1.23	104.2	13.8	104.2	13.8	12.93	-1	-73	12		
NN	00 02 16	+34 22.8	0.776	83.0	+6.4 VAR	G2 V	6.11	0.62	0.09		29.8	10.7	49.0	04. s	4.56	-70	-26	-8	225239	BD+33 4828
NN	00 02 21	+22 59.5	0.380	91.5		G9 V	7.82	0.74	0.29	0.33			39.0	07. r	5.78				225261	BD+22 4950
Gl 1	00 02 28	-37 36.2	6.097	112.5	22.9	M4 V	8.54	1.46	0.96	0.92	221.8	7.7	221.8	7.7	10.27	-78	-101	-35	225213	CD-37 15492
Gl 2	00 02 32	+45 30.6	0.894	100.5	0.1	dM2 e	9.93	1.49	1.18	0.85	87.0	3.8	87.0	3.8	9.63	-39	-23	-17		BD+44 4548
NN	00 02 43	+48 12.0	0.009	305.5		G5	8.30						51.0	05. o	6.84				15	BD+47 4377
Gl 3	00 02 48	-68 06.2	0.582	190.7	41	K5 V	8.48	1.06	1.03	0.42	72.5	18.2	53.0	08. r	7.1	39	-54	3	55	CP-68 3597
NN	00 02 54	-50 20.0	0.167	276.0		M5	11.95	1.50		+0.95t			47.0	10. r	10.31					
Gl 4 A	00 03 02	+45 32.2	0.839	101.8	+0.0 SB	dK6 e	8.97	1.44	1.21	+0.71 J	87.0	3.8	87.0	3.8	8.67	-36	-22	-17	38	BD+45 4408
Gl 4 B	00 03 02	+45 32.1	0.885	98.3	0.1	M0.5 V	9.02	1.45	1.20		87.0	3.8	87.0	3.8	8.72	-40	-23	-15		
Gl 4.1A	00 03 38	+58 09.5	0.260	76.7	-11.6	G5 V	6.43c	+0.64c	+0.11c		46.5	5.8	46.5	5.8	4.77c	-18	-22	2	123	BD+57 2865
Gl 4.1B	00 03 38	+58 09.5	0.260	76.7	-16	dG8	7.20c	+0.78c	+0.33c		46.5	5.8	46.5	5.8	5.54c	-16	-26	3		
NN	00 03 40	-66 07.5	0.593	160.6		M4	12.16	1.55		1.04			55.0	11. r	10.86					
Gl 4.2A	00 03 44	-49 21.2	0.592	93.9	2.6	G1 IV	5.71	0.52	0.03	0.17	48.3	8.2	48.3	8.2	4.13	-48	-31	-11	142	CD-49 14337
Gl 4.2B	00 03 44	-49 21.2	0.592	93.9			11.50				48.3	8.2	48.3	8.2	9.9 *					
Gl 5	00 04 01	+28 44.7	0.422	114.1	-5.5	K0 Ve	6.14	0.75	0.33		70.2	9.0	70.2	9.0	5.37	-17	-21	-11	166	BD+28 4704
GJ 1002	00 04 13	-07 47.5	2.041	203.6	-42	M5-5.5	13.75	1.98	+1.60:	1.63	212.8	3.3	212.8	3.3	15.39	37	-41	28		
GJ 1003	00 04 46	+28 58.8	1.890	127.2		m	14.18	1.49	1.40	1.14	53.5	2.7	53.5	2.7	12.82					
Wo 9003	00 04 58	-24 05.9	0.348	77.5	-46	K0 V	8.70	0.80	0.35		39.2	13.6	26.0	04. r	5.77	-66	-23	36	283	CD-24 8
NN	00 05 26	+07 44.0	0.546	222.4		M3.5	13.07	1.52		1.04	44.0	9.4	44.0	9.4	11.29					
NN	00 05 53	+17 08.8	0.105	238.3		dM0	10.79	1.47		0.75			47.0	08. r	9.15					
NN	00 05 54	-57 22.0	0.368	264.0		M4	12.07	1.54		+1.13t			74.0	16. r	11.42					
Gl 6	00 06 06	+36 21.0	0.167	222.2	-15.2	F8 IV	6.21	0.49	-0.06:		46.2	6.8	46.2	6.8	4.53	20	-11	-3	400	BD+35 8
NN	00 06 20	+20 33.9	0.244	194.0		m	13.54			1.36			94.0	14. r	13.41					
Gl 7	00 06 29	-27 24.1	0.683	83.7		m	11.72	1.50	1.15	0.72	56.3	26.4	29.0	05. r	9.03					CD-27 16
Gl 8	00 06 30	+58 52.4	0.553	108.4	+11.3 SB?	F2 III-IV	2.27	0.34	0.11		69.2	7.0	69.2	7.0	1.47	-34	-6	-18	432	BD+58 3
Gl 9.1	00 06 53	-46 01.4	0.214	145.0	-9.2	K0 III	3.88	1.03	0.84	+0.46C	64.5	15.3	64.5	15.3	2.9	-5	-13	11	496	CD-46 18
NN	00 08 31	-06 03.7	0.252	88.0	-5.2	dM2	10.86	1.47	1.18	0.72			43.0	07. r	9.03	-24	-14	1		BD-06 15
NN	00 08 42	+58 04.5	0.235	92.0		K7	9.48	1.22	1.07	0.51			46.0	06. r	7.79					
Gl 10	00 08 43	-15 44.5	0.279	197.5	14.6	F7 V	4.89	0.49	-0.02	+0.29C	65.8	13.6	62.0	08. r	3.85	16	-10	-17	693	BD-16 17
Gl 10.1	00 09 03	-59 11.3	0.290	90.2	-4.6	G4 V	8.35	0.62	0.13	+0.32C	49.6	15.3	20.0	04. r	4.86	-61	-31	-7	741	CP-59 8
NN	00 09 12	-35 24.8	0.211	54.2	-13.5	F4 V	5.25	0.44			32.2	11.9	44.0	06. r	3.47	-25	4	9	739	CD-35 42
GJ 1004	00 09 40	+50 09.2	0.718	216.0		DA8	14.36	0.42	-0.42		90.7	3.7	90.7	3.7	14.15					
Gl 11 A	00 10 26	+69 03.2	0.772	113.9		dM4 J	13.06	+1.60 J	+1.27 J	+1.10 J	49.6	3.8	49.6	3.8	11.54					
Gl 11 B	00 10 26	+69 03.2	0.772	113.9			13.40				49.6	3.8	49.6	3.8	11.9 *					
NN A	00 10 40	+80 23.2	0.294	56.0		M1.5	11.12	1.50	1.21	0.92			61.0	13. r	10.05					
NN B	00 10 48	+80 23.1	0.294	56.0		m	17.4 P						61.0	13. r	16.3 P					
NN	00 11 42	-13 27.1	0.911	217.7		DC8	15.90	0.58	-0.27		50.8	7.8	50.8	7.8	14.43					
GJ 1005 A	00 12 53	-16 24.3	0.863	133.6	-29	M4	12.03	+1.72 J	+1.26 J	+1.21 J	188.7	8.4	188.7	8.4	13.41	-7	-27	23		
NN	00 13 06	-30 02.7	0.130	135.0		dM3.4	14.31	1.57	0.82	1.33			56.0	11. r	13.05					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 12	00 13 12	+13 16.4	0.695	62.7		dM3.5	12.58	1.66	1.33	1.12	86.3	6.8	86.3	6.8	12.26					
NN A	00 13 26	-68 16.4	0.628	103.8		m	10.95			0.82			50.0	06. r	9.44					
NN B	00 13 17	-68 16.0	0.628	103.8		m	12.50			1.04			50.0	06. r	11.0 *					
NN	00 13 33	-48 32.1	0.238	198.0		M5	11.54	1.46		+1.01t			64.0	14. r	10.57					
GJ 1006 A	00 13 36	+19 35.6	1.037	137.5		M4	12.27	1.50	+1.0 :	1.25	65.5	1.6	65.5	1.6	11.35					
GJ 1006 B	00 13 38	+19 35.8	1.037	137.5		M4.5	13.22	1.60	+1.2 :	1.26	65.5	1.6	65.5	1.6	12.3					
Wo 9006	00 13 46	+15 38.5	0.257	54.0		m	14.8 P				43.3	10.2	43.3	10.2	13.0 P					
NN	00 13 56	-80 07.7	0.460	99.0		G6 V	6.60						52.0	12. r	5.2				1237	CP-80 7
NN	00 14 21	+19 47.2	0.244	84.0		m	13.77			1.20			45.0	08. r	12.04					
GJ 1007	00 14 22	+04 51.3	0.635	185.0		m	13.79	1.62		1.30	56.6	4.5	56.6	4.5	12.55					
Gl 13	00 14 24	-52 55.9	0.361	61.0	-14.3	SB G2 V	6.84	0.64	0.06	+0.38C	67.4	11.9	67.4	11.9	5.98	-29	4	5	1273	CP-53 42
Gl 14	00 14 26	+40 40.2	0.562	79.7	+3.0	VAR dM0.5	9.00	1.36	1.18	0.61	71.0	4.6	71.0	4.6	8.26	-35	-13	0		BD+40 45
NN	00 14 41	+28 54.0	0.791	57.5		M2	11.55			0.90	31.5	24.1	51.0	08. r	10.09					
NN	00 14 54	-09 01.0	0.388	107.0		M0	12.49	1.57	1.25		46.6	6.0	46.6	6.0	10.83					
NN	00 15 07	-08 57.7	0.270	86.0		dM0	11.00	1.42	1.20	0.73	36.6	5.0	36.6	5.0	8.82					BD- 9 40
NN	00 15 22	-18 11.4	0.223	71.0		m	13.20	1.58		1.08			39.0	08. r	11.16					
Wo 9008	00 15 25	-13 44.0	0.404	89.4	28.2	G2 V	6.50	0.59	0.13		32.0	9.3	42.0	07. r	4.62	-40	-14	-33	1388	BD-14 42
Gl 15 A	00 15 31	+43 44.4	2.912	81.8	+12.0	SB M2 V	8.08	1.56	1.22	0.88	289.5	4.9	289.5	4.9	10.39	-48	-11	-4	1326	BD+43 44
Gl 15 B	00 15 31	+43 44.4	2.912	81.8	11.3	M6 Ve	11.06	1.79	1.39	1.24	289.5	4.9	289.5	4.9	13.37	-47	-12	-3		
Gl 16	00 15 42	+09 55.5	0.020	180.0		dM0	10.90	1.50	1.20	0.89	35.9	6.0	35.9	6.0	8.68					
Gl 16.1	00 16 07	-08 19.7	0.443	108.6	-10.4	G5 IV-V	6.46	0.68	0.29	0.22	51.4	20.5	51.4	20.5	5	-26	-33	1	1461	BD-08 38
NN	00 16 16	+27 32.3	0.402	105.0		m	13.86			1.25			52.0	09. r	12.44					
GJ 1008	00 16 33	-10 14.3	0.276	200.0		K7 V	9.94	1.33	1.16	0.59			46.0	08. r	8.25					BD-10 47
Gl 17	00 17 29	-65 10.1	2.072	55.7	9	F9 V	4.22	0.58	0.02	0.22	139.0	10.1	139.0	10.1	4.94	-60	-4	-38	1581	CP-65 13
GJ 2003	00 17 36	-17 20.3	0.180	65.0		M1	11.69	1.55	1.18	0.84			41.0	07. r	9.75					
NN	00 17 48	+32 49.3	1.362	129.2	-30	M6	16.05	1.98			79.9	3.7	79.9	3.7	15.56	-26	-73	-37		
Gl 17.1	00 18 52	-46 00.7	0.791	174.2	2.5	M1	10.40	1.48	1.21	0.76	49.7	6.7	49.7	6.7	8.88	27	-68	20		CP-46 29
NN	00 19 15	-46 21.4	0.483	216.8		M3:	12.29	1.46		+1.11t			59.0	14. r	11.1					
NN	00 19 16	+48 56.0	0.220	98.0		m	12.84			1.08			45.0	09. r	11.11					
GJ 1009	00 19 27	-31 41.0	0.130	163.0		dM2	11.16	1.48	1.08	0.96			69.0	13. r	10.35					
NN	00 19 37	+42 20.3	0.321	213.0		DC9	16.50	0.72	-0.16				42.0	04. w	14.62					
Gl 17.2	00 19 52	-27 18.3	0.476	149.3	0.4	K3 V	8.30	0.90	0.62	0.32	47.6	11.4	39.0	06. r	6.26	-1	-58	-4	1815	CD-27 101
Gl 17.3	00 20 18	-12 29.2	0.396	80.6	-2.6	G2 V	6.38	0.66	0.22	0.23	48.6	10.0	53.0	08. r	5	-33	-13	0	1835	BD-13 60
GJ 1010 A	00 20 41	+76 54.7	0.800	273.0		k-m	11.30	1.49	1.17	0.89	63.7	5.3	63.7	5.3	10.32					
GJ 1010 B	00 20 43	+76 54.8	0.800	273.0		m	14.0 :			1.21	63.7	5.3	63.7	5.3	13.0 :					
GJ 2004	00 20 46	-33 26.8	0.147	332.5		K3/4 V	8.75	1.07	0.90	0.39			43.0	05. r	6.92				1910	CD-33 118
NN	00 20 50	-51 10.3	0.555	91.5		M4	11.88	1.48		1.00	15.1	17.0	55.0	11. r	10.58					CD-51 89
GJ 1011	00 20 52	+24 01.5	0.259	298.0		k-m	14.27	1.59	1.22	1.28	61.1	4.1	61.1	4.1	13.2					
Gl 18	00 21 53	-27 18.3	0.679	82.4	3.7	K3 V	7.92	0.95	+0.66:	0.36	81.2	29.2	52.0	08. r	6.5	-57	-23	-10	2025	CD-27 108
NN	00 21 55	+29 45.8	0.605	90.2		m	14.54	1.67		1.40	53.0	5.1	53.0	5.1	13.16					
GJ 2005	00 22 12	-27 26.0	0.614	354.9	-220	M5.5	15.42			1.78	132.8	9.1	132.8	9.1	16.04	-29	8	219		
NN	00 22 45	+22 37.0	0.520	204.7		m	14.3 *			1.30			53.0	09. r	12.9 *					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM	
Gl 19	00 23 09	-77 32.1	2.250	81.6	22.9	G2 IV	2.80	0.62	0.10	0.23	155.4	9.3	155.4	9.3	3.76	-51	-42	-29	2151	CP-77	16
Gl 20	00 23 45	-43 57.4	0.112	70.2	11.3	A7 Vn	3.94	0.17	0.10		71.2	11.9	71.2	11.9	3.2	-5	-4	-12	2262	CD-44	101
Gl 21	00 24 00	+69 52.1	0.230	219.0		dM0	10.52	1.49	1.22	0.82	54.4	6.1	54.4	6.1	9.2						
NN	00 24 22	+49 25.5	0.477	123.6		m	14.25			1.28	47.1	3.1	47.1	3.1	12.62						
GJ 1012	00 26 08	-06 55.8	0.870	202.3	51	M4	12.19	1.48	1.05	1.19	74.8	5.6	74.8	5.6	11.56	38	-12	-64			
NN	00 26 09	+50 05.9	0.440	74.0		m	13.15			1.26			76.0	13. r	12.55						
GJ 1013	00 29 02	-06 07.9	1.098	163.1		m	12.75	1.64	1.20	1.16	61.6	4.8	61.6	4.8	11.7						
Gl 22 A	00 29 20	+66 57.8	1.748	97.8	-4	dM2.5e	10.38	+1.54 J	+1.16 J	+0.99 J	100.6	2.2	100.6	2.2	10.39	-68	-44	-18		BD+66	34
Gl 22 B	00 29 20	+66 57.8	1.748	97.8		dM3.5	12.4 *				100.6	2.2	100.6	2.2	12.4 *						
NN	00 29 34	-03 10.7	0.653	76.7		g-k	17.34				43.1	1.0	43.1	1.0	15.51						
NN	00 29 56	-63 21.9	0.518	101.7		K7	9.61	1.35		0.63	34.3	4.9	34.3	4.9	7.29					CP-63	51
NN	00 30 00	+07 13.0	0.186	111.0		m	12.70			1.24			86.0	16. r	12.37						
Wo 9015 A	00 30 28	-63 18.4	0.092	111.7	5	A0 V	5.75	+0.04 J	+0.02 J		47.8	8.0	47.8	8.0	4.15	-4	-9	-3	3003	CP-63	52
Wo 9015 B	00 30 28	-63 18.4	0.092	111.7		A	6.0 *				47.8	8.0	47.8	8.0	4.4 *						
NN	00 31 30	+70 55.5	0.596	120.0		k-m	13.52	1.65		1.17	50.5	3.1	50.5	3.1	12.04						
Wo 9016	00 31 43	+47 38.4	0.410	80.2	-10.5	F8	7.37	0.54	0.02		43.6	13.6	20.0	03. s	3.88	-80	-55	12	3079	BD+47	138
Gl 22.2	00 32 05	-52 39.0	0.233	80.5	34.8	F3 IV-V	5.57	0.46	-0.02	+0.26C	49.0	15.3	49.0	15.3	4	-11	-20	-34	3158	CP-53	117
Gl 23 A	00 32 40	-03 52.1	0.411	92.9	+11.2 SB	F6 V	5.65	+0.57 J	+0.07 J	+0.32CJ	61.4	3.8	61.4	3.8	4.59	-28	-13	-13	3196	BD-04	62
Gl 23 B	00 32 40	-03 52.1	0.411	92.9	+8.8 SB	G1 V	6.4 *				61.4	3.8	61.4	3.8	5.3 *	-28	-14	-11			
GJ 1014	00 33 16	+10 12.4	1.186	110.5			15.32	1.89		1.50	64.0	5.2	64.0	5.2	14.35						
NN	00 33 18	-48 16.5	0.111	150.2	7.6	F6 V	5.51	0.44	-0.01				40.0	05. r	3.52	2	-15	-3	3302	CD-48	121
NN	00 33 26	+45 14.5	0.298	242.0		M2	11.71	1.54		0.98			58.0	11. r	10.53						
NN	00 33 49	+08 36.0	0.042	190.3		G5	7.87						46.0	04. o	6.18				3335	BD+08	80
Gl 24 A	00 34 14	-49 24.3	0.407	108.5	-3.0 SB	G3 V	6.79	0.64	+0.12*	0.22	37.6	11.9	33.0	04. r	4.38	-39	-43	7	3405	CD-49	141
Gl 24 B	00 33 40	-49 24.1	0.410	109.4	4.7	K0 V	8.37	0.78	+0.43*	0.26	77.4	11.9	33.0	04. r	5.96	-37	-46	0	3359	CD-49	138
Gl 25 A	00 34 47	-25 02.5	1.394	90.3	+18.6 SB	G7 V	6.23	+0.72 J	+0.20 J	+0.27 J	72.1	8.7	72.1	8.7	5.52	-77	-47	-24	3443	CD-25	225
Gl 25 B	00 34 47	-25 02.5	1.394	90.3	25	G8 V	6.4 *				72.1	8.7	72.1	8.7	5.7 *	-77	-46	-30			
GJ 2010	00 34 56	-21 10.1	0.316	229.0		DA7	14.53	0.45	-0.57				62.0	07. w	13.49						
NN	00 35 28	+52 03.6	0.250	192.0		M0	10.48	1.42	1.27	0.66			44.0	07. r	8.7						
NN	00 35 48	+51 11.4	0.270	277.0		m	12.60			1.07			49.0	10. r	11.05						
Gl 26	00 36 13	+30 20.5	1.561	88.3	-0.2	dM4	11.06	1.53	1.08	1.00	79.5	2.2	79.5	2.2	10.56	-80	-48	-2			
NN	00 36 40	+60 16.9	0.294	211.0		m	12.83			1.03			39.0	08. r	10.79						
Gl 27	00 36 45	+20 58.9	0.588	231.2	-32.9	K0+ V	5.85	0.85	0.57	0.28	95.1	6.0	95.1	6.0	5.74	38	-20	9	3651	BD+20	85
Gl 27.1	00 37 34	-44 31.5	0.546	115.5		M0.5	11.40	1.49	1.10	0.83	31.1	16.0	43.0	08. r	9.57					CD-44	170
Gl 27.2	00 38 02	-24 04.4	0.722	117.0	-50.4	G3 V	6.15	0.71	0.21	0.26	40.1	7.3	40.1	7.3	4.17	-44	-76	45	3795	CD-24	263
Gl 28	00 38 04	+39 55.3	0.746	152.4	-64.2	K2 Ve	7.36	0.94	0.72	0.31	58.5	9.6	58.5	9.6	6.2	19	-82	-26	3765	BD+39	154
Gl 29	00 38 06	-59 44.1	0.990	62.8	1.5	G1 V	5.90	0.56	0.01	0.18	56.7	8.2	56.7	8.2	4.67	-78	-12	-25	3823	CP-60	46
NN	00 38 16	+31 06.8	0.319	188.0		m	13.83			1.25			53.0	10. r	12.45						
GJ 1015 A	00 38 28	+55 33.6	0.313	104.0		m	14.02	1.55			43.3	3.6	43.3	3.6	12.2						
GJ 1015 B	00 38 29	+55 33.7	0.313	104.0		DQ5	14.08	0.02	-0.81		43.3	3.6	43.3	3.6	12.26						
GJ 2012	00 38 58	-22 37.2	0.567	229.0		DQ9	14.53	0.62	-0.14	0.29	100.8	11.4	100.8	11.4	14.55						
GJ 1016	00 39 05	-33 53.9	0.450	237.0		k	10.60	1.40	1.17	0.70			45.0	07. r	8.87					CD-34	239

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
GJ 1017	00 39 45	-52 38.5	0.736	117.4		m	12.25*			0.37	45.7	11.0	45.7	11.0	10.5 *					
GJ 1018	00 39 53	-36 59.5	0.180	293.0		m	12.65:	1.54		1.11			54.0	11. r	11.31:					
Gl 29.1	00 40 05	+35 16.4	0.266	70.0	-0.5 SB	dM0 e	10.52	1.50	1.08	0.88	47.2	11.9	47.2	11.9	8.9	-24	-10	7		BD+34 106
Gl 30	00 40 52	+33 34.6	0.406	209.3	-34.7	dK5	8.73	1.12	1.09	0.44	54.7	7.0	54.7	7.0	7.42	39	-29	-9		BD+33 99
GJ 1019	00 40 56	+28 11.1	1.062	187.0		m	14.52	1.59	0.79	1.21	51.9	5.0	51.9	5.0	13.1					
NN	00 41 02	+23 36.9	0.213	149.9		dM0	10.97	1.34	1.10	0.63	42.3	5.0	42.3	5.0	9.1					BD+23 97
Gl 31	00 41 05	-18 15.6	0.234	81.0	13.3	K1 IIIe	2.04	1.01	0.88		54.5	8.5	54.5	8.5	0.72	-19	-6	-13	4128	BD-18 115
NN	00 41 05	-41 33.6	0.744	222.5		M4	13.1 *			1.33			101.0	16. r	13.1 *					
NN	00 41 36	+75 39.9	0.395	103.2	-8.4	G8	7.19	0.75	0.40		23.2	8.3	48.0	08. r	5.6	-29	-25	-12	4075	BD+75 36
NN	00 41 42	+12 20.8	0.330	127.0		m	12.79	1.49	1.02	1.15			55.0	11. r	11.49					
NN	00 41 42	+08 51.2	0.809	91.5		m	13.8 *			1.35			81.0	12. r	13.3 *					
Wo 9024	00 41 58	-26 47.5	0.345	62.4	55.4	G5 V	7.79	0.67	0.17		39.8	18.8	28.0	05. r	5.03	-57	-3	-56	4208	CD-27 223
Gl 31.2A	00 42 07	-19 13.4	0.350	60.0	27	dM2	10.78	1.44	1.11	0.66	56.4	18.8	41.0	08. r	8.84	-42	2	-25		BD-19 111
Gl 31.2B	00 42 05	-19 13.7	0.350	60.0		m	16.3 P				56.4	18.8	41.0	08. r	14.4 P					
Gl 31.3	00 42 16	-22 16.8	0.107	324.6	13.2	F2 V	5.23	0.34	+0.10:	+0.21C	46.3	11.9	46.3	11.9	3.6	0	12	-12	4247	CD-22 239
NN	00 42 29	-15 32.3	0.662	151.8		m	14.2 *			1.37			72.0	11. r	13.5 *					
Gl 31.4	00 42 31	+01 31.2	0.572	185.3	9.9	K2 V	8.01	1.00	0.90	0.35	43.2	13.6	51.0	07. r	6.55	27	-32	-34	4256	BD+01 131
Gl 31.5	00 42 32	-65 54.8	0.760	167.0	97.7	G3 V	6.54	0.65	0.12	0.24	50.4	9.5	49.0	08. r	4.99	49	-107	-32	4308	CP-66 53
GJ 1020	00 42 58	-13 09.1	0.202	190.9	-12.8	G0 V	6.15	0.61	0.10				50.0	08. r	4.64	14	-16	8	4307	BD-13 128
NN	00 43 12	-51 54.	0.094	124.0		M3	11.91	1.48		+0.91t			43.0	09. r	10.08					
Gl 32 A	00 43 25	-42 10.9	0.312	104.1	-26.3	K5 V	8.41	1.17	1.14	0.49	81.4	9.8	81.4	9.8	7.96	-17	-8	26	4378	CD-42 249
Gl 32 B	00 43 25	-42 10.9	0.262	114.1	-22.6	K7 V	9.06	1.27	1.18	0.57	81.4	9.8	81.4	9.8	8.61	-12	-8	23		
GJ 1021	00 43 25	-47 49.6	0.202	65.1	-11.4	G5 IV	5.80	0.64	+1.70C	0.22	48.1	18.8	48.1	18.8	4.2	-22	0	7	4391	CD-48 176
NN	00 44 27	-26 24.6	0.286	47.0		M3 :	13.98	1.64	1.24				40.0	19. r	12					
NN	00 44 40	-23 46.8	0.207	141.0		m	14.40			1.32			54.0	09. r	13.06					
Wo 9029 A	00 45 08	-37 12.5	0.393	207.4	-26	F7/8 V	7.85	0.54	-0.03	0.21	40.7	10.2	40.7	10.2	5.9	37	-19	33	4597	CD-37 273
Wo 9029 B	00 45 07	-37 13.4	0.396	206.0		m	15.5 P				40.7	10.2	40.7	10.2	13.5 P					
Gl 33	00 45 45	+05 01.4	1.367	146.4	-10	K2 V	5.74	0.88	0.58	0.33	135.9	3.7	135.9	3.7	6.41	-1	-47	-13	4628	BD+04 123
Gl 34 A	00 46 03	+57 33.1	1.213	114.9	8.2	G3 V	3.45	0.57	0.02	0.22	168.4	3.1	168.4	3.1	4.58	-30	-11	-15	4614	BD+57 150
Gl 34 B	00 46 03	+57 33.1	1.213	114.9	10.5	K7 V	7.51	1.39	1.03	0.59	168.4	3.1	168.4	3.1	8.64	-31	-9	-16		
NN	00 46 06	+26 45.0	0.314	209.0		M4	12.38	1.52	1.20				43.0	20. r	10.5					
NN	00 46 10	+44 18.5	0.187	127.0		m	13.06			1.16			54.0	11. r	11.72					
Gl 34.1	00 46 21	+16 40.3	0.199	180.8	+3.8 SB	F8 V	5.07	0.51	0.00		45.6	13.6	55.0	05. s	3.77	6	-8	-15	4676	BD+16 76
Gl 35	00 46 31	+05 09.2	2.980	155.7	54	DZ7	12.38	0.55	0.02	0.16	230.9	2.1	230.9	2.1	14.2	2	-49	-38		
NN	00 46 43	-50 24.9	0.323	131.0		M2	10.75	1.43		+0.75t			48.0	09. r	9.16					CD-50 210
Gl 36	00 46 57	-23 29.2	0.534	77.8	5	G9 V	7.16	0.78	0.32	0.29	62.5	9.0	62.5	9.0	6.14	-38	-14	-5	4747	CD-23 315
GJ 1022	00 47 18	-61 17.7	1.119	94.0	-2	M6	12.16	1.46	1.05	0.99			46.0	09. r	10.47	-94	-67	5		
Gl 37	00 47 37	-10 54.8	0.322	225.5	+8.2 SB?	F7 IV-V	5.17	0.50	-0.02	+0.29C	61.8	7.2	61.8	7.2	4.12	23	-2	-13	4813	BD-11 153
NN A	00 47 52	+24 32.7	0.220	102.0		m	12.70			+1.21 J			71.0	14. r	12					
NN B	00 47 52	+24 32.7	0.220	102.0		m	13.3 *						71.0	14. r	12.6 *					
NN	00 47 54	-27 42.6	0.166	65.8		A3	9.60	0.89	0.40		40.9	20.5	20.0	03. r	6.11					CD-28 258
Gl 38	00 48 23	+58 01.5	1.549	75.9	-16.6	dM2	10.67	1.39		0.69	53.5	3.4	53.5	3.4	9.31	-104	-84	34		

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 39	00 48 43	+18 28.3	0.270	173.3	6.5	dK6	9.24	1.21	1.18	0.49	46.1	13.3	48.0	08. r	7.65	5	-13	-24	4913	BD+17 112
GJ 2015	00 48 56	-27 39.5	0.016	115.6		K0	10.41	1.08	0.92		64.9	20.5	21.0	04. r	7.02					CD-28 262
Gl 40 A	00 49 04	-23 10.8	0.681	114.1	15.4	K5 V	8.96:	1.29	1.12	0.55	69.2	7.5	69.2	7.5	8.16:	-26	-38	-17	4967	CD-23 332
Gl 40 B	00 49 06	-23 10.7	0.678	113.5		m	17.3 P				69.2	7.5	69.2	7.5	16.5 P					
Gl 41	00 50 04	+60 51.0	0.193	340.5	20.8	F8 V	4.82	0.53	0.12		64.9	15.3	76.0	12. r	4.22	-8	20	11	5015	BD+60 124
NN	00 50 06	-41 31.	0.059	212.0		M3	11.92	1.49		+0.90t			42.0	08. r	10.04					
Gl 42	00 50 34	-30 37.7	0.622	85.9	-7. SB	K3 V	7.17	0.93	0.68	0.33	89.0	23.8	69.0	11. r	6.36	-38	-20	7	5133	CD-31 325
GJ 1023 A	00 51 05	+68 46.6	0.094	253.9		G0	9.70	0.55	0.07		53.3	28.0	53.3	28.0	8.3				5109	BD+68 58
GJ 1023 B	00 51 07	+68 46.6	0.090	250.6			10.40	0.64	0.16		53.3	28.0	53.3	28.0	9					BD+68 58
Gl 42.1	00 52 19	+23 49.9	0.249	226.1	-8.6	G5	7.38	0.65	0.10		49.4	18.8	32.0	04. r	4.91	35	-4	-15	5294	BD+23 125
Gl 43	00 53 10	-52 06.5	0.470	41.0		m	12.36	1.51		+1.19C	61.6	13.6	61.6	13.6	11.31					
NN	00 53 20	-11 44.1	0.451	348.0		DA7	15.25	0.35	-0.48				43.0	07. w	13.42					
NN	00 53 23	-29 56.9	0.452	64.5	9.5	K5 V	9.48	1.18	1.14	0.47	20.8	20.5	40.0	06. r	7.49	-53	-8	-10	5425	CD-30 277
NN	00 53 42	+68 46.6	0.749	107.3	-49.4	K4 V	9.10	1.03	0.88	0.41	43.4	10.8	37.0	05. r	6.94	-51	-89	-32	5351	BD+68 60
NN	00 53 54	-28 24.5	0.160	136.0			10.96	0.96	0.72	0.38	43.9	20.5	43.9	20.5	9.2					CD-28 291
GJ 1024	00 53 58	+17 11.6	0.728	113.9		m	13.71	1.64	1.31	1.26	57.4	4.5	57.4	4.5	12.5					
Gl 44	00 54 48	-02 05.0	0.321	238.2	-47.8	K1	9.46	0.86	0.48	+0.43C	70.0	10.2	70.0	10.2	8.69	33	-15	38		BD-02 129
Gl 45	00 55 10	-62 31.0	1.035	82.9	11	K7 V	9.50	1.30	1.25	0.54	59.9	8.2	59.9	8.2	8.39	-69	-44	-13	5633	CP-62 75
Gl 46	00 55 58	-28 07.3	1.305	102.7	43	M3.5	11.77	1.57	1.14	1.19	71.7	14.5	71.7	14.5	11.05	-60	-64	-40		CD-28 302
GJ 2017	00 57 26	-25 51.6	0.050	225.1		G0	9.87*	+0.50*			57.9	20.5	57.9	20.5	8.7 *					CD-26 322
Gl 46.1	00 57 36	+17 55.8	0.095	167.0	-36.7	G5	7.33	1.07	0.94		50.8	11.9	50.8	11.9	5.9	17	-27	20	5857	BD+17 135
NN	00 57 38	+66 40.8	0.270	257.0		m	13.28			1.14			45.0	09. r	11.55					
GJ 2018	00 57 51	-25 53.0	0.426	95.0		K2	9.95	1.11	1.05	0.41	55.9	20.5	27.0	03. r	7.11					CD-26 323
GJ 2019	00 58 12	-26 54.3	0.120	175.3		K0	10.11	0.76	0.28		49.9	20.5	49.9	20.5	8.6					CD-27 323
Gl 47	00 58 13	+61 06.5	0.840	158.0	8.7	dM2.5e	10.83	1.57		0.98	92.4	2.9	92.4	2.9	10.66	-19	-3	-40		
GJ 1025	00 58 20	-04 43.5	1.326	70.5	8		13.32	1.73	1.27	1.20			60.0	12. r	12.21	-101	-26	10		
Gl 48	00 58 48	+71 25.0	1.783	101.2	0.8	dM3.5e	10.04	1.46	1.15	1.08	115.5	4.1	115.5	4.1	10.35	-61	-38	-11		BD+70 68
Wo 9035	00 59 04	+81 50.0	0.186	252.2	-50.7	dG2	8.45	0.60	0.02		40.2	11.9	40.2	11.9	6.5	42	-27	-24	5817	BD+81 27
NN	00 59 04	+53 54.8	0.385	250.0		m	15.12	1.84					66.0	25. r	14.2					
GJ 2020	00 59 24	-26 09.3	0.088	183.5		F0 V	9.75	0.33	0.01		84.9	20.5	84.9	20.5	9.4				6088	CD-26 334
Gl 49	00 59 27	+62 04.5	0.686	84.3	-5.6 SB?	K5 V	9.56	1.50	1.18	0.89	112.6	10.0	112.6	10.0	9.82	-21	-21	4		BD+61 195
Gl 50	00 59 27	-10 08.9	0.566	202.2	-0.4	K5 V	10.50	1.25	1.12	0.54	42.6	11.5	29.0	05. r	7.81	74	-49	-26		BD-10 216
NN	00 59 29	-26 01.9	0.130	38.0			11.84	1.23		0.53	41.9	20.5	41.9	20.5	10					
NN	00 59 48	+04 47.4	0.386	54.7	19.7	K0	8.20	1.00	0.86		20.9	12.1	43.0	08. r	6.37	-46	6	-2	6101	BD+ 4 158
NN	00 59 54	-10 41.0	0.131	357.0	-20	K7 V	10.04	1.35	1.22	0.64	19.5	15.3	49.0	09. r	8.49	-2	6	23		BD-11 192
Gl 51	01 00 08	+62 05.8	0.727	82.5		M5	13.66	1.68	0.79	1.51	110.9	8.5	110.9	8.5	13.88					
NN	01 00 28	+31 24.9	0.269	85.0		m	13.64			1.18			44.0	09. r	11.86					
GJ 1026 A	01 00 32	+19 49.8	0.644	86.2		M1.5	11.88:			+1.02 J	58.5	6.6	58.5	6.6	10.72:					
GJ 1026 B	01 00 32	+19 49.8	0.644	86.2		M3.5	12.4 *				58.5	6.6	58.5	6.6	11.2 *					
GJ 1027	01 01 14	+04 48.3	0.388	52.0	61	DA6	13.96	0.31	-0.57		46.8	3.8	46.8	3.8	12.31	-42	6	1		
Wo 9036	01 01 59	-25 52.1	0.338	185.7	2.8	K5 V	9.80	1.19	1.14	0.48	40.7	9.1	35.0	05. r	7.52	29	-35	-4	6378	CD-26 348
GJ 1028	01 02 21	-18 23.9	1.342	71.5		m	14.46	1.87		1.50	100.0	5.0	100.0	5.0	14.46					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Wo 9037	01 02 22	-39 44.9	0.549	196.9	22.4	G3 IV	7.72	0.60	-0.03	0.22	42.1	9.0	42.1	9.0	5.84	50	-42	-10	6434	CD-40 239
GJ 1029	01 02 47	+28 13.6	1.906	95.0		m	14.80	1.89	1.44	1.53	79.6	3.6	79.6	3.6	14.3					
Gl 52	01 03 45	+63 40.2	1.576	77.9	2.9	K7 V	8.98	1.30	1.21	0.56	67.2	3.4	67.2	3.4	8.12	-90	-59	30		BD+63 137
GJ 1030	01 04 03	+15 00.5	0.320	199.0		k-m	11.43	1.47	1.23	0.93	63.4	6.0	63.4	6.0	10.44					
Gl 52.1	01 04 35	-51 15.5	0.497	88.6	8.7	K1 V	8.85	0.94	+0.69:	0.34	47.0	8.5	47.0	8.5	7.21	-40	-31	-5	6673	CD-51 273
NN	01 04 52	-32 41.6	0.180	:176.		m	10.76	1.38	1.22	0.70			42.0	07. r	8.88					CD-33 408
Gl 53 A	01 04 56	+54 40.5	3.770	114.7	-98.1	SB G5 VI	5.17	0.69	0.09	0.28	134.5	2.9	134.5	2.9	5.81	-41	-156	-34	6582	BD+54 223
Gl 53 B	01 04 56	+54 40.5	3.770	114.7			11. :				134.5	2.9	134.5	2.9	12. :					
Gl 52.2	01 04 56	+33 56.1	1.464	69.9		M3	13.35	1.59	1.18		44.5	3.5	44.5	3.5	11.59					
Gl 53.1A	01 04 56	+22 41.7	0.500	168.2	6.7	K4 V	8.41	1.12	1.06	0.43	52.1	8.8	47.0	05. r	6.77	5	-29	-41	6660	BD+22 176
Gl 53.1B	01 04 56	+22 41.7	0.500	168.2		M3	13.60			1.16	52.1	8.8	47.0	05. r	11.96					
GJ 1031	01 05 52	-29 04.3	0.714	100.4		dM5	13.42	1.70		1.29			76.0	13. r	12.82					
Gl 53.2	01 06 01	+16 59.1	0.583	187.6	-36	dK6	10.55	1.27	1.23	0.56	45.0	15.3	31.0	06. r	8.01	58	-67	-37		BD+16 120
NN	01 06 04	-10 26.8	0.252	122.3	12.9	K1.5 III	3.45	1.16	1.19		40.6	8.9	40.6	8.9	1.49	-15	-24	-15	6805	BD-10 240
Wo 9043	01 06 35	-31 11.7	0.223	125.3	7.9	G8/K0 V	9.10	0.79	0.37	+0.40C	39.7	11.9	21.0	03. r	5.71	-17	-48	-3	6880	CD-31 455
GJ 1032	01 06 47	-24 57.4	0.255	86.0		dM2	12.38	1.53	1.28	1.06			52.0	10. r	10.96					
GJ 2021	01 06 53	-24 46.3	0.265	132.0		m	14.52			1.38			65.0	09. r	13.58					
Gl 53.3	01 06 55	+35 21.4	0.208	121.6	-0.8	M0 IIIe	2.05	1.57	1.96		48.7	7.5	48.7	7.5	0.49	-11	-15	-8	6860	BD+34 198
Gl 54	01 08 34	-67 43.1	0.718	34.0	26.1	k	9.80	1.54	1.17	1.08	120.9	9.0	120.9	9.0	10.21	-16	-10	-34		CP-68 41
NN	01 08 46	+15 10.5	0.215	125.0		m	14.36			1.55			118.0	21. r	14.72					
NN A	01 09 19	+04 39.6	0.623	146.4		m	12.89	1.62		1.14	64.6	2.7	64.6	2.7	11.94					
NN B	01 09 21	+04 38.6	0.623	146.4		m	13.91	1.70		1.24	64.6	2.7	64.6	2.7	12.96					
NN	01 09 55	-02 07.3	0.050	:180.		DAwk	14.09						99.0	11. p	14.07					
Gl 54.1	01 09 59	-17 16.4	1.345	62.3	28	dM5 e	12.05	1.84	1.40	1.41	267.4	3.0	267.4	3.0	14.19	-28	0	-24		
NN	01 10 13	+41 23.4	0.324	96.4		G5	7.28	0.78	0.31				47.0	06. r	5.64				7205	BD+40 248
GJ 1033	01 11 00	-23 10.	0.090	88.0			14.16	1.58	0.96	1.34			62.0	13. r	13.12					
NN	01 11 48	-37 12.9	0.745	61.1		dM2.5	13.85	1.66	1.34	1.19			43.0	08. r	12.02					
Gl 54.2A	01 11 53	-08 11.5	0.303	23.7	21.2	F5 V	5.14	0.45	-0.06	0.16	56.8	6.1	56.8	6.1	3.91	-26	17	-11	7439	BD-08 216
Gl 54.2B	01 11 51	-08 10.7	0.312	25.0	22.1	K1 V	7.85	0.78	0.35	0.27	56.8	6.1	56.8	6.1	6.62	-27	17	-12	7438	BD-08 215
Wo 9046	01 12 11	-42 09.5	0.125	241.8		G0 V	8.47	0.56	0.08		42.0	11.9	42.0	11.9	6.6				7498	CD-42 432
NN	01 12 30	-54 13.	0.324	21.0		M3	11.09	1.48		+0.87t			57.0	11. r	9.87					
Gl 54.3	01 12 51	-65 01.4	0.353	149.6		K0 IV/V	9.05	0.76	0.36	+0.38C	47.5	10.2	47.5	10.2	7.43				7621	CP-65 125
Gl 55	01 12 56	-45 47.9	0.688	74.6	11.6	F8 V	4.96	0.58	0.10	+0.30C	65.9	14.9	82.0	15. r	4.53	-36	-18	-11	7570	CD-46 346
Gl 55.1A	01 13 19	-69 05.1	0.414	73.9		K2 V	7.80	+0.98 J	+0.82:J	+0.46CJ	28.6	22.1	53.0	09. r	6.42				7693	CP-69 44
Gl 55.1B	01 13 19	-69 05.1	0.414	73.9			8.2 *				28.6	22.1	53.0	09. r	6.8 *					
GJ 1034	01 13 40	+24 04.2	1.841	112.2		m	15.04	1.84	+1.12:	1.28	48.5	5.2	48.5	5.2	13.47					
Gl 55.2	01 13 54	+25 04.2	0.433	102.0	-30	dK5	10.08	1.36	1.21	0.62			42.0	11. r	8.2	-20	-52	15		
Gl 55.3A	01 14 05	-69 08.5	0.422	74.0	4	F6 IV J	4.99	+0.47 J	+0.02 J	+0.26CJ	50.7	12.3	50.7	12.3	3.5	-35	-18	-6	7788	CP-69 45
Gl 55.3B	01 14 04	-69 08.4	0.416	73.4	4.9	G5	7.2 *				50.7	12.3	50.7	12.3	5.7 *	-34	-18	-7		
GJ 1035	01 14 18	+83 53.3	1.081	295.1		m	14.77	1.79		1.44	73.2	5.0	73.2	5.0	14.09					
GJ 1036	01 14 57	-35 58.6	0.193	154.0		m	11.42	1.53	1.19	0.96			63.0	12. r	10.42					CD-36 491
Gl 56	01 15 05	-15 45.6	0.544	150.1	-8.8	K3 V	9.77	1.00	0.76	0.40	66.3	12.6	26.0	04. r	6.84	10	-99	-4	7808	BD-16 214

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B−V	U−B	R−I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	01 15 06	+28 24.7	0.459	233.2		M0.5	11.56			0.85			40.0	06. r	9.57					
NN	01 15 18	+05 13.1	0.649	171.3		dM2	11.05			0.82			50.0	08. r	9.54					
GJ 1037	01 15 20	+15 55.1	0.653	181.7		DQ6	13.82	0.12	-0.80	-0.02	63.8	3.6	63.8	3.6	12.84					
Gl 56.1	01 15 47	-13 09.2	0.696	165.8		M3	11.76	1.47		0.96	45.1	7.6	45.1	7.6	10.03					
Gl 56.2	01 15 49	-48 24.9	0.250	63.0		M1	11.55	1.44		+0.91C	45.6	13.6	30.0	05. r	8.94					CD-48 329
Gl 56.3A	01 16 06	-01 07.6	0.507	120.3	18.2	K1 V	8.00	0.82	0.44	0.30	52.8	19.2	39.0	05. r	5.96	-34	-49	-24	7895	BD-01 167
Gl 56.3B	01 16 05	-01 08.0	0.505	121.5		M0	10.70	1.41	1.17	0.63	52.8	19.2	39.0	05. r	8.66					
Gl 56.4	01 16 43	+79 53.5	0.330	108.0	-14	dK8	9.66	1.29	1.27	0.63	40.9	11.9	56.0	07. r	8.4	-16	-25	-10		BD+79 38
NN	01 17 00	-26 40.0	0.022	347.0		m	13.46						41.0	04. p	11.52					
NN A	01 17 10	+38 43.5	0.365	60.0		dM0	11.39	1.31		0.58	43.1	11.5	24.0	03. r	8.29					
NN B	01 17 11	+38 43.7	0.365	60.0		k-m	14.35			1.14	43.1	11.5	24.0	03. r	11.25					
NN	01 17 28	-27 42.5	0.374	98.0		m	14.20			1.22			40.0	07. r	12.21					
NN	01 17 42	+38 04.3	0.040	122.0		dK8	10.64	1.14	1.17	0.49	40.3	16.0	24.0	03. r	7.54					
Gl 56.5	01 17 50	+76 27.0	0.049	225.9	-21.8	dK0	7.11	0.82	0.45		41.7	8.5	57.0	09. r	5.89	14	-15	-8	7924	BD+75 58
Gl 57	01 19 16	-41 54.7	1.345	109.4	29	dM0.5	10.14	1.40	1.10	0.69	63.4	13.6	59.0	11. r	8.99	-58	-95	-7		CD-42 469
NN	01 19 37	-46 58.5	0.123	236.0		M3	11.36	1.44		+0.85t			46.0	09. r	9.67					CD-47 399
NN A	01 19 46	-27 09.1	0.231	198.8		K2 V	8.3 *			0.34			46.0	04. r	6.6 *				8326	CD-27 457
NN B	01 19 48	-27 10.0	0.242	196.0		m	14.85			1.41			46.0	04. r	13.16					
NN A	01 20 12	+00 16.7	0.567	202.4		m	13.97	+1.76 J		+1.37 J	69.2	4.6	69.2	4.6	13.17					
NN B	01 20 12	+00 16.7	0.567	202.4		m	15.0 *				69.2	4.6	69.2	4.6	14.2 *					
NN	01 20 20	+07 09.3	0.257	21.4		G5	7.33						66.0	06. p	6.43				8357	BD+ 6 211
NN	01 20 24	-26 04.	0.119	58.0		m	13.05						45.0	06. p	11.32					
Gl 57.1A	01 20 33	-13 13.6	0.477	94.3	30.6	K0 IV	7.85	0.90	0.70	0.28	48.4	13.6	44.0	09. r	6.07	-46	-29	-24	8389	BD-13 249
Gl 57.1B	01 20 31	-13 13.1	0.474	94.0	58.3	dK7 J	10.38	+1.38 J	+1.26 J	+0.71 J	48.4	13.6	44.0	09. r	8.6	-53	-25	-51		
Gl 57.1C	01 20 31	-13 13.1	0.474	94.0			13.1 *				48.4	13.6	44.0	09. r	11.3 *					
Wo 9056	01 22 10	+18 14.6	0.581	108.8	7.9	K2	8.49	0.89	0.59	0.30	61.0	24.4	33.0	05. r	6.08	-57	-59	-14	8553	BD+17 202
GJ 1038	01 22 43	-33 06.8	0.290	60.5		k-m	9.80	1.45	1.15	0.65			59.0	09. r	8.65					CD-33 514
NN	01 22 58	+09 30.2	0.478	151.6		dM3.5	13.13	1.68	1.38	1.23	31.5	20.5	67.0	16. r	12.3					
GJ 1039	01 23 02	-26 16.0	0.551	156.8		DC7	14.95	0.40	-0.55				54.0	05. w	13.61					
Gl 58.2	01 26 20	+21 28.0	0.499	111.7	+11.3 SB	K2 V	7.73	0.96	0.68		32.4	10.2	55.0	09. r	6.43	-33	-27	-13	8997	BD+20 226
NN	01 30 05	-22 09.0	1.062	210.7		M1.5	11.21	1.50	1.20	0.84	27.6	10.3	51.0	10. r	9.75					CD-22 526
Gl 59 A	01 30 53	-24 25.9	0.317	119.7	-49.1	G8 V	6.97	0.76	0.32	+0.38C	70.4	8.7	70.4	8.7	6.21	0	-17	51	9540	CD-24 658
Gl 59 B	01 30 35	-24 29.7	0.326	118.0		m	12.77	1.30	1.15		70.4	8.7	70.4	8.7	12.01					
Gl 59.1	01 30 55	+68 41.5	0.399	288.1	-33.4	G6 V	6.53	0.68	0.24		38.2	10.2	53.0	09. r	5.15	48	-6	2	9407	BD+68 113
NN	01 31 17	-44 09.5	0.237	74.6		K0/1 V	7.84	0.83	0.50				42.0	05. r	5.96				9619	CD-44 434
Wo 9057	01 31 35	+34 25.4	0.016	42.9	-4.5	F8	9.56	0.52	0.02		40.8	15.0	40.8	15.0	7.6	2	-3	3		BD+33 256
NN	01 32 39	+41 47.2	0.229	144.0		dM0	10.99	1.30	1.26	0.53	40.6	6.2	40.6	6.2	9.03					
Gl 60 A	01 32 42	-30 10.0	0.198	52.6	34.2	K3 V	7.78	+0.92 J	+0.57 J	+0.39 J	64.3	18.1	58.0	07. r	6.6	-20	-5	-32	9770	CD-30 529
Gl 60 B	01 32 42	-30 10.0	0.198	52.6		K4 V	8.0 *				64.3	18.1	58.0	07. r	6.8 *					
Gl 60 C	01 32 42	-30 10.0	0.198	52.6		M2 V	10.4 *				64.3	18.1	58.0	07. r	9.2 *					
NN	01 33 42	-27 02.	0.026	11.0		m	13.33						51.0	07. p	11.87					
Gl 61	01 33 51	+41 09.4	0.415	204.4	-28.7	F8 V	4.09	0.54	0.06	+0.18t	57.4	4.8	57.4	4.8	2.88	32	-23	-21	9826	BD+40 332

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 62	01 34 49	-29 38.8	0.296	102.3	11.2	K0 V	8.14	0.86	+0.61:	0.28	45.5	13.7	36.0	05. r	5.92	-26	-31	-4	10002	CD-30 549
Gl 63	01 35 07	+56 58.9	0.397	204.4	-17.5	dM3	11.19	1.39		0.86	90.3	7.9	90.3	7.9	10.97	16	-12	-19		
NN	01 35 15	-49 26.7	0.534	75.2		K7	10.5 *			0.72	34.1	18.8	47.0	07. r	8.9 *					CD-49 451
Gl 64	01 35 26	-05 14.7	0.675	121.0		DA7	12.84	0.35	-0.49	0.12	81.4	3.4	81.4	3.4	12.39					
GJ 1040	01 35 32	+44 20.1	0.176	50.5		dK8	10.84	1.20		0.52	78.0	11.5	25.0	03. r	7.83					
NN	01 35 54	+00 23.7	0.529	72.9		k	11.55			0.93			54.0	10. r	10.21					
Gl 65 A	01 36 25	-18 12.7	3.368	80.4	29	dM5.5e	12.57	+1.85 J	+1.10 J	+1.69 J	380.7	4.3	380.7	4.3	15.47	-43	-19	-19		
Gl 65 B	01 36 25	-18 12.7	3.368	80.4	32	dM5.5e	12.7 *				380.7	4.3	380.7	4.3	15.6 *	-44	-19	-22		
NN	01 36 55	+04 48.2	0.168	33.0		M5	12.83						41.0	03. p	10.89					
NN	01 37 24	+31 32.3	0.481	90.7		m	13.91			1.29			61.0	10. r	12.84					
Gl 65.2	01 37 37	-46 45.7	0.080	166.0	29.4	M0	9.86	1.16	1.14	+0.57C	65.4	10.2	65.4	10.2	8.94	4	-15	-25		CP-47 195
NN	01 37 39	+63 33.6	0.013	311.9	-7	B5	10.07	0.47	0.23		76.7	25.6	76.7	25.6	9.5	5	-5	0		BD+63 219
Wo 9059	01 37 52	+66 39.7	0.748	110.3	14.4	G5 V	7.68	0.68	0.21		42.9	8.5	31.0	05. r	5.14	-99	-57	-18	10145	BD+66 145
Gl 66 A	01 37 54	-56 26.9	0.278	84.6	19.5	K2 V	5.80	0.86	0.57	0.30	148.9	5.4	148.9	5.4	6.66	-4	-14	-16	10361	CP-56 329
Gl 66 B	01 37 54	-56 26.9	0.278	84.6	22.5	K3 V	5.90	0.80	0.60	0.31	148.9	5.4	148.9	5.4	6.76	-3	-16	-18	10360	CD-56 328
Gl 67	01 38 44	+42 21.8	0.826	100.4	+3.1 SB	G1.5 V	4.95	0.62	0.12	+0.21t	73.1	3.9	73.1	3.9	4.27	-42	-34	0	10307	BD+41 328
Gl 67.1	01 39 09	-83 13.8	0.180	44.0	5.4	G2 V	5.88	0.61	0.09	0.21			58.0	09. r	4.7	-11	-6	-10	10800	CD-83 22
Gl 67.2	01 39 28	-45 40.3	0.247	90.2	-4.5	G5 V	9.30	0.69	0.25	0.25	52.9	11.9	52.9	11.9	7.92	-17	-12	9	10513	CP-46 177
Gl 68	01 39 47	+20 01.6	0.749	203.5	-33.7	K1 V	5.22	0.84	0.50	0.30	126.5	5.8	126.5	5.8	5.73	36	-26	1	10476	BD+19 279
Gl 69	01 40 12	+63 34.8	0.696	214.6	-50.7	K5 V	8.41	1.22	1.13	0.48	75.1	3.1	75.1	3.1	7.79	45	-28	-42	10436	BD+63 229
NN	01 40 18	-24 53.	0.035	190.0		m	12.02						41.0	06. p	10.08					
NN	01 40 25	+27 35.5	0.552	92.3		K7	10.40	1.46	1.26	0.71			52.0	08. r	8.98					BD+27 273
NN	01 40 34	-53 59.4	0.202	119.9	12.9	F8 V	5.52	0.53	0.00				53.0	07. r	4.14	-4	-21	-4	10647	CP-54 365
NN	01 40 45	-42 27.2	0.686	101.5		M0	11.25			0.78	32.1	15.3	40.0	06. r	9.26					CD-42 594
Gl 70	01 40 46	+04 04.9	0.861	209.5	-25.8	dM2	10.93	1.54		1.00	113.8	23.9	113.8	23.9	11.21	40	-20	2		
NN	01 41 29	-24 06.3	0.046	79.0		m	13.28						45.0	06. p	11.55					
NN	01 41 36	-67 32.2	1.048	197.8	51	DA7	13.88	0.44	-0.42	0.07			79.0	18. w	13.37	51	-23	29		
Gl 71	01 41 45	-16 12.0	1.924	296.4	-17	G8 Vp	3.49	0.72	0.22	0.26	286.0	4.9	286.0	4.9	5.77	18	28	13	10700	BD-16 295
Gl 73	01 42 18	+16 06.0	0.815	239.7		M3	14.11	1.67		1.30	61.2	3.9	61.2	3.9	13.04					
Gl 74	01 43 58	+12 09.8	0.078	163.7	21.9	dK8	8.90	1.05	0.91	0.40	38.1	5.4	40.0	05. r	6.91	-10	1	-21	10853	BD+11 231
Gl 75	01 44 06	+63 36.4	0.636	112.8	4	K0 V	5.63	0.81	0.40	0.26	97.2	4.6	97.2	4.6	5.57	-26	-16	-6	10780	BD+63 238
NN	01 44 06	-08 53.8	0.434	114.1		M3	12.99	1.58		1.20			57.0	13. r	11.77					
NN	01 45 17	+20 57.7	0.417	120.0		M3	12.16	1.58		1.03			56.0	14. r	10.9					
Gl 76	01 45 20	-26 59.7	0.295	200.4	25	K1 V	8.98	0.81	+0.44:	0.28	54.8	13.6	23.0	04. r	5.79	48	-34	-30	11020	CD-27 605
NN	01 45 52	+32 26.3	0.349	330.0	-26.5	F8 V	5.79	0.55	-0.01		38.6	9.4	49.0	06. r	4.24	25	9	34	11007	BD+31 316
Gl 77	01 46 12	-41 44.7	0.445	69.9	35.7	G4 V	7.14	0.65	0.20	+0.32C	63.3	13.6	37.0	07. r	4.98	-54	-31	-27	11112	CD-42 638
Wo 9061 A	01 47 08	-10 56.0	0.176	239.1	-0.9	F3 III	4.67	0.33	0.03	0.08	44.2	7.5	40.0	05. r	2.68	20	3	-6	11171	BD-11 352
Wo 9061 B	01 46 56	-10 57.0	0.175	239.8	-2.5	dG1	6.77	0.62	0.12	0.22	44.2	7.5	40.0	05. r	4.78	20	3	-5	11131	BD-11 351
NN	01 47 44	+18 02.9	0.250	105.0		M0	10.79	1.38	1.27				39.0	18. r	8.7					
NN A	01 48 12	+64 11.4	0.280	138.0	-15	dM2	11.37			0.98			67.0	13. r	10.5	-3	-22	-12		
NN B	01 48 12	+64 11.2	0.280	138.0		DA6	14.5 :						67.0	13. r	13.6 :					
NN	01 48 32	-06 21.8	0.584	113.5		m	14.6 *			1.53			100.0	17. r	14.6 *					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	01 48 38	+21 09.1	0.360	180.0		M4	13.90			1.27			56.0	10. r	12.64					
NN	01 48 56	+46 45.2	0.138	1.0	64	DA3	12.44	0.06	-0.63				61.0	07. w	11.37	-13	17	5		
Gl 78	01 49 19	-11 02.6	0.793	133.7	0	M3.5	11.80	1.50		0.94	86.0	13.3	86.0	13.3	11.47	-7	-43	-1		
Gl 78.1	01 50 13	+29 20.2	0.231	177.0	-16.2 SB	F6 IV	3.42	0.48	0.06		53.4	10.9	53.4	10.9	2.06	14	-21	-8	11443	BD+28 312
NN	01 50 22	+65 55.9	0.135	195.0		G5	8.48	1.01	0.97				42.0	04. o	6.6				11373	BD+65 210
Gl 79	01 50 25	-22 40.9	0.832	89.5	14.1	K5/M0 V	8.90	1.41	1.25	0.68	83.7	10.6	83.7	10.6	8.51	-39	-30	-3	11507	CD-23 693
Gl 80	01 51 52	+20 33.9	0.144	137.9	-4.0 SB	A5 V	2.64	0.13	0.10	-0.02	59.0	13.0	59.0	13.0	1.49	-1	-12	-2	11636	BD+20 306
Gl 81 A	01 54 01	-51 51.4	0.743	66.1	-6.3	G5 IV	3.70	0.85	0.45	0.31	54.8	9.0	54.8	9.0	2.39	-61	-18	10	11937	CP-52 241
Gl 81 B	01 54 01	-51 51.4	0.743	66.1			10.7 *				54.8	9.0	54.8	9.0	9.4 *					
Gl 81.1A	01 54 43	-10 29.0	0.440	238.8	-9.9	G5 IV	6.42	0.82	0.46	0.29	45.1	24.8	33.0	15. r	4	62	8	-14	11964	BD-10 403
Gl 81.1B	01 54 45	-10 29.4	0.438	239.0	-9	m	11.21	1.38	1.18		45.1	24.8	33.0	15. r	8.8	61	8	-15		
Gl 81.2	01 54 52	-60 28.4	0.473	66.6	0.4	K5 V	8.60	1.16	1.11	0.45	54.4	11.9	57.0	09. r	7.38	-37	-14	1	12058	CP-60 167
Gl 81.3	01 55 06	-52 00.8	0.430	54.0	3.8	F8 V	6.10	0.48	-0.04	+0.28C	53.4	11.1	40.0	04. s	4.11	-50	-9	-5	12042	CP-52 242
Gl 82	01 55 54	+58 16.9	0.351	124.0	-8.8	dM4 e	12.21	1.56		1.28	78.5	4.9	78.5	4.9	11.68	-9	-20	-6		
Gl 82.1	01 56 10	+32 58.3	0.431	144.9	-35.5	dG7	7.14	0.78	0.42				51.0	08. r	5.68	12	-52	-5	12051	BD+32 360
GJ 1041 A	01 56 36	+03 16.5	0.291	90.0		k-m	10.98	+1.52 J	+0.98 J	+1.09 J			93.0	18. r	10.82					BD+02 305
GJ 1041 B	01 56 36	+03 16.5	0.291	90.0		m	14.0 *						93.0	18. r	13.8 *					
NN	01 56 57	+43 31.2	0.276	155.0		m	13.01			1.07			41.0	08. r	11.07					
NN	01 57 09	+36 25.4	0.268	165.0		m	13.93:			1.19			40.0	08. r	11.94:					
Gl 83	01 57 12	-61 48.8	0.270	83.0	+15.2 VAR	F0 V	2.86	0.28	0.14	+0.16C	39.6	8.8	39.6	8.8	0.85	-23	-27	-6	12311	CP-62 162
NN	01 57 25	+73 18.1	0.319	104.0		m	14.12	1.90		+1.43t			95.0	17. r	14.01					
Gl 83.1	01 57 28	+12 50.1	2.097	147.8	-31	dM8 e	12.28	1.80	1.35	1.39	223.8	2.9	223.8	2.9	14.03	14	-52	5		
NN	01 57 56	+63 31.8	0.290	246.0		M4	11.03	1.54		1.07			100.0	20. r	11.03					
NN	01 58 21	-10 35.5	0.516	223.9		m	14.1 *			1.22			42.0	08. r	12.2 *					
Wo 9067 A	01 59 28	+03 42.1	0.482	225.3	-48	K4	10.62	1.22			42.2	16.0	26.0	04. r	7.69	98	-17	-9		BD+03 275
Wo 9067 B	01 59 28	+03 42.3	0.482	225.3		M1.5	12.4 *				42.2	16.0	26.0	04. r	9.5 *					
NN	01 59 37	+10 06.0	0.715	246.4		m	15.61	2.02			112.0	1.9	112.0	1.9	15.86					
NN	02 00 01	+13 20.3	0.472	103.0		dM5 :	14.27						58.0	06. p	13.09					
NN	02 00 49	+35 21.1	0.061	250.8		G5	8.36						78.0	08. o	7.82				12545	BD+34 363
NN	02 01 01	-21 27.8	0.464	209.7		M3	11.21	1.46		1.00	33.9	23.9	77.0	18. r	10.6					BD-21 368
Gl 83.4A	02 01 55	-45 39.2	0.333	78.6	42.7	G3 V	7.31	0.69	0.22	+0.37C	49.4	11.9	37.0	07. r	5.15	-36	-38	-30	12759	CD-46 604
Gl 83.4B	02 01 55	-45 39.2	0.333	78.6			11.5 *				49.4	11.9	37.0	07. r	9.3 *					
NN	02 01 57	-02 06.8	0.832	224.2		m	13.9 *			1.22			46.0	08. r	12.2 *					
NN	02 02 35	-15 55.0	0.034	156.0		K0 V	7.78						42.0	04. o	5.9				12786	BD-16 365
Gl 84	02 02 37	-17 51.1	1.299	96.8	-35	M3	10.19	1.51	1.15	1.02	118.0	8.5	118.0	8.5	10.55	-22	-36	46		BD-18 359
Gl 84.1A	02 03 07	-28 18.8	0.548	40.2		M0.5	10.92	1.40	1.15	0.73	51.9	13.9	47.0	07. r	9.28					CD-28 657
Gl 84.1B	02 03 08	-28 17.9	0.548	40.2		M3.5	12.80	1.50	1.12	1.15	51.9	13.9	47.0	07. r	11.16					
NN	02 03 23	+64 03.1	0.284	125.0		m	14.31			1.28			48.0	08. r	12.72					
NN	02 03 38	-30 25.0	0.537	282.2		M3.5	12.15			1.08			65.0	13. r	11.21					
Gl 84.2A	02 03 48	+44 57.2	0.510	147.9	62	dM0	10.28	1.49	1.24		55.3	6.7	55.3	6.7	8.99	-61	12	-44		
Gl 84.2B	02 03 48	+44 57.2	0.510	147.9			14.2 *				55.3	6.7	55.3	6.7	12.9 *					
Gl 84.3	02 04 21	+23 13.6	0.239	126.8	-14.4 SB	K2 IIIab	2.00	1.15	1.13		46.6	7.6	46.6	7.6	0.34	-1	-28	3	12929	BD+22 306

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Wo 9073 A	02 05 02	-00 51.0	0.421	215.5	-40.2	G2 V	6.90	0.61	0.16	0.21	40.4	8.1	32.0	04. r	4.43	71	-22	1	13043	BD-01 293
Wo 9073 B	02 05 00	-00 49.8	0.434	215.0	-39.4	K4	10.52	1.24	1.23	0.52	40.4	8.1	32.0	04. r	8.05	72	-23	-1		
NN	02 05 38	+49 13.0	0.384	135.0		M5 :	12.47	1.54		1.17			70.0	14. r	11.7					
NN	02 05 55	+88 10.0	0.433	348.0		m	12.89			1.11			49.0	10. r	11.34					
Gl 85	02 05 56	-66 48.7	1.798	77.7	-33	m	11.52	1.53	1.08	0.88	64.6	20.5	49.0	09. r	9.97	-153	-72	53		
NN	02 06 46	-16 34.9	0.556	82.3		K7	10.95			0.74	40.3	9.4	40.0	06. r	8.96					BD-17 400
Gl 85.1	02 07 07	+35 12.0	0.567	213.0		M3	13.74	1.48	1.08		44.9	10.2	44.9	10.2	12					
NN	02 07 10	-14 35.4	0.629	123.3		M3	11.82	1.54		1.02			63.0	15. r	10.8					
NN	02 07 33	+11 18.0	0.086	193.0		dM4	12.72						90.0	30. p	12.5					
GJ 1042	02 08 13	+39 41.6	1.144	115.7	29	DZ7	14.52	0.33	-0.47		59.2	10.4	59.2	10.4	13.38	-45	-81	-5		
Gl 86	02 08 25	-51 04.1	2.264	72.9	53.1	K0 V	6.12	0.82	0.44	0.32	89.4	9.0	89.4	9.0	5.88	-103	-77	-25	13445	CD-51 532
Gl 87	02 09 51	+03 22.0	2.598	223.5	-2.7	dM2.5	10.06	1.44	1.08	0.87	86.7	7.4	86.7	7.4	9.75	117	-13	-80		BD+02 348
GJ 1043	02 10 00	+20 58.6	0.168	88.6	6	F5 V	5.27	0.43	-0.05				43.0	05. r	3.44	-17	-9	2	13555	BD+20 348
NN	02 10 02	-63 28.0	0.778	242.9		m	12.25			1.06			56.0	11. r	10.99					
Gl 87.1A	02 10 14	-02 37.6	0.373	99.9	-6.0 SB	F8 V	5.67	0.56	0.07	0.19	39.7	10.7	34.0	04. r	3.33	-28	-41	17	13612	BD-03 336
Gl 87.1B	02 10 13	-02 37.8	0.379	98.7	-5.6	G5 V	7.74	0.68	0.22	0.22	39.7	10.7	34.0	04. r	5.4	-30	-40	17		BD-03 335
NN	02 10 19	-00 13.8	0.546	89.2		m	13.5 *			1.24			60.0	11. r	12.4 *					
Gl 88	02 10 27	-17 55.4	0.519	66.9	34.9	M0	11.09	1.47	+1.2 :	0.73	44.9	16.3	40.0	08. r	9.1	-67	-20	-11		
Gl 89	02 10 42	-30 57.5	0.019	55.8	+10. VAR	A2 Vn	5.28	-0.02	-0.06	-0.00C	63.0	15.3	63.0	15.3	4.3	-3	-3	-9	13709	CD-31 882
GJ 1044	02 10 50	-21 25.6	0.332	80.0		K7 V	9.88	1.36	1.26	0.58			47.0	09. r	8.24					BD-21 397
Gl 90	02 11 35	+67 26.6	0.597	119.3	-12.1	K2 V	7.09	0.90	0.67		33.6	17.6	70.0	11. r	6.32	-23	-34	-9	13579	BD+67 191
Gl 91	02 11 40	-32 16.0	0.957	126.4	45.5	M2.5	10.32	1.50	1.11	0.94	108.5	15.3	108.5	15.3	10.5	-15	-51	-31		CD-32 828
GJ 1045	02 12 14	+17 11.5	0.594	143.3		m+	14.44	1.62	1.08	1.29	47.4	3.8	47.4	3.8	12.82					
NN	02 12 35	+33 44.1	0.424	156.5		m	13.58			1.24			58.0	11. r	12.4					
NN	02 13 12	+39 37.6	0.196	239.0		DA6	14.54	0.23	-0.61				45.0	04. w	12.81					
NN	02 13 22	-12 54.5	0.544	67.1		M3	13.00	1.50		1.12			44.0	11. r	11.2					
Gl 91.2A	02 13 25	-18 28.2	0.193	199.4	5.3	K3 V	8.42	+1.02 J	+0.80 J	+0.40 J			44.0	06. r	6.64	15	-11	-11	14001	BD-18 394
Gl 91.2B	02 13 25	-18 28.2	0.193	199.4		K	9.1 *						44.0	06. r	7.3 *					
Gl 91.3	02 13 46	+42 44.6	1.009	125.2		DC9	16.20	0.72	-0.01		50.9	4.6	50.9	4.6	14.73					
NN	02 13 47	+13 22.1	0.660	128.2		m	15.79	1.98			118.2	6.8	118.2	6.8	16.15					
Gl 92	02 14 00	+33 59.8	1.179	101.2	-6.6 SB	G0 Ve	4.87	0.61	0.02	0.24	98.1	5.0	98.1	5.0	4.83	-33	-46	11	13974	BD+33 395
NN	02 14 08	+35 12.9	0.595	116.4		m+	15.99				96.6	1.1	96.6	1.1	15.91					
NN A	02 14 27	-31 13.4	0.711	68.9		M4	12.0 *			1.16			88.0	17. r	11.7 *					CD-31 909
NN B	02 14 21	-31 12.2	0.711	68.9		M4	13. :			1.26			88.0	17. r	13. :					
Gl 92.1	02 14 52	+56 20.0	0.401	122.2	3.2	K1 V	8.27	0.92	0.70		46.7	10.3	41.0	06. r	6.33	-34	-30	-11	14039	BD+55 570
Gl 92.2	02 15 00	+44 02.4	0.535	104.8		M3	13.49	1.53		1.21	44.5	25.6	45.0	11. r	11.8					
Gl 93	02 15 50	-54 13.5	0.626	52.0		m	11.43	1.41	1.00	0.76	73.2	13.6	73.2	13.6	10.75					CD-54 487
Gl 94	02 16 00	+35 07.7	0.792	121.5		M3.5	12.55	1.47	1.08		54.8	8.5	54.8	8.5	11.24					
NN	02 16 11	+23 39.1	0.289	108.0		m	14.17			1.26			47.0	08. r	12.53					
Gl 95	02 16 44	-26 10.9	0.500	333.9	7	G5 V	6.34	0.73	0.18	0.26	80.5	9.4	80.5	9.4	5.87	-11	27	-10	14412	CD-26 828
GJ 1046	02 16 59	-37 00.9	1.497	68.5	47	M3	11.62	1.50	1.17	1.01			66.0	16. r	10.7	-103	-53	-16		
NN A	02 17 21	+37 33.8	0.350	101.0		m	12.68			+1.05 J			40.0	08. r	10.69					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN B	02 17 21	+37 33.8	0.350	101.0		k	16.7 *						40.0	08. r	14.7 *					
GJ 1047 A	02 17 59	+36 39.8	0.919	128.3		m	14.05	+1.68 J		+1.13 J	46.3	3.6	46.3	3.6	12.38					
GJ 1047 B	02 17 59	+36 39.8	0.919	128.3		m	14.05				46.3	3.6	46.3	3.6	12.38					
GJ 1047 C	02 17 57	+36 39.5	0.919	128.3		m	14.26	1.70	1.50	1.16	46.3	3.6	46.3	3.6	12.59					
NN	02 18 10	+02 45.0	0.288	153.0		m	14.78	1.69					41.0	17. r	12.8					
NN	02 18 39	-39 15.7	0.215	98.8		K3/4 V	8.74	1.04	0.84	0.38			41.0	05. r	6.8				14629	CD-39 684
Gl 96	02 18 57	+47 39.1	0.226	77.2	-37.3	VAR dM1.5e	9.41	1.49	1.18	0.77	86.8	2.8	86.8	2.8	9.1	19	-31	15		BD+47 612
Wo 9079	02 19 11	-31 09.8	0.561	80.2	54	K3 V	8.81	0.93	0.66	0.32	42.3	7.8	32.0	05. r	6.34	-78	-57	-23	14680	CD-31 943
NN	02 19 14	-07 06.5	0.311	77.7		K0	8.98	1.08	0.96				40.0	07. r	6.99					BD- 7 410
Gl 97	02 20 15	-24 02.6	0.206	106.5	18.4	G1 V	5.20	0.60	0.12	0.24	83.3	25.7	83.0	13. r	4.8	-11	-13	-14	14802	CD-24 1038
Gl 97.1	02 20 51	-68 53.2	0.045	275.7	+6.	VAR A3 Vn	4.08	0.03	0.05	+0.02C	48.1	17.0	48.1	17.0	2.5	4	-1	-6	15008	CP-69 113
NN	02 21 54	+25 45.1	0.191	228.0		m	11.62			0.83			39.0	07. r	9.58					
NN	02 22 33	+37 19.1	0.276	103.0		m	14.05			1.27			52.0	09. r	12.63					
Wo 9082	02 23 23	+05 33.2	0.391	70.4	10	G9	7.95	0.81	0.32		44.0	20.5	36.0	06. r	5.73	-46	-17	19	15096	BD+05 336
Gl 98 A	02 25 09	+04 12.3	0.255	34.2	10.4	K7 V	9.36	+1.39 J	+1.11 J	+0.67 J	60.9	3.8	60.9	3.8	8.28	-21	7	4	15285	BD+03 339
Gl 98 B	02 25 09	+04 12.3	0.255	34.2		K7 V	9.5 *				60.9	3.8	60.9	3.8	8.4 *					
NN	02 25 30	+02 58.0	0.845	180.5		m	17.46	+2.06:			45.1	7.9	45.1	7.9	15.73					
NN	02 25 42	+01 13.2	0.296	112.0		m	13.05			1.09			43.0	09. r	11.22					
Gl 99 A	02 25 46	+32 02.1	0.421	72.0	-9.7	dM0 pJ	10.20	+1.36 J	+1.23 J	+0.64 J	32.2	5.6	32.2	5.6	7.74	-34	-33	41		BD+31 434
Gl 99 B	02 25 46	+32 02.1	0.421	72.0			10.5 *				32.2	5.6	32.2	5.6	8.0 *					
Gl 99.1	02 25 52	+29 42.5	0.093	318.8	41	G0 V	5.88	0.58	0.01	0.21	31.7	4.3	31.7	4.3	3.39	-26	32	-14	15335	BD+29 423
NN	02 26 12	+11 52.0	0.067	42.0		M1	12.01	1.57	1.17	1.01			56.0	11. r	10.75					
Gl 100 A	02 26 41	-20 12.3	0.689	70.6	23	K4 V	8.86	+1.18 J	+1.03 J	0.48	38.9	19.0	49.0	06. r	7.31	-65	-28	5	15468	BD-20 465
Gl 100 B	02 26 41	-20 12.3	0.689	70.6			11.4 *				38.9	19.0	49.0	06. r	9.9 *					
Gl 100 C	02 26 12	-20 15.9	0.668	65.7		M3	12.85	1.61	1.22	1.06	38.9	19.0	49.0	06. r	11.3					
Gl 100.1	02 27 39	+05 02.6	0.098	101.2	30	DA3	12.79	-0.04	-0.83				45.0	05. w	11.06	3	-11	14		
Gl 101	02 27 44	+57 09.5	1.042	88.5		M3.5	13.21	1.52		1.18	60.0	5.1	60.0	5.1	12.1					
Wo 9083	02 28 55	+02 02.8	0.023	89.5	26.1	K3 III	5.25	1.27	1.41		40.0	17.0	40.0	17.0	3.3	-17	2	-20	15694	BD+01 438
Gl 101.1	02 29 18	-46 54.4	0.290	177.0	34.5	m	11.27	1.03	+0.9 :	+0.54C	64.0	10.2	64.0	10.2	10.3	14	-29	-24		CD-47 765
NN	02 30 10	+14 48.9	0.050	324.2	+8.8	SB F8 V	6.02	0.54	0.04				44.0	07. r	4.24	-5	8	-4	15814	BD+14 419
NN	02 30 15	-14 24.5	0.693	174.6		DC	15.76	0.75	-0.01		64.6	6.6	64.6	6.6	14.81					
NN	02 30 20	+07 40.1	0.031	13.9		G5	8.89	1.15	0.75				40.0	08. r	6.9				15833	BD+ 7 398
Gl 102	02 30 44	+24 42.9	0.687	176.8		M4	12.96	1.70	1.20	1.31	102.4	7.7	102.4	7.7	13.01					
NN	02 30 48	+41 33.6	0.303	74.0		m	13.62			1.16			41.0	08. r	11.68					
NN	02 31 01	+14 47.1	0.431	85.0		M3.5	13.76	1.63		1.16			39.0	10. r	11.7					
Gl 103	02 32 28	-44 00.6	0.297	168.5	+41.9	SB K7 Ve	8.85v	1.39	1.02	0.77	87.2	10.7	87.2	10.7	8.55v	6	-30	-33	16157	CD-44 775
NN	02 32 30	+23 21.			-12	M3 e	13.71	1.58	1.00	+1.22t			48.0	10. r	12.12	9	-5	7		
NN	02 32 37	-72 54.5	0.238	37.8		K4 V	8.90	1.04	0.99	0.41			41.0	06. r	6.96				16348	CP-73 178
Wo 9085	02 32 49	-03 46.3	0.469	200.0	-50.7	G5 IV	6.82	0.67	0.21		42.4	8.2	42.4	8.2	4.96	66	-28	15	16141	BD-04 426
NN	02 32 55	+55 15.8	0.355	222.0		m	13.22			1.11			42.0	09. r	11.34					
Gl 104	02 33 03	+20 00.3	0.272	121.0	-22.3	dM2	10.66	1.51	1.17	0.95	69.0	6.3	69.0	6.3	9.85	8	-25	13		BD+19 381
Gl 105 A	02 33 20	+06 39.0	2.322	51.0	26	K3 V	5.82	0.98	0.80	0.36	129.4	4.3	129.4	4.3	6.38	-81	0	36	16160	BD+06 398

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 105 B	02 33 31	+06 38.0	2.322	51.4	25.7	dM4.5	11.66	1.60	1.11	1.25	129.4	4.3	129.4	4.3	12.22	-81	0	36		
GJ 1048	02 33 45	-23 44.3	0.082	80.9		K2 V	8.43	1.08	0.96	0.40			50.0	08. r	6.92				16270	CD-24 1154
NN A	02 33 49	+31 51.4	0.330	260.0		M3	13.63			+1.22 J			41.0	07. r	11.69					
NN B	02 33 49	+31 51.4	0.330	260.0		M3.5	13.9 *						41.0	07. r	12.0 *					
Wo 9086	02 34 06	-47 52.9	0.210	119.0		G0	11.99	0.55	0.00	+0.3 C	42.6	13.6	42.6	13.6	10.1					
Wo 9087	02 34 09	-03 22.4	0.335	81.6	9	K3	8.10	0.95	0.73		38.0	17.5	48.0	08. r	6.51	-29	-17	7	16287	BD-03 410
NN	02 34 24	+06 41.				M5 e	16.00			+1.85C			48.0	09. r	14.41					
NN	02 34 54	+00 08.5	0.543	107.0		m	15.16	1.67	1.23		40.6	4.3	40.6	4.3	13.2					
Gl 105.1	02 34 54	-34 47.5	0.259	183.5	10.3	G5 IV	5.78	0.65	0.20	0.21	55.2	8.5	55.2	8.5	4.49	15	-17	-8	16417	CD-35 903
Wo 9089	02 35 31	+30 36.4	0.625	231.4	-103	G1 V	7.34	0.60	0.00		44.0	12.1	31.0	03. s	4.8	133	-34	-31	16397	BD+30 421
NN	02 35 52	+06 24.8				DA8	15.09	0.44	-0.51				59.0	10. w	13.94					
NN	02 36 37	+07 15.5	0.446	105.1		m	14.27			1.26			45.0	08. r	12.54					
Gl 105.3	02 36 56	-26 31.8	0.277	139.6	16.1	G2 V-VI	8.76	0.60	0.01	+0.34C	47.5	11.9	47.5	11.9	7.1	-2	-31	-9	16623	CD-26 957
Gl 105.4A	02 37 09	-12 05.0	0.276	148.3	+15.7 SB	F5 V	5.50	+0.44 J	-0.01 J	+0.25CJ	68.6	7.2	68.6	7.2	4.68	-4	-20	-14	16620	BD-12 501
Gl 105.4B	02 37 09	-12 05.0	0.276	148.3	16.8	F5 V	5.6 *				68.6	7.2	68.6	7.2	4.8 *	-5	-20	-15		
GJ 1049	02 37 36	-58 24.1	0.038	333.0		M0 Ve	9.65	1.39	1.10	0.76			77.0	16. r	9.08					CD-58 538
GJ 1050	02 37 44	-34 19.5	1.721	161.7	-71	m	11.75	1.52	1.09	1.04			66.0	13. r	10.85	79	-80	88		
NN	02 37 46	-09 40.0	0.160	240.8	-4	F8 V	5.78	0.52	0.00				45.0	06. r	4.05	16	4	-5	16673	BD-10 525
Gl 105.5	02 38 07	+00 58.9	0.370	49.7	79	dM0 p	9.52	1.20	1.09	0.50	41.6	6.3	43.0	05. r	7.69	-81	7	-37		BD+00 444
Wo 9094	02 38 28	-30 21.0	0.574	81.3	33.2	G0 V	8.02	0.56	-0.02	0.22	42.0	9.3	21.0	03. s	4.63	-104	-81	22	16784	CD-30 990
Gl 105.6	02 39 05	+39 59.0	0.184	186.0	-22.8 SB	F9 V	4.92	0.59	0.14	+0.19t	42.7	7.4	42.7	7.4	3.07	19	-21	-11	16739	BD+39 610
Gl 106	02 40 30	+19 13.1	0.432	90.7	+29.2 SB	dK4	8.28	1.07	0.95	0.40	54.7	10.2	54.0	08. r	6.94	-45	-16	-2	16909	BD+18 339
Gl 106.1A	02 40 42	+03 01.6	0.207	224.5	-5.1	A3 V	3.56	+0.09 J	+0.07 J		46.9	4.3	46.9	4.3	1.92	19	-2	-10	16970	BD+02 422
Gl 106.1B	02 40 42	+03 01.6	0.207	224.5	-12.5	dF3	6.3 *				46.9	4.3	46.9	4.3	4.7 *	24	-3	-4		
Gl 106.1C	02 39 54	+03 09.9	0.215	220.0		K5	10.16	1.36	1.28	0.57	42.0	4.2	42.0	4.2	8.28					BD+02 418
Gl 107 A	02 40 46	+49 01.1	0.346	104.0	24.4	F7 V	4.13	0.49	0.00	0.18	79.3	4.1	79.3	4.1	3.63	-32	0	0	16895	BD+48 746
Gl 107 B	02 40 46	+49 01.1	0.346	104.0	25.1	M1 V	10.06	1.48		0.89	79.3	4.1	79.3	4.1	9.56	-33	0	0		
Gl 108	02 40 51	-51 00.9	0.405	56.4	15.5	G3 IV	5.41	0.56	0.09	+0.30C	68.3	9.7	68.3	9.7	4.58	-27	-15	-8	17051	CD-51 641
NN	02 40 55	-39 08.8	0.558	103.9		M3.5	13.1 *			1.10			45.0	09. r	11.4 *					
Gl 109	02 41 18	+25 19.0	0.923	113.8	29.9	dM3.5	10.57	1.56	1.21	1.08	125.6	2.7	125.6	2.7	11.06	-40	-18	-13		
GJ 1051	02 41 22	-09 02.4	0.924	140.5	6	M2.5	11.92	1.46	1.07	0.85	57.3	13.4	57.3	13.4	10.7	0	-77	-4		
NN	02 42 11	-36 31.1	0.034	102.9		G5 V	7.12						53.0	05. o	5.74				17169	CD-36 1033
Wo 9099	02 42 14	+09 54.3	0.284	96.2	+30.4 SB	F0 IV	4.27	0.31	0.08	0.05	48.3	13.7	48.3	13.7	2.7	-37	-14	-11	17094	BD+09 359
NN A	02 42 20	+44 44.4	0.422	107.0		K6	10.85	1.40	1.27	0.77			47.0	08. r	9.21					
NN B	02 42 22	+44 44.6	0.435	106.7		m	15. *						47.0	08. r	13. *					
Gl 111	02 42 46	-18 47.0	0.334	83.5	+25.6 SB	F6 V	4.46	0.48	-0.01	+0.17t	71.0	17.7	73.0	09. r	3.78	-26	-17	-13	17206	BD-19 518
Gl 112	02 43 20	+25 26.5	0.286	121.1	14.5	K1 IV	7.88	0.84	0.50	0.29	52.6	11.0	52.6	11.0	6.48	-22	-17	-8	17190	BD+25 449
Gl 112.1	02 43 34	+11 34.1	0.332	126.7	11.3	dK8	8.59	1.28	1.24	0.52	56.1	13.8	73.0	09. r	7.91	-14	-18	-8	17230	BD+11 383
NN	02 43 39	-05 10.3	2.524	138.1		m	15.86:	+1.50:			61.0	8.2	61.0	8.2	14.79:					
NN	02 43 51	+16 13.1	0.981	235.7	-34	M6	16.86	2.02			66.7	6.5	66.7	6.5	15.98	72	1	-29		
GJ 1052	02 43 58	-02 39.6	0.513	154.8		DA7	15.53	0.36	-0.51		47.7	5.7	47.7	5.7	13.92					
NN	02 45 03	+54 11.1	0.613	224.1		DC9	15.32	0.93	0.35		97.0	3.6	97.0	3.6	15.25					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 113 A	02 45 12	+26 51.7	0.304	115.7	11.1	K1 Ve	7.61	0.83	0.43		55.6	15.4	46.0	07. r	5.92	-24	-23	-4	17382	BD+26 465
Gl 113 C	02 45 12	+26 52.0	0.296	112.0		m	16.5 P				55.6	15.4	46.0	07. r	14.8 P					
Gl 113.1	02 45 42	+30 54.6	0.273	128.5	-2.8 SB	G9 e	6.76	0.96	0.63		49.9	15.3	78.0	12. r	6.22	-5	-16	-1	17433	BD+30 448
Gl 114	02 47 49	+15 30.6	0.525	137.6	-25	dK6	8.90	1.20	1.10	0.43	57.3	23.9	49.0	08. r	7.35	9	-56	6	17660	BD+15 395
Gl 114.1A	02 48 31	-53 21.3	0.531	348.4		k-m	10.72	1.51	1.20	0.93	44.4	9.8	44.4	9.8	8.96					CD-53 570
NN	02 48 51	+29 17.1	0.180	204.0		m	13.96			1.30			62.0	10. r	12.92					
Gl 115	02 48 52	-44 17.0	0.270	187.1	30.5	F8 V	8.17	0.55	-0.01:	+0.34C	61.9	13.6	61.9	13.6	7.13	14	-25	-23	17865	CD-44 863
Gl 116	02 48 58	+34 11.9	1.342	136.1	-45.7	dM0	9.55	1.34	1.02		66.7	7.8	66.7	7.8	8.67	0	-105	-9		BD+33 529
NN	02 49 11	+06 01.5	0.487	103.3		dM3	13.19	1.58					44.0	20. r	11.4					
NN	02 49 23	+60 39.0	0.172	120.8	-69.6	K5 V	9.16	1.07	1.03	0.42	30.3	12.2	39.0	06. r	7.12	37	-63	-3		BD+65 585
NN	02 49 28	+26 46.4	0.215	178.0		dM0	11.11	1.49		0.84			52.0	09. r	9.69					
Gl 117	02 50 07	-12 58.3	0.435	115.2	+18.8 VAR	K2 V	6.03	0.87	0.55	0.31	120.4	8.8	120.4	8.8	6.43	-14	-18	-11	17925	BD-13 544
NN	02 50 14	-33 39.3	0.434	92.4	60.9	K1 V	8.09	0.84	+1.93C	0.30	39.3	8.2	38.0	05. r	5.99	-47	-60	-30	17970	CD-33 992
Gl 118	02 51 14	-63 53.5	1.149	58.4	94	m	11.38	1.56	1.20	1.05	81.0	17.0	81.0	17.0	10.92	-48	-85	-62		
NN	02 51 58	+61 19.1	0.148	75.0	29.2	F4 V	5.59	0.45	0.10				42.0	08. r	3.71	-30	10	12	17948	BD+60 591
Gl 118.1A	02 52 00	-36 06.3	0.562	106.8	+5.5 SB	K3 V	8.23	0.93	0.65	0.36	47.9	8.2	43.0	06. r	6.4	-23	-53	23	18168	CD-36 1091
Gl 118.1B	02 52 00	-36 06.9	0.532	106.7		M3 :	13.10	1.52	1.21	1.06	47.9	8.2	43.0	06. r	11.27					
Gl 118.2A	02 52 41	+26 40.4	0.324	124.6	31.8	dK2	7.60	0.93	0.71	0.30	39.6	6.5	53.0	06. r	6.22	-37	-14	-17	18143	BD+26 484
Gl 118.2B	02 52 41	+26 40.4	0.324	124.6	27	dM0	9.80	1.40	1.50		39.6	6.5	52.0	06. r	8.38	-33	-17	-14		
Gl 118.2C	02 52 38	+26 40.3	0.322	125.0		m	13.86	1.58	1.17	1.25	39.6	6.5	52.0	06. r	12.44					
Gl 119 A	02 52 50	+55 14.5	0.833	123.9	76.6	M1	10.48	1.39	1.19	0.78	44.8	3.9	44.8	3.9	8.74	-114	-18	-15		
Gl 119 B	02 52 50	+55 14.8	0.833	123.9		M3	11.65	1.42	1.10	1.02	44.8	3.9	44.8	3.9	9.91					
Wo 9106	02 53 27	+13 42.8	0.113	235.5	3.1	K0	9.05	0.81	0.46		41.1	18.8	23.0	03. r	5.86	13	4	-19	18257	BD+13 476
Gl 120	02 54 43	+10 35.8	1.821	102.9	49	dM4	13.03	1.56	1.11	1.10	46.8	7.5	46.8	7.5	11.38	-126	-141	27		
Gl 120.1A	02 55 02	-25 10.1	0.025	126.4	50.6	K1/2 V	8.03	+0.87 J	+0.52 J				44.0	04. r	6.25	-20	-17	-44	18455	CD-25 1169
Gl 120.1B	02 55 02	-25 10.1	0.025	126.4			8.2 *						44.0	04. r	6.4 *					
Gl 120.1C	02 55 01	-25 10.5	0.039	145.9	+49.6 SB	K2 V	7.83	0.95	0.74				44.0	04. r	6.05	-18	-18	-43	18445	CD-25 1168
NN	02 55 46	-13 05.5	0.651	28.8	107	M2.5	12.67	1.73		1.04			45.0	13. r	10.9	-113	9	-58		
GJ 2028	02 55 54	-70 34.0	0.682	97.9	107	DA6	14.08	0.23	-0.59				43.0	05. w	12.25	-20	-95	-2		
NN	02 56 00	+36 25.0	0.680	115.5		M3.5	13.04	1.52		1.16			53.0	14. r	11.7					
NN	02 56 14	+31 34.3	0.228	15.0		m	13.41			1.12			40.0	08. r	11.42					
Gl 120.2	02 59 28	+26 24.9	0.280	124.5	9.6	G8 V	6.62	0.72			36.8	7.4	42.0	04. s	4.74	-20	-26	-5	18803	BD+26 503
Wo 9107	02 59 28	-28 16.9	0.514	147.4	43.3	G5 IV	5.88	0.79	0.33	0.31	39.5	7.6	39.5	7.6	3.86	4	-71	-25	18907	CD-28 987
NN A	02 59 32	-16 47.0	0.435	232.0		M3	10.96	+1.69 J		+1.16 J			131.0	30. r	11.55					
NN B	02 59 32	-16 47.0	0.435	232.0		M3	11.8 *						131.0	30. r	12.4 *					
NN A	03 00 03	+61 31.2	0.993	132.8	3.8	G4 V	6.62	0.63	0.15		36.2	7.2	45.0	06. r	4.89	-72	-72	-25	18757	BD+61 513
NN B	03 00 37	+61 33.1	0.996	133.7		M3	12.6 *				36.2	7.2	45.0	06. r	10.9 *					
Gl 121	03 00 11	-23 49.2	0.157	250.8	-9.8	A4 IV	4.08	0.16	0.08	+0.10C	61.6	13.3	61.6	13.3	3.03	13	8	3	18978	CD-24 1387
Gl 121.1	03 00 20	-18 21.6	0.435	66.0		m	11.80	1.53		+1.30C	64.1	15.3	64.1	15.3	10.8					
Gl 121.2	03 01 09	-05 51.5	0.436	127.1	-20.6	dG5	8.09	0.67	0.11	+0.36C	49.1	10.1	49.1	10.1	6.55	8	-40	23	19034	BD-06 594
NN A	03 01 17	-13 02.1	0.262	112.0		k-m	13.37			1.17			48.0	06. r	11.78					
NN B	03 01 24	-13 02.9	0.262	112.0		k-m	13.50			1.18			48.0	06. r	11.91					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B−V	U−B	R−I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	03 01 47	-20 33.9	0.685	135.9		M3	12.84	1.59		1.19			65.0	13. r	11.9					
Gl 122	03 03 15	+75 51.8	0.555	157.5	34	dM0	9.82	1.38	1.26	0.63	51.8	7.2	51.8	7.2	8.39	-57	4	-20		
NN A	03 03 38	+40 10.1	0.434	249.0	-51.1	K5	9.71	+1.19 J	+1.06 J	+0.56 J	32.6	15.3	40.0	07. r	7.72	68	-4	-25		BD+39 0710
Gl 123	03 03 50	+01 47.2	0.992	156.8	-30.2	M0 V	9.09	1.38	1.22	0.62	63.6	4.0	63.6	4.0	8.11	36	-71	3	19305	BD+01 543
NN	03 04 57	-13 57.0	0.261	182.5	12.3	G5 V	6.97	0.65	0.15	0.21	43.4	17.0	40.0	06. r	4.98	14	-24	-19	19467	BD-14 604
NN	03 05 03	+42 51.0	0.558	139.8		m	14.7 *	+1.5 *			40.7	8.0	40.7	8.0	12.7 *					
NN	03 05 04	-04 09.6	0.461	217.0		dK7	10.87	1.43		0.72			42.0	07. r	8.99					
GJ 1053	03 05 16	+73 35.8	2.104	120.0		sdM6	14.64	1.79		1.45	82.9	4.9	82.9	4.9	14.23					
Gl 124	03 05 27	+49 25.4	1.267	93.6	49.5	G0 V	4.05	0.60	0.12	0.20	92.4	4.5	92.4	4.5	3.88	-77	-17	22	19373	BD+49 857
GJ 1054 A	03 05 49	-28 24.4	0.376	250.0		K7 V	10.24	1.41	1.08	0.76			46.0	07. r	8.55					CD-28 1030
GJ 1054 B	03 05 47	-28 25.5	0.376	250.0		m+	13.09	1.64	1.22	1.07			46.0	07. r	11.4					
NN	03 05 53	-24 57.6	0.333	64.0		m	9.5 *			0.66			68.0	10. r	8.7 *					CD-25 1273
Gl 125	03 06 09	+45 32.9	0.540	232.4	-9.3	dM1	10.15	1.49	1.21	0.94	76.7	11.4	76.7	11.4	9.57	19	2	-29		
GJ 1055	03 06 17	+09 50.5	0.646	153.1		m	14.85	1.72	+1.30:	1.45	84.2	4.0	84.2	4.0	14.48					
NN	03 06 33	+58 15.0	0.272	146.0		M3	11.72	1.50		0.92			48.0	09. r	10.13					
GJ 1056	03 07 13	-60 21.9	0.242	54.1		K5 V	9.35	1.22	1.14	0.50			47.0	08. r	7.71				19819	CD-60 637
NN	03 07 37	+05 43.6	0.563	191.5		dM4	11.88			0.98			53.0	10. r	10.5					
NN	03 07 48	+61 21.0	0.090	8.0		dK8	10.12	1.32		0.64	29.0	8.5	48.0	07. r	8.53					BD+60 637
Gl 126	03 09 33	-46 42.7	0.440	25.0		m	11.52	1.44	1.21	+1.03C	74.6	10.2	74.6	10.2	10.88					CD-46 943
NN	03 09 38	-38 58.4	0.859	103.1		M3.5	11.51	1.51	1.22	0.90			57.0	14. r	10.3					
Gl 127 A	03 09 57	-29 11.0	0.727	27.6	-20	F7 IV	3.95	+0.51 J	+0.05 J	+0.20 J	72.7	7.7	72.7	7.7	3.26	-36	20	30	20010	CD-29 1177
Gl 127 B	03 09 57	-29 11.0	0.727	27.6		G7 V	6.7 *				72.7	7.7	72.7	7.7	6.0 *					
Gl 127.1A	03 10 04	-68 47.2	0.080	130.0		DA3	11.40	0.05	-0.55		84.9	10.2	84.9	10.2	11.04					BD-69 177
Gl 127.1B	03 10 04	-68 47.2	0.080	130.0			14.73	0.62			84.9	10.2	84.9	10.2	14.37					
Gl 128 A	03 10 13	-01 22.9	0.202	108.2	+19.2 SB?	F8 V	5.06	0.57	0.12	+0.30C	53.3	9.9	53.3	9.9	3.69	-19	-16	-8	19994	BD-01 457
Gl 128 B	03 10 13	-01 22.9	0.202	108.2			11.5 *				53.3	9.9	53.3	9.9	10.1 *					
Gl 130	03 10 30	-38 17.2	1.434	59.7	98	M3	11.46	1.56	1.22	0.90	80.3	41.1	60.0	14. r	10.4	-123	-77	-38		CD-38 1058
GJ 1057	03 10 39	+04 35.2	1.706	86.4		m	13.80	1.82	1.15	1.48	118.1	3.8	118.1	3.8	14.16					
Wo 9111	03 10 58	+52 10.1	0.517	205.7	-55	dM0	10.24	1.26			41.8	6.8	41.8	6.8	8.35	45	-40	-54		BD+51 697
NN	03 11 10	+28 30.2	0.836	158.1		m	16.77	2.15			67.0	8.7	67.0	8.7	15.9					
NN	03 11 14	+48 20.3	0.322	163.0		M1	11.43	1.49	1.13				54.0	26. r	10.1					
NN	03 11 18	-54 18.0	0.081	163.0		DZ7	14.75	0.52	-0.42				91.0	12. w	14.55					
NN	03 11 47	+00 28.1	0.060	297.0			10.9 P				70.1	25.6	70.1	25.6	10.1 P					
Wo 9112	03 12 04	+08 48.1	0.565	134.5	-21.5	K1 V	7.83	0.86	0.57	0.31	43.6	5.6	43.6	5.6	6.03	9	-63	12	20165	BD+08 482
NN	03 12 12	-09 51.2				M0	11.63	1.55	1.14	0.82			40.0	07. r	9.64					
Gl 130.1A	03 12 17	+57 59.3	0.591	126.7	22	M1.5	10.92	+1.54 J		+0.95 J	70.6	3.9	70.6	3.9	10.16	-42	-17	-4		
Gl 130.1B	03 12 17	+57 59.3	0.591	126.7	22.1	M2	11.2 *				70.6	3.9	70.6	3.9	10.4 *	-42	-17	-4		
Gl 131	03 12 35	-26 38.0	0.269	69.4	14.9	K7 V	9.15	1.24	1.10	0.49	58.2	10.8	58.2	10.8	7.97	-23	-14	-1	20280	CD-26 1207
Gl 132	03 13 24	-45 50.7	0.210	313.0	4	G3 V	6.76	0.58	-0.01	+0.33C	64.9	10.1	64.9	10.1	5.82	-3	11	-11	20407	BD-46 968
NN	03 13 48	+45 11.4	0.261	255.0		m	12.39			1.13			66.0	13. r	11.49					
Gl 133	03 13 56	+79 46.9	0.488	51.7	-10.2	M2	11.20	1.56	1.18	0.94	73.8	7.4	73.8	7.4	10.54	5	-21	25		
NN	03 14 36	+60 25.8	0.600	128.4		M3.5	13.33	1.51		1.11			40.0	10. r	11.3					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	03 14 45	+25 04.5	0.854	115.1		k	11.85	1.45	1.10	0.89			41.0	07. r	9.91					
Gl 134	03 14 52	+38 04.7	0.772	141.2	-3.7	dM1.5e	10.28	1.48	1.20	0.86	64.2	3.7	64.2	3.7	9.32	-18	-52	-16	275122	BD+37 748
NN	03 15 30	+32 28.0	0.210	108.0		m	11.33	1.47	1.37	0.80			42.0	07. r	9.45					
Gl 135	03 16 30	-03 01.4	0.272	110.9	22.5	G1.5 V	7.03	0.66	0.09	+0.34C	64.2	18.8	39.0	06. r	4.99	-25	-31	-5	20619	BD-03 534
Gl 136	03 16 41	-62 46.0	1.495	63.2	12.2	G2 V	5.54	0.64	0.08	0.23	93.6	9.1	93.6	9.1	5.4	-63	-42	13	20766	CP-63 217
Gl 137	03 16 44	+03 11.3	0.284	70.1	+18.9 SB?	G5 Ve	4.82	0.68	0.20	0.23	104.5	4.8	104.5	4.8	4.92	-22	-4	-4	20630	BD+02 518
Gl 138	03 17 07	-62 41.8	1.483	63.7	11.5	G1 V	5.24	0.60	0.00	0.23	87.5	8.8	87.5	8.8	4.95	-66	-44	15	20807	CP-62 265
Gl 138.1A	03 17 54	+08 51.3	0.298	103.2	+7.2 SB	dG2	8.45	0.68	0.16	+0.39C	50.7	11.9	22.0	03. r	5.16	-32	-52	21	20727	BD+08 496
Gl 138.1B	03 17 59	+08 51.4	0.299	103.0		k-m	15.13			1.18	50.7	11.9	22.0	03. r	11.84					
Gl 139	03 17 56	-43 15.6	3.127	76.3	+86.7 SB	G5 V	4.26	0.71	0.22	+0.27t	159.6	9.6	159.6	9.6	5.28	-81	-94	-27	20794	CD-43 1028
NN	03 18 17	+52 09.4	0.392	228.1		K3	9.07	0.99	0.84		42.1	11.5	33.0	05. r	6.66				232781	BD+51 722
NN	03 19 19	-06 51.1	0.312	103.0		M2	11.37	1.50		0.96			63.0	12. r	10.37					
NN A	03 19 27	+26 58.7	0.208	113.0		K7	11.03	1.43	1.34				45.0	22. r	9.3					
NN B	03 19 48	+26 58.0	0.208	113.0		a	18. *						45.0	22. r	16. *					
GJ 1058	03 19 27	+02 46.4	0.803	155.9		m	14.78	1.76		1.33	59.4	5.9	59.4	5.9	13.65					
GJ 1059	03 19 41	+41 50.3	0.719	143.4		m	15.33	1.89		1.48	65.4	3.4	65.4	3.4	14.41					
NN	03 20 39	+11 30.7	0.275	241.0		m	12.19	1.56	1.25	1.09	54.8	10.9	54.8	10.9	10.88					
GJ 2030 A	03 20 51	-07 58.1	0.216	180.3	42.2	G2 V	6.19	0.71	0.15	0.27	35.0	8.3	55.0	05. s	4.89	-16	-19	-39	21019	BD-08 643
GJ 2030 B	03 20 51	-07 58.1	0.216	180.3			12.3 *				35.0	8.3	55.0	05. s	11.0 *					
Gl 140 A	03 21 09	+23 36.6	0.227	122.0		dM0	10.64	+1.51 J	1.28	+0.90 J			60.0	08. r	9.53					
Gl 140 B	03 21 09	+23 36.6	0.227	122.0			12.0 *						60.0	08. r	10.9 *					
Gl 140 C	03 21 16	+23 35.9	0.227	122.0		m	11.89	1.50		1.01			60.0	08. r	10.78					
Gl 140.1A	03 21 43	-50 10.5	0.367	41.5	-12.2	K5 V	8.47	+1.13 J	+0.98 J	0.38	51.0	8.2	44.0	05. r	6.69	-38	3	17	21209	CP-50 441
Gl 140.1B	03 21 42	-50 10.6	0.363	35.1	-12	k	10.32	1.39	1.31	0.60	51.0	8.2	44.0	05. r	8.54	-38	7	14		
NN A	03 21 45	-40 15.2	0.077	99.8		K0 V	6.92						69.0	07. o	6.11				21175	CD-40 898
Gl 141	03 22 32	-05 31.7	0.802	196.8	-13.6	K5 V	7.86	1.16	1.15	0.41	66.5	8.3	66.5	8.3	6.97	47	-28	-20	21197	BD-05 642
NN	03 22 38	-01 59.0	0.903	163.8		DZ9	16.12	0.80	-0.20				62.0	06. w	15.08					
NN	03 23 04	+05 41.5	0.210	228.0		m+	14.70			1.46			77.0	12. r	14.13					
NN	03 23 53	+19 04.3	0.200	:176.		m	14.96			1.42			60.0	09. r	13.85					
Gl 141.2	03 24 07	-30 47.7	0.301	47.7	20.3	G8 V	7.88	0.71	0.21	+0.38C	53.2	15.3	32.0	06. r	5.41	-47	-12	3	21411	CD-31 1384
NN	03 24 55	+09 45.7				K7	10.45	1.39	1.25	0.62			40.0	06. r	8.46					+ 9 440
Gl 142	03 25 36	-19 58.9	0.616	59.1	37.9	K7 V	8.39	1.33	1.20	0.57	71.8	12.0	71.8	12.0	7.67	-51	-20	-7	21531	BD-20 643
NN	03 25 49	+26 19.0	0.237	115.0		m	13.40			1.21			55.0	10. r	12.1					
Gl 143	03 26 08	-63 40.1	0.439	124.1	57.3	K5 V	8.0 :	1.12	1.08	0.43	59.8	6.1	59.8	6.1	6.9 :	9	-64	-17	21749	CP-63 231
NN A	03 26 19	-15 47.7	0.214	82.0		m	14.28			1.29			43.0	06. r	12.45					
NN B	03 26 19	-15 47.9	0.214	82.0		m	14.37			1.23			43.0	06. r	12.54					
GJ 1060 A	03 26 45	-27 29.3	0.839	63.7		DA5	14.0 *				57.6	11.7	57.6	11.7	12.8 *					
GJ 1060 B	03 26 45	-27 29.4	0.839	63.7		sdM3	13.8 *			1.18	57.6	11.7	57.6	11.7	12.6 *					
Gl 143.1	03 26 57	-11 50.7	0.281	165.0		M0 V	9.98	1.42	+1.3 :	0.66	55.2	23.0	55.0	11. r	8.68					BD-12 662
NN A	03 27 37	+19 56.0	0.176	108.9	24.3	G5	8.32	0.74	0.32	0.25	45.2	7.7	45.2	7.7	6.6	-28	-11	-6	21663	BD+19 547
NN B	03 27 37	+19 56.0	0.176	108.9	27.1	dK6	10.75	1.42	1.23		45.2	7.7	45.2	7.7	9.03	-30	-10	-7		
NN	03 27 37	+19 55.7	0.165	105.8	20.2	K7 V	10.79	1.39	1.24	0.66	62.4	10.3	62.4	10.3	9.77	-22	-6	-5		

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 143.2A	03 28 30	-63 06.8	0.537	45.2	12	F5 IV-V	4.71	0.39	-0.04	0.11	56.9	7.0	56.9	7.0	3.49	-42	-20	-3	22001	CP-63 234
Gl 143.2B	03 28 36	-63 07.3	0.524	44.9		m	10.75	1.42		0.80	56.9	7.0	56.9	7.0	9.53					
Gl 143.3	03 28 59	+14 09.7	0.678	178.4		sdM3	12.27	1.55	1.00	1.00	51.3	3.0	51.3	3.0	10.82					
NN	03 29 05	+37 53.6	0.084	234.5		G5	7.28						65.0	07. o	6.34				21809	BD+37 783
Gl 144	03 30 34	-09 37.6	0.980	271.1	16.9	K2 V	3.73	0.88	0.58	0.30	305.6	2.6	305.6	2.6	6.16	-4	7	-21	22049	BD-09 697
Gl 145	03 31 17	-44 52.3	0.342	296.0	-36	M3.5	11.48	1.57	1.20	1.04	82.4	17.0	82.4	17.0	11.06	7	36	17		CD-45 1184
NN	03 31 53	+28 05.7	0.528	121.9		m	16.67	1.94			35.3	4.7	35.3	4.7	14.41					
NN	03 32 09	-05 00.3	0.520	127.2		k-m	13.1 *			1.22			66.0	12. r	12.2 *					
NN	03 32 18	+69 01.1	0.203	123.0		m	14.17			1.26			47.0	08. r	12.53					
Gl 146	03 33 26	-48 35.3	0.504	51.3	19.5	K7 V	8.60	1.31	1.18	0.57	85.3	7.8	85.3	7.8	8.25	-28	-19	-6	22496	CP-48 376
NN	03 34 04	+03 19.7	0.159	127.0		dM5 :	13.86						70.0	10. p	13.09					
GJ 1061	03 34 16	-44 40.3	0.831	118.8	-20	M4.5	13.03	1.90	1.52	1.60			233.0	57. r	14.9	4	-2	26		
Gl 147	03 34 19	+00 14.7	0.535	206.1	+27.9	SB? F8 V	4.28	0.57	0.08	0.20	59.4	8.4	59.4	8.4	3.15	6	-18	-47	22484	BD-00 572
NN	03 34 21	-41 09.4	0.522	204.7		M3	13.05			1.09			42.0	08. r	11.17					
NN A	03 34 41	+17 41.7	0.180	98.0		g-k	12.74			1.00			43.0	06. r	10.91					
NN B	03 34 42	+17 41.5	0.180	98.0		g-k	13.29			1.19			43.0	06. r	11.46					
GJ 1062	03 35 48	-11 36.7	3.033	152.1	-140	M2	13.01	1.66	1.38	0.90	64.8	3.6	64.8	3.6	12.07	163	-178	103		
NN	03 36 30	+24 48.2	0.232	27.0		dM3.1	12.79			1.15			59.0	12. r	11.64					
NN	03 36 35	+25 19.4	0.629	157.1		M3.5	12.70			1.10	1.9	14.8	54.0	10. r	11.36					
Wo 9119 A	03 36 39	+33 18.7	0.038	268.5	9.4	dK5	9.07	1.06	0.99	0.40			42.0	06. r	7.19	-6	6	-5	278874	BD+32 652
Wo 9119 B	03 36 38	+33 18.8	0.038	268.5			12.87	1.49		1.13			42.0	05. r	10.99					
Wo 9120	03 36 40	+25 19.6	0.629	157.1		M3.5	13.1 *			1.13	46.9	16.3	48.0	09. r	11.5 *					
Gl 147.1	03 37 49	-03 22.5	0.724	106.9	120.3	F9 V	6.68	0.54	-0.08	0.23	46.9	8.4	46.9	8.4	5.04	-107	-77	-49	22879	BD-03 592
NN	03 38 00	-69 07.1	0.608	32.9		m	11.95			1.04			61.0	12. r	10.88					
NN	03 38 15	-02 29.4	0.432	119.4	48	K0	6.96	0.96	0.76	0.34	25.3	8.2	75.0	10. r	6.34	-39	-31	-24	22918	BD-02 0690
Gl 148	03 38 34	+03 27.3	0.234	192.2	4.2	dM0 p	9.59	1.37	1.20	0.61	44.8	5.2	44.8	5.2	7.85	10	-15	-18		BD+03 515
NN	03 39 42	+12 22.9	1.572	151.5		M0.5	12.91	1.54	1.24	0.86	45.1	7.8	45.1	7.8	11.18					
NN	03 40 20	-51 35.1	0.074	293.1		K4 V	9.07	1.10	0.93	0.44			42.0	06. r	7.19				23295	CD-51 881
Gl 149 A	03 40 36	-24 37.2	0.379	173.6	20.7	K4	9.20	1.13	1.11	0.44	59.1	11.9	41.0	07. r	7.26	21	-39	-20		CD-24 1826
Gl 149 B	03 40 38	-24 36.9	0.380	174.0		m	15.6 P				59.1	11.9	41.0	07. r	13.7 P					
Gl 150	03 40 51	-09 55.9	0.752	352.3	-5.1	K0 IVe	3.53	0.92	0.68	0.32	103.5	4.6	103.5	4.6	3.6	-15	29	13	23249	BD-10 728
NN	03 40 57	-09 43.6	0.522	54.5		m	14.7 *			1.41			66.0	10. r	13.8 *					
Gl 150.1A	03 41 02	+16 31.1	0.300	160.0	36.1	dM0	9.96	1.45	1.27	0.70	53.3	8.0	62.0	07. r	8.92	-29	-17	-26		BD+16 502
Gl 150.1B	03 40 55	+16 30.8	0.300	160.0	13.3	dM0	10.81	1.48	1.22	0.86	53.3	8.0	62.0	07. r	9.77	-10	-19	-15		
Gl 150.2	03 41 16	+45 52.8	0.337	107.6	20.3	K0	7.71	0.86	0.54		48.9	13.6	45.0	07. r	5.98	-35	-19	10	23140	BD+45 805
Wo 9124	03 41 17	+24 38.6	0.050	165.0		F8	10.66	0.66	0.13		44.5	10.2	44.5	10.2	8.9					
Wo 9125	03 41 17	+24 37.6	0.050	165.0		G0	10.81	0.70	0.19	0.27	48.5	17.0	48.5	17.0	9.2					
Wo 9126	03 41 21	+24 43.1	0.023	241.7	2	K2	8.85	1.71	1.99		51.5	18.8	51.5	18.8	7.4	-1	1	-3	23232	BD+24 543
Wo 9127	03 41 23	+24 36.6	0.050	165.0		G3	11.09	0.86	0.48		46.5	10.2	46.5	10.2	9.43					
Gl 151	03 41 41	+18 17.7	1.204	159.4		DQ8	15.19	0.31	-0.54	0.13	56.3	4.2	56.3	4.2	13.94					
GJ 1063	03 42 05	+11 45.7	0.320	67.8	81.9	dK8	9.15	1.18	1.16	0.48			48.0	06. r	7.56	-85	-5	-19		BD+11 514
Gl 152	03 42 18	-38 26.5	0.361	35.9	+32.	VAR K0 V	6.99	0.88	0.58	0.28	64.2	15.3	61.0	09. r	5.92	-36	-16	-16	23484	CD-38 1264

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	03 42 52	+73 23.6	0.515	126.1		m	11.31	1.54		0.89	58.1	3.3	58.1	3.3	10.13					
Gl 153 A	03 43 04	+68 30.9	0.291	27.0	4.3	K7	9.33	1.28	1.20	0.54	51.8	3.1	51.8	3.1	7.9	4	3	26	23189	BD+68 278
Gl 153 B	03 43 05	+68 31.2	0.309	21.0	3.1	M2.5 J	11.30	+1.54 J	+1.20 J	+0.90 J	51.8	3.1	51.8	3.1	9.87	7	5	27		
Gl 153 C	03 43 05	+68 31.2	0.309	21.0			11.6 *				51.8	3.1	51.8	3.1	10.2 *					
Gl 154	03 43 18	+26 03.8	0.410	119.0	36.3	K7	9.61	1.47	1.22	0.72	68.9	4.6	68.9	4.6	8.8	-42	-17	-8	23453	BD+25 613
Gl 154.1A	03 43 19	-28 01.2	0.364	63.6	32.9	K5 V	8.25	+1.00 J	+0.80:J	+0.40 J	35.4	11.9	48.0	07. r	6.66	-41	-26	-4	23588	CD-28 1276
Gl 154.1B	03 43 19	-28 01.2	0.364	63.6		M3 V	11.6 *				35.4	11.9	48.0	07. r	10.0 *					
Gl 154.2	03 43 34	-64 57.8	0.325	75.6	+50.8 SB	K0 IV	3.85	1.13	1.10	0.41	43.7	12.8	43.7	12.8	2.1	-17	-57	-17	23817	CP-65 263
GJ 1064 A	03 43 37	+41 17.4	1.375	153.9	49.6	K1 V	8.15	0.78	0.20		48.9	6.1	48.9	6.1	6.6	-86	-93	-65	23439	BD+41 750
GJ 1064 B	03 43 37	+41 17.5	1.400	154.6	+51.5 SB	K2 V	8.75	0.90	0.45		48.9	6.1	48.9	6.1	7.2	-88	-93	-68		
Wo 9131	03 44 06	+23 50.5	0.044	158.1	4.3	F0 V	8.38	0.29	0.08		48.6	17.0	48.6	17.0	6.8	-4	-3	-3	23585	BD+23 528
NN	03 44 21	-11 27.0	0.551	78.8		M2.5	12.70	1.53		1.04			41.0	09. r	10.76					
NN	03 44 37	+08 33.1	0.789	144.0		k-m	14.51	1.87		1.39	79.7	3.5	79.7	3.5	14.02					
Gl 155	03 44 42	-23 23.8	0.552	196.9	6.9	F3 III	4.22	0.42	0.01	0.14	56.1	9.2	56.1	9.2	2.96	36	-22	-21	23754	CD-23 1565
Wo 9132	03 45 08	+23 59.4	0.041	166.5	7.1	F6 V	9.24	0.54	0.12		45.1	11.9	45.1	11.9	7.5	-6	-2	-5	23713	BD+23 548
Gl 155.1	03 45 23	+02 38.5	0.539	225.2		M1	11.04	1.50		0.82	48.0	8.7	48.0	8.7	9.45					
NN	03 46 07	+63 18.5	0.271	177.0		M3	11.39	1.42	1.23	+0.85t			45.0	09. r	9.66					
Wo 9134	03 47 24	-64 59.4	0.365	74.4	19.3	G5 V	7.85	0.66	0.17	0.22	42.6	11.9	26.0	04. r	4.92	-41	-52	20	24293	CP-65 272
Wo 9135	03 48 04	+23 45.2	0.166	106.0	38	dK6	10.23	1.16	1.04	0.45	46.8	15.3	27.0	03. r	7.39	-45	-17	-3	283066	BD+23 571
GJ 1065	03 48 18	-06 13.6	1.428	196.8		dM4	12.79	1.70	1.40	1.16	104.9	3.7	104.9	3.7	12.89					
NN	03 48 27	-01 01.3	0.525	175.6		m	18.02			1.86	68.2	1.8	68.2	1.8	17.19					
NN	03 49 49	+16 52.7	0.766	147.5		M4.5	13.7 *			1.41	70.0	13.0	104.0	15. r	13.8 *					
NN	03 50 33	+28 00.1	0.105	93.3	20.3	G8 V	7.84	0.84					41.0	05. r	5.9	-23	-3	0	24365	BD+27 589
Gl 155.2	03 50 44	+61 01.4	0.506	118.2	47.9	K0 V	7.86	0.83	0.46	0.31	45.4	8.1	45.4	8.1	6.15	-68	-14	15	24238	BD+60 762
Gl 155.3	03 51 31	-37 11.9	1.144	199.4	-67	M2.5	12.14	1.45	1.04	0.93	51.7	9.8	51.7	9.8	10.71	120	8	31		CD-37 1501
NN	03 51 37	+16 28.3	0.274	128.4	22.2	G5	6.81						47.0	05. o	5.17	-24	-25	-7	24496	BD+16 527
NN	03 52 01	-09 18.3				M3	11.22	1.53	1.14	0.95			67.0	13. r	10.35					
NN	03 52 03	+59 29.7	0.310	303.9		G0	6.54						47.0	05. o	4.9				24409	BD+59 736
Gl 156	03 52 09	-06 58.8	0.531	357.6	64.5	M0 V	9.02	1.36	1.26	0.62	69.8	6.1	69.8	6.1	8.24	-66	13	-30		BD-07 699
Gl 156.1A	03 52 55	+53 25.3	0.458	139.6	-5	dM1.5e	10.86	1.43	+1.21:	0.84	53.6	11.9	53.6	11.9	9.51	-17	-37	-7		
NN	03 54 22	-25 19.3	0.295	159.7		G8 V	6.88						55.0	06. o	5.58				24892	CD-25 1653
Gl 156.2	03 54 49	+76 01.6	0.637	147.3	20	K4 V	8.26	1.15	1.04		49.2	4.8	49.2	4.8	6.72	-59	-24	-9	24451	BD+75 154
GJ 1066	03 54 53	-41 29.3	0.105	28.0		K4 V	8.94	1.21	1.14	0.50			53.0	08. r	7.56				25004	CD-41 1208
Gl 157 A	03 54 57	-01 18.0	0.245	233.2	5.7	K4 V	8.04	1.11	1.03	0.45	71.7	15.5	68.0	09. r	7.2	6	1	-17	24916	BD-01 565
Gl 157 B	03 54 57	-01 18.0	0.245	233.2	+14.0 SB	dM3 e	11.61	1.47	1.08	1.02	71.7	15.5	68.0	09. r	10.77	0	-1	-22		
Gl 157.1	03 56 49	+25 57.2	0.778	107.5	94	dM4	12.62	1.49	1.67	1.14	43.8	5.2	43.8	5.2	10.83	-115	-52	3		
Wo 9141	03 57 20	+51 15.4	0.852	156.7		M3.5	13.65				38.9	8.5	38.9	8.5	11.6					
NN	03 57 46	+08 06.0	0.519	222.1		DC9	15.87	0.69	0.00		56.7	3.7	56.7	3.7	14.64					
NN	03 58 31	-23 13.2				M0	11.47	1.48	1.17	0.83			43.0	07. r	9.64					
Gl 158	03 59 53	+35 09.3	2.201	127.7	-25.6	K1 V	8.51	0.87	0.37	0.34	54.8	7.4	54.8	7.4	7.2	-40	-187	21	25329	BD+34 796
Gl 159	04 00 03	-00 24.2	0.288	150.3	+17.7 VAR	F6 V	5.37	0.50	0.00	0.19	55.2	4.8	55.2	4.8	4.08	-8	-27	-12	25457	BD-00 632
Wo 9142	04 01 57	+00 06.9	0.408	209.0	-38	G8	8.33	0.77	0.37		40.9	7.3	40.9	7.3	6.39	59	-10	-12	25682	BD-00 636

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 160	04 02 22	+21 52.5	0.222	129.0	23.9	G5 V	5.90	0.62	0.12	0.22	57.5	5.8	57.5	5.8	4.7	-25	-15	-7	25680	BD+21 587
NN	04 02 59	+05 36.6	0.152	146.0		dM5 e	12.89						63.0	08. p	11.89					
NN	04 03 26	+82 47.4	0.273	160.0	7	dM0	10.82	1.44	1.25	0.71	36.3	11.9	42.0	07. r	8.94	-29	-9	-9		
Wo 9143	04 03 34	-27 47.2	0.222	64.1	63.3	F1 IV	5.58	0.32	0.05		43.1	10.2	43.1	10.2	3.8	-47	-39	-30	25945	CD-27 1540
Gl 161	04 04 23	+69 24.8	0.308	165.1	-10.8	dK2	7.70	0.91	0.77		57.0	9.4	52.0	07. r	6.28	-10	-23	-17	25665	BD+69 238
Gl 160.2	04 04 23	-20 58.5	0.770	177.2	28	dM0	9.68	1.22	1.14	0.48	49.3	6.4	49.3	6.4	8.14	37	-61	-34		BD-21 784
NN	04 05 13	-24 36.6	0.658	162.8		M3.5	12.4 *			1.19			81.0	16. r	11.9 *					
Gl 161.1	04 05 16	+37 54.6	0.261	139.9	26.2	F7 V	5.52	0.46	-0.03		47.8	13.6	43.0	05. r	3.69	-33	-18	-8	25998	BD+37 882
Gl 161.2	04 05 21	-40 53.4	0.339	344.0		k	10.98	1.13		+0.62C	45.9	13.6	19.0	03. r	7.37					CD-41 1288
Gl 162	04 05 23	+33 30.2	0.575	77.0	36.8	M1	10.18	1.51	1.18	0.83	72.7	7.8	72.7	7.8	9.49	-47	-7	22		
Gl 162.1	04 06 49	-64 21.5	0.389	32.5	27.5	G3 V	6.38	0.64	0.10	0.22	39.3	16.9	49.0	08. r	4.83	-34	-28	-15	26491	CP-64 305
NN	04 07 15	-08 01.5	0.114	18.1	-9.4	G2 IV-V	7.04						42.0	05. o	5.16	-2	9	13	26337	BD- 8 801
GJ 1067	04 07 26	+70 04.4	0.100	289.0		dM0	9.69	1.23	1.19	0.50	47.4	10.2	41.0	05. r	7.75					
NN	04 07 30	+49 24.5	0.483	166.4		M3.5	13.45			1.15			43.0	08. r	11.62					
NN	04 07 34	+64 36.6	0.647	130.0		m	13.71	1.69		1.32	84.5	2.9	84.5	2.9	13.34					
Gl 163	04 07 56	-53 30.7	1.211	60.4	66	M3.5	11.81	1.50	1.18	1.08	64.9	10.1	64.9	10.1	10.87	-74	-82	-3		
NN	04 08 37	+76 09.9	0.239	166.4	10.4	G5	8.19	0.84	0.52		42.4	10.7	36.0	05. r	5.97	-30	-8	-12	26018	BD+75 166
Gl 164	04 09 09	+52 29.7	0.910	203.7		M3.5	13.50	1.67		1.37	75.3	7.0	75.3	7.0	12.88					
GJ 1068	04 09 17	-53 42.0	2.521	198.1	27	pec	13.58	1.93	2.11	1.30			80.0	22. r	13.1	146	-32	-24		
Gl 165 A	04 09 27	+50 24.2	0.457	242.8		M3.5	13.67 J	+1.75 J		+1.31 J	61.9	8.5	61.9	8.5	12.63 J					
Gl 165.1	04 11 20	+58 24.0	0.287	139.4	21.9	K3	8.67	1.00	0.84		50.9	8.5	50.9	8.5	7.2	-33	-10	-1	26581	BD+58 724
NN	04 11 26	-54 00.1	0.838	39.2		m	13.87	1.56	1.13	1.19			40.0	08. r	11.88					
Gl 165.2	04 11 53	+02 53.6	0.280	19.7	53.3	K3 V	8.79	0.97	0.78	+0.47C	48.3	13.5	37.0	06. r	6.63	-63	10	-4	26794	BD+02 665
GJ 1069	04 12 40	-04 32.5	0.133	136.8		K5 V	9.39	1.22	1.12	0.51			46.0	08. r	7.7					BD-04 782
NN	04 12 43	+15 34.9	0.128	103.5		M2	11.01	1.24		0.51	97.0	38.0	23.0	03. r	7.82				285590	
Gl 166 A	04 12 58	-07 43.8	4.083	213.1	-42.7	K1 Ve	4.43	0.82	0.45	0.31	207.1	2.5	207.1	2.5	6.01	95	-11	-39	26965	BD-07 780
Gl 166 B	04 13 04	-07 44.1	4.073	212.4	-21	DA4	9.52	0.03	-0.68	-0.10	207.1	2.5	207.1	2.5	11.1	112	-6	-24	26976	BD-07 781
Gl 166 C	04 13 04	-07 44.1	4.073	212.4	-45.9	dM4.5e	11.17	1.67	0.83	1.31	207.1	2.5	207.1	2.5	12.75	97	-11	-36		
GJ 2033	04 14 22	-12 41.0	0.256	340.0		k-m	10.87	1.55	1.35				106.0	49. r	11					
NN	04 14 35	+08 42.3	0.379	159.0		dM4 e	13.82			1.40			95.0	14. r	13.71					
Gl 167	04 14 39	-53 26.3	0.881	63.1	-23.2	K5 V	7.64	1.13	1.06	0.42	75.6	9.4	75.6	9.4	7.03	-37	-8	46	27274	CP-53 672
Gl 167.1	04 14 43	-51 36.7	0.212	28.2	25.2	F4 III	4.25	0.30	0.02	0.18	44.4	16.7	44.4	16.7	2.5	-25	-18	-13	27290	CD-51 1066
Gl 167.2	04 15 03	-26 10.6	0.700	58.6	55	M0	11.80	1.38	+1.1 :	0.74	51.7	10.2	51.7	10.2	10.37	-73	-43	5		
NN	04 15 31	+75 01.8	0.778	132.8		M3	12.16	1.51		1.03			54.0	13. r	10.8					
Gl 167.3	04 15 37	-59 25.3	0.170	197.5	29.3	K2 IV	4.44	1.07	1.08	+0.37t	67.0	8.4	67.0	8.4	3.57	12	-22	-20	27442	CP-59 324
NN	04 16 37	-49 10.5	0.506	5.3		M4	13.2 *			1.11			46.0	09. r	11.5 *					
NN	04 18 46	+51 49.6	0.175	119.1		G5	7.73						46.0	05. o	6.04				27456	BD+51 913
NN	04 18 52	+21 12.9	0.254	151.0		k-m	13.03	1.56	1.08				42.0	19. r	11.1					
GJ 1070	04 19 08	+38 54.2	0.712	136.2		k-m	15.27	1.71		1.42	53.7	4.7	53.7	4.7	13.92					
NN	04 19 13	+19 08.5	0.119	260.0		dM4.5e	12.9 *	1.70					104.0	42. r	13.0 *					
Gl 168.1	04 19 15	+19 21.9	0.003	18.4			15.04:	+1.0 :		0.70	70.1	18.8	70.1	18.8	14.3 :					
Gl 168.2	04 19 18	+19 22.3	0.280	148.0		m	15.77:	+1.0 :		1.10	59.1	15.3	59.1	15.3	14.6 :					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	04 19 24	+15 23.9	0.070	115.0		m	17. *			+2.74C*			42.0	06. p	15. *					
GJ 2034	04 19 36	-48 46.1	0.556	175.6		DA8	14.36	0.52	-0.45				123.0	14. w	14.81					
NN	04 20 15	+09 17.2	0.079	314.4		G5	8.04						40.0	05. o	6.05				27733	BD+ 9 568
NN	04 21 07	+16 36.2	0.120	100.0		dM0	12.55	1.49		0.82	49.0	22.0	25.0	04. r	9.54					
NN	04 21 16	-57 33.2	0.534	208.5		m	11.8 *			1.04			65.0	13. r	10.9 *					
NN	04 21 36	+32 20.2	0.274	121.0		k-m	12.44	1.51	1.15				39.0	19. r	10.4					
NN	04 22 08	+16 52.3	0.104	105.9	43	M2	10.31	1.04	0.93	0.37	39.0	13.0	19.0	02. r	6.7	-46	-21	-3	285742	BD+16 593
NN A	04 22 32	+07 56.1	0.145	86.0		m	12.63			1.05			42.0	05. r	10.75					
NN B	04 22 34	+07 57.2	0.145	86.0		m	14.97			1.31			42.0	05. r	13.09					
NN	04 22 58	+15 24.3	0.130	103.0		dM0	12.13	1.40	1.04		52.0	17.0	52.0	17.0	10.7					
NN	04 23 07	+12 05.2	0.261	210.0		DC8	15.5 :						81.0	11. w	15.0 :					
Wo 9155 A	04 23 13	-57 11.0	0.234	237.5	-5.2	G4 V	6.88	+0.66 J	+0.19 J		39.7	6.9	40.0	05. r	4.89	21	15	-10	28255	CP-57 659
Wo 9155 B	04 23 13	-57 11.1	0.029	93.9	-3.7	G6 V	7.3 *				39.7	6.9	40.0	05. r	5.3 *	-1	1	5		
NN	04 23 19	-40 09.3	0.674	182.8		M3.5	14.1 *			1.33			60.0	13. r	13.0 *					
NN	04 23 23	+59 28.8	0.234	151.0		m	14.45			1.28			45.0	08. r	12.72					
NN	04 23 40	+04 26.3	0.856	132.3		DC9	17.11	1.10					43.0	04. w	15.28					
NN	04 23 43	+03 30.7	1.033	186.4		m	18.32				58.7	1.8	58.7	1.8	17.16					
NN	04 24 24	+17 07.6	0.110	105.0		dM1	13.06	1.49		0.91	51.0	17.0	25.0	05. r	10.05					
Wo 9156	04 24 42	-64 11.8	0.333	350.0	52.7	G5 V	7.91	0.65	0.16		43.8	10.2	26.0	04. r	4.98	-50	-26	-58	28471	CP-64 334
NN	04 25 06	+11 40.7	0.575	147.3		k	13.85			1.20			43.0	08. r	12.02					
Gl 169	04 26 02	+21 48.7	0.185	337.4	-31.4	K7 V	8.27	1.35	1.22	0.62	85.4	5.8	85.4	5.8	7.93	30	7	13	28343	BD+21 652
NN	04 26 28	+14 07.2	0.292	54.0		m	13.5 :			1.31			79.0	13. r	13.0 :					
NN	04 26 31	-25 16.4	0.521	187.3		M2.5	12.0 *			1.02			55.0	09. r	10.7 *					
Gl 169.1A	04 26 47	+58 53.9	2.383	144.8	17	dM4	11.08	1.65	1.20	1.14	181.9	1.1	181.9	1.1	12.38	-48	-43	-6		
Gl 169.1B	04 26 47	+58 53.9	2.383	144.8		DC5	12.44	0.31	-0.52	-0.49	181.9	1.1	181.9	1.1	13.74					
Gl 170	04 26 59	+39 44.9	0.588	154.3		M4.5	13.91	1.73	1.33	1.41	95.9	3.1	95.9	3.1	13.82					
NN	04 27 31	+17 23.3	0.070	113.0		k-m	14.57	1.75			63.0	26.0	63.0	26.0	13.6					
Gl 170.1	04 27 42	+16 05.2	0.100	110.5	41	A6 IV	4.78	0.17	0.13		52.3	11.9	52.3	11.9	3.37	-40	-8	-11	28527	BD+15 637
NN	04 29 11	+64 31.7	0.088	299.3		G0	7.74						40.0	05. o	5.75				28495	BD+64 458
NN	04 30 36	+20 38.7	0.546	126.6		m	14.6 *			1.39			64.0	09. r	13.6 *					
NN	04 30 59	+34 43.5	0.336	148.0		g-k	13.13	1.57	1.17				43.0	20. r	11.3					
Wo 9158	04 31 11	+05 17.1	0.281	196.7		K1	7.93	0.79	0.35		43.7	20.5	37.0	06. r	5.77				28946	BD+05 678
NN	04 31 22	-37 03.0	0.052	333.7		K3/5 V	8.79	0.99	0.84	0.40			41.0	04. r	6.85				29086	CD-37 1799
NN A	04 31 29	+39 02.4	0.137	217.8		K5	9.3 *				40.0	5.3	40.0	5.3	7.3 *				276666	BD+38 912
Gl 171	04 31 59	+55 18.9	0.621	116.2	+50.	SB K2 V	8.34	0.90	0.67		34.6	12.2	39.0	06. r	6.3	-75	-39	32	237287	BD+55 900
GJ 1071	04 32 26	-43 37.6	0.096	143.2		K5 V	8.86	1.11	1.00	0.42			46.0	07. r	7.17				29220	CD-43 1472
NN	04 32 50	-35 45.4	0.248	201.6		G8 V	7.58c	+0.81c					43.0	06. r	5.75c				29231	CD-35 1797
NN A	04 33 03	+16 24.6	0.094	112.1	54	K	11.2 *				43.1	9.0	43.1	9.0	9.4 *	-52	-10	-14		
Gl 171.1A	04 33 03	+16 24.6	0.200	161.1	54.5	K5 III	0.85	1.54	1.90	0.70	49.4	4.9	49.4	4.9	-0.68	-49	-19	-25	29139	BD+16 629
Gl 171.1B	04 33 03	+16 24.6	0.200	161.1		dM2	13.5 *				49.4	4.9	49.4	4.9	12.0 *					
Gl 171.2A	04 33 42	+27 02.0	0.288	122.3	+35.2	SB dK5 ep	8.42	1.12	0.88	0.51	61.1	3.0	61.1	3.0	7.35	-38	-17	-2	283750	BD+26 730
Gl 171.2B	04 33 39	+27 03.9	0.278	118.0		DC8	15.80	0.65	-0.05		61.1	3.0	61.1	3.0	14.73					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 172	04 33 43	+52 48.0	0.556	145.2	+32.9 SB?	K8 Ve	8.61	1.40	1.14	0.65	98.5	2.4	98.5	2.4	8.58	-41	-9	-1	232979	BD+52 857
NN	04 33 52	+11 07.0	0.632	58.6		k-m	14.30	1.62	1.16	1.24	40.4	6.2	40.4	6.2	12.33					
NN	04 34 55	-29 09.6	0.517	71.0		M3.5	13.7 *			1.17			41.0	08. r	11.8 *					
NN	04 35 04	+28 07.1	0.366	98.0		m	12.53	1.65	1.29	1.26			100.0	17. r	12.53					
NN	04 35 06	-02 35.5				M1	10.59	1.45	1.06	0.86			68.0	12. r	9.75					
Gl 173	04 35 21	-11 08.1	0.318	227.0	-7	dM1	10.36	1.50	1.17	0.93	94.0	8.5	94.0	8.5	10.23	15	2	-9		BD-11 916
NN	04 35 24	-08 53.9	1.520	171.2		DQ7	13.77	0.33	-0.72		105.1	2.6	105.1	2.6	13.88					
Wo 9160 A	04 35 53	-14 24.0	0.176	207.5	41.8	K2 IIIb	3.91	+1.10 J	+1.01 J		41.0	8.5	41.0	8.5	1.97	-14	-24	-37	29503	BD-14 933
Wo 9160 B	04 35 53	-14 24.0	0.176	207.5			7.3 *				41.0	8.5	41.0	8.5	5.4 *					
Gl 173.1A	04 36 58	+09 46.8	0.364	182.8	-21.3 SB	K3 V	9.20	1.02	0.82	0.43	49.4	6.8	49.4	6.8	7.67	31	-24	-11	286955	BD+09 621
Gl 173.1B	04 36 59	+09 46.1	0.358	179.0		k-m	14.19	1.57	1.06	1.10	49.4	6.8	49.4	6.8	12.66					
NN	04 38 06	+02 08.2				M0	11.24	1.47	1.26	0.89			55.0	10. r	9.94					
Wo 9163 A	04 38 06	-09 17.3	0.158	226.0		dM0	10.97	+1.48 J	+1.17 J	+0.82 J			51.0	08. r	9.51					BD- 9 956
Gl 174	04 38 22	+20 48.6	0.353	223.5	7	K3 V	8.00	1.10	0.91	0.49	71.2	8.9	71.2	8.9	7.26	0	-3	-24	29697	BD+20 802
Gl 174.1A	04 38 57	-41 57.5	0.166	242.7	0.8	F2 V	4.44	0.34	0.01	+0.20C	44.8	23.3	44.8	23.3	2.7	11	6	-12	29875	CD-42 1587
Gl 174.1B	04 38 57	-41 57.5	0.166	242.7			12.5 *				44.8	23.3	44.8	23.3	10.8 *					
Gl 175 A	04 39 29	-59 02.5	0.166	11.8	10.1	G5 V J	7.19	+0.68 J	+0.24 J	+0.22 J	63.2	18.8	39.0	07. r	5.15	-20	-7	-7	30003	CP-59 370
Gl 175 B	04 39 29	-59 02.5	0.166	11.8			7.4 *				63.2	18.8	39.0	07. r	5.4 *					
Gl 176	04 39 58	+18 52.8	1.286	146.7	+26.0 SB?	dM2.5e	9.98	1.52	1.18	0.96	107.4	3.2	107.4	3.2	10.14	-23	-57	-12		BD+18 683
Gl 176.1	04 40 17	-37 14.5	0.199	11.7	26.8	F1 V	5.05	0.38	0.02	+0.22C	56.9	13.6	56.9	13.6	3.8	-25	-12	-14	29992	CD-37 1867
Gl 176.2	04 40 29	+27 35.9	0.271	167.6	17.1	K3	8.00	0.90	0.63		44.9	6.3	44.9	6.3	6.26	-17	-24	-16	29883	BD+27 688
NN	04 40 31	+18 54.7	0.030	29.0			13.4 *				40.3	10.2	40.3	10.2	11.4 *					
NN	04 41 19	+27 46.5	0.420	166.0		M2.5	11.26	1.53	1.21				77.0	36. r	10.7					
NN	04 41 28	+29 43.9	0.271	214.0		k-m	13.45	1.60	1.55				45.0	20. r	11.7					
NN	04 42 28	+48 40.0	1.204	122.5		m	17.29				51.8	1.0	51.8	1.0	15.86					
NN	04 42 56	+42 15.5	0.065	0.0	28.8	G0	6.52						52.0	06. o	5.1	-26	13	3	30090	BD+42 1045
Gl 176.3	04 44 23	-50 09.6	0.552	232.5	17	K0 V	7.59	0.89	0.57	0.29	49.9	5.9	49.9	5.9	6.08	37	4	-41	30501	CD-50 1492
NN	04 44 36	+02 04.3	0.260	268.0		k	11.34	1.48	1.20				53.0	26. r	10					
Gl 177	04 45 21	-17 01.5	0.213	36.8	21.7	G1 V	5.49	0.63	0.13	0.22	78.9	9.2	78.9	9.2	4.98	-23	-9	-3	30495	BD-17 954
NN	04 45 39	-11 01.2	0.110	142.1		K7 V	9.53	1.14	1.10	0.48			41.0	06. r	7.59				30523	BD-11 965
NN	04 46 35	+45 53.9	0.319	139.0		k-m	11.79	1.47	1.21				41.0	20. r	9.9					
Gl 178	04 47 07	+06 52.5	0.464	88.1	24.4	F6 V	3.19	0.45	-0.01	0.16	133.1	7.4	133.1	7.4	3.81	-26	-14	3	30652	BD+06 762
NN	04 47 44	+26 02.4	0.617	111.9		m	12.84	1.54	1.33	1.03			39.0	08. r	10.8					
GJ 1072	04 47 49	+22 02.7	0.744	123.6		m	15.21	1.95	0.94	1.52	71.4	5.7	71.4	5.7	14.48					
Wo 9168	04 48 03	+45 45.5	0.674	144.8	25.9	G1 IV-V	6.97	0.58	0.04	0.23	40.9	10.8	40.9	10.8	5	-51	-64	-6	30649	BD+45 992
NN	04 48 04	-35 11.5	0.114	194.4		K2 V	7.45c	+0.90c					60.0	09. r	6.34c				30876	CD-35 1948
GJ 1073	04 49 02	+40 38.3	1.633	133.2		k	13.43	1.61		1.29	77.4	2.8	77.4	2.8	12.87					
Gl 179	04 49 24	+06 23.8	0.340	152.0	-7.8	dM4 e	11.98	1.56	1.22		76.7	9.0	76.7	9.0	11.4	12	-19	1		
GJ 2035	04 50 04	+22 09.3	0.195	131.7		K5 V	8.77	1.01	0.90	+0.41t			43.0	07. r	6.94				30973	BD+21 717
Gl 180	04 51 35	-17 50.7	0.765	143.8	-15	M3 :	10.90	1.54		0.94	83.8	8.2	83.8	8.2	10.52	30	-30	17		
NN	04 51 46	-20 37.4	0.244	349.0		M0 V	10.12	1.25	1.22	0.56			40.0	07. r	8.13					BD-20 958
NN	04 52 15	-35 29.2	0.197	36.9		K0 V	7.60c	+0.77c					43.0	06. r	5.77c				31392	CD-35 1989

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
GJ 2036 A	04 52 30	-55 56.	0.130	59.0		M2 Ve	11.13	1.57	1.08	1.10			95.0	22. r	11					
GJ 2036 B	04 52 30	-55 56.	0.130	59.0			12.15	1.60	1.28				95.0	22. r	12					
Wo 9169 A	04 53 17	+04 35.5	0.233	145.6		F8	7.02	0.55	0.06		40.2	13.6	29.0	04. r	4.33				31412	BD+04 782
Wo 9169 B	04 53 15	+04 35.7	0.230	148.0		k	14.6 P				40.2	13.6	29.0	04. r	11.9 P					
GJ 2037	04 53 42	-28 38.3	0.285	137.9	12.1	K3/4 V	8.13	1.07	0.96	0.39	30.1	11.9	57.0	06. r	6.91	5	-26	2	31560	CD-28 1839
GJ 1074	04 54 50	+50 52.4	0.590	123.2		M1	10.98	1.48		0.80	54.8	11.9	54.8	11.9	9.67					
Gl 181	04 55 00	+49 46.5	0.155	136.7	-33.9	dM2 e	9.78	1.44	1.22	0.71	57.7	6.5	57.7	6.5	8.59	27	-25	-2		BD+49 1280
Gl 181.1	04 55 14	-61 13.9	1.102	123.0	42	m	12.06	1.48	1.11	0.75	45.2	10.6	27.0	04. r	9.22	75	-141	117		
Gl 182	04 56 59	+01 42.6	0.160	195.0	18.2	dM0.5	10.09	1.39	1.13	0.75	52.9	20.2	61.0	13. r	9.02	-10	-12	-16		
NN	04 58 11	+24 48.4	0.457	150.0		M2.5	11.51	1.48	1.21		34.3	14.7	63.0	16. r	10.5					
Gl 183	04 58 20	-05 48.6	1.233	153.5	+22.2	SB K3 V	6.22	1.06	1.02	0.36	110.7	3.9	110.7	3.9	6.44	5	-56	-11	32147	BD-05 1123
NN	04 59 12	+03 41.7				M1	11.28	1.52	1.20	0.86			51.0	09. r	9.82					
NN	04 59 14	+09 54.8	0.120	157.0		dM3	11.47	1.52	0.98	1.24			142.0	32. r	12.23					
Gl 184	04 59 17	+53 04.8	1.989	139.4	66	dM0	9.93	1.41	1.16	0.76	67.5	5.2	67.5	5.2	9.08	-117	-100	16		BD+52 911
NN	04 59 33	-07 00.6	0.773	224.5		m	12.1 *			1.33			163.0	26. r	13.2 *					
Gl 185 A	05 00 20	-21 19.4	0.308	211.1	-17.2	M0 V J	8.46	+1.41 J	+1.15 J	+0.72 J	129.6	7.5	129.6	7.5	9.02	19	7	2	32450	BD-21 1051
Gl 185 B	05 00 20	-21 19.4	0.308	211.1			10.5 *				129.6	7.5	129.6	7.5	11.1 *					
NN	05 00 48	+24 54.3	0.174	135.1	51.1	G8 V	7.44	0.80					46.0	06. r	5.75	-51	-16	-6	32387	BD+24 739
NN	05 01 07	-17 26.2	0.501	202.8		M3	11.69	1.63		1.11			85.0	20. r	11.3					
Gl 186	05 01 15	-23 19.3	0.327	64.3	+110.1	VAR K5 V	9.28	1.28	1.23	0.63	50.2	7.2	50.2	7.2	7.78	-81	-73	-35		CD-23 2363
Gl 186.1A	05 01 20	-56 09.7	0.722	356.8	2.9	G5 V	7.02	0.63	0.03	0.25	50.7	8.2	38.0	04. r	4.92	-88	15	-13	32778	CD-56 1071
Gl 186.1B	05 01 28	-56 10.5	0.620	354.0		m	10.60	1.36	1.14	0.62	50.7	8.2	38.0	04. r	8.5					CP-56 768
NN	05 01 29	+10 59.1	0.212	341.0		m	13.75			1.32			73.0	12. r	13.07					
Gl 187	05 01 30	-49 13.3	0.047	301.9	21.4	F2 V	5.37	0.43	-0.01	+0.24C	42.2	9.8	39.0	05. r	3.33	-6	-13	-17	32743	CD-49 1541
Gl 187.1	05 02 30	-42 25.8	0.227	128.0	59.8	K0	10.04	0.74	0.20	+0.40C	52.1	10.2	52.1	10.2	8.62	-9	-58	-24	273011	CP-42 588
Gl 187.2A	05 02 45	+51 32.0	0.178	187.5	+0.6	SB F0 V	5.00	0.33	-0.01		47.1	21.6	47.1	21.6	3.4	-7	-11	-12	32537	BD+51 1024
NN	05 02 53	-12 04.3	0.187	254.0	2.1	M4 e	12.97			+1.46C			54.0	12. r	11.63	4	5	-15		
NN	05 03 24	+04 16.2	0.375	76.0		g	11.54	1.51	1.17				59.0	28. r	10.4					
NN	05 03 39	-17 27.3	0.687	15.6		DC9?	15.97	0.74	0.00		46.2	4.6	46.2	4.6	14.29					
NN	05 03 51	+14 23.0	0.379	131.0	32.5	K0 V	7.75	0.80	0.41		25.8	20.5	41.0	07. r	5.81	-29	-46	2	32850	BD+14 831
Gl 188 A	05 04 30	+18 34.8	0.535	87.0	20.6	G4 V	5.60	+0.65 J	+0.14 J	+0.23 J	58.8	4.3	58.8	4.3	4.45	-27	-25	31	32923	BD+18 779
Gl 188 B	05 04 30	+18 34.8	0.535	87.0		G4 V	5.70*				58.8	4.3	58.8	4.3	4.55*					
Gl 189	05 04 39	-57 32.4	0.121	344.0	-2.4	F7 V	4.71	0.52	-0.04	0.20	87.8	23.2	73.0	09. r	4.03	-7	4	-1	33262	CP-57 735
NN A	05 04 42	-21 39.0				M2	10.29	1.52		0.90			83.0	12. r	9.89					BD-21 1074
NN B	05 04 41	-21 39.0				M3:	11.66	+1.51 J		+1.14 J			83.0	12. r	11.26					
NN	05 04 54	+17 55.3	0.287	160.0		k	11.78	1.66	1.32	1.08			81.0	18. r	11.32					
NN	05 04 54	+09 24.7	0.381	179.1	-22.2	G1 IV	6.17	0.62	0.10	0.22	40.2	3.3	40.2	3.3	4.19	36	-31	-16	33021	BD+09 736
GJ 1075	05 04 56	-57 37.3	0.119	346.4		K7 V	9.02	1.40	1.20	0.65			81.0	16. r	8.56					CD-57 1079
Wo 9175	05 05 23	-05 09.0	0.128	230.9	-9.2	A3 III	2.79	0.13	0.10	-0.01	49.7	5.6	49.7	5.6	1.27	13	4	-7	33111	BD-05 1162
Gl 189.2	05 06 15	-04 31.2	0.054	72.8	+10.4	SB? F2 V	5.11	0.44	-0.05	+0.26C	48.4	10.2	46.0	06. r	3.42	-10	-6	1	33256	BD-04 1056
NN	05 06 18	+15 24.3	0.642	166.8		M3	12.48	1.50	1.00	1.04	33.6	20.7	48.0	11. r	10.89					
Gl 190	05 06 21	-18 12.9	1.376	156.6	7	M4	10.30	1.50	1.04	1.16	90.6	18.8	90.6	18.8	10.09	40	-61	-2		

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	05 06 33	+48 47.1	0.454	154.9		M2	11.39	1.53	1.20				72.0	34. r	10.7					
GJ 2039	05 07 58	+16 22.3	0.280	146.3	-9.6	K0	8.55	1.12	1.17	0.47			59.0	07. r	7.4	12	-21	2	33428	BD+16 715
NN	05 08 03	+18 34.5	0.682	199.4		m	14.2 *			1.24			43.0	08. r	12.4 *					
Wo 9177	05 09 13	-44 38.1	0.200	28.8	56.1	G8 IV/V	8.71	0.77	+1.88C	0.82	39.9	20.5	39.9	20.5	6.7	-37	-43	-23	33811	CD-44 1905
Gl 191	05 09 41	-44 59.9	8.706	131.1	245.5	M0 V	8.85	1.55	1.21	0.79	258.3	7.6	258.3	7.6	10.91	19	-287	-54	33793	CD-45 1841
Gl 192	05 09 44	+19 36.2	0.352	48.0	-28.6	M3.5:	10.76	1.54	1.23	0.95	70.4	5.0	70.4	5.0	10	23	5	29		
NN	05 11 19	+19 49.7	0.332	135.5		K4	9.47	1.17	1.11		40.3	14.1	38.0	07. r	7.37				241814	BD+19 872
NN	05 11 21	+07 57.1	0.352	217.0		DA8	15.89	0.42	-0.40				40.0	04. w	13.9					
Gl 193	05 12 04	-15 52.8	0.311	136.6	32.6	G8 V	7.44	0.73	0.27	+0.36C	62.0	13.6	40.0	07. r	5.45	-7	-49	-4	34101	BD-15 978
NN	05 12 42	-07 23.8	0.545	145.4		m	11.55			0.82			39.0	07. r	9.51					
Gl 194 A	05 12 59	+45 57.0	0.431	169.2	+22.2 SB	G5 III	0.71	+0.80 J	+0.44 J	+0.28 J	79.0	4.2	79.0	4.2	0.2	-29	-16	-9	34029	BD+45 1077
Gl 194 B	05 12 59	+45 57.0	0.431	169.2	33.9	G0 III	0.96*				79.0	4.2	79.0	4.2	0.45*	-40	-12	-8		
Gl 195 A	05 13 42	+45 47.5	0.415	170.3	31.2	dM2	10.20	+1.50 J	+1.24 J	+0.94 J	76.3	2.8	76.3	2.8	9.61	-37	-13	-9		
Gl 195 B	05 13 42	+45 47.5	0.415	170.3		M4 :	13.7 *				76.3	2.8	76.3	2.8	13.1 *					
NN	05 13 51	-31 21.2	0.576	63.8		m	12.15			0.99			48.0	09. r	10.56					
Gl 196	05 14 17	+79 10.7	0.179	333.3	-10.7	F6 V	5.05	0.47	-0.13		52.9	6.1	52.9	6.1	3.67	19	4	-4	33564	BD+79 169
Gl 197	05 15 37	+40 03.4	0.844	141.6	66.5	G2 IV-V	4.71	0.63	0.12	0.20	69.5	7.4	69.5	7.4	3.92	-77	-42	5	34411	BD+39 1248
NN A	05 16 18	+58 45.0	0.526	160.3		m	13.44	1.62			39.0	2.1	39.0	2.1	11.4					
NN B	05 16 17	+58 44.7	0.526	160.3		m	14.03	1.64			39.0	2.1	39.0	2.1	11.99					
Gl 198	05 16 37	-18 10.9	0.383	81.6	40.3	G0 V	5.96	0.57	0.07	0.21	63.7	15.3	49.0	08. r	4.41	-35	-40	13	34721	BD-18 1051
Gl 200 A	05 16 40	-03 07.6	0.734	80.0	86.5	K3 V	7.70	+1.04 J	+0.86 J	+0.47 J	79.7	5.7	79.7	5.7	7.21	-81	-53	6	34673	BD-03 1061
Gl 200 B	05 16 40	-03 07.6	0.734	80.0		M2	11.7 *				79.7	5.7	79.7	5.7	11.2 *					
Gl 199 A	05 16 40	-21 26.7	0.140	253.0	+27.6 VAR	K3/5 V	9.33	+1.27 J	+1.23 J	+0.64 J	53.6	9.8	61.0	08. r	8.26	-14	-12	-23	34751	BD-21 1131
Gl 199 B	05 16 40	-21 26.7	0.140	253.0			13.5 *				53.6	9.8	61.0	08. r	12.4 *					
Gl 200.1	05 16 48	-53 43.6	0.512	154.2		k	13.19	1.16	0.72	0.50	44.9	10.2	44.9	10.2	11.45					
NN	05 16 50	-72 17.6	0.840	356.3		m	11.70	1.40	1.11	0.96			52.0	10. r	10.28					
GJ 2040	05 16 57	+03 49.4	0.014	226.3		M0 V	9.86	1.42					60.0	15. r	8.8				242703	BD+03 849
NN	05 16 59	+55 43.1	0.278	150.0		m	13.01			1.09			43.0	09. r	11.18					
NN	05 17 44	-15 53.5	0.248	42.0		K3 V	8.79	1.00	0.73	0.40			39.0	06. r	6.75				34865	BD-15 1016
GJ 1076	05 19 13	+54 45.5	0.394	167.7	49.3	K3 p	9.46	1.04	0.91	0.38	51.1	13.6	29.0	04. r	6.77	-73	-33	-14		BD+54 886
GJ 1077	05 19 38	-78 19.6	1.108	176.1	-17	M1.5 V	11.91	1.48	1.20	1.08	76.8	13.0	76.8	13.0	11.34	59	25	29		
GJ 2041	05 20 12	+00 09.8	0.031	140.9		K5 V?	8.82	1.11					47.0	07. r	7.18				35152	BD+00 1032
Gl 201	05 20 43	+17 16.7	0.251	89.1	37.8	dK5 e	7.95	1.09	1.00	0.44	61.2	6.8	61.2	6.8	6.88	-39	-15	9	35171	BD+17 917
GJ 1078	05 20 47	+22 30.2	0.383	141.0		m	15.52	1.83	1.65		48.5	4.5	48.5	4.5	13.95					
Gl 202	05 21 30	+17 20.3	0.245	92.8	38.1	F8 Ve	4.99	0.53	-0.06		65.2	9.0	65.2	9.0	4.06	-38	-15	7	35296	BD+17 920
GJ 1079	05 24 22	-32 32.7	0.266	110.3		K2/3 V	7.74	0.94	0.68	0.35			55.0	07. r	6.44				35854	CD-32 2337
Gl 203	05 25 16	+09 36.8	0.783	195.1		M3.5	12.48	1.64	1.21	1.18	99.7	3.2	99.7	3.2	12.47					
GJ 1080	05 25 38	+02 56.7	1.186	198.1		M5 V	12.80	1.60	0.99	1.06	52.3	2.2	52.3	2.2	11.39					
Gl 204	05 25 57	-03 31.7	0.862	202.4	-56	K5 V	7.65	1.10	1.06	0.43	71.2	6.9	71.2	6.9	6.91	77	-3	-22	36003	BD-03 1110
NN A	05 26 03	+12 30.9	0.234	156.3	8.6	G0 V	6.75	0.58	0.07	0.29	39.5	10.2	39.5	10.2	4.7	-2	-29	-6	35956	BD+12 801
NN B	05 26 08	+12 29.7	0.235	153.0		m	13.98	1.65	1.37		39.5	10.2	39.5	10.2	12					
GJ 2043 A	05 26 35	+15 32.3	0.199	207.0		dM2	10.63	1.47	1.29	0.77			46.0	06. r	8.94					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
GJ 2043 B	05 26 34	+15 32.4	0.199	207.0		m	14.68			1.28			46.0	06. r	12.99					
NN	05 26 38	+32 03.2	0.700	198.4		M3	12.15	+1.48.	1.15		34.1	5.0	34.1	5.0	9.81					
Gl 204.1	05 27 03	-60 27.3	0.189	232.2	12.9	G5 Ve	6.99	0.77	0.31	0.26	44.8	17.0	49.0	08. r	5.44	12	-3	-19	36435	CP-60 424
Wo 9181	05 27 06	-75 43.7	0.331	196.5	43	F8 V	7.17	0.54	0.01		42.1	11.9	27.0	03. s	4.33	66	-16	-26	36767	CP-75 314
Gl 204.2	05 27 23	-03 28.4	0.570	214.0		M3.5	12.02	1.53	1.32	1.05	53.1	4.5	53.1	4.5	10.65					
Gl 205	05 28 55	-03 41.1	2.235	159.9	8.5	M1.5 V	7.96	1.47	1.21	0.85	172.3	3.1	172.3	3.1	9.14	23	-57	-11	36395	BD-03 1123
NN	05 29 08	-30 13.5	0.571	142.0		m	13.0 *			1.13			50.0	10. r	11.5 *					
NN	05 29 12	+79 31.0	1.192	141.2	-92	m	18.40				45.2	1.4	45.2	1.4	16.68	-21	-154	-8		
Gl 206	05 29 30	+09 47.3	0.293	233.0	+21.7 SB	dM4 e	11.52	1.63	1.07	+1.20:	70.9	2.7	70.9	2.7	10.77	-16	-6	-24		
GJ 1081	05 29 38	+44 47.2	0.369	172.0		k-m	12.21	1.60	1.20	1.16	65.9	2.7	65.9	2.7	11.3					
Gl 207	05 29 53	+29 21.4	0.330	245.2		K7	12.07	1.46	1.19		54.1	15.3	54.1	15.3	10.7					
NN	05 30 13	+51 11.1	0.242	187.0		M3	11.07	1.46	1.20	0.78			45.0	07. r	9.34					
Gl 207.1	05 31 09	+01 54.8	0.317	236.0	22	dM2.5e	11.53	1.57	0.99	1.09	66.3	8.9	66.3	8.9	10.64	-13	-7	-28		
NN A	05 31 30	+10 17.5	0.380	197.0		M3	12.32			1.06			51.0	07. r	10.86					
NN B	05 31 30	+10 17.4	0.380	197.0		M3.5	13.62			1.21			51.0	07. r	12.16					
NN	05 31 51	+28 04.2	0.347	139.0		K7	10.08	1.27	1.29				41.0	08. r	8.14				244957	
NN	05 32 02	+13 51.1	0.410	197.0		M3.5	11.81	1.59		1.15	80.7	5.7	80.7	5.7	11.34					
GJ 1082	05 32 48	+41 28.2	0.100	285.0		DA7	14.75	0.32	-0.54				53.0	06. w	13.37					
NN	05 33 30	-07 41.0	0.485	17.8		M4	12.80	1.63		1.23			79.0	19. r	12.3					
Gl 208	05 33 44	+11 17.9	0.057	195.0	21.2	dM0	8.80	1.40	1.18	0.65	86.1	5.6	86.1	5.6	8.48	-19	-7	-6	245409	BD+11 878
Gl 209	05 34 04	+20 42.4	0.443	191.3	-23.2	G4 IV-V	7.67	0.66	0.12		56.2	15.3	56.2	15.3	6.4	28	-24	-23	37124	BD+20 1018
NN	05 34 18	+51 24.9	0.560	281.3	-44	K2 V	7.73	0.83	0.44		39.7	7.0	39.7	7.0	5.72	48	31	-57	37008	BD+51 1094
NN	05 35 20	+45 25.3	0.127	146.8		G5	8.08						42.0	05. o	6.2				37199	BD+45 1150
Wo 9185	05 35 24	-62 50.2	0.272	346.0	21	K5 V	9.33	1.13	1.07	0.43	42.0	13.6	38.0	06. r	7.23	-32	-14	-19	37656	CP-62 494
Gl 209.1	05 35 47	-28 43.1	0.057	314.4	39.4	F5 V	5.30	0.46	0.10	+0.26C	45.6	10.2	49.0	08. r	3.75	-24	-24	-21	37495	CD-28 2321
Wo 9187	05 36 28	-07 14.4	0.056	198.6	-1.3 SB	A4 IV	4.80	0.14	0.11		41.3	15.3	41.3	15.3	2.9	5	-2	-4	37507	BD-07 1142
Gl 210	05 36 30	-42 59.7	0.294	21.6	+35.1 VAR	G0 V	7.44	0.60	0.07	+0.34C	59.8	13.6	28.0	05. r	4.68	-55	-25	4	37655	CD-43 1954
NN A	05 36 45	-46 07.6	0.471	192.8	11.4	G5 V	7.34	0.78			33.2	10.2	40.0	05. r	5.35	50	-15	-23	37706	CD-46 1936
NN B	05 36 46	-46 07.6	0.522	197.4	13.5	K5 V	9.7 *				33.2	10.2	40.0	05. r	7.7 *	54	-15	-30		
Gl 211	05 37 17	+53 27.8	0.512	178.0	1.8	K1 Ve	6.23	0.84	0.51	0.29	82.7	2.5	82.7	2.5	5.82	-14	-22	-13	37394	BD+53 934
GJ 1083 A	05 37 21	+24 46.9	0.364	163.0		m	14.85J	+1.88 J		+1.73 J	96.7	2.5	96.7	2.5	14.78J					
Gl 212	05 37 27	+53 28.3	0.495	177.7	2	M1	9.75	1.48	1.20	0.82	86.1	4.6	86.1	4.6	9.43	-13	-21	-12	233153	BD+53 935
NN	05 37 27	+12 37.6	0.250	188.0		M3	11.36	1.46		0.85			47.0	08. r	9.72					
Wo 9188	05 39 07	+15 18.8	0.089	120.3		dM0	10.61	1.46	1.23	0.71			47.0	07. r	8.97					
Gl 213	05 39 14	+12 29.3	2.571	128.4	105.6	M4	11.53	1.62	1.20	1.27	166.5	3.9	166.5	3.9	12.64	-89	-92	9		
GJ 2045	05 39 46	-05 30.1	0.971	352.3		m	15.28	1.86			78.1	2.7	78.1	2.7	14.74					
Gl 215	05 41 05	+62 13.7	0.838	166.3	-19.6	K7	9.02	1.40	1.23	0.63	71.6	2.8	71.6	2.8	8.29	-13	-54	-18		BD+62 780
Wo 9189	05 41 08	-80 30.5	1.100	16.9	9.4	G1 V	5.65	0.60	0.11	0.19	42.9	17.0	62.0	10. r	4.61	-73	-43	2	39091	CP-80 161
NN	05 41 35	+32 22.3	0.085	168.8		G5	8.15						48.0	05. o	6.56				38114	BD+32 1077
NN	05 42 00	+69 44.0	0.915	125.9		m	16.47	1.69			42.4	4.4	42.4	4.4	14.61					
Gl 216 A	05 42 23	-22 27.8	0.476	218.5	-9.7	F6 V	3.58	0.47	0.01	0.16	124.9	6.9	124.9	6.9	4.06	17	5	-10	38393	BD-22 1211
Gl 216 B	05 42 21	-22 26.2	0.470	220.7	-8.4	K2 V	6.13	0.94	0.74	0.35	124.9	6.9	124.9	6.9	6.61	16	5	-11	38392	BD-22 1210

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 217	05 42 35	+37 16.4	0.709	136.8	-26.9	K1 V	7.36	0.83	0.51		56.7	5.1	56.7	5.1	6.13	20	-61	10	38230	BD+37 1312
NN	05 43 02	+44 06.4	0.683	239.6		M4	12.79	1.55		1.25	39.2	10.2	39.2	10.2	10.8					
NN	05 44 39	-05 12.9	0.804	135.9		m	14.54	1.78			62.5	3.4	62.5	3.4	13.52					
Gl 217.1	05 44 41	-14 50.4	0.022	264.4	16.3	A3 V	3.55	0.10	0.07	-0.05	48.7	5.9	48.7	5.9	1.99	-12	-9	-8	38678	BD-14 1232
NN	05 44 44	-00 01.8				M0	10.99	1.45	1.15	0.74			42.0	07. r	9.11					
Gl 217.2	05 45 06	-70 10.8	1.263	345.6	13.8	K0 V	8.08	0.76	0.27	0.28	47.7	19.3	32.0	05. r	5.61	-177	-13	-60	39194	CP-70 447
NN	05 45 41	+07 44.9	0.276	165.0		m	14.19			1.25			45.0	08. r	12.46					
Gl 218	05 45 53	-36 20.6	0.692	96.6	56	M3	10.73	1.48	1.11	0.90	95.5	8.2	95.5	8.2	10.63	-19	-63	2		CD-36 2458
NN	05 45 57	-11 09.3	0.425	329.0		M0.5	11.00	1.42		0.72	36.3	10.2	42.0	08. r	9.12					
GJ 1084	05 46 00	-48 32.2	0.320	176.0		M0 V	9.74	1.38	1.22	0.62	21.6	18.8	57.0	11. r	8.52					CD-48 1982
GJ 1085	05 46 06	-04 06.4	0.232	165.6	31.9	G2 V	5.97	0.64	0.10	0.22			59.0	09. r	4.82	-17	-30	-13	38858	BD-04 1244
Gl 219	05 46 06	-51 05.0	0.081	4.7	20	A5 V	3.85	0.17	0.09	+0.09C	59.8	10.7	59.8	10.7	2.73	-10	-16	-9	39060	CD-51 1620
GJ 1086	05 48 46	-00 11.3	0.213	22.0		DQP8	14.55	0.48	-0.45		90.5	2.8	90.5	2.8	14.33					
Gl 220	05 50 10	+24 15.4	0.610	169.1		M1.5	10.81	1.48	1.22	0.89	52.2	4.2	52.2	4.2	9.4					
Gl 221	05 50 34	-06 00.0	0.333	180.0	22.2	M0 V	9.70	1.33	1.25	0.62	50.8	11.6	50.8	11.6	8.23	0	-33	-20		BD-06 1339
Gl 222 A	05 51 25	+20 16.1	0.210	244.0	-13.4 SB	G0 V	4.40 J	+0.59 J	+0.06 J	+0.20 J	103.1	2.8	103.1	2.8	4.47 J	14	3	-9	39587	BD+20 1162
NN	05 51 34	+48 59.9	0.004	146.7		K2	7.83	1.07	0.74				61.0	09. r	6.76				40676	BD+48 1318
Gl 223	05 51 52	+02 08.6	0.644	173.7	-41.8	K3 V	8.83	1.02	0.90	0.38	66.7	11.9	39.0	06. r	6.79	73	-47	-21	39715	BD+02 1085
Gl 223.1	05 52 11	-09 24.3	0.452	18.0		dM0	10.71	1.17	1.04	0.48	51.0	10.2	23.0	03. r	7.52					BD-09 1261
Gl 223.2	05 52 39	-04 08.8	2.377	166.6		DZ9	14.45	1.05	0.77	0.29	154.8	2.9	154.8	2.9	15.4					
Gl 224	05 53 12	+13 55.5	0.608	143.4	0.3	G5 IV	6.61	0.65	0.13	0.22	47.4	12.0	47.4	12.0	5	14	-59	7	39881	BD+13 1036
Gl 224.1	05 53 43	-63 06.3	0.554	13.8	25.1	K1 III/IV	4.65	1.05	0.96	0.36	50.6	14.8	50.6	14.8	3.2	-49	-31	-1	40409	CP-63 498
GJ 1087	05 53 47	+05 22.2	1.056	207.0		DAP9	14.10	0.60	-0.14	0.25	125.1	4.1	125.1	4.1	14.59					
Gl 225	05 54 08	-14 10.5	0.146	340.4	-1.4	F1 III	3.72	0.33	0.01	+0.20C	73.4	16.5	73.4	16.5	3.05	-5	8	1	40136	BD-14 1286
NN A	05 55 14	+58 35.6	0.253	184.0		M1	10.25	1.51	1.25	0.83			76.0	09. r	9.65					
NN B	05 55 32	+58 34.3	0.253	184.0		m	13.56			1.31			76.0	09. r	12.96					
NN A	05 55 27	+68 09.7	1.174	161.4		k-m	12.90	1.56			49.5	1.7	49.5	1.7	11.37					
NN B	05 55 24	+68 08.8	1.174	161.4		m	13.31	1.59			49.5	1.7	49.5	1.7	11.78					
NN	05 55 52	+44 56.7	0.056	269.7	-19.4 SB	A2 IV	1.90v	0.03	0.05		44.3	5.5	44.3	5.5	0.13v	18	-1	-9	40183	BD+44 1328
NN A	05 55 53	-04 39.1	0.227	163.5		G0	6.99						40.0	05. o	5				40397	BD- 4 1310
NN C	05 55 49	-04 38.1	0.230	159.0		k-m	16.3 P						40.0	05. o	14.3 P					
NN	05 56 43	+59 36.5	0.831	190.1		m	11.71	1.60		1.21	132.2	2.9	132.2	2.9	12.32					
NN	05 57 26	+02 42.3	0.241	108.0		M4	11.33	1.68	1.10		186.3	6.2	186.3	6.2	12.68					
Gl 225.1	05 58 12	-37 03.6	0.286	49.5	40	G5 V	8.60	0.63	0.05	+0.34C	46.9	10.2	46.9	10.2	6.96	-32	-37	6	40865	CD-37 2534
Gl 225.2A	05 58 28	-31 02.2	0.560	314.4	101.7	K5 V	8.28	+1.14 J	+0.94 J	+0.52 J	50.7	10.0	66.0	08. r	7.38	-77	-52	-58	40887	CD-31 2902
Gl 225.2B	05 58 28	-31 02.2	0.560	314.4			9.1 *				50.7	10.0	66.0	08. r	8.2 *					
Gl 225.2C	05 58 28	-31 02.2	0.560	314.4	105	K5 V	8.3 *				50.7	10.0	66.0	08. r	7.4 *	-78	-55	-59		
NN	05 58 36	+49 52.4	0.801	174.5		m	14.47	1.87	1.45		107.8	3.0	107.8	3.0	14.63					
Gl 226	05 59 42	+82 07.9	1.337	180.7	-21	M2.5	10.50	1.51	1.19	1.01	105.0	2.2	105.0	2.2	10.61	-36	-47	-25		
NN	05 59 43	+47 48.8	0.595	187.6		M3.5	13.94			1.23			45.0	08. r	12.21					
NN	06 00 14	-20 20.1	0.579	356.4		m	13.25			1.16			49.0	10. r	11.7					
Gl 226.1	06 00 47	+26 09.4	0.642	149.4		M3.5	13.67	1.65		1.08	47.9	8.5	47.9	8.5	12.07					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	06 01 25	+18 41.9	0.012	173.2		G5	7.98						51.0	06. o	6.52				41190	BD+18 1074
Gl 226.2	06 02 37	+67 59.1	0.090	193.0	1.6	dK8	9.75	1.25	1.20	0.50	50.9	10.2	40.0	05. r	7.76	-8	-5	-5		
Gl 226.3	06 02 48	+35 23.8	0.314	202.2	-14.8	G0 V	6.11	0.60	0.06		46.6	15.3	49.0	08. r	4.56	11	-20	-25	41330	BD+35 1334
Wo 9200	06 03 02	-45 02.1	0.260	339.7	25.8	G0 IV-V	6.35	0.52	0.00		40.2	10.3	40.2	10.3	4.4	-35	-11	-15	41700	CD-45 2300
Wo 9201	06 03 15	-55 18.2	0.760	65.7	6	k	12.15	1.46	1.11	0.93	40.6	10.3	40.0	08. r	10.16	-31	-43	73		
Gl 227	06 03 49	+15 33.0	0.164	227.8	-11.7	dK0 e	6.76	0.81	0.42	0.26	65.3	10.2	65.3	10.2	5.83	12	0	-11	41593	BD+15 1065
NN	06 03 54	+33 33.3	0.430	161.0		M3	12.44	1.45		0.97			41.0	10. r	10.5					
Wo 9202	06 05 25	-59 31.5	0.793	196.0	25.4	K0 V	8.46	0.85	0.45	0.29	40.8	7.8	31.0	05. r	5.92	113	-4	-52	42286	CP-59 584
Wo 9203	06 05 57	+26 34.0	0.570	255.0		M3	13.34	1.50		0.91	40.8	13.6	24.0	06. r	10.2					
NN	06 07 40	+25 57.1	0.568	161.8		M1.5	11.55	1.46	1.20	0.89	34.7	5.9	34.7	5.9	9.25					
Gl 228 A	06 08 09	+10 20.6	0.970	175.8	55.5	dM2.5 J	10.58	+1.46 J	+1.08 J	+1.03 J	100.8	4.6	100.8	4.6	10.6	-37	-57	-23		BD+10 1032
Gl 228 B	06 08 09	+10 20.6	0.970	175.8			12.5 *				100.8	4.6	100.8	4.6	12.5 *					
Gl 229	06 08 28	-21 50.6	0.737	190.2	5.2	M1 Ve	8.14	1.50	1.23	0.82	174.9	6.7	174.9	6.7	9.35	12	-12	-12	42581	BD-21 1377
NN	06 08 48	+63 24.7	0.248	137.0	17.9	dK8	9.69	1.21	1.18	+0.50:	34.2	18.4	40.0	06. r	7.7	-25	-18	16		BD+63 0639
NN	06 09 18	+06 47.9	0.319	142.3	-52.4	G4 V	6.87	0.63	0.13		42.7	19.9	39.0	06. r	4.83	62	-16	11	42618	BD+06 1155
GJ 1088	06 09 25	-43 24.5	0.740	9.5	28	M3.5	12.32	1.59	1.26	1.16			75.0	19. r	11.7	-51	-18	5		
Wo 9204	06 09 55	-41 33.7	0.292	164.6	15	K2 V	9.29	0.95	0.68	0.35	43.7	13.6	27.0	04. r	6.45	43	-31	-6	42931	CD-41 2266
NN	06 10 06	+51 41.1	0.370	258.0		m	12.86			1.14			55.0	11. r	11.56					
Wo 9205	06 10 18	+70 48.2	0.444	180.6	25	dG7	7.43	0.77	0.37		42.7	11.9	44.0	06. r	5.65	-50	-19	-5	42250	BD+70 395
Gl 230	06 10 26	+10 38.7	0.302	164.2	+6.0 SB?	G2 V	6.45	0.67	0.15	0.22	56.9	6.1	56.9	6.1	5.23	3	-25	-6	42807	BD+10 1050
Wo 9206	06 10 51	-65 10.8	0.764	167.1		k	11.35	1.46		0.76	42.7	14.5	37.0	06. r	9.19					
NN	06 11 41	-23 50.9	0.125	336.0	22.4	G5 V	6.38	0.72					61.0	08. r	5.31	-21	-10	-7	43162	CD-23 3577
Gl 231	06 11 44	-74 44.2	0.247	149.6	34.9	G5 V	5.08	0.72	0.33	0.23	114.1	10.2	114.1	10.2	5.37	17	-30	-12	43834	CP-74 374
NN	06 11 54	+19 10.5	0.217	208.4	35.7	F6 V	5.20	0.44	0.00		37.7	11.9	46.0	06. r	3.51	-33	-19	-18	43042	BD+19 1270
Wo 9207	06 13 38	+12 17.3	0.202	23.3	8.7	F5 IV-V	5.04	0.42	-0.02		43.4	10.2	43.4	10.2	3.2	-13	10	17	43386	BD+12 1084
Gl 231.1A	06 14 37	+05 07.0	0.261	306.7	9.6	F9 V	5.70	0.60	0.10	0.22	50.4	9.6	61.0	09. r	4.63	-16	13	-9	43587	BD+05 1168
Gl 231.1B	06 14 32	+05 08.1	0.290	302.0	8.9	m+	13.42	1.41	1.10	1.24	50.4	9.6	61.0	09. r	12.35	-15	15	-12		
Wo 9209 A	06 15 37	-59 11.4	0.333	189.6	-3	G3 V	6.43	0.59	0.14	0.19	42.0	13.6	44.0	07. r	4.65	34	7	-8	44120	CP-59 619
Wo 9209 B	06 15 37	-59 11.4	0.333	189.6	40	DB4	14.09	-0.09	-0.95		42.0	13.6	44.0	07. r	12.31	34	8	-7		
Gl 231.3	06 16 55	-06 37.6	0.669	187.0		M4	13.06	1.70		1.11	67.6	13.6	67.6	13.6	12.21					
NN	06 17 34	+44 16.2	0.305	145.0		m	12.27			0.96			42.0	08. r	10.39					
NN	06 18 05	+06 46.7	0.515	93.3		DA9	16.37	0.55	-0.17		44.8	4.2	44.8	4.2	14.63					
GJ 2049	06 19 50	-22 42.1	0.671	292.6		M1.5	10.76	1.44	1.23	0.98	27.8	23.9	76.0	17. r	10.16					CD-22 3005
Gl 232	06 21 37	+23 28.1	0.763	132.4		M4.5	13.06	1.76		1.30	120.0	1.9	120.0	1.9	13.46					
NN	06 21 39	+56 12.5	0.530	166.3		m	14.55	1.76	1.23		44.9	4.7	44.9	4.7	12.81					
NN	06 22 47	-28 45.0	0.204	233.6	-4.4	G0 V	6.39	0.62					45.0	06. r	4.66	10	6	-18	45184	CD-28 2981
Gl 233 A	06 23 14	+18 47.3	0.210	214.6	-8.4 SB	K2 V e	6.76	0.94	0.63		66.6	4.2	66.6	4.2	5.88	9	-5	-14	45088	BD+18 1214
Wo 9212 A	06 25 10	-25 49.3	0.290	220.0	35.8	F9 V	6.07	0.53	0.05		43.7	15.3	35.0	04. s	3.79	0	-30	-44	45588	CD-25 3237
Wo 9212 B	06 25 10	-25 49.3	0.290	220.0		K7	11.57	1.04	0.14		43.7	15.3	35.0	04. s	9.29					
Gl 234 A	06 26 51	-02 46.2	0.997	134.8	16.7	M4.5 J	11.13	+1.71 J	+1.20 J	+1.37 J	242.1	1.7	242.1	1.7	13.05	-4	-25	4		
Gl 234 B	06 26 51	-02 46.2	0.997	134.8			14.6 *				242.1	1.7	242.1	1.7	16.5 *					
NN	06 27 08	+50 05.0				M0	11.09	1.50	1.14	0.84			52.0	09. r	9.67					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	06 28 18	+41 32.1	0.196	183.0		m	14.83			1.53			90.0	15. r	14.6					
Gl 236	06 30 07	-26 59.5	0.461	116.0	113	M0	11.41	1.37		+0.89C	67.3	8.5	67.3	8.5	10.55	-44	-108	-11		
Gl 237	06 30 22	-43 29.8	0.264	262.0	27	g-k	10.59	1.48	1.23	0.73	58.3	15.3	50.0	08. r	9.08	-9	-14	-33		CP-43 912
NN	06 32 45	-69 55.2	0.701	17.4		m	13.0 *			1.08			42.0	09. r	11.1 *					
Gl 238	06 33 07	-58 29.9	0.885	332.8	-16	m	11.62	1.51	1.16	1.02	71.0	11.9	71.0	11.9	10.88	-56	23	-7		
NN	06 33 20	+11 40.1	0.901	190.2		k-m	14.22	1.65		1.30	55.1	3.6	55.1	3.6	12.93					
Gl 239	06 34 19	+17 36.2	0.885	293.4	-56.1	dM1	9.63	1.49	1.21	0.73	99.1	3.1	99.1	3.1	9.61	43	46	-32	260655	BD+17 1320
Gl 239.1	06 34 30	-19 12.7	0.083	139.6	4.1	K1 III	3.96	1.05	1.01		54.7	6.5	54.7	6.5	2.65	2	-8	1	47205	BD-19 1502
Gl 240	06 35 55	-49 59.7	0.220	90.0	16	K0	9.62	1.46	1.22	0.76	69.7	10.2	69.7	10.2	8.84	0	-21	7		CP-49 990
NN	06 36 56	+28 38.2	0.250	174.0		k-m	11.93	1.50	1.19				46.0	22. r	10.2					
NN A	06 37 28	-61 29.3	0.072	330.0	32.3	G0 V	6.34	+0.62 J	+0.12 J				46.0	07. r	4.65	-6	-28	-16	48189	CP-61 688
NN B	06 37 28	-61 29.3	0.072	330.0			8.3 *						46.0	07. r	6.6 *					
Gl 240.1	06 37 44	+79 37.4	0.613	187.7	+15.7	SB? F8 V	5.45	0.50	-0.02		47.5	6.0	47.5	6.0	3.83	-57	-26	-8	46588	BD+79 212
Gl 241	06 38 12	+24 00.6	0.338	143.5	-44.6	dK6	8.13	1.02	0.92	0.38	57.0	6.4	57.0	6.4	6.91	49	-19	-2	47752	BD+24 1357
NN	06 38 36	+15 48.9	0.363	175.0		M3	13.77			1.20			40.0	08. r	11.78					
NN	06 38 48	-55 34.0	0.380	269.0		K7 V	9.94	1.31	1.18	0.52			40.0	07. r	7.95					CD-55 1514
Wo 9216	06 38 53	+71 56.8	0.555	193.1	-12	K7	10.95	1.48	1.21	0.80	37.8	9.4	37.8	9.4	8.8	-39	-50	-31		
NN A	06 39 33	+03 37.9	0.287	173.0		m	12.06			1.11			64.0	09. r	11.09					
NN B	06 39 36	+03 38.6	0.287	173.0		m	13.33			1.22			64.0	09. r	12.36					
NN A	06 39 54	+51 12.1	0.922	173.6		M3.5 J	12.44	+1.59 J	+1.25 J		52.1	4.3	52.1	4.3	11.02					
NN B	06 39 54	+51 12.1	0.922	173.6			14.9 *				52.1	4.3	52.1	4.3	13.5 *					
Gl 242	06 42 29	+12 57.1	0.225	210.8	+30.0	VAR F5 III	3.36	0.43	0.06		50.2	11.2	50.2	11.2	1.86	-25	-22	-16	48737	BD+13 1396
NN A	06 42 51	+32 36.5	0.462	280.1	-34.5	K3 V	8.77:	0.96	0.70		47.1	7.5	47.1	7.5	7.14:	24	27	-45	263175	BD+32 1398
NN B	06 42 53	+32 36.4	0.528	280.5		M0.5	12.17	1.53	1.23		47.1	7.5	47.1	7.5	10.54					
Gl 243	06 42 52	-27 17.6	0.288	357.9	-12.1	G2 V	6.45	0.54	-0.03	+0.32C	60.5	13.6	40.0	06. r	4.46	-22	25	15	48938	CD-27 3248
Gl 244 A	06 42 57	-16 38.8	1.328	204.3	-9.4	VAR A1 V	-1.43	0.00	-0.04	-0.11	380.4	2.9	380.4	2.9	1.47	15	1	-11	48915	BD-16 1591
Gl 244 B	06 42 57	-16 38.8	1.328	204.3		DA2	8.44	-0.03?	-1.04		380.4	2.9	380.4	2.9	11.34					
Gl 245	06 43 08	+43 37.8	0.164	359.0	-23.9	G0 V	5.24	0.56	0.05		66.2	8.5	66.2	8.5	4.34	25	8	-3	48682	BD+43 1595
Gl 245.1	06 43 31	-31 44.1	0.387	213.4	32	F6 V	5.92	0.49	-0.04	+0.28C	50.4	9.3	41.0	04. s	3.98	11	-30	-44	49095	CD-31 3640
Gl 246	06 44 15	+37 35.1	0.968	193.3	80	DA2	12.06	-0.08	-0.92		62.6	3.1	62.6	3.1	11.04	-47	-58	-32		
NN	06 44 47	+02 34.4	0.436	275.0		DA8	15.68	0.32	-0.53		54.6	5.5	54.6	5.5	14.37					
Gl 247	06 45 27	+60 23.2	0.476	29.1	-52.9	dM0 p	8.58	1.22	1.17	0.48	50.6	2.9	50.6	2.9	7.1	69	4	8	48948	BD+60 1003
GJ 1091	06 45 27	+37 12.0	0.140	263.0			13.34	1.35		0.99	44.3	5.4	44.3	5.4	11.57					
GJ 1092	06 45 41	+37 11.7	1.618	172.3		m	13.76	1.66	0.94	1.25	75.8	3.9	75.8	3.9	13.16					
NN	06 46 16	+35 12.1	0.315	154.0		K5	10.17	1.32	1.27	0.57			40.0	06. r	8.18					
Gl 248	06 47 41	-61 53.2	0.276	345.1	20.6	A7 IV	3.27	0.21	0.13	+0.14C	50.9	10.2	50.9	10.2	1.8	-25	-19	-9	50241	CP-61 720
Gl 249	06 47 49	+47 26.2	0.736	198.2	22.2	dK6	8.99	1.24	1.16	0.50	50.4	11.1	56.0	10. r	7.73	-43	-42	-28	49601	BD+47 1355
Gl 249.1	06 48 30	-46 33.6	0.370	359.0	20.1	F5 III	5.13	0.45	-0.03	0.26	48.5	12.3	48.5	12.3	3.6	-39	-14	4	50223	CD-46 2703
NN A	06 49 29	+60 56.8	1.147	152.3		M3.5	11.06	+1.54 J		+1.39CJ	91.5	3.6	91.5	3.6	10.87					
NN	06 49 36	+18 20.0	0.208	40.0		m	13.18			1.17			53.0	10. r	11.8					
Gl 250 A	06 49 52	-05 06.7	0.544	269.8	-9.6	K3 V	6.59	1.05	0.95	0.39	108.9	5.4	108.9	5.4	6.78	2	15	-21	50281	BD-05 1844
Gl 250 B	06 49 52	-05 07.7	0.541	270.0	-6.9	M2	10.09	1.50	1.26	0.98	108.9	5.4	108.9	5.4	10.28	-1	13	-21		

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Wo 9219	06 51 34	-28 28.2	0.519	147.5	72.1	G5 IV	6.03	0.72	0.27	0.24	41.4	8.4	41.4	8.4	4.12	13	-92	-7	50806	CD-28 3554
Gl 251	06 51 35	+33 20.3	0.851	242.3	22.9	dM4	10.01	1.57	1.21	1.11	173.6	2.2	173.6	2.2	11.21	-28	-3	-16		
Wo 9220 A	06 51 49	+13 14.6	0.100	139.8	+14.8 SB	A9 V p	4.74	0.31	0.03		40.7	8.4	39.0	04. s	2.7	-9	-16	5	50635	BD+13 1462
Wo 9220 B	06 51 49	+13 14.6	0.100	139.8	22.3	G6 V	7.68	0.72	0.20		40.7	8.4	39.0	04. s	5.64	-16	-19	5		
Gl 251.1	06 52 10	+12 13.7	0.333	190.0	16.4	dM1.5	10.55	1.24	1.23	0.50	44.0	20.7	29.0	05. r	7.86	-2	-48	-31		BD+12 1343
Gl 252	06 52 14	+25 26.4	0.049	301.8	-15.1	G0 V	5.74	0.57	0.00	0.22	52.7	11.5	59.0	08. r	4.59	13	6	-5	50692	BD+25 1496
NN	06 52 18	+55 02.9	0.706	199.2		k-m	11.8 *				58.6	5.6	58.6	5.6	10.6 *					
NN A	06 52 59	+40 08.8	0.466	164.4	50.9	K5 V	9.12	1.12	1.05	0.43	38.1	3.0	38.1	3.0	7.02	-54	-55	10		BD+40 1758
NN B	06 52 59	+40 08.8	0.466	164.4	51.2	M1	11.10	1.43		0.81	38.1	3.0	38.1	3.0	9	-54	-54	11		
NN	06 53 17	+62 23.7	0.516	139.9		m	13.65			1.47			129.0	20. r	14.2					
Gl 253	06 53 51	-55 11.5	0.182	187.6	40.1	G7 V	8.17	0.78	0.37	0.24			69.6	08.5d	7.38	8	-36	-20	51608	CP-55 1095
Gl 254	06 53 52	+30 49.6	0.230	157.6	-7.8	K7	9.72	1.36	1.23	0.62	72.8	20.5	56.0	11. r	8.46	9	-19	-2	266611	BD+30 1367
Wo 9222	06 54 41	-74 39.8	0.197	341.4	-0.9	F8 V +A/F	7.65	0.53	0.05		41.0	13.6	20.0	03. r	4.16	-45	-9	-6	52449	CP-74 421
NN	06 55 22	+14 17.3	0.009	219.7		G5	8.28						48.0	05. o	6.69				51534	BD+14 512
Gl 255 A	06 55 30	-35 26.4	0.040	296.9	10.1	F8 IV-V	6.91	+0.46 J	-0.06 J	+0.26CJ	68.4	13.6	68.4	13.6	6.09	-6	-8	-4	51825	CD-35 3233
Gl 255 B	06 55 30	-35 26.4	0.040	296.9		F8 IV-V	7.1 *				68.4	13.6	68.4	13.6	6.3 *					
Gl 256	06 56 07	-12 55.3	0.119	134.4	-7.7	K4 V	9.15	1.16	1.06	0.50	36.8	10.7	47.0	07. r	7.51	13	-3	4	51849	BD-12 1724
Gl 257 A	06 56 21	-44 13.3	1.134	265.0		M3	11.50	+1.66 J	+1.21 J	+1.12 J	116.9	8.1	116.9	8.1	11.8					CD-44 3045
Gl 257 B	06 56 21	-44 13.3	1.134	265.0		M3	11.7 *				116.9	8.1	116.9	8.1	12.0 *					
GJ 1093	06 56 29	+19 25.8	1.225	137.3		m	14.83	1.93		1.60	128.9	3.5	128.9	3.5	15.38					
NN	06 56 53	-10 11.2	0.729	181.9		m	13.5 :			1.20			51.0	10. r	12.0 :					
NN	06 57 36	+32 02.5	0.684	150.6		DC9	16.57	0.96	0.42		53.6	0.9	53.6	0.9	15.22					
Gl 257.1	06 57 49	+48 27.4	0.700	127.3	-22.8	K3 V	8.00	0.99	0.87		33.2	7.9	54.0	08. r	6.66	23	-56	25	51866	BD+48 1469
Gl 258	06 59 07	+68 21.7	0.341	82.0		M3.5	11.96	1.53		1.08	56.5	13.6	56.5	13.6	10.7					
Gl 259	06 59 11	-25 52.6	0.207	79.7	12.6	K0 Ve	6.71	0.89	0.62	0.30	67.4	13.6	74.0	11. r	6.06	-5	-14	11	52698	CD-25 3913
Gl 260	06 59 25	-61 16.1	0.300	323.8	21.3	K0 IV-V	6.82	0.80	0.43	+0.39C	61.5	13.6	63.0	11. r	5.82	-21	-17	-15	53143	CP-61 754
Gl 261	06 59 27	-06 22.1	0.898	185.0		DA	15.27	0.88			79.0	24.6	79.0	24.6	14.8					
NN	06 59 54	+52 47.5	1.166	141.7		M4.5	13.30	1.84		1.43	109.1	2.8	109.1	2.8	13.49					
NN	06 59 56	-67 50.9	0.240	351.0	38.6	K3 III	5.17	1.40	1.65	0.52	41.1	13.1	41.1	13.1	3.2	-22	-40	-14	53501	CP-67 686
NN	07 00 05	+34 46.2	0.183	331.0		m	13.17			1.26			75.0	13. r	12.55					
GJ 1094	07 00 17	-06 43.3	0.358	213.9		K5 V	8.38	1.08	0.96	0.40	63.3	3.3	63.3	3.3	7.39				52919	BD-06 1902
Gl 262	07 00 20	+29 25.4	0.841	169.1	25.4	G4 V	5.94	0.60	0.04	0.21	58.6	11.9	55.0	09. r	4.64	-19	-74	-8	52711	BD+29 1441
NN	07 01 46	+25 04.6	0.328	215.0		M1	11.62	1.48	1.16				40.0	09. r	9.63					
Gl 263	07 01 56	-10 25.3	0.806	188.5	-87	M3.5	11.29	1.52	1.10	0.97	61.5	5.4	61.5	5.4	10.23	98	25	-34		
Gl 264	07 02 18	-43 29.5	0.404	346.6	88	K5 V	8.68	1.18	1.13	0.49	55.0	17.0	60.0	09. r	7.57	-54	-74	-20	53680	CP-43 1184
Gl 264.1A	07 02 25	-43 32.3	0.398	343.8	86.4	G3 V	5.55	0.64	0.05	0.22	50.2	8.4	66.0	07. r	4.65	-50	-73	-21	53705	CD-43 2906
Gl 264.1B	07 02 25	-43 32.3	0.398	343.8	90.4	K0 V	6.79	0.80	0.37	0.28	50.2	8.4	66.0	07. r	5.89	-51	-77	-22	53706	CD-43 2907
Gl 265 A	07 02 35	+27 32.9	0.122	205.2	-25.3	M0 Ve	10.22	1.32	1.20	0.45	59.7	13.6	59.7	13.6	9.1	23	-3	-14		BD+27 1311
NN	07 02 46	+67 16.8	0.279	254.0		dM0	11.18	1.51		0.88			56.0	10. r	9.92					
NN	07 03 51	+48 46.2	0.309	185.0		m	13.40			1.25			65.0	12. r	12.46					
NN	07 04 06	+69 56.1	0.344	213.0		m	12.54			1.02			44.0	09. r	10.76					
Gl 266	07 04 32	+03 31.8	0.320	183.0		dM0	9.84	1.29		0.53	42.3	10.3	42.0	05. r	7.96					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Wo 9224	07 04 48	-47 30.6	0.200	139.0		k	10.54	1.17	1.17	+0.60C	39.4	15.3	24.0	03. r	7.44					CD-47 2804
NN	07 04 54	+29 55.1	0.343	206.6	21	K3	8.32	0.93	0.58				40.0	07. r	6.33	-25	-30	-24	53927	BD+30 1423
NN	07 05 28	+30 47.6				M0	11.36	1.49	1.17	0.79			41.0	07. r	9.42					BD+ 7 1684
Gl 268	07 06 39	+38 37.5	1.052	207.9	+37.9 SB	M4.5 Ve	11.49	1.71	1.20	1.37	164.6	3.1	164.6	3.1	12.57	-44	-20	-8		
NN A	07 06 51	+37 45.3	0.367	220.0		sdM6	14.67	1.65	1.27	1.25	41.5	2.9	41.5	2.9	12.76					
NN B	07 06 52	+37 45.3	0.367	220.0		DQ8	15.68	0.30	-0.70		41.5	2.9	41.5	2.9	13.77					
NN	07 08 16	+52 21.7	0.240	205.0		M0	11.29	1.48	1.21	0.83			46.0	08. r	9.6					
NN	07 08 34	-14 21.5	0.539	302.5		K5	9.94	1.35	1.25	0.57	36.9	9.0	44.0	08. r	8.16					BD-14 1750
NN	07 09 27	-48 51.1	0.192	354.1	63.6	K2 III	5.12	1.26	1.27	0.47	40.6	23.9	40.6	23.9	3.2	-32	-58	-13	55526	BD-48 2765
Gl 268.1	07 11 08	-46 40.5	0.172	306.2	1.1	F0 IV	4.48	0.32	-0.01	+0.20C	46.1	10.2	46.1	10.2	2.8	-15	5	-9	55892	CD-46 2977
GJ 1095	07 12 08	+47 19.9	0.188	170.4	85.2	G0 V	5.64	0.58	0.03		39.3	10.6	58.0	09. r	4.46	-80	-2	33	55575	BD+47 1419
Gl 268.2	07 12 42	-63 15.9	0.623	333.3	-20	K5 V	9.10	1.25	1.22	0.53	52.3	7.2	52.3	7.2	7.69	-57	18	0	56533	CP-63 703
GJ 1096	07 13 03	+33 14.8	0.426	198.0		m+	14.48	1.75	+0.86?	1.37	67.1	4.7	67.1	4.7	13.61					
Gl 268.3	07 13 14	+27 14.0	0.240	187.0		dM0	10.85	1.54	1.28	1.12	69.4	18.8	126.0	25. r	11.35					BD+27 1348
NN	07 13 20	+58 29.8	0.096	211.0		DA4	12.0 :						82.0	11. w	11.6 :					
NN	07 13 33	-12 57.8	0.531	289.3	60	G2 V	7.75	0.61	-0.02	0.23	43.2	6.0	43.2	6.0	5.93	-72	-15	-40	56274	BD-12 1871
Wo 9228	07 13 59	-15 29.7	0.059	251.8	10	A3 V	5.44	0.08	0.06		21.2	16.2	21.2	16.2	2.1	-8	-6	-13	56405	BD-15 1734
Gl 268.4	07 14 19	-40 56.6	0.332	309.6	16.3	G3 V	9.09	0.66	0.10	+0.35C	45.5	11.9	45.5	11.9	7.4	-34	-3	-18	56640	CP-40 1403
NN	07 14 35	+19 39.9	0.426	233.3		m	12.80	1.56	1.22	1.08	46.6	2.5	46.6	2.5	11.14					
NN	07 14 44	+39 22.0	0.280	260.0		M0.5	10.33	1.51	1.20	0.80			66.0	13. r	9.43					
Gl 268.5	07 15 11	-13 54.6	0.267	216.0		K5	12.11	1.43		+0.84C	44.0	18.8	19.0	04. r	8.5					
Wo 9231 A	07 15 13	+16 37.9	0.062	229.7	-9.2	A3 V	3.58	0.11	0.10	-0.05	46.0	6.4	46.0	6.4	1.89	8	1	-8	56537	BD+16 1443
Wo 9231 B	07 15 13	+16 37.9	0.062	229.7			10. *				46.0	6.4	46.0	6.4	8. *					
Gl 269 A	07 16 03	-46 53.7	0.578	358.1	59	K1 V	7.15	+0.99 J	+0.78 J	+0.36 J	81.6	7.8	81.6	7.8	6.71	-43	-53	-3	57095	CD-46 3046
Gl 269 B	07 16 03	-46 53.7	0.578	358.1		K4 V	7.9 *				81.6	7.8	81.6	7.8	7.5 *					
Gl 270	07 16 15	+32 55.7	0.574	125.9	-68.9	dM1.5	10.07	1.44	+0.80?	0.70	60.3	6.7	60.3	6.7	8.97	76	-31	0		BD+33 1505
Gl 271 A	07 17 08	+22 04.6	0.029	239.1	-15.3 SB	F1 IV-V	3.53	0.34	0.04	0.10	62.4	5.7	62.4	5.7	2.51	14	4	-6	56986	BD+22 1645
Gl 271 B	07 17 08	+22 04.6	0.029	239.1	2.2	K3 V	8.2 *				62.4	5.7	62.4	5.7	7.2 *	-3	-1	-1		
NN	07 19 33	+30 46.5	0.715	214.0		k-m	13.34	1.50	1.04		42.0	3.3	42.0	3.3	11.46					
Gl 272	07 19 37	+46 11.3	0.280	215.0	-30.3	dM2	10.53	1.46		0.84	58.6	6.5	58.6	6.5	9.37	18	-17	-28		
GJ 2057	07 20 59	+13 04.1	0.440	169.5	38.8	K2	8.20	0.94	0.80	0.34			43.0	06. r	6.37	-17	-60	-4	57901	BD+13 1655
NN	07 21 30	-82 54.8	0.676	352.7		m	11.75			0.89			44.0	08. r	9.97					
NN	07 24 31	+22 08.9	0.292	237.0		m	11.23	1.49	1.20	0.92	51.5	2.5	51.5	2.5	9.79					
Gl 273	07 24 43	+05 22.7	3.761	171.2	18.2	M3.5	9.85	1.56	1.16	1.21	264.4	2.0	264.4	2.0	11.96	16	-66	-17		BD+05 1668
Gl 273.1	07 25 49	+32 05.7	0.232	44.4	-4.1	dK8	7.74	0.94	0.65	0.37	48.3	5.9	48.3	5.9	6.16	10	11	18	58830	BD+32 1561
Gl 274 A	07 25 54	+31 53.1	0.232	41.6	+3.1 SB?	F0 V	4.18	0.32	-0.03		59.1	5.0	59.1	5.0	3.04	2	9	16	58946	BD+32 1562
Gl 274 B	07 25 54	+31 53.1	0.232	41.6			12.5 *				59.1	5.0	59.1	5.0	11.4 *					
NN	07 26 00	-18 42.0	0.588	3.9		k-m	13.65			1.35			86.0	13. r	13.32					
Wo 9234	07 26 09	+49 46.7	0.139	133.0	-26.7	F6 V	5.36	0.45	-0.06		44.7	10.2	44.0	05. r	3.58	25	-18	-4	58855	BD+49 1630
Gl 275	07 26 11	-51 18.0	0.283	267.6	3.4	G5 IV-V	6.73	0.70	0.26		56.5	15.3	56.5	15.3	5.5	-9	4	-22	59468	CD-51 2507
GJ 1097	07 26 14	-03 11.2	0.940	150.9		M3	11.43	+1.50:	1.17	1.10	90.8	2.7	90.8	2.7	11.22					
Gl 275.1	07 26 52	+68 43.7	0.220	238.0	4	dM0	10.89	1.43		0.83	53.0	11.9	55.0	09. r	9.59	-15	-2	-12		

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	07 27 00	-07 26.9	0.142	24.8	9.1	F8 V	5.86	0.48	-0.02				40.0	05. r	3.87	-13	2	14	59380	BD- 7 1996
Gl 275.2A	07 27 02	+48 19.4	1.295	189.8		sdM5	13.56	1.71	1.22		86.5	2.3	86.5	2.3	13.25					
Gl 275.2B	07 27 06	+48 17.8	1.295	189.8		DC	14.63	0.99	0.36		86.5	2.3	86.5	2.3	14.32					
NN	07 27 48	+58 02.0	0.929	178.6	16	M6 :	17.4 *						55.0	04. s	16.1 *	-45	-68	0		
Gl 276	07 28 18	+14 43.5	0.297	167.6	65.6	dK8	8.98	1.10	1.06	0.45	45.6	5.4	45.6	5.4	7.27	-47	-54	11	59582	BD+14 1684
NN	07 28 32	+39 20.2	0.293	146.0		m	13.08			1.10			43.0	09. r	11.25					
Gl 277 A	07 28 40	+36 19.8	0.440	231.5	+0.1 SB	dM3.5e	10.58	1.47	1.15	1.07	83.0	2.4	83.0	2.4	10.18	-9	-9	-22		BD+36 1638
Gl 277 B	07 28 39	+36 20.4	0.441	231.0	0.1	dM4.5e	11.78	1.52	1.18	1.22	83.0	2.4	83.0	2.4	11.38	-9	-10	-22		
GJ 1098	07 28 49	+64 16.1	0.258	164.0		DC9	16.38	0.91					55.0	06. w	15.08					
NN	07 28 56	-37 14.0	0.096	297.4	8.6	G4 V	6.64	0.63					44.0	05. r	4.86	-11	-4	-7	59967	CD-37 3637
NN A	07 29 11	+17 25.7	0.270	238.0		dM0	11.02	1.38	1.28	0.67	40.4	4.6	40.4	4.6	9.05					
NN B	07 29 10	+17 25.7	0.270	238.0		m	12.95				40.4	4.6	40.4	4.6	10.98					
NN A	07 29 42	-08 46.3	0.185	209.9	55	F9 V	5.90	0.54	-0.08	0.21			46.0	06. r	4.21	-32	-47	-12	59984	BD-08 1964
NN B	07 29 42	-08 46.3	0.185	209.9			8.6 *						46.0	06. r	6.9 *					
Gl 277.1	07 29 57	+63 03.1	0.424	261.8		dM0	10.49	1.55		0.80	70.4	4.6	70.4	4.6	9.73					
NN	07 30 50	+22 30.6	1.104	122.8		m	16.46	1.60			40.7	1.0	40.7	1.0	14.51					
NN	07 31 12	+54 58.0	0.104	291.0		dM0	11.29	1.55		0.98			71.0	14. r	10.55					
Gl 278 A	07 31 25	+32 00.0	0.198	238.9	+6.0 SB	A1 V	1.94	+0.04 J	+0.02 J		68.3	2.8	68.3	2.8	1.11	-10	-4	-10	60179	BD+32 1581
Gl 278 B	07 31 25	+32 00.0	0.198	238.9	-1.2 SB	A m	2.85				68.3	2.8	68.3	2.8	2.02	-4	-3	-13	60178	
Gl 278 C	07 31 26	+31 58.8	0.232	241.4	-1.9 SB	M0.5Ve	9.07J	+1.49 J	+1.04 J	+0.78 J	68.3	2.8	68.3	2.8	8.24J	-4	-3	-15		BD+32 1582
NN	07 31 39	+22 26.9	0.200	119.0		k	11.53	1.50	1.32				55.0	27. r	10.2					
GJ 1099	07 31 43	+01 06.2	0.628	175.6		m	11.93	1.47	1.11	1.03	68.2	2.6	68.2	2.6	11.1					
Gl 279	07 31 55	-22 11.2	0.062	313.2	61	F6 IV	4.45	0.51	0.05	+0.30C	48.0	8.2	48.0	8.2	2.86	-38	-48	-3	60532	BD-21 2007
Wo 9237	07 33 32	-03 02.5	0.304	289.4		G0	7.16	0.57	0.03		39.1	15.3	28.0	05. r	4.4				60779	BD-02 2197
NN	07 33 43	+07 11.7	0.354	145.0		m	13.22			1.48			162.0	26. r	14.27					
Wo 9238	07 34 49	+28 23.8	0.503	129.1		M3	13.85	1.47	0.92	0.99	39.7	3.4	39.7	3.4	11.84					
NN	07 34 52	-51 48.5	0.612	41.0		m	12.45			1.12			62.0	12. r	11.41					
NN	07 35 18	+85 06.0	0.373	204.0		m	12.80			1.09			48.0	10. r	11.21					
NN A	07 36 22	+33 34.9	0.243	222.0		m	11.83	1.46	1.19	0.93	26.4	2.5	26.4	2.5	8.94					
NN B	07 36 23	+33 35.0	0.243	222.0		m+	18. *				26.4	2.5	26.4	2.5	15. *					
NN	07 36 29	-21 06.1	0.681	138.1		m	11.7 *			1.09			79.0	16. r	11.2 *					
Gl 280 A	07 36 41	+05 21.3	1.247	214.5	-4.0 SB	F5 IV-V	0.38	0.42	0.02	0.14	285.8	5.3	285.8	5.3	2.66	5	-8	-19	61421	BD+05 1739
Gl 280 B	07 36 41	+05 21.3	1.247	214.5		DA	10.7 *				285.8	5.3	285.8	5.3	13.0 *					
Gl 281	07 36 48	+02 18.2	0.270	205.0	10	dM0	9.61	1.44	1.28	0.71	70.0	3.4	70.0	3.4	8.84	-4	-17	-12		BD+02 1729
Gl 282 A	07 37 29	-03 28.7	0.297	165.7	-21.1	K2 Ve	7.20	0.96	0.73	0.32	74.3	6.5	74.3	6.5	6.55	27	0	-8	61606	BD-03 2001
Gl 282 B	07 37 33	-03 29.0	0.279	165.1	-13.4	K5	8.94	1.33	1.24	0.57	74.3	6.5	74.3	6.5	8.29	21	-5	-6		BD-03 2002
NN	07 38 01	+49 20.4	0.076	261.2	7.6	dK8	9.73	1.19	1.06	0.47	46.5	18.3	36.0	04. r	7.51	-11	2	-5		BD+49 1658
Gl 283 A	07 38 02	-17 17.4	1.252	116.6	11	DZQ6	13.00	0.24	-0.62	0.04	112.0	5.0	112.0	5.0	13.25	56	3	28		
Gl 283 B	07 38 02	-17 17.4	1.252	116.6		m	16.42	1.83			112.0	5.0	112.0	5.0	16.67					
NN	07 39 15	+05 09.6	0.285	253.0		m	12.71			1.08			48.0	10. r	11.12					
NN	07 40 18	+18 18.3	0.500	188.5		k-m	11.34	1.40	1.05	0.87			49.0	09. r	9.79					BD+18 1719
Gl 284	07 41 24	-45 02.7	0.561	188.3	+28.0 VAR	G6 IV	5.06	0.77	0.32	0.27	54.1	10.2	54.1	10.2	3.73	34	-30	-34	62644	CD-44 3675

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 285	07 42 04	+03 40.8	0.604	221.4	26.8	dM4.5e	11.20v	1.60	1.00	+1.4 v	161.1	4.1	161.1	4.1	12.24v	-20	-23	-10		
Gl 285.1	07 42 11	+70 19.9	0.169	212.3	-22.6 SB	dG5	7.09	0.66	0.27		29.8	11.1	40.0	07. r	5.1	2	-23	-20	61994	BD+70 474
Gl 286	07 42 16	+28 08.9	0.628	265.3	3.6	K0 IIIb	1.14	1.00	0.85	0.35	100.3	5.3	100.3	5.3	1.15	-16	4	-25	62509	BD+28 1463
Gl 287	07 42 25	+02 15.7	0.225	167.3	-21	dM0	10.20	1.37	1.31	0.60	36.2	11.5	43.0	06. r	8.37	30	-8	-11		BD+02 1766
Gl 288 A	07 43 43	-34 04.4	1.700	350.2	102.6	G0 V	5.36	0.59	-0.06	0.23	62.5	8.6	62.5	8.6	4.34	-151	-56	36	63077	CD-33 4113
Gl 288 B	07 43 51	-33 49.2	1.630	348.0		m	16.59	1.20		+0.57C	62.5	8.6	62.5	8.6	15.57					
GJ 1100	07 44 46	-13 48.6	0.492	165.7		M1	11.50	1.41		0.75	46.7	6.1	46.7	6.1	9.85					
GJ 1101	07 44 56	+83 31.3	0.646	205.2		m	13.09	1.68		1.28	80.1	3.1	80.1	3.1	12.61					
Gl 289	07 45 15	+20 30.4	1.728	124.2	48.4	M2	11.46	1.52	1.10	0.89	66.7	2.7	66.7	2.7	10.58	16	-103	81		
GJ 1102 A	07 47 33	+07 20.7	1.778	173.2		DC9	16.69	1.10			58.6	2.0	58.6	2.0	15.53					
GJ 1102 B	07 47 32	+07 20.9	1.778	173.2		DC9	16.98	1.30			58.6	2.0	58.6	2.0	15.82					
Gl 290	07 48 07	+80 23.7	0.489	279.2	-7.2	G8 V	6.56	0.73	0.28		60.5	8.8	60.5	8.8	5.47	-9	9	-37	62613	BD+80 238
Wo 9242	07 48 31	-59 15.0	0.376	126.2	3.1	G5 V	7.50	0.68	0.19		42.3	18.8	33.0	05. r	5.09	48	-8	23	64184	CP-59 907
NN	07 49 11	+05 41.0	0.572	134.9		m	14.75	1.82		1.47	62.8	3.6	62.8	3.6	13.74					
GJ 1103 A	07 49 20	+00 08.1	0.766	160.6	52	m	13.50	+1.68 J	+1.05 J	+1.43 J	113.8	3.3	113.8	3.3	13.78	-19	-57	7		
GJ 1103 B	07 49 21	+00 08.2	0.766	160.6		m	15.0 *				113.8	3.3	113.8	3.3	15.3 *					
Gl 291 A	07 49 27	-13 45.8	0.350	191.0	-21.5 SB	F9 V	5.72c	+0.57c	+0.05c	+0.24tJ	62.7	4.1	62.7	4.1	4.71c	28	3	-20	64096	BD-13 2267
Gl 291 B	07 49 27	-13 45.8	0.350	191.0		G4 V	6.17c	+0.65c	+0.14c		62.7	4.1	62.7	4.1	5.16c					
Gl 291.1	07 49 42	-50 10.7	0.210	320.0		K2	10.06	1.22	1.18		46.6	10.2	46.6	10.2	8.4					CP-49 1388
NN	07 49 45	+26 03.5	0.159	167.7		K4	8.60	1.04	0.90	0.40			46.0	05. r	6.91					BD+26 1665
NN	07 49 53	+06 26.4	0.227	168.0		m	13.56			1.14			40.0	08. r	11.57					
GJ 1104	07 50 22	+30 45.7	1.972	158.4	-235.0 VAR	G2 VI	8.30	0.61	-0.13	0.26	44.1	3.1	44.1	3.1	6.52	251	-170	-90	64090	BD+31 1684
Gl 292 A	07 50 24	-34 34.7	0.310	319.8	26.7	F5 V	5.05	+0.44 J	-0.06 J	+0.16 J	69.9	6.5	69.9	6.5	4.27	-28	-18	-5	64379	CD-34 4036
Gl 292 B	07 50 24	-34 34.7	0.310	319.8		K3	8.6 *				69.9	6.5	69.9	6.5	7.8 *					
Gl 292.1	07 51 59	+19 22.5	0.461	167.8	-18.7	dK6	7.78	0.95	0.80	0.36	35.5	4.0	35.5	4.0	5.53	35	-51	-17	64468	BD+19 1869
Gl 292.2	07 52 03	-01 16.8	0.283	259.0	+102.0 SB	G8 V	7.43	0.73	0.16	0.30	51.9	10.2	43.0	07. r	5.6	-86	-63	-5	64606	BD-01 1883
NN A	07 52 52	-29 12.6	0.548	148.3		M4	13.38			+1.33 J			80.0	13. r	12.9					
Gl 293	07 52 52	-67 38.4	2.041	135.6		DQ9	14.08	0.66	-0.17	0.15	144.7	13.9	144.7	13.9	14.88					
GJ 1105	07 54 47	+41 26.9	0.685	163.0	-11	k	12.00	1.63	1.15	1.21	123.5	3.0	123.5	3.0	12.46	10	-26	-3		
Gl 293.1A	07 55 25	-00 40.7	0.181	270.0	-4	K5 V	8.06	+1.04 J	+0.99 J	+0.42 J	52.9	8.6	52.9	8.6	6.68	-5	6	-15	65277	BD-00 1866
Gl 293.1B	07 55 25	-00 40.7	0.181	270.0			13.3 *				52.9	8.6	52.9	8.6	11.9 *				65277	
NN	07 55 29	+07 25.2	0.336	266.0		m	13.77			1.31			70.0	11. r	13					
NN A	07 55 41	+15 38.5	0.115	218.0		m	14.24			1.25			48.0	05. r	12.65					
NN B	07 55 40	+15 38.3	0.115	218.0		m	15.09			1.39			48.0	05. r	13.5					
GJ 1106	07 55 54	-33 49.2	0.320	14.9		K5 V	8.84	1.16	1.02	0.46			53.0	08. r	7.46					CD-33 4354
Gl 293.2	07 55 57	-25 29.2	0.435	123.8	-5.1	K3 V	8.42	1.05	+0.84:	0.38	51.2	8.5	51.2	8.5	6.97	35	-12	17	65486	CD-25 5342
NN	07 56 17	+15 31.7	0.188	255.0		m	12.33			0.98			43.0	08. r	10.5					
NN	07 56 37	+20 59.3	0.588	161.7	-28.2	K0 V	7.70	0.82	0.48	0.28	28.0	9.2	42.0	06. r	5.82	46	-53	-15	65430	BD+21 1731
Wo 9247	07 56 45	-34 48.7	0.410	295.6	23.7	G6 V	7.95	0.74	0.25		41.8	7.8	41.8	7.8	6.06	-44	-9	-26	65721	CD-34 4160
NN	07 56 48	-36 52.9	0.196	162.5		K0/1 V	7.00	0.98	0.69	0.38	19.1	15.3	84.0	11. r	6.62				65723	CD-36 4067
Gl 294 A	07 56 52	-60 10.1	0.540	76.7	+14.1 SB	G2 V	5.60	0.57	0.02	0.20	63.0	6.0	63.0	6.0	4.6	12	-24	34	65907	CD-59 1773
Gl 294 B	07 57 00	-60 09.8	0.528	77.8		k	9.88	+1.34 J	+1.09 J	+0.76 J	63.0	6.0	63.0	6.0	8.88					CD-59 1774

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 294 C	07 57 00	-60 09.8	0.528	77.8			13.5 *				63.0	6.0	63.0	6.0	12.5 *					
Gl 295	07 57 27	+29 22.0	1.181	187.8	14.7	G8 V	7.00	0.71	0.18	0.28	51.5	4.6	51.5	4.6	5.56	-13	-103	-35	65583	BD+29 1664
Gl 295.1	07 57 28	+13 56.2	0.140	216.0	30	K5 e	10.36	1.26	1.30	0.50	55.9	18.8	31.0	05. r	7.82	-26	-26	-6		BD+14 1802
Gl 296	07 58 15	-39 53.5	0.849	142.7	5.5	K7 V	9.66	1.34	1.21	0.59	59.1	15.6	53.0	10. r	8.28	72	-25	7	66020	CP-39 1929
NN A	07 59 47	+03 29.1	0.552	229.5		k-m	13.7 *			1.17			41.0	08. r	11.8 *					
NN B	07 59 45	+03 28.5	0.552	229.5		m+	17. *						41.0	08. r	15. *					
NN	08 00 53	+44 06.2	0.132	95.0	-3	K5	9.83	1.27	1.19	0.54	19.2	23.9	43.0	07. r	8	10	-4	11		BD+44 1710
NN	08 02 08	-65 52.7	0.189	227.3		K1 V	7.14c	+0.94c					69.0	10. r	6.33c				67199	CP-65 0858
GJ 1107	08 02 29	+34 13.4	0.280	146.0	-4.9	dM0 p	10.14	1.35	1.25	0.56	54.5	8.0	54.5	8.0	8.82	11	-22	5		BD+34 1740
NN	08 02 37	+56 02.4	0.182	128.0		M0	11.48	1.49	1.28				53.0	26. r	10.1					
NN	08 02 57	+26 25.5				M0	10.21	1.46	1.20	0.72			58.0	09. r	9.03					BD+26 1715
NN	08 03 33	+36 54.6	0.395	199.0		m	12.95			1.15			54.0	11. r	11.61					
NN	08 04 06	+58 39.5	0.181	248.0		m	12.69			1.09			50.0	10. r	11.18					
Wo 9251 A	08 04 28	+07 31.8	0.136	181.3	20	dK8	10.45	+1.24 J	+1.18 J	0.46	48.4	7.4	27.0	02. r	7.61	-6	-30	-4		BD+07 1919
Wo 9251 B	08 04 28	+07 31.8	0.127	184.1		K8	10.86			0.56	48.4	7.4	27.0	02. r	8.02					
Gl 296.1	08 04 58	-29 15.2	0.494	136.3	-17.6	G4 IV-V	6.80	0.60	0.03	0.22	51.5	9.5	51.5	9.5	5.36	48	-1	8	67458	CD-29 5555
Gl 296.2	08 05 11	+69 52.2	0.205	54.6	-14.1	SB F8 V	6.57	0.58	0.01		46.0	10.2	37.0	05. r	4.41	28	2	9	66751	BD+70 497
NN A	08 05 18	+21 15.3	0.466	221.3		K5	9.80	+1.38 J	+1.24 J				59.0	27. r	8.7					BD+21 1764
NN B	08 05 18	+21 15.2	0.487	227.2		m	11.0 *						59.0	27. r	9.9 *					
GJ 1108 A	08 05 46	+32 58.2	0.219	194.3	4	dM0.5e	10.05	1.35	1.13	0.67	35.4	13.6	58.0	10. r	8.87	-5	-17	-6		BD+33 1646
GJ 1108 B	08 05 45	+32 57.9				dM3 e	12.12	1.53		1.17	35.4	13.6	58.0	10. r	10.94					
NN	08 06 24	-66 09.0	0.473	128.0		DQ5	13.92	0.05	-0.90				43.0	05. w	12.09					
NN	08 06 36	+22 03.2	0.338	258.0		m	11.81	1.53	1.22	0.94			50.0	09. r	10.3					
Gl 297.1	08 08 11	-61 09.0	0.338	207.4	25	F5 V	4.76	0.43	-0.03	+0.26C	53.0	7.2	53.0	7.2	3.38	18	-16	-31	68456	CP-60 1074
NN	08 08 16	+04 07.8	0.350	164.0		m	13.51			1.22			55.0	10. r	12.21					
Gl 297.2A	08 08 21	-13 39.1	0.263	282.1	+33.0	SB? F7 V	5.54	0.49	0.00	0.18	48.8	5.0	48.8	5.0	3.98	-35	-19	-12	68146	BD-13 2420
Gl 297.2B	08 08 15	-13 39.9	0.249	282.0	+34.4	SB? M3	11.82	1.51		0.99	48.8	5.0	48.8	5.0	10.26	-35	-20	-11		
Wo 9256	08 08 31	+32 36.9	0.807	215.7	30.6	G4 V	6.81	0.69	0.13		43.7	7.3	43.7	7.3	5.01	-51	-64	-43	68017	BD+32 1695
Gl 298	08 08 42	-52 49.7	0.820	319.5	85	m	11.77	1.50	1.08	1.06	46.0	18.7	68.0	13. r	10.93	-60	-80	-24		
Gl 299	08 09 11	+08 59.7	5.211	167.1	-35	dM5	12.83	1.77	1.40	1.31	148.0	2.6	148.0	2.6	13.68	106	-124	-48		
NN	08 10 10	-83 05.1	0.610	307.5		m	12.55			1.03			45.0	09. r	10.82					
Wo 9258	08 10 25	-07 03.1	0.162	119.5	-20.5	K0	7.93	0.90	0.58		41.3	22.2	45.0	06. r	6.2	26	7	3	68586	BD-06 2514
Gl 300	08 10 29	-21 23.5	0.707	177.5		M4	12.10:	+1.60:		1.31	170.0	10.2	170.0	10.2	13.25:					
Gl 301 A	08 10 50	-13 45.5	0.556	206.7	+20.0	SB? M0 V	9.74	+1.41 J	+1.23 J	+0.66 J	54.8	10.3	54.8	10.3	8.43	5	-37	-37		BD-13 2439
Gl 301 B	08 10 50	-13 45.5	0.556	206.7			10.7 *				54.8	10.3	54.8	10.3	9.4 *					
Wo 9259	08 11 10	-40 23.0	0.265	126.0	38.7	G8 (IV)	9.39	0.82	0.43	+0.41C	41.7	13.6	41.7	13.6	7.5	19	-44	8	68916	CD-40 3981
NN	08 11 48	+10 20.5	0.018	254.2		G5	7.32						80.0	09. o	6.84				68835	BD+10 1756
NN	08 11 51	+13 10.5	0.433	282.1		K4	8.85	1.20	1.13				53.0	10. r	7.47				68834	BD+13 1870
GJ 2066	08 13 34	+01 27.4	0.370	277.0		m	10.10	1.53	1.20	0.96	114.0	3.9	114.0	3.9	10.38					
NN A	08 14 19	-35 43.7	0.028	13.6		G8/K0 V	7.2 c	+0.94c					71.0	12. r	6.5 c				69565	CD-35 4406
NN B	08 14 19	-35 43.7	0.028	13.6			11.0 :						71.0	12. r	10.3 :					
NN	08 14 45	+31 17.0	0.240	341.0		k	11.22	1.49	1.22				60.0	29. r	10.1					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B−V	U−B	R−I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	08 14 51	-76 00.0	0.657	329.8		k-m	11.85			1.04			63.0	13. r	10.85					
Gl 301.1	08 15 05	+30 46.1	0.872	199.0	11.6	K4 V	8.85	1.14	1.11	0.42	46.3	4.6	46.3	4.6	7.18	-20	-79	-37		BD+31 1781
Gl 302	08 16 01	-12 27.7	1.033	164.0	30.5	G7.5 V	5.97	0.76	0.32	0.26	79.3	6.4	79.3	6.4	5.47	29	-62	-10	69830	BD-12 2449
NN	08 16 26	-15 02.7	0.073	131.0	55	K3 V	9.84:	1.13	+1.09:	0.48	48.8	4.0	48.8	4.0	8.28:	-24	-49	13		BD-14 2469
GJ 1109	08 16 41	-36 30.2	0.147	309.8	5.1	A7 III	4.45	0.22	0.11		55.8	10.3	55.8	10.3	3.18	-13	-2	-3	70060	CD-36 4449
Gl 303	08 17 02	+27 22.9	0.381	182.3	+33.0 SB?	F6 V	5.14	0.47	-0.06		63.8	8.5	63.8	8.5	4.16	-25	-35	9	69897	BD+27 1589
NN	08 18 08	+14 14.0	0.274	197.0	15	K5	9.82	1.29	1.21	0.55	35.8	20.5	44.0	08. r	8.04	-8	-30	-11		BD+14 1876
Gl 304	08 19 41	-39 32.9	0.308	317.5	48.1	G6 V	7.17	0.71	0.29	+0.35C	59.4	11.9	59.4	11.9	6.04	-34	-42	-5	70642	CD-39 4247
NN	08 19 50	+31 44.8	0.007	225.6		G5	8.11						54.0	06. o	6.77				70401	BD+32 1724
Gl 305	08 19 51	-76 45.7	0.156	46.2	-13.2	F6 IV	4.07	0.40	-0.02	+0.24C	57.4	6.2	57.4	6.2	2.86	-6	6	16	71243	CP-76 507
NN	08 20 10	+84 34.1	0.358	54.0		m	13.42	1.62	1.26	1.14			43.0	09. r	11.59					
Gl 305.1	08 20 34	+22 00.9	0.378	132.0	-27.3	dM0 e	9.54	1.18	1.12	0.48	30.7	19.0	41.0	07. r	7.6	46	-23	4		BD+22 1921
NN	08 21 00	+69 13.0	1.377	205.4		dM5.2	15.67	2.09			79.9	6.5	79.9	6.5	15.18					
NN	08 22 03	+32 46.9	0.686	178.9	-78.3	K3	10.05	1.06	0.86	0.42	39.5	12.6	25.0	04. r	7.04	72	-116	-66		BD+33 1694
Gl 306	08 22 05	-03 35.3	0.218	261.4	+73.0 SB	F3 V	5.61	0.46	-0.06	+0.28C	55.0	5.4	55.0	5.4	4.31	-56	-50	7	70958	BD-03 2333
Gl 306.1	08 23 46	-29 45.7	0.337	153.9	+15.9 VAR	G4 V	7.81	0.67	0.17	0.27	53.4	13.6	30.0	05. r	5.2	44	-33	-7	71334	CD-29 6145
Gl 307.1	08 24 08	+45 49.4	0.353	182.5	-31.9	G5 V	6.32	0.62	0.12		46.5	9.1	50.0	08. r	4.81	20	-35	-22	71148	BD+46 1398
NN	08 25 12	-65 58.2	0.162	191.3	27.4	K2 III	3.76	1.13	1.14		39.8	10.2	39.8	10.2	1.8	18	-20	-20	71878	CP-65 933
Gl 308 A	08 25 15	+35 11.2	1.102	251.5		M0 V	11.48	+1.55 J	+1.20 J	+0.77 J	51.2	15.3	34.0	07. r	9.14					
Gl 308 B	08 25 15	+35 11.2	1.102	251.5			11.56				51.2	15.3	34.0	07. r	9.22					
GJ 1110	08 25 20	+20 18.9	0.667	202.3	142	g-k	13.08	1.48	1.06	1.04	44.8	3.7	44.8	3.7	11.34	-113	-107	29		
Gl 308.1	08 25 39	+61 54.2	0.864	145.7		dM0	10.33	1.37	1.17	0.65	23.2	5.0	45.0	07. r	8.6					
NN	08 25 40	-44 49.7	0.577	342.7		M3	11.85			1.16			87.0	16. r	11.55					
GJ 1111	08 26 53	+26 57.2	1.290	242.2	-5	M6.5	14.81	2.06	2.11	1.94	275.8	3.0	275.8	3.0	17.01	-6	-6	-21		
GJ 1112	08 27 32	+32 52.4	0.548	195.6	-18	DA7	15.72	0.30	-0.54		45.4	3.8	45.4	3.8	14.01	45	-43	-58		
GJ 2069 A	08 28 46	+19 34.0	0.282	245.0		M5 e	11.89			1.26			114.0	13. r	12.17					
GJ 2069 B	08 28 46	+19 34.2	0.282	245.0			13.32			1.36			114.0	13. r	13.6					
NN A	08 28 55	-05 51.8	0.432	259.0		M1.5	11.21	1.41		0.84			49.0	08. r	9.66					
NN B	08 29 00	-05 52.0	0.432	259.0		M3	12.36	1.47		1.03			49.0	08. r	10.81					
NN	08 29 01	-10 19.5	0.661	241.4		m	15.0 *			1.45			65.0	10. r	14.1 *					
NN	08 29 58	-01 24.0	0.500	161.0		m	18.44				50.8	0.5	50.8	0.5	16.97					
Gl 308.3	08 30 27	-50 01.3	0.290	317.0		m	10.80	1.21	1.10	+0.63C	53.2	17.0	23.0	03. r	7.61					CP-49 1686
NN	08 30 34	+18 42.5	0.625	187.3		m	14.75			1.33			48.0	08. r	13.16					
Gl 309	08 30 54	-31 20.4	1.350	304.0	15.7	K0 V	6.39	0.78	0.32	0.28	82.3	11.4	82.3	11.4	5.97	-75	5	-25	72673	CD-31 6229
NN	08 31 12	+68 14.9	1.010	233.1		M3	11.67	1.57		1.08	76.2	3.0	76.2	3.0	11.08					
Wo 9269	08 31 36	-23 11.1	0.337	302.6	19.4	K1(IV)+G	7.21	0.74	0.38		39.0	13.6	39.0	13.6	5.2	-44	-4	-12	72769	BD-22 2317
GJ 2070	08 31 53	-00 58.0	0.472	155.9		M3.5	12.73	1.62					66.0	23. r	11.8					
Gl 310	08 31 55	+67 28.1	1.066	272.0	11.6	dM1	9.30	1.42	1.23	0.71	67.3	5.1	67.3	5.1	8.44	-51	16	-54		BD+67 552
NN	08 31 59	-00 33.2	0.210	271.6		G5	7.32						47.0	05. o	5.68				72760	BD- 0 2024
Gl 310.1A	08 33 12	+06 47.7	0.178	229.4	+26.6 SB	F8 V	5.99	0.52	0.04		43.7	7.0	43.7	7.0	4.19	-22	-24	-5	72945	BD+07 1997
Gl 310.1B	08 33 12	+06 47.9	0.194	224.3	29.2	G5 IV-V	7.25	0.71	0.27		43.7	7.0	43.7	7.0	5.45	-23	-27	-5	72946	
NN	08 34 20	+15 19.0	0.897	188.0		k	11.8 *			1.04			65.0	13. r	10.9 *					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 311	08 34 47	+65 11.7	0.089	344.5	-12.7	G1 V	5.64	0.62	0.07	+0.21t	72.2	8.2	72.2	8.2	4.93	10	0	-10	72905	BD+65 643
Wo 9273	08 35 24	-06 37.9	0.280	275.5		G0	6.75	0.66	0.19		41.3	11.9	45.0	06. r	5.02				73350	BD-06 2664
Gl 312	08 35 31	-39 58.3	0.304	274.5	-1.5	G4 IV-V	6.54	0.60	0.12	0.20	58.0	15.3	58.0	15.3	5.4	-16	4	-18	73524	CD-39 4574
NN	08 36 29	+67 50.3	0.723	245.2		m	14.68	1.68			41.5	5.5	41.5	5.5	12.77					
Gl 314 A	08 36 57	-22 29.4	0.494	331.0	+47.7	SB G3 V	5.28	+0.73 J	+0.35 J	+0.23 J	63.3	7.9	63.3	7.9	4.29	-52	-27	14	73752	BD-22 2345
Gl 314 B	08 36 57	-22 29.4	0.494	331.0		K0 V	6.8 *				63.3	7.9	63.3	7.9	5.8 *					
Gl 315	08 37 07	+11 42.4	0.519	192.1	-13.4	K1 V	7.64	0.82	0.46	0.31	50.7	6.9	50.7	6.9	6.17	20	-33	-32	73667	BD+12 1888
NN A	08 37 07	+09 06.8	0.285	320.0		m+	12.93	1.58	1.29				40.0	07. r	10.94					
NN B	08 37 07	+09 06.8	0.285	320.0		m+	12.96			1.05			40.0	07. r	10.97					
GJ 1113	08 37 15	+43 17.8	0.347	208.5	56.1	K2 V	9.32	1.08	0.96	0.40	62.9	9.2	62.9	9.2	8.31	-54	-20	23	73554	BD+43 1844
NN	08 37 21	+59 41.6	1.310	191.2		m	15.05	1.93	1.54	1.62	100.2	3.9	100.2	3.9	15.05					
Gl 316	08 37 32	-06 17.7	0.167	138.8	-6	dM0	9.90	1.39	1.22	0.62	34.8	6.5	52.0	08. r	8.48	16	-4	0		BD-05 2603
Gl 316.1	08 37 42	+18 35.0	0.908	240.0		m	17.68	2.02		+1.74C	64.5	15.8	64.5	15.8	16.7					
Gl 317	08 38 49	-23 17.3	0.930	329.2	-53	m	11.98	1.52		1.17	101.3	27.0	87.0	17. r	11.68	-25	69	-5		
Gl 318	08 39 36	-32 46.9	1.709	322.0	58	DA6	11.88	0.22	-0.59	0.04	112.3	7.2	112.3	7.2	12.13	-73	7	1		CD-32 5613
Gl 318.1	08 39 58	+44 40.6	0.468	241.9		M1.5:	14.11	1.63		1.03	47.2	10.2	47.2	10.2	12.48					
Gl 319 A	08 40 02	+09 44.7	0.673	162.4	+20.4	SB? M0 J	9.70	+1.41 J	+1.27 J	+0.73 J	66.8	2.3	66.8	2.3	8.82	11	-51	4		BD+10 1857
Gl 319 B	08 40 02	+09 44.7	0.673	162.4			13.1 *				66.8	2.3	66.8	2.3	12.2 *					
Gl 319 C	08 40 09	+09 44.5	0.673	162.4	22.4	M3.5	11.79	1.54	1.20	1.05	66.8	2.3	66.8	2.3	10.91	10	-52	5		
Gl 319.1A	08 40 22	-42 44.9	0.290	251.1	23.2	K1 V	8.12	0.90	0.64	0.36	48.8	13.6	42.0	06. r	6.24	-14	-21	-31	74385	CP-42 2834
Gl 319.1B	08 40 22	-42 45.6	0.306	254.0		M1 :	12.68	1.52	1.52	1.00	48.8	13.6	42.0	06. r	10.8					
Gl 320	08 41 26	-38 42.4	0.452	318.1	14.3	K1 V	6.56	0.93	0.66	0.30	95.9	8.2	95.9	8.2	6.47	-25	-10	-1	74576	CD-38 4789
Gl 321	08 41 53	+41 51.8	0.711	203.5	-24.6	K3 V	8.58	0.94	0.73	0.35	56.3	7.4	56.3	7.4	7.33	2	-53	-37	74377	BD+42 1922
NN	08 41 57	-10 12.9	0.605	148.8		m	14.0 *			1.23			45.0	08. r	12.3 *					
Gl 321.1	08 42 37	-42 28.0	0.024	294.3	-2.3	G5 III	4.06	0.87	0.52		48.8	15.3	48.8	15.3	2.5	-2	3	-1	74772	CD-42 4569
Gl 321.2	08 42 58	-42 26.9	0.294	178.9	5	G5 V	7.21	0.74	0.29	0.23	46.0	20.5	40.0	06. r	5.22	27	-9	-21	74842	CD-42 4577
Gl 321.3A	08 43 19	-54 31.5	0.082	164.6	2.2	A0 V	2.02	+0.04 J	+0.07 J	-0.07 J	49.8	7.3	49.8	7.3	0.51	7	-2	-3	74956	CP-54 1788
Gl 321.3B	08 43 19	-54 31.5	0.082	164.6			5.0 *				49.8	7.3	49.8	7.3	3.5 *					
Gl 321.3C	08 43 26	-54 30.9	0.080	164.0			11.0 *				49.8	7.3	49.8	7.3	9.5 *					
Gl 321.3D	08 43 26	-54 30.9	0.080	164.0			13.5 *				49.8	7.3	49.8	7.3	12.0 *					
NN	08 44 22	+61 20.5	0.585	136.9		m	15.17	1.82	1.51				60.0	23. r	14.1					
NN	08 47 13	+53 05.1	0.259	248.0		m	15.40	1.78	1.31				46.0	17. r	13.7					
Gl 322	08 47 34	+66 19.1	0.142	43.6	-20.9	dM0	9.28	1.34	1.22	0.57	57.4	4.8	57.4	4.8	8.07	23	-2	-8		BD+66 582
NN	08 47 52	+35 00.7	0.061	240.4		G0	7.60						43.0	05. o	5.77				75404	BD+35 1880
Gl 323 A	08 48 02	+08 03.1	0.060	270.0	-10	dM0 pJ	9.77	+1.36 J	+1.20 J	+0.62 J	58.8	12.5	54.0	08. r	8.43	3	6	-9		BD+08 2131
Gl 323 B	08 48 02	+08 03.1	0.060	270.0			9.9 *				58.8	12.5	54.0	08. r	8.6 *					
GJ 1114	08 48 57	+18 18.9	0.893	265.6		M2	11.54	1.48		0.89	61.0	3.4	61.0	3.4	10.47					
Gl 324 A	08 49 37	+28 31.4	0.528	243.9	27.2	G8 V	5.95	0.86	0.62	0.26	76.4	3.7	76.4	3.7	5.37	-37	-18	-9	75732	BD+28 1660
Gl 324 B	08 49 42	+28 30.5	0.538	243.7	25.2	M3.5	13.14	1.64	1.20	1.30	76.4	3.7	76.4	3.7	12.56	-36	-18	-10		
GJ 1115	08 50 40	+35 25.0	0.350	213.1	44.7	dM0	9.30	1.14	1.10	0.48	41.1	13.6	45.0	07. r	7.57	-46	-34	9		BD+35 1890
Gl 325 A	08 50 44	+70 59.4	1.386	255.2	44.3	K5 V	8.70	+1.39 J	+1.25 J	+0.63 J	88.4	3.3	88.4	3.3	8.43	-83	9	-24	75632	BD+71 482
Gl 325 B	08 50 44	+70 59.4	1.407	254.1	44.3	K6 V	8.9 *				88.4	3.3	88.4	3.3	8.6 *	-84	8	-24		

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	08 51 07	-03 17.9	0.576	250.2		m	18.80				116.8	1.5	116.8	1.5	19.14					
Gl 326 A	08 51 42	-12 55.6	0.622	148.2		M6 J	12.52	+1.61 J		+1.10 J	68.7	9.9	68.7	9.9	11.7					
Gl 326 B	08 51 42	-12 55.6	0.622	148.2			12.8 *				68.7	9.9	68.7	9.9	12.0 *					
Gl 327	08 51 50	-05 14.6	0.414	273.6	31.8	G3 V	6.00	0.67	0.21	0.21	88.6	6.5	88.6	6.5	5.74	-32	-21	-3	76151	BD-04 2490
Gl 328	08 52 32	+01 45.1	1.066	176.7	-3.1	dM1	9.99	1.40	1.23	0.68	64.3	5.9	64.3	5.9	9.03	41	-58	-33		BD+02 2098
Gl 329	08 52 47	-24 12.3	0.380	290.8	63.3	K2/3 III	8.66	1.00	+0.86:	+0.44C	65.3	13.6	65.3	13.6	7.73	-45	-52	1	76378	CD-23 7884
NN	08 53 10	-23 40.8	0.596	274.4		m	14.0 *			1.38			82.0	12. r	13.6 *					
NN	08 53 47	-54 46.3	0.092	153.1	-2	F6 V	5.71	0.48	0.00				41.0	05. r	3.77	10	3	-2	76653	CP-54 1925
Gl 330	08 54 21	+11 50.7	0.335	186.0	-12.1	dM5	10.60	1.53	1.21	0.84	65.5	5.7	65.5	5.7	9.68	15	-15	-17		BD+12 1944
NN	08 54 39	+73 09.4	0.893	90.4		m	14.32	1.70	1.25		72.8	5.8	72.8	5.8	13.63					
NN	08 55 10	-71 24.4	0.544	334.2		m	14.5 *			1.26			41.0	07. r	12.6 *					
GJ 1116 A	08 55 27	+19 57.4	0.874	267.7	-34	m	14.06	1.84		+1.76 J	191.3	2.5	191.3	2.5	15.47	10	13	-37		
GJ 1116 B	08 55 27	+19 57.5	0.874	267.7		m	14.92	1.93			191.3	2.5	191.3	2.5	16.33					
Gl 330.1	08 55 44	+20 44.6	0.677	105.6	-50.8	dK5	9.26	1.11	1.01	0.48	39.1	5.6	39.1	5.6	7.22	93	-6	23		BD+21 1949
Gl 331 A	08 55 48	+48 14.4	0.500	242.4	+9.0 SB	A7 IV	3.14	0.19	0.08		71.3	8.2	71.3	8.2	2.41	-28	-13	-16	76644	BD+48 1707
Gl 331 B	08 55 48	+48 14.4	0.500	242.4	15	dM1 J	10.8 *				71.3	8.2	71.3	8.2	10.1 *	-32	-12	-12		
Gl 331 C	08 55 48	+48 14.4	0.500	242.4			11.0 *				71.3	8.2	71.3	8.2	10.3 *					
GJ 1117	08 56 11	+33 08.8	0.314	271.0		DQ6	15.18	0.01	-0.92		49.2	3.4	49.2	3.4	13.64					
NN	08 56 14	+08 40.4	0.459	134.2		k	10.89	1.67	1.21	1.27			224.0	36. r	12.64					
NN	08 56 23	-15 56.5	0.318	49.0	120.8	F6 V	5.83	0.53	0.08	0.23	25.5	13.5	60.0	05. s	4.72	-49	-94	63	76932	BD-15 2656
GJ 1118	08 56 58	-31 01.0	1.005	136.6	50	k-m	13.80	1.64	1.20	1.29			62.0	11. r	12.76	62	-66	13		
GJ 1119	08 57 11	+46 47.3	0.712	221.0		m	13.32	1.72		1.36	96.6	2.7	96.6	2.7	13.24					
Gl 332 A	08 57 24	+41 58.9	0.506	240.2	+27.1 SB	F3 V	4.11	0.37	0.02		66.3	6.1	66.3	6.1	3.22	-42	-17	-6	76943	BD+42 1956
Gl 332 B	08 57 24	+41 58.9	0.506	240.2		G5 V	6.18	0.65	0.19		66.3	6.1	66.3	6.1	5.29					
NN	08 57 26	+48 38.0	1.130	193.3		k-m	14.13	1.70		1.18	50.7	3.3	50.7	3.3	12.66					
NN	08 57 34	-27 37.2	0.068	219.7	63.2	G5 V	6.87	0.69	0.26				46.0	08. r	5.18	-17	-61	6	77137	CD-27 6141
Gl 333	08 57 52	-47 15.0	0.847	323.6	22	M3	12.19	1.56	+1.34:	+0.91:	72.8	18.8	72.8	18.8	11.5	-56	-20	4		
Gl 333.2A	08 58 11	+05 26.6	0.305	230.0	-37.1	dM4	12.34	1.45	1.07	1.08	42.0	5.1	42.0	5.1	10.46	15	5	-48		
Gl 333.2B	08 58 13	+05 26.4	0.305	230.0	-37	dM4	12.68	1.47	1.08	1.12	42.0	5.1	42.0	5.1	10.8	15	5	-48		
Gl 333.1	08 58 11	-58 53.5	0.327	327.5	11.4	F3 V	5.16	0.42	-0.02:		53.0	7.2	53.0	7.2	3.78	-27	-15	2	77370	CP-58 1327
NN	08 58 19	+68 15.2	0.419	31.0		m	12.65			1.22	98.3	7.0	98.3	7.0	12.61					
GJ 1120 A	08 58 31	+15 28.0	0.343	201.5	-12	K5	9.43	+1.30 J	+1.22 J	+0.55 J	55.0	8.0	55.0	8.0	8.13	10	-19	-24	77175	BD+15 1957
GJ 1120 B	08 58 31	+15 27.9	0.388	196.7	-12.7	K5	9.49				55.0	8.0	55.0	8.0	8.19	12	-23	-25		
NN	08 58 36	+02 08.4	0.384	258.0		k	11.82	1.50	1.19				49.0	23. r	10.3					
NN	08 59 37	+08 40.1	0.600	106.2		k	11.75	1.45	1.10	1.02			60.0	12. r	10.64					
NN	09 00 26	+73 27.1	0.560	215.7		DC9	16.97						41.0	05. w	15.03					
Gl 333.3	09 01 40	-66 11.8	0.099	179.0	5.9 SB	A5 V	4.01	0.14	0.13	+0.07C	49.4	15.3	49.4	15.3	2.5	8	-3	-7	78045	CP-65 1065
NN	09 02 29	+03 02.0	0.306	278.0		m	11.61			0.94			54.0	10. r	10.27					
NN	09 03 31	+13 03.8	0.392	224.0		m	13.31			1.17			50.0	10. r	11.8					
Gl 334	09 04 20	-08 36.5	0.376	305.8	+37.1 SB?	dM0	9.51	1.42	1.26	0.68	74.0	4.2	74.0	4.2	8.86	-39	-19	9		BD-08 2582
NN	09 04 24	+66 47.8	0.317	118.0		m	12.96			1.08			43.0	09. r	11.13					
NN	09 04 49	-21 56.4	0.513	215.9		k-m	14.3 *			1.42			82.0	12. r	13.9 *					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	09 05 21	+51 48.5	0.142	255.8	-0.1	A m	4.48	0.27	0.12				45.0	05. o	2.75	-10	-3	-10	78209	BD+52 1365
Gl 334.1	09 05 22	+73 36.9	0.318	210.0	-27	K7	10.17	1.26	1.28		48.6	7.2	48.6	7.2	8.6	-4	-37	-18		BD+73 447
Gl 334.2	09 05 47	+34 05.2	0.222	237.6	26.8	F9 V	5.93	0.60	0.04				52.0	08. r	4.51	-30	-14	4	78366	BD+34 1949
Wo 9286	09 05 51	+26 50.2	0.396	199.8	+10.4 SB	G5 IV	5.99	0.65	0.20	0.23	41.5	8.5	41.5	8.5	4.08	-10	-44	-12	78418	BD+27 1715
Gl 335 A	09 06 01	+67 20.4	0.099	188.1	-2.9	F7 IV-V	4.84	+0.49 J	+0.02 J		54.0	13.6	54.0	13.6	3.5	-2	-9	0	78154	BD+67 577
Gl 335 B	09 06 01	+67 20.4	0.099	188.1		K2 V	8.44*				54.0	13.6	54.0	13.6	7.1 *					
GJ 1121	09 06 14	+40 18.7	0.806	223.8		m	14.55	1.82		1.27	45.9	3.4	45.9	3.4	12.86					
NN	09 06 26	-10 33.2	0.383	253.2		G4	7.15	0.61	+1.68C		39.2	13.6	33.0	04. r	4.74				78612	BD-10 2754
Wo 9287 A	09 06 26	-25 38.2	0.331	268.1	36.1	G1 V	6.77	0.57	0.03		43.4	15.3	34.0	05. r	4.43	-41	-33	-26	78643	CD-25 6905
Wo 9287 B	09 06 26	-25 38.2	0.331	268.1			13. *				43.4	15.3	34.0	05. r	11. *					
Gl 336	09 06 29	+33 01.9	0.639	210.3	9.9	dM2	9.96	1.39	1.23	0.71	47.2	8.6	47.2	8.6	8.33	-23	-56	-23		BD+33 1814
NN	09 06 46	+84 23.1	0.669	308.5	-28.7	m	11.92			0.88			39.0	07. r	9.88	-3	19	-84		
NN	09 07 00	+06 54.				M4 e	13.35	1.57		1.13			42.0	08. r	11.47					
NN	09 07 16	+05 24.5	0.084	236.8		K4	8.38	1.01	0.91	0.35			44.0	05. r	6.6				78727	BD+ 5 2131
Gl 336.1	09 08 11	+46 49.4	0.390	267.0		dM0	10.94	1.44		0.77	44.2	3.9	44.2	3.9	9.17					
NN	09 09 02	+49 24.9	0.191	195.7		G5	7.68						45.0	05. o	5.95				78899	BD+49 1815
Gl 336.2A	09 09 03	-45 06.2	0.180	278.0	18.1	K0 V	9.78	0.78	0.40	+0.40CJ	45.2	10.2	45.2	10.2	8.06	-15	-18	-11	79170	CP-44 3489
Gl 336.2B	09 09 03	-45 06.2	0.180	278.0	26.5	K0 V	10.30	0.91	0.65		45.2	10.2	45.2	10.2	8.58	-16	-26	-11		
NN	09 09 06	+28 07.1	0.484	203.8		m	12.29	1.56	1.18	1.10			62.0	13. r	11.25					
Gl 337 A	09 09 34	+15 11.9	0.580	293.8	+50.2 SB	K0 V J	7.25	+0.73 J	+0.25 J	+0.26 J	45.6	4.2	45.6	4.2	5.54	-78	-1	-2	79096	BD+15 2003
Gl 337 B	09 09 34	+15 11.9	0.580	293.8			7.3 *				45.6	4.2	45.6	4.2	5.6 *					
Gl 337.1	09 10 25	+61 37.9	0.033	191.3	-14.6 SB	F9 V	5.13	0.58	0.10		43.7	8.3	56.0	05. s	3.87	9	-8	-9	79028	BD+62 1058
Gl 338 A	09 10 59	+52 54.1	1.662	249.6	+13.7 SB	M0 Ve	7.62	1.39	1.20	0.68	162.5	2.0	162.5	2.0	8.67	-43	-14	-21	79210	BD+53 1320
Gl 338 B	09 11 01	+52 54.2	1.690	246.9	+14.7 SB	M0 Ve	7.71	1.42	1.25	0.69	162.5	2.0	162.5	2.0	8.76	-44	-16	-20	79211	BD+53 1321
Gl 338.1A	09 11 57	+77 27.2	1.055	269.5	-4	K5 J	10.67	+1.38 J	+1.22 J	+0.62 J	41.6	3.7	41.6	3.7	8.77	-81	-4	-88		BD+77 361
Gl 338.1B	09 11 57	+77 27.2	1.055	269.5			11.0 *				41.6	3.7	41.6	3.7	9.1 *					
Gl 339 A	09 12 17	+04 39.0	0.106	279.8	16.2	dK5	8.04	+1.02 J	+0.85 J	+0.45 J	48.9	5.3	48.9	5.3	6.49	-17	-8	2	79555	BD+05 2143
Gl 339.1	09 12 29	+53 38.9	1.550	223.5		DXP7	13.85	0.34	-0.52		96.7	1.8	96.7	1.8	13.78					
NN	09 12 36	+54 13.8	0.075	39.3	-18.7 SB	A5 V	4.83	0.19	0.08		40.7	11.9	40.7	11.9	2.9	18	3	-10	79439	BD+54 1285
Gl 339.3	09 13 45	-37 12.2	0.022	105.6	5.8	F5 III	4.62	0.45	0.10		62.5	13.6	62.5	13.6	3.6	1	-6	2	79940	CD-36 5505
NN	09 14 02	+58 38.9	1.134	180.6		m	15.11	1.85		1.43	64.8	4.0	64.8	4.0	14.17					
NN	09 14 05	-18 25.0	0.339	297.0		M2	10.75	1.55		0.93			80.0	15. r	10.27					
NN	09 14 06	+00 56.3	0.093	258.3		F6 III-IV	6.71	0.41	0.05		39.3	15.3	39.3	15.3	4.7				79873	BD+01 2267
Gl 340 A	09 14 56	+28 46.7	0.516	174.0	-19.1	K3 V	7.86	+1.00 J	+0.82 J	+0.37 J	58.2	2.9	58.2	2.9	6.68	23	-36	-16	79969	BD+29 1883
Gl 340 B	09 14 56	+28 46.7	0.516	174.0		K3 V	8.1 *				58.2	2.9	58.2	2.9	6.9 *					
NN	09 15 22	-61 52.3	0.923	314.4		m	12.7 *			1.14			59.0	12. r	11.6 *					
NN	09 15 25	+27 31.2				K5	9.55	1.34	1.26	0.56			52.0	08. r	8.13					BD+27 1739
NN	09 15 29	+62 16.2	0.425	217.2		m	11.28			0.80			42.0	07. r	9.4					
NN A	09 15 51	+26 58.1	0.382	210.0		k-m	11.77	1.50	1.23				50.0	24. r	10.3					
NN B	09 15 46	+26 58.8	0.382	210.0		m	16. *						50.0	24. r	14. *					
GJ 1122 A	09 16 12	+38 44.0	0.250	272.0		m	14.52	1.68		1.34	49.6	2.7	49.6	2.7	13					
GJ 1122 B	09 16 12	+38 44.1	0.250	272.0		m	14.67	1.68		1.35	49.6	2.7	49.6	2.7	13.15					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	09 16 33	+73 19.8	0.996	249.8		m	15.02	1.90					87.0	35. r	14.7					
Gl 340.1A	09 16 36	-68 28.7	0.108	247.0	32.3	F4 V	6.13	+0.42 J	-0.04 J	+0.25CJ	56.5	13.6	28.0	03. r	3.37	1	-28	-24	80671	CP-68 918
Gl 340.1B	09 16 36	-68 28.7	0.108	247.0			6.13*				56.5	13.6	28.0	03. r	3.37*					
NN	09 16 44	-57 34.0	0.484	346.7	24	K7 V	9.52	1.19	1.00	0.54	29.5	11.4	47.0	08. r	7.88	-38	-32	23	80545	CD-57 2585
Gl 340.2	09 16 54	+01 06.6	0.199	225.0	47.5	K0	8.16	0.87	0.61	+0.43C	50.0	13.6	40.0	06. r	6.17	-29	-44	6	80367	BD+01 2277
NN	09 17 22	+26 56.9	1.007	120.8	-7	m	15.56	1.92			48.3	7.8	48.3	7.8	13.98	75	-45	47		
GJ 1123	09 17 32	-77 37.0	1.023	139.3	0	m	13.10	1.64	1.15	1.39			123.0	19. r	13.55	36	15	0		
Gl 340.3	09 18 16	-05 32.4	0.373	251.4	36.5	dK8	9.09	1.16	1.13	0.44	49.3	18.5	44.0	05. r	7.31	-37	-36	-15	80632	BD-05 2778
NN	09 18 21	+03 35.8	1.178	163.2		m	13.33	1.60	1.38	1.10	60.8	4.2	60.8	4.2	12.25					
NN	09 18 36	+43 43.3	0.309	250.0		m	14.02			1.29			58.0	10. r	12.84					
GJ 1124	09 19 17	+40 25.2	0.507	223.0	-43.0	SB K2 V	7.63	0.99	0.76		54.1	7.6	54.1	7.6	6.3	10	-32	-52	80715	BD+40 2197
Gl 341	09 20 24	-60 04.2	0.879	282.6	36.2	M0 V	9.50	1.48	1.18	0.78	99.4	23.5	99.4	23.5	9.5	-29	-38	-27	304636	CP-59 1362
Gl 341.1	09 21 06	+80 48.2	0.446	179.1	-21.4	K5	9.30	1.23	1.21	0.46	58.1	6.8	58.1	6.8	8.12	-3	-42	6		BD+81 297
NN	09 21 19	+00 21.4	0.300	227.0		M3:	11.54	1.51	1.23				59.0	28. r	10.4					
Gl 342	09 21 35	+76 09.1	0.360	254.9	-5.9	dK5 e	9.03	1.19	1.18	0.46	57.6	17.0	48.0	08. r	7.44	-25	-12	-23	80768	BD+76 351
Gl 343	09 22 49	+18 53.5	0.538	236.0	1	M2	13.43	1.61		0.94	60.5	17.0	23.0	05. r	10.24	-48	-61	-79		
NN	09 24 07	+50 52.4	0.228	235.0		m	11.93			0.95			48.0	09. r	10.34					
Gl 343.1	09 24 20	+39 43.5	0.190	133.0	-21	dK8 e	9.84	1.29	1.17	0.55			44.0	06. r	8.06	26	-13	-5		BD+40 2208
NN	09 25 12	+13 58.1	0.067	232.0		G5	7.81						49.0	05. o	6.26				81762	BD+14 2097
Gl 344 A	09 25 18	-05 51.1	0.240	251.0	+55.9	SB G2 V J	5.80	+0.65 J	+0.12 J	+0.24 J	32.0	10.6	54.0	05. s	4.46	-35	-47	11	81809	BD-05 2802
Gl 344 B	09 25 18	-05 51.1	0.240	251.0	53.7		6.6 *				32.0	10.6	54.0	05. s	5.3 *	-34	-45	10		
Gl 346	09 26 24	-09 02.8	0.050	158.0		dM0	10.52	1.43	+1.02:	0.72	9.2	13.8	49.0	08. r	8.97					BD-08 2689
Gl 347 A	09 26 25	-07 08.5	0.692	193.8	8.5	M3.5	12.08	1.53	1.11	1.04	59.8	4.7	59.8	4.7	10.96	16	-42	-33		
Gl 347 B	09 26 28	-07 08.5	0.692	193.8		m	15.00	1.87	1.25	+1.73C	59.8	4.7	59.8	4.7	13.88					
Gl 348 A	09 26 37	-02 33.0	0.134	104.2	+10.8	SB F6 V	4.60	0.45	0.00	+0.26C	70.4	6.9	70.4	6.9	3.84	2	-9	11	81997	BD-02 2901
Gl 348 B	09 26 37	-02 31.9	0.146	103.1	11.5	K0	7.18	0.87	0.57		70.4	6.9	70.4	6.9	6.42	3	-9	12		BD-02 2902
NN	09 26 53	+39 50.7	0.244	145.0		m	12.13			1.03			54.0	11. r	10.79					
Wo 9299	09 27 07	-05 09.2	0.489	274.3		K7	9.74	1.31	1.30	0.54			45.0	06. r	8.01					BD- 4 2639
Gl 349	09 27 19	+05 52.4	0.519	281.9	27.6	K3 Ve	7.20	1.00	0.90	0.37	88.6	13.1	88.6	13.1	6.94	-37	-13	1	82106	BD+06 2182
NN	09 27 37	+63 16.9	0.111	76.8	-10.4	F0 IV	3.67	0.33	0.10	0.18	39.8	7.8	39.8	7.8	1.67	17	0	1	81937	BD+63 845
GJ 1125	09 28 12	+00 33.0	0.790	228.3	-40	M3.5	11.71	1.59	1.22	1.14	98.4	3.2	98.4	3.2	11.67	11	6	-54		
GJ 1126 A	09 28 20	-31 53.2	0.331	344.6		K3 V	8.38	0.98	0.69	0.42			45.0	06. r	6.65				82342	CD-31 7352
GJ 1126 B	09 28 20	-31 53.2	0.393	349.0		g	13.08	1.46	0.97	1.10			45.0	06. r	11.35					
Gl 351.1	09 28 44	+20 30.8	0.800	178.5		M3	12.20	1.48		0.96	49.3	10.2	49.3	10.2	10.66					
Gl 351 A	09 28 44	-40 14.8	0.201	290.1	8.8	F3 IV	4.12	+0.36 J	-0.03 J	+0.22CJ	64.2	5.1	64.2	5.1	3.16	-14	-9	-5	82434	CD-39 5580
Gl 351 B	09 28 44	-40 14.8	0.201	290.1		F0 IV	4.65*				64.2	5.1	64.2	5.1	3.69*					
Gl 352 A	09 28 53	-13 16.1	0.731	85.4	7.3	M3 J	10.81	+1.53 J	+1.16 J	+1.04 J	107.9	9.1	107.9	9.1	10.98	19	-3	27		BD-12 2918
Gl 352 B	09 28 53	-13 16.1	0.731	85.4			10.8 *				107.9	9.1	107.9	9.1	11.0 *					
Gl 353	09 28 54	+36 32.9	0.584	200.9	20.1	dM2	10.19	1.50	+1.26?	0.78	65.5	3.6	65.5	3.6	9.27	-21	-42	3		BD+36 1970
Gl 354 A	09 29 31	+51 54.4	1.095	240.4	+15.3	SB F6 IV	3.17	0.46	0.02	0.16	69.1	8.4	69.1	8.4	2.37	-61	-37	-27	82328	BD+52 1401
Gl 354 B	09 29 31	+51 54.4	1.095	240.4			13.8 *				69.1	8.4	69.1	8.4	13.0 *					
Gl 354.1A	09 29 50	+27 12.8	0.292	209.6	9.3	dG9	7.01	0.77	0.33		53.6	15.3	53.0	09. r	5.63	-11	-25	-5	82443	BD+27 1775

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 354.1B	09 29 54	+27 13.2	0.274	210.0		m	16.5 P				53.6	15.3	53.0	09. r	15.1 P					
Gl 355	09 30 01	-10 57.8	0.253	274.1	10.9	K0	7.82	0.92	0.54	+0.51C	62.3	13.4	52.0	08. r	6.4	-22	-9	-9	82558	BD-10 2857
Gl 355.1	09 30 06	+70 03.1	0.098	319.3	-28.1	G4 III-IV	4.56	0.77	0.34		40.4	8.5	40.4	8.5	2.59	14	-6	-26	82210	BD+70 565
Gl 355.2	09 30 54	-20 53.6	0.027	293.6	16.3	K0 IV	5.01	1.02	0.87	+0.44C	50.6	17.0	50.6	17.0	3.5	-7	-14	5	82734	BD-20 2936
NN	09 31 26	+61 28.0				M3	11.95	1.54	1.21	0.97			51.0	10. r	10.49					
Gl 356 A	09 32 40	+36 02.2	0.775	251.4	14.9	G8 V	5.41	0.77	0.44	0.26	87.0	8.5	87.0	8.5	5.11	-38	-17	-16	82885	BD+36 1979
Gl 356 B	09 32 40	+36 02.2	0.775	251.4			13.0 *				87.0	8.5	87.0	8.5	12.7 *					
Wo 9303	09 33 12	+37 45.2	0.105	224.0		K5	11.02	1.44		0.73			40.0	06. r	9.03					
NN	09 33 38	-05 53.3	0.780	245.1		m	14.0 *			1.20			40.0	08. r	12.0 *					
Gl 357	09 33 43	-21 25.4	0.915	169.4	-78	M3 V	10.92	1.57	1.18	1.00	111.6	16.7	111.6	16.7	11.16	49	53	-49		
NN	09 33 57	+40 48.2	0.188	244.0		m	14.03			1.24			47.0	09. r	12.39					
GJ 1127	09 34 22	+22 55.3	0.231	219.3	-36.9	dM0	9.48	1.28	1.27	0.52	7.1	5.7	50.0	08. r	7.97	17	-5	-39		BD+23 2121
Gl 358	09 37 49	-40 50.7	0.663	305.0	142	M3	10.75	1.53	1.17	1.07	97.6	11.0	97.6	11.0	10.7	-36	-140	18		CD-40 5404
Gl 359	09 38 11	+22 15.5	0.672	135.1		M4	14.23	1.78	+1.10:	1.38	82.2	5.4	82.2	5.4	13.8					
Gl 360	09 38 22	+70 15.9	0.727	246.4	6.9	M3	10.57	1.50		1.02	74.1	10.5	74.1	10.5	9.92	-41	-16	-16		
Gl 361	09 38 30	+13 26.4	0.648	253.5	11.4	dM2 e	10.37	1.50	1.25	0.92	80.3	18.4	80.3	18.4	9.89	-30	-18	-20		
Gl 362	09 38 39	+70 16.3	0.727	246.4	6	M3	11.22	1.52		1.12	90.0	10.9	90.0	10.9	10.99	-34	-13	-13		
Gl 363	09 38 57	+56 13.2	0.890	235.7		M3.5	12.50	1.53	+1.35?	1.22	69.3	6.8	69.3	6.8	11.7					
GJ 2074	09 39 21	+07 11.0	0.044	201.0		DA7	14.90	0.30	-0.55				58.0	07. w	13.72					
Gl 364	09 39 59	-23 41.4	0.476	302.6	35.2	F9 IV	4.93	0.53	0.01	+0.28C	82.0	21.5	82.0	21.5	4.5	-34	-28	8	84117	CD-23 8646
Gl 365	09 40 17	+42 55.9	0.837	177.8	-12.1	K5 V	8.12	1.15	1.15	0.42	50.5	7.3	50.5	7.3	6.64	14	-78	-1	84035	BD+43 1953
NN	09 40 17	-19 00.2	0.520	243.6		M3	11.96	1.58		1.03			62.0	15. r	10.9					
NN	09 41 05	+27 12.1	0.603	260.8		M3	12.05	1.56	+1.20:	1.15			76.0	19. r	11.5					
NN	09 41 18	-06 49.7	0.441	187.5		DA9	16.41	0.56	-0.30				43.0	08. w	14.58					
Gl 366	09 41 42	+76 17.3	0.991	173.2	-27.8	M1.5	10.62	1.41	1.09	0.86	63.5	4.7	63.5	4.7	9.63	0	-75	25		
GJ 1128	09 41 57	-68 40.3	1.120	356.8	-21	m	12.78	1.73	1.22	1.42			161.0	23. r	13.81	-27	8	27		
Gl 366.1A	09 41 58	-27 32.4	0.059	301.2	24	F6 V	5.45	+0.51 J	+0.35 J	+0.30CJ	51.2	15.3	52.0	09. r	4.03	-9	-22	7	84367	CD-27 6881
Gl 366.1B	09 41 58	-27 32.4	0.059	301.2		F8 V	5.6 *				51.2	15.3	52.0	09. r	4.2 *					
GJ 1129	09 42 32	-17 58.8	1.633	264.0	9	m	12.60	1.59	1.28	1.27			98.0	17. r	12.56	-57	-19	-52		
Gl 367	09 42 37	-45 32.3	0.746	217.3	60	M3	10.11	1.53	1.13	0.94	108.8	6.7	108.8	6.7	10.29	4	-63	-26		CD-45 5378
NN	09 43 40	-04 12.0	0.547	287.6		m	14.15			1.32			61.0	10. r	13.08					
NN	09 44 30	+60 29.5	0.888	257.3		M2	12.73	1.64	1.39				81.0	35. r	12.3					
NN	09 44 53	+13 10.4	0.246	340.0		m	13.38			1.20			54.0	10. r	12.04					
Gl 368	09 45 22	+46 15.3	0.242	113.1	5	G0.5 Va	5.09	0.62	0.10	+0.22t	75.3	4.7	75.3	4.7	4.47	8	-4	13	84737	BD+46 1551
NN	09 46 55	+53 29.2	0.268	265.0		DQ6	15.20	0.13	-0.70		43.9	3.5	43.9	3.5	13.41					
Gl 368.1A	09 47 02	-52 23.1	0.358	312.5	4.4	K1 V	7.93	+0.90 J	+0.65 J	+0.46CJ	44.5	13.6	45.0	08. r	6.2	-37	-9	2	85228	CP-52 2830
Gl 368.1B	09 47 02	-52 23.1	0.358	312.5			12.0 *				44.5	13.6	45.0	08. r	10.3 *					
Gl 369	09 48 40	-12 04.5	1.791	143.4	62.2	dM2	10.04	1.48	1.18	0.78	84.8	7.6	84.8	7.6	9.68	72	-91	23		BD-11 2741
Gl 370	09 49 05	-43 15.7	0.649	135.2	-9.6	K5 V	7.64	1.18	1.12	0.50	103.2	9.1	103.2	9.1	7.71	29	10	-4	85512	CP-42 4101
Gl 371	09 49 37	+03 27.4	0.440	270.7	+21.5 VAR	dM0 p	8.86	1.23	1.21	0.47	39.4	4.7	39.4	4.7	6.84	-51	-19	-19	85488	BD+03 2279
NN	09 50 04	+03 22.0	0.060	239.0	13	K4	10.58	1.40	1.24	0.63	52.7	8.5	52.7	8.5	9.19	-8	-11	4		
Gl 372	09 50 41	-03 26.9	0.471	191.0		dM0	10.54	1.52	+1.2 :	0.98			98.0	19. r	10.5					BD-02 3000

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	09 51 09	+21 10.6	0.506	320.7		m	14.05			1.44			98.0	15. r	14.01					
GJ 1130 A	09 51 17	-31 30.9	0.204	228.9		M0 V	10.21	1.38	1.15	0.68			50.0	06. r	8.7					CD-31 7745
GJ 1130 B	09 51 17	-31 30.9	0.204	228.9			14.42	1.70		1.30			50.0	06. r	12.91					
Gl 373	09 52 29	+63 02.0	0.658	207.3	14.9	dM1	9.00	1.43	1.19	0.73	98.3	5.4	98.3	5.4	8.96	-24	-22	12		BD+63 869
NN	09 52 45	+35 36.1	0.238	190.0		M4	12.73			1.11			57.0	12. r	11.51					
NN	09 53 40	+22 53.5	0.536	239.9		m	14.2 *			1.33			62.0	10. r	13.2 *					
Gl 374	09 54 09	-40 32.9	0.156	243.6	57	K4 V	9.00	0.96	0.73	0.34	67.6	15.3	32.0	05. r	6.53	-9	-60	-10	86249	CP-40 4033
NN	09 54 38	+41 17.7	0.122	256.1	-8.9 SB	F6 Vas	5.14	0.46	0.00		38.7	10.2	50.0	06. r	3.63	-3	-4	-14	86146	BD+41 2033
NN	09 55 00	+24 47.5	0.391	220.0	124	DA6	15.09	0.25	-0.54		41.2	4.5	41.2	4.5	13.16	-58	-59	39		
NN	09 55 19	+12 02.9	0.467	249.8		m	14.66			1.31			46.0	07. r	12.97					
NN A	09 56 13	+44 05.0	0.228	199.0		m	13.89			1.22			45.0	06. r	12.16					
NN B	09 56 15	+44 05.0	0.228	199.0		m	14.16			1.24			45.0	06. r	12.43					
Gl 375	09 56 34	-46 10.7	0.676	136.1	44	M3.5	11.27	1.55	0.91	1.19	69.1	13.8	69.1	13.8	10.47	49	-41	-2		CD-45 5627
NN	09 56 35	+47 26.8	0.281	163.0		m	14.09			1.25			47.0	09. r	12.45					
Gl 375.1	09 57 02	-49 45.8	0.140	282.0	38		11.68	0.91	0.70	+0.51C	44.7	13.6	44.7	13.6	9.9	-9	-40	-4		
NN	09 57 13	+24 47.6	0.237	259.5	13.4	K0 V	7.90v	0.88	0.43	0.38	29.7	8.5	48.0	09. r	6.31v	-24	-11	-4	86590	BD+25 2191
Wo 9309	09 57 28	-50 21.3	0.180	289.0		g-k	12.1 P				41.8	10.2	41.8	10.2	10.2 P					CD-50 4715
Gl 376	09 58 08	+32 10.2	0.684	230.5	55.8	G2 Va	5.35	0.66	0.27		64.5	6.6	64.5	6.6	4.4	-57	-45	20	86728	BD+32 1964
Gl 377	09 59 01	-30 09.5	1.297	297.9	60	M3	11.43	1.49	1.10	1.07	73.3	6.9	73.3	6.9	10.76	-88	-54	4		CD-29 8019
GJ 2077	09 59 08	+14 55.9	0.314	274.0	-140	DC7	15.37	0.36	-0.49				46.0	05. w	13.68	65	79	-158		
Gl 378	09 59 14	+48 21.1	1.571	203.8	-9.8	dM2	10.07	1.37	1.13	0.82	68.0	5.0	68.0	5.0	9.23	-25	-106	-16		BD+48 1829
NN	09 59 14	-15 11.0	0.248	279.3		K3 V	8.64	1.02	0.75	0.36			40.0	06. r	6.65				86972	BD-14 3003
Gl 378.1	09 59 23	+44 49.3	0.290	250.9	+33.5 SB?	dK8	9.04	1.07	0.98	0.40	52.6	10.2	38.0	04. r	6.94	-47	-14	8	86856	BD+45 1791
NN	09 59 59	+15 13.9	0.279	150.0		m	14.23	1.70					56.0	23. r	13					
NN	10 00 58	+06 12.4	0.659	257.8		m	13.17			1.13			46.0	09. r	11.48					
NN	10 01 56	+05 48.5				M0	12.66	1.50	1.22	1.03			42.0	08. r	10.78					
NN	10 03 43	+41 57.8	0.557	217.2		M0	11.32	1.49	1.22				39.0	10. r	9.3					
GJ 1131	10 04 09	+69 29.4	0.872	269.6		m	14.34	1.75			56.3	4.6	56.3	4.6	13.09					
Gl 378.2	10 04 22	+03 12.6	0.110	218.0	-15.4	dM0 e	9.95	1.39	1.28	0.64	42.2	11.9	53.0	08. r	8.57	5	2	-17		BD+03 2316
Gl 378.3	10 04 29	+35 29.4	0.052	91.3	-17.6	A7 V	4.48	0.18	0.08		47.8	11.9	47.8	11.9	2.9	14	2	-11	87696	BD+35 2110
Wo 9315	10 04 48	-14 03.7	0.123	166.0		K7 V	10.19	1.32	+1.20:	0.59			41.0	08. r	8.25					BD-13 3031
NN	10 06 19	+51 32.4	0.927	209.3		k-m	13.47	1.66			75.0	3.2	75.0	3.2	12.85					
Gl 379 A	10 06 24	+75 23.0	0.349	40.0	-48.9	dK6 eJ	10.18	+1.40 J	+1.19 J	+0.59 J	54.2	7.5	54.2	7.5	8.85	48	-5	-31		BD+75 403
Gl 379 B	10 06 24	+75 23.0	0.349	40.0			10.3 *				54.2	7.5	54.2	7.5	9.0 *					
Gl 379.1A	10 07 22	-35 36.7	0.442	271.2	36.8	F8 V	6.15	0.60	0.16	0.22	46.7	7.8	46.7	7.8	4.5	-37	-42	-15	88218	CD-35 6194
Gl 379.1B	10 07 22	-35 36.7	0.442	271.2			10.9 *				46.7	7.8	46.7	7.8	9.2 *					
Gl 379.2	10 07 40	-36 30.8	0.488	319.1	111.1	G3 V-VI	8.08	0.60	+0.01:	0.22	46.2	9.4	22.0	03. r	4.79	-102	-101	52	88261	CD-36 6180
Gl 380	10 08 19	+49 42.5	1.454	248.9	-25.4	K2 Ve	6.59	1.36	1.28	0.60	213.2	2.7	213.2	2.7	8.23	-9	-20	-35	88230	BD+50 1725
NN	10 08 48	+35 33.6	0.281	150.0		M4	14.50			1.27			42.0	07. r	12.62					
Gl 381	10 09 31	-02 25.8	0.829	142.0	40	dM0	10.63	1.57	1.20	1.00	117.3	9.0	117.3	9.0	10.98	17	-42	25		
Gl 382	10 09 46	-03 29.7	0.280	214.1	7.7	dM2	9.27	1.48	1.19	0.92	116.7	4.9	116.7	4.9	9.61	-3	-13	-3		BD-03 2870
Gl 383	10 09 47	-18 22.2	0.525	270.1	-1.7	K7 V	9.94	1.48	1.23	0.71	70.4	9.0	70.4	9.0	9.18	-28	-5	-21		BD-17 3088

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 383.1	10 10 44	+52 45.9	0.773	173.9	-24.8	dM0	9.53	1.10	0.94	0.47	54.6	22.2	38.0	06. r	7.43	25	-96	12	233719	BD+53 1395
NN	10 10 52	-35 29.8	0.532	292.7		M3.5	12.95			1.08			45.0	09. r	11.22					
Gl 384 A	10 10 56	-47 13.8	0.269	302.7	0.3	G8 V	8.27	+0.80 J	+0.34 J	+0.43CJ	65.2	15.3	29.0	05. r	5.58	-44	-6	-1	88746	CP-46 4357
Gl 384 B	10 10 56	-47 13.8	0.269	302.7			10.9 *				65.2	15.3	29.0	05. r	8.2 *					
Gl 385	10 10 59	-84 52.4	0.010	158.0			10.22:	0.34		+0.14t	56.6	15.3	56.6	15.3	9.0 :					
Gl 385.1	10 11 12	-32 47.1	0.376	279.4	41.9	G1 V	6.38	0.59	0.09	0.20	53.7	7.1	53.7	7.1	5.03	-31	-44	-1	88742	CD-32 7158
Wo 9321	10 11 15	-07 08.2	0.192	275.2	14.6	dF6	7.21	0.49	0.05		40.9	17.0	16.0	02. s	3.23	-52	-17	-20	88697	BD-06 3109
Wo 9322	10 11 32	+03 24.3	0.473	150.0	-24	G1 V	7.76	0.60	-0.02		42.9	8.8	26.0	03. s	4.83	78	-36	-24	88725	BD+03 2338
GJ 2079	10 11 35	+21 19.7	0.230	204.0	10.1	dM0 e	10.20	1.36	1.15	0.76	33.9	18.8	59.0	13. r	9.05	-5	-20	1		
NN	10 11 45	+21 25.1	0.166	237.5	16.8	F9 V	6.03	0.55	0.12				46.0	07. r	4.34	-17	-17	4	88737	BD+21 2165
NN	10 12 15	+31 40.2	0.239	183.0		m	13.60			1.23			55.0	10. r	12.3					
GJ 1132	10 12 54	-46 54.7	1.137	292.2	-1	k	13.50	1.72	1.34	1.22			58.0	11. r	12.32	-90	-13	-20		
NN	10 12 57	-82 37.8	0.556	303.7		k	11.07	1.42	1.15	0.73			39.0	06. r	9.03					
NN	10 13 12	-55 55.	0.136	298.0	11	DZ9	15.10	0.68	-0.12				90.0	10. w	14.87	-14	32	-1		
Gl 386	10 14 20	-11 42.2	0.744	213.9	-20	dM0	10.98	1.47	1.10	1.05	89.7	10.5	89.7	10.5	10.74	4	-8	-43		
Gl 387 A	10 14 30	+23 21.5	0.429	255.1	37.5	F8 Vbw	5.82	0.50	-0.05	+0.17t	60.8	7.6	60.8	7.6	4.74	-42	-25	12	89125	BD+23 2207
Gl 387 B	10 14 30	+23 21.5	0.429	255.1	38.4	M1	11.4 *				60.8	7.6	60.8	7.6	10.3 *	-42	-25	12		
NN	10 15 50	+44 18.2	0.308	168.5	-8.3	G5 V	6.65	0.66	0.15	0.22	26.2	10.2	46.0	07. r	4.96	14	-30	2	89269	BD+44 1973
NN	10 16 06	-26 14.9	0.053	133.2	29.8	K0 V	7.94	0.94					46.0	06. r	6.25	3	-28	12	89391	CD-25 7916
Gl 388	10 16 54	+20 07.3	0.506	264.0	12.3	M4.5Ve	9.40	1.54	1.08	1.13	203.9	2.8	203.9	2.8	10.95	-15	-8	3		BD+20 2465
Gl 388.1	10 17 01	+19 43.5	0.328	226.7	6.1	F6 IV	4.81	0.45	0.01		50.9	15.3	50.9	15.3	3.3	-14	-26	-11	89449	BD+20 2466
NN	10 17 33	+49 33.0	0.382	253.0		m	13.16			1.08			39.0	08. r	11.12					
Gl 388.2	10 18 25	-15 13.9	0.359	320.7	+82.8 SB	F8 V	7.18	0.55	-0.04	+0.32C	46.2	11.9	30.0	03. s	4.57	-68	-50	54	89707	BD-14 3093
Wo 9326	10 19 13	+41 29.0	0.178	219.6	-6.5	F7 V	5.77	0.53	0.07		47.4	15.1	48.0	08. r	4.18	-3	-16	-10	89744	BD+41 2076
GJ 1133	10 19 37	+63 42.6	0.276	44.0		DA7	14.71	0.38	-0.51		61.4	4.1	61.4	4.1	13.65					
NN	10 20 03	+15 35.9	0.282	248.1	19.4	dG2	7.28	0.65	0.15		40.0	8.0	34.0	04. r	4.94	-33	-28	-8	89906	BD+16 2116
Wo 9327	10 20 33	+65 49.2	0.027	200.0	-2.6 SB	A0 p	4.97	-0.06	-0.13		41.8	15.3	41.8	15.3	3.1	0	-4	-1	89822	BD+66 664
Gl 389 A	10 20 37	-59 55.1	0.557	141.2	24.7	M3	10.72	1.43	+1.12 J	0.80	55.0	7.1	55.0	7.1	9.42	50	-11	-17		
Gl 389 B	10 20 37	-59 54.9	0.557	141.2		m	12.63	1.49		1.07	55.0	7.1	55.0	7.1	11.33					
NN	10 21 37	-29 23.6	0.105	336.5		G5 V	6.94	0.65	0.39				43.0	07. r	5.11				90156	CD-29 8316
NN	10 21 40	+12 12.5				M0	12.46	1.57	1.28	1.01			45.0	09. r	10.73					
Gl 389.1	10 21 45	-10 08.9	0.403	132.0		dK8	10.00	1.24	1.17	0.51	42.2	6.7	36.0	05. r	7.78					BD-09 3063
NN	10 22 44	+26 39.0	0.537	212.4		k-m	13.19	1.57	1.20	1.21			59.0	11. r	12.04					
Gl 390	10 22 44	-09 58.6	0.722	276.1	7	M1.5	10.17	+1.49:	1.14	0.86	79.9	7.5	79.9	7.5	9.68	-39	-11	-16		BD-09 3070
NN A	10 22 57	+50 42.6	0.627	214.4		k-m	13.52			1.21			51.0	07. r	12.06					
NN B	10 22 58	+50 42.8	0.627	214.4		m	13.68			1.22			51.0	07. r	12.22					
Wo 9329	10 23 18	-44 38.2	0.170	295.0			11.19	0.94	0.76	+0.46C	42.0	11.9	42.0	11.9	9.3					CD-44 6469
Gl 391	10 23 24	-73 46.6	0.033	207.0	-4.7 SB?	F2 IV	4.00	0.35	-0.01		58.4	13.1	58.4	13.1	2.83	-2	5	-1	90589	CP-73 733
Gl 392 A	10 24 59	+49 03.2	0.886	175.0	-6.8	F9 V	6.44	0.60	0.05	0.24	51.9	6.1	51.9	6.1	5.02	17	-77	18	90508	BD+49 1961
Gl 392 B	10 24 59	+49 03.2	0.886	175.0			12.5 *				51.9	6.1	51.9	6.1	11.1 *					
Gl 392.1	10 25 10	+82 48.9	0.087	286.8	+4.2 SB	F2 V	5.26	0.37	-0.05		45.5	11.9	45.5	11.9	3.6	-9	3	-4	90089	BD+83 297
NN	10 25 21	+48 29.8	0.633	102.9		m	13.25	1.67			48.6	3.3	48.6	3.3	11.68					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	10 25 43	-06 20.5	0.468	232.2	28.2	K0 V	7.86	0.80	0.46		30.3	7.0	39.0	06. r	5.82	-26	-53	-23	90711	BD-05 3071
NN	10 25 53	+32 29.6	0.511	292.9		m	13.00			1.14			52.0	10. r	11.58					
NN	10 26 00	+00 14.9				DA	13.83						55.0	06. w	12.53					
Gl 393	10 26 23	+01 06.4	0.949	218.2	8.3	dM2.5	9.64	1.52	1.20	0.96	136.2	4.1	136.2	4.1	10.31	-7	-29	-16		BD+01 2447
Gl 394	10 27 14	+56 15.4	0.185	258.1	+9.1 VAR	K7 Ve	8.69	1.33	1.24	0.55	72.1	13.7	72.1	13.7	7.98	-15	-3	2	237903	BD+56 1458
Gl 395	10 27 26	+56 14.3	0.181	258.8	+8.6 SB?	F8 V	4.84	0.52	-0.01	0.16	78.0	3.8	78.0	3.8	4.3	-14	-2	2	90839	BD+56 1459
NN	10 27 32	+60 00.7	0.528	237.1		K4	8.77	1.15		0.43	23.6	6.7	50.0	08. r	7.26				90875	BD+60 1266
NN	10 27 35	+33 06.0	0.555	229.4		M6 e:	12.72	1.45	1.13	1.10			48.0	11. r	11.13					
Gl 396	10 28 15	+84 39.4	0.056	11.3	9	K0	7.30	0.82	0.51		66.1	18.8	53.0	07. r	5.92	-3	10	2	90343	BD+85 161
Gl 397	10 28 27	+45 47.5	0.822	225.4	23.9	K7 V	8.86	1.33	1.28	0.59	67.6	13.1	67.6	13.1	8.01	-41	-46	7		BD+46 1635
Gl 397.1A	10 28 30	+57 22.2	0.251	325.0	-2	dM0 e	9.65	1.38		0.61	48.1	11.9	57.0	08. r	8.43	-9	13	-14		BD+57 1274
Gl 397.1B	10 28 17	+57 20.5	0.251	325.0		m	16.2 P				48.1	11.9	57.0	08. r	15.0 P					BD
NN A	10 28 39	-21 23.1	0.429	144.0		K7 V	10.68	+1.38 J	+1.35 J	+0.66 J			43.0	06. r	8.85					BD-20 3198
NN C	10 28 39	-21 23.1	0.429	144.0			13.13	1.57		1.21			43.0	06. r	11.3					
Gl 397.2	10 29 25	-53 27.7	0.467	295.8	21	F6 V	4.89	0.50	-0.02	+0.30C	47.8	14.5	51.0	05. s	3.43	-37	-30	-2	91324	CP-53 3909
Wo 9333	10 30 35	-41 12.4	0.100	96.0			11.12	0.90	0.58	+0.41C	41.0	18.8	41.0	18.8	9.2					CD-40 6102
NN A	10 31 32	+46 33.8	0.411	257.0		m	13.13			1.14			49.0	10. r	11.58					
NN B	10 31 28	+46 34.0	0.411	257.0		m+	15.5 :						49.0	10. r	14.0 :					
NN	10 32 04	+69 43.0	1.752	250.5		k-m	11.93	1.55	1.02		75.6	4.4	75.6	4.4	11.32					
Gl 398	10 33 28	+05 22.7	0.642	278.1	21	dM4 e	12.60	1.60	1.12	1.19	73.0	4.3	73.0	4.3	11.92	-44	-17	-2		
Gl 398.1	10 34 03	-11 57.7	0.727	158.7	-6.2	F7 V	5.71	0.52	0.00	0.18	44.0	9.2	46.0	06. r	4.02	60	-31	-33	91889	BD-11 2918
NN	10 35 30	+48 47.4	0.216	248.0		m	13.49			1.16			44.0	09. r	11.71					
NN	10 36 32	-20 25.8	0.628	330.3		DQP9	16.46						69.0	07. w	15.65					
Gl 399	10 37 12	-06 39.7	0.725	261.2		m	11.30	1.53		1.01	88.5	15.2	88.5	15.2	11.03					
GJ 1135	10 38 52	-36 37.9	0.252	133.4		M0 V	9.97	1.48	1.17	0.80			75.0	17. r	9.35					CD-36 6589
GJ 1134	10 38 53	+37 52.6	1.505	256.1	10	m	12.98	1.68	1.17	1.30	96.2	2.3	96.2	2.3	12.9	-61	-36	-24		
GJ 1136 A	10 39 35	-36 22.2	0.169	291.9		K7 V	10.19	1.46	1.19	0.73			56.0	08. r	8.93					CD-35 6662
GJ 1136 B	10 39 35	-36 22.2	0.169	291.9			11.67	1.52	1.11	0.96			56.0	08. r	10.41					
NN	10 41 08	-28 48.0	0.242	249.0		K1 V	7.74	0.89	0.56				48.0	08. r	6.15				92945	CD-28 8394
GJ 1137	10 42 02	-33 18.7	0.176	216.8	41.7	K2 V	8.30	0.95	0.72	0.37			44.0	07. r	6.52	2	-46	-2	93083	CD-32 7598
NN A	10 42 06	+32 40.5	0.213	277.0		m	13.55			1.17			44.0	09. r	11.77					
NN B	10 42 08	+32 40.2	0.213	277.0		m	15.5 :						44.0	09. r	13.7 :					
Gl 400 A	10 42 30	+38 46.4	0.160	346.5	-3.2	dM2	9.30	+1.41 J	+1.20 J	+0.74 J	81.5	8.1	81.5	8.1	8.86	-2	8	-5		BD+39 2376
Gl 400 B	10 42 30	+38 46.4	0.160	346.5	-4.1		12.2 *				81.5	8.1	81.5	8.1	11.8 *	-2	8	-6		
NN	10 42 40	-60 57.2	1.657	348.1		m	13.92	1.82		+1.68C	222.8	13.6	222.8	13.6	15.66					
Gl 401 A	10 43 19	-18 50.5	1.980	250.5	36	M1	11.03	1.44	0.96	0.77	77.3	13.9	77.3	13.9	10.47	-77	-80	-60		BD-18 3019
Gl 401 B	10 43 19	-18 50.5	1.980	250.5		DQ9	16.5 P				77.3	13.9	77.3	13.9	15.9 P					
NN	10 43 27	+09 57.9	0.288	201.0		m	13.55			1.16			43.0	09. r	11.72					
NN	10 44 13	-24 19.2	0.146	233.8		K5 V	9.39	1.16	1.00	0.46			40.0	06. r	7.4				93380	CD-23 9524
NN	10 44 38	+21 45.7	0.397	260.0	35.3	K5	10.13	1.22	1.18	0.48	53.1	3.7	53.1	3.7	8.76	-41	-25	14		BD+22 2271
NN	10 45 41	-11 03.1	1.644	158.5	-7	M6.5	15.60	2.10		1.99	221.0	3.6	221.0	3.6	17.32	29	-11	-18		
NN	10 45 51	+19 25.0	0.246	109.0		m	13.45			1.14			42.0	08. r	11.57					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B−V	U−B	R−I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	10 46 29	+05 18.7	0.624	216.6		m	19.11				40.9	2.3	40.9	2.3	17.17					
GJ 1138	10 47 00	+35 49.5	1.231	213.2		m	13.02	1.66	1.15	1.31	102.4	3.7	102.4	3.7	13.07					
NN	10 47 30	-79 12.0	0.505	244.6		m	13.45			1.25			63.0	11. r	12.45					
NN	10 47 39	+33 22.3	0.629	171.1		m	13.07	1.52			42.0	3.3	42.0	3.3	11.19					
NN A	10 47 42	+52 03.9	0.203	267.5		G5	8.33						40.0	04. r	6.34				93811	BD+52 1514
NN B	10 47 40	+52 00.9	0.203	273.0		m	14.10			1.24			40.0	04. r	12.11					
Gl 402	10 48 19	+07 05.1	1.150	225.1	-0.9	SB dM5	11.65	1.67	1.16	1.25	145.1	4.8	145.1	4.8	12.46	-10	-28	-22		
NN	10 48 33	+36 23.4	0.182	265.0		m	13.46			1.16			45.0	09. r	11.73					
Gl 402.1	10 49 29	+00 06.5	0.262	168.5		dK8	10.20	0.90		0.37	46.8	15.3	46.8	15.3	8.6					BD+00 2709
Gl 403	10 49 30	+14 15.7	1.126	279.6		dM3	12.67	1.65	1.25	1.16	83.7	17.0	83.7	17.0	12.28					
NN	10 49 31	+00 48.6	0.287	273.0		m	13.85			1.28			60.0	10. r	12.74					
NN	10 49 41	+06 11.1	0.639	257.8		m	14.4 *			1.28			46.0	08. r	12.7 *					
Wo 9336	10 50 39	-20 21.5	0.314	210.7	-13.1	G3/5 V	7.05:	0.64	0.19		43.9	13.6	37.0	05. r	4.89:	1	-12	-41	94340	BD-19 3122
GJ 1139	10 50 40	+76 19.9	0.465	287.5	-24.4	K4	9.65:	1.10	1.02	0.48	56.1	10.7	35.0	06. r	7.37:	-37	-17	-54		BD+76 404
Gl 403.1	10 51 03	-19 52.1	0.255	162.6	-3.8	F6 V	5.23	0.46	0.06	+0.27C	52.3	18.8	51.0	08. r	3.77	18	-6	-15	94388	BD-19 3125
Gl 404	10 51 12	-44 08.7	0.265	270.9	6.4	F8 IV-V	8.09	0.52	-0.09	+0.32C	57.2	8.5	57.2	8.5	6.88	-18	-12	-8	94444	CP-43 4994
Gl 404.1	10 51 27	-58 35.2	0.074	70.2	8.1	K1 III	3.78	0.95	0.65	+0.46C	57.0	17.0	57.0	17.0	2.6	7	-6	4	94510	CP-58 2834
Wo 9340	10 51 50	-30 53.3	0.351	198.9	92.5	G2 V	8.35	0.60	0.02	0.22	41.7	11.9	41.7	11.9	6.5	16	-99	4	94518	CD-30 8807
Gl 405	10 52 53	+56 18.0	0.548	283.1		M1.5	12.72	1.53		0.96	61.4	11.9	61.4	11.9	11.66					
NN	10 53 05	-09 05.8	0.528	329.5		M4	13.54	1.63		1.19			50.0	13. r	12					
NN	10 53 55	+07 39.4	0.263	253.0		K0	7.34	0.92	0.66		37.9	11.9	63.0	08. r	6.34				94765	BD+08 2434
Gl 406	10 54 06	+07 19.2	4.696	234.6	13	M6	13.45v	2.00	+1.21:	1.84	418.3	2.5	418.3	2.5	16.56v	-26	-44	-19		
Gl 406.1	10 54 21	+69 51.8	0.638	275.3	7	dM0.5	10.28	1.40	1.35	0.65	41.4	8.7	41.4	8.7	8.37	-66	-12	-30		BD+70 639
GJ 1140	10 55 07	-07 15.4	0.816	274.0		DA6	14.31	0.32	-0.52		83.3	3.8	83.3	3.8	13.91					
Wo 9342	10 55 28	+48 33.6	0.100	145.0		dM0	10.52	1.37	1.28	0.58	53.6	6.0	53.6	6.0	9.17					BD+49 2004
NN	10 56 14	-30 52.5	0.531	261.4		m	11.95			1.01			56.0	11. r	10.69					
NN	10 56 24	+30 31.5	0.631	238.4		m	15.36	1.75			44.7	8.2	44.7	8.2	13.61					
Gl 407	10 56 40	+40 41.9	0.324	279.2	11.6	G0 V	5.05	0.61	0.13		71.9	13.1	71.9	13.1	4.33	-24	-3	1	95128	BD+41 2147
Gl 408	10 57 25	+23 06.3	0.465	239.9	3	M3	10.02	1.54	1.22	1.04	144.6	4.4	144.6	4.4	10.82	-9	-12	-4		
NN	10 58 12	+12 20.				M5 e	15.96			1.50			49.0	08. r	14.41					
NN	10 58 41	+03 16.8	1.103	112.3		m	14.07	1.73	1.27	1.28	71.9	3.1	71.9	3.1	13.35					
NN	10 58 47	+15 17.0	0.329	179.7	-56.4	G8	7.66	0.94	0.48		39.8	25.9	48.0	08. r	6.07	30	-7	-57	95486	BD+15 2276
Wo 9343	10 58 50	+56 39.1	0.086	69.8	-12.0	SB A1 V	2.37	-0.02	0.01		46.3	11.8	46.3	11.8	0.7	13	2	-8	95418	BD+57 1302
Gl 409	10 59 29	-17 41.2	0.020	207.0			11.87	0.61		+0.32C	55.5	8.5	55.5	8.5	10.59					
GJ 1141 A	10 59 38	+16 47.4	0.196	152.0		dM0	11.51	1.48		0.85	68.4	7.3	68.4	7.3	10.69					
GJ 1141 B	10 59 38	+16 47.4	0.196	152.0		dM0	11.63	1.48		0.88	68.4	7.3	68.4	7.3	10.81					
Gl 410	10 59 57	+22 14.2	0.152	112.8	-13.9	dM2 e	9.60	1.48	1.19	0.77	90.9	6.3	90.9	6.3	9.39	12	3	-10	95650	BD+22 2302
NN	11 00 24	+36 55.3	0.185	280.0		m	13.67			1.22			51.0	09. r	12.21					
Gl 411	11 00 37	+36 18.3	4.807	186.8	-84.3	M2 Ve	7.48	1.51	1.12	0.92	397.3	1.8	397.3	1.8	10.48	46	-53	-74	95735	BD+36 2147
NN	11 01 29	+40 16.5	0.229	248.0		K5	10.74	1.40	1.23				44.0	21. r	9					
NN	11 02 43	+45 16.9	0.270	139.0		m	11.11	1.48	1.29	0.76			42.0	07. r	9.23					
NN A	11 02 55	-27 01.4	0.190	267.4	19.1	F3 IV J	5.63	+0.37 J	+0.04 J		40.3	11.9	40.3	11.9	3.7	-17	-24	0	96202	CD-26 8338

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 412 A	11 03 00	+43 47.0	4.528	282.1	68.8	M2 Ve	8.74	1.54	1.18	0.81	188.8	6.1	188.8	6.1	10.12	-132	-6	12		BD+44 2051
Gl 412 B	11 03 02	+43 46.7	4.531	281.9		M6 e	14.40v	+2.09v		1.80	188.8	6.1	188.8	6.1	15.78v					
NN	11 03 04	+10 31.0	0.919	139.1		M3.5	12.4 *			1.06			55.0	11. r	11.1 *					
Gl 412.1	11 04 29	-62 09.2	0.041	281.3	-2	G8 III	4.62	1.03	0.82	0.33	53.7	11.9	53.7	11.9	3.27	-4	1	-1	96566	CP-61 2067
Gl 412.2	11 05 31	-29 54.1	0.526	254.8	12.7	G2 V	6.54	0.60	0.08	0.21	49.5	9.0	49.5	9.0	5.01	-34	-31	-23	96700	CD-29 8875
GJ 1142 A	11 05 34	-04 57.2	0.422	184.0		dM6	12.56	1.52	+1.25:	1.08	20.6	13.0	50.0	10. r	11.05					
GJ 1142 B	11 05 28	-04 52.9	0.422	184.0	15.4	DA3	12.92	+0.05:	-0.69	-0.12	20.6	13.0	50.0	10. r	11.41	20	-9	-44		
Gl 412.3	11 05 43	-27 59.8	0.496	267.0	14.9	K7 V	9.33	1.25	1.18	0.54	48.4	21.8	54.0	09. r	7.99	-35	-28	-11		CD-27 7881
NN	11 07 07	+02 43.6	0.283	276.5	7.7	G5	7.68	0.78	0.40				40.0	05. r	5.69	-32	-12	-5	96937	BD+03 2466
Gl 413.1	11 07 07	-24 19.3	0.911	240.5	-5	M3	10.44	1.53	+1.1 :	0.96	102.1	8.4	102.1	8.4	10.49	-22	-17	-32		CD-23 9765
Wo 9350	11 07 20	-42 11.2	0.396	132.0	8	K1	9.74	0.78	0.35		40.5	15.3	40.5	15.3	7.8	45	-1	-12		CD-41 6367
NN	11 07 26	-10 00.9				M0 V	10.54	1.40	1.27	0.64			41.0	08. r	8.6					BD-09 3222
NN	11 08 03	+48 13.7	0.586	210.6		m	14.52			1.29			46.0	08. r	12.83					
Gl 414 A	11 08 20	+30 43.2	0.614	109.8	-15.4	K8 V	8.33	1.34	1.29	0.59	73.2	3.9	73.2	3.9	7.65	43	2	0	97101	BD+31 2240
Gl 414 B	11 08 18	+30 43.2	0.618	110.2	-15	M2 V	9.98	1.52	1.15	0.92	73.2	3.9	73.2	3.9	9.3	43	1	1		BD+31 2238
Gl 414.1A	11 08 35	+43 41.7	0.766	236.9	-10.5	M3	11.47	+1.49 c		+1.05 J	61.0	3.0	61.0	3.0	10.4	-30	-48	-21		
Gl 414.1B	11 08 35	+43 41.7	0.766	236.9	-19	M3	11.82	+1.54 c			61.0	3.0	61.0	3.0	10.75	-27	-49	-29		
Gl 415	11 08 43	-10 41.2	1.067	302.4	40	K4	9.24	1.10	0.92	0.48	51.0	11.9	43.0	07. r	7.41	-119	-22	29	97214	BD-10 3216
Gl 416	11 09 01	-14 42.7	0.925	129.3	-9.8 VAR	K4 V	9.05	1.21	1.08	0.54	54.8	8.4	54.8	8.4	7.74	79	-1	-16	97233	BD-14 3277
NN	11 09 09	+33 48.4	0.203	299.0		dM4	12.38			1.19			82.0	16. r	11.95					
Gl 416.1	11 09 12	-22 33.1	0.105	179.9	6.4	A2 III	4.48	0.03	0.06	+0.01C	52.3	14.3	52.3	14.3	3.1	5	-10	-3	97277	BD-22 3095
NN	11 09 33	-25 51.8	0.279	105.0	56.7	G8/K0 V	7.05	0.77	0.38		24.0	11.9	45.0	04. s	5.32	34	-42	34	97343	BD-25 8519
Gl 417	11 09 49	+36 05.3	0.302	236.6	-3.2	G0 V	6.41	0.61	0.10				44.0	07. r	4.63	-17	-26	-11	97334	BD+36 2162
NN	11 10 00	+19 12.4				M1	10.77	1.50	1.19	0.88			68.0	12. r	9.93					
Gl 418	11 10 39	+04 45.3	0.320	261.7	20.8	K5 V	8.69	1.18	1.12	0.46			56.0	09. r	7.43	-25	-23	6	97503	BD+05 2463
NN	11 10 40	+00 30.7	0.471	240.0		K7	10.24	1.46	1.24		38.0	17.0	50.0	15. r	8.7					
Gl 419	11 11 27	+20 47.9	0.196	133.4	-20.2	A4 V	2.56	0.12	0.12		45.6	17.3	45.6	17.3	0.9	24	-2	-15	97603	BD+21 2298
NN	11 11 53	+25 58.9	0.117	292.2	2	K1 V	7.76	0.84	0.44				44.0	07. r	5.98	-13	0	-2	97658	BD+26 2184
Gl 420 A	11 11 57	+73 44.8	0.417	284.9	8.1	dK5	7.68	1.06	0.92	0.40	81.6	9.7	81.6	9.7	7.24	-24	1	-7	97584	BD+74 456
Gl 420 B	11 11 57	+73 44.8	0.417	284.9	8.6	M2	11.4 *				81.6	9.7	81.6	9.7	11.0 *	-25	2	-7		
GJ 1143 A	11 12 21	-22 49.6	0.450	215.3		K4 V	8.98	1.14	+1.02:	0.51			51.0	08. r	7.52				97782	BD-22 3102
GJ 1143 B	11 12 21	-22 49.6	0.450	215.3			13.5 *						51.0	08. r	12.0 *					
NN	11 12 33	+19 44.0	0.476	162.6		m	12.89	1.58	1.18	1.16			57.0	11. r	11.67					
Gl 421 A	11 12 50	-17 51.7	0.754	169.3	5	K7 V	9.97	1.36	1.21	0.60	63.6	4.8	63.6	4.8	8.99	37	-30	-31		BD-17 3336
Gl 421 B	11 12 51	-17 51.6	0.754	169.3	+18.0 SB	K7 V	10.04	1.38	1.21	0.61	63.6	4.8	63.6	4.8	9.06	37	-40	-23		BD-17 3337
Gl 421 C	11 12 46	-17 50.6	0.754	169.3	18	M3.5	13.64	1.58	1.05	1.16	63.6	4.8	63.6	4.8	12.66	37	-40	-23		
NN	11 13 01	+55 36.2				M0	11.22	1.41	1.06	0.79			42.0	07. r	9.34					
Gl 421.1A	11 13 12	+53 02.7	0.171	72.6	-42.1	F6 V	6.50	0.43	-0.12		54.1	10.2	26.0	03. s	3.57	43	8	-29	97855	BD+53 1480
Gl 421.1B	11 13 12	+53 02.9	0.191	73.6	-42.4	F9 V	8.03	0.60	-0.04		54.1	10.2	26.0	03. s	5.1	46	10	-28		
GJ 1144	11 13 52	-14 25.1	0.227	245.0		K7 V	10.00	1.40	1.20	0.66			53.0	11. r	8.62					BD-13 3333
Gl 422	11 14 03	-57 17.5	2.733	294.9	-72	m	11.65	1.47	0.92	1.10	76.7	14.2	76.7	14.2	11.07	-183	9	8		
NN	11 14 13	-27 40.3	0.951	211.7		M4	13.7 *			1.28			64.0	11. r	12.7 *					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
GJ 1145	11 14 40	-27 32.4	0.186	122.5		M0 V	9.79	1.40	1.21	0.64			58.0	12. r	8.61					CD-27 7978
Wo 9356	11 14 42	-01 42.5	0.567	268.1	4	dK6	9.78	1.17	1.18	0.44	47.5	9.1	32.0	04. r	7.31	-72	-33	-28		BD-01 2505
Gl 423 A	11 15 31	+31 48.6	0.727	216.2	-15.9 SB	G0 Ve	4.33	+0.59 J	+0.04 J	+0.22tJ	130.5	22.3	96.0	13. r	4.24	-3	-33	-21	98231	BD+32 2132
Gl 423 B	11 15 31	+31 48.6	0.727	216.2	-13.6 SB	G0 Ve	4.8 *				130.5	22.3	96.0	13. r	4.7 *	-3	-33	-19	98230	
Gl 423.1	11 15 47	-04 47.5	0.810	101.4	13.1	G8 V	7.29	0.73	0.28	0.28	51.6	9.7	44.0	07. r	5.51	82	9	31	98281	BD-04 3049
Gl 424	11 17 29	+66 07.0	2.961	273.6	60	M1 V	9.31	1.41	1.08	0.75	114.0	3.5	114.0	3.5	9.59	-137	-10	-2		BD+66 717
Gl 425 A	11 18 57	-20 10.7	0.233	126.6	7.4	K4/5 V J	8.74	+1.36 J	+1.20 J	0.58	63.5	8.2	63.5	8.2	7.75	18	-6	2	98712	BD-19 3242
Gl 425 B	11 18 57	-20 10.7	0.233	126.6		m	11.0 *				63.5	8.2	63.5	8.2	10.0 *					
GJ 1146	11 19 06	+06 26.1	1.749	206.0		k-m	13.58	1.64	+1.27?	1.09	54.0	4.2	54.0	4.2	12.24					
Gl 426 A	11 19 12	+18 27.9	0.183	235.4	-4.1	K0	8.03	+0.89 J	+0.64 J		26.2	32.2	40.0	06. r	6.04	-9	-16	-12	98736	BD+19 2443
Gl 426 B	11 19 12	+18 27.9	0.183	235.4		K7	10.7 *				26.2	32.2	40.0	06. r	8.7 *					
NN	11 19 20	-12 56.6	0.515	261.0	30	M8	19.57				70.2	2.1	70.2	2.1	18.8	-27	-37	6		
NN	11 19 21	+47 11.1	0.265	232.4		K6	9.80			0.53			43.0	06. r	7.97					BD+47 1863
GJ 2084 A	11 19 37	-24 30.2	0.089	249.6		K4 V J	9.08	1.26	1.07	0.62			68.0	12. r	8.24				98800	CD-24 9706
NN	11 20 33	+26 10.4	1.059	252.0		m	15.14	1.84			57.7	5.5	57.7	5.5	13.95					
NN	11 20 37	+45 05.2	0.315	248.0		m	12.74			1.03			41.0	08. r	10.8					
GJ 2085	11 21 13	+08 50.1	1.036	278.4	58	dM1	11.18	1.48	1.14	0.82	39.4	14.5	48.0	09. r	9.59	-104	-50	23		
NN	11 21 29	-18 05.3	0.616	266.7		M3	13.05			1.22			60.0	13. r	11.94					
Gl 427	11 21 39	+21 38.1	1.050	270.2	51	DA7	14.24	0.28	-0.53		74.2	3.0	74.2	3.0	13.59	-60	-26	-17		
NN A	11 22 13	+78 32.6	0.678	248.9		M2.5	12.15			0.97			44.0	06. r	10.37					
NN B	11 22 01	+78 33.7	0.678	248.9		M3	12.65			1.01			44.0	06. r	10.87					
NN	11 22 18	+40 16.7	0.122	254.0	4	dM0	10.33	1.36	1.25	0.64	26.2	15.3	44.0	09. r	8.55	-11	-8	0		
Gl 428 A	11 22 29	-61 22.4	0.490	277.1	4.7	K7 V	7.50	+1.26 J	+1.18 J	+0.54 J	90.9	8.6	90.9	8.6	7.29	-21	-14	-5	99279	CP-60 2911
Gl 428 B	11 22 29	-61 22.4	0.490	277.1	4.5	M0 Ve	8.3 *				90.9	8.6	90.9	8.6	8.1 *	-21	-14	-5		
NN	11 23 33	-63 41.8	0.318	257.3	-5.0 SB	F7 V +F7V	5.17	0.50	0.02		40.9	5.7	40.9	5.7	3.23	-31	-7	-19	99453	CP-63 1893
Gl 429 A	11 24 13	+03 17.1	0.747	283.6	3.8	K0 IV	6.50	0.80	0.48	0.24	60.4	6.4	60.4	6.4	5.41	-57	-12	-9	99491	BD+03 2502
Gl 429 B	11 24 14	+03 16.7	0.745	284.7	1.7	K2 IV-V	7.58	1.00	0.92	0.34	60.4	6.4	60.4	6.4	6.49	-57	-10	-11	99492	BD+03 2503
NN	11 25 04	+04 15.2	0.095	288.0		dM0	10.68	1.42		0.69	27.8	6.0	43.0	07. r	8.85					BD+ 4 2470
Gl 429.2	11 25 26	-08 53.7	0.994	148.6		M2	12.37	1.46	1.02	0.84	41.8	5.3	41.8	5.3	10.48					
NN	11 26 08	+48 30.3	0.074	327.7		G5	7.89						43.0	05. o	6.06				99748	BD+49 2059
NN	11 26 23	+10 26.8	0.929	306.5		M3	12.56	1.60	1.14	1.20	63.8	8.5	63.8	8.5	11.58					
NN	11 26 42	+18 33.2				DC8	13.79						114.0	13. w	14.07					
Gl 429.3	11 27 28	-51 23.3	0.358	283.4	+7. VAR	F6 V	7.38	0.41	-0.08		51.1	10.2	51.1	10.2	5.92	-28	-18	-2	100004	CD-50 6060
Gl 429.4	11 28 18	-56 51.5	0.557	272.7	-2.7	K4 Ve	8.33	1.06	0.99	0.37	47.2	8.4	50.0	07. r	6.82	-48	-18	-14	304391	CP-56 4554
Gl 430	11 28 22	+63 26.0	0.060	81.0	-6	dM0	10.02	1.33	1.26	0.61	35.1	11.9	48.0	09. r	8.43	8	0	-3		BD+63 965
NN	11 28 35	-14 39.6	1.393	164.0		m	14.29	1.81		1.40			78.0	11. r	13.75					
Gl 430.1	11 29 08	+22 56.5	0.580	270.0	-5.1	dM1 e	10.30	1.48	1.22	0.81	56.7	13.6	56.7	13.6	9.1	-41	-17	-20		BD+23 2359
NN A	11 29 10	+14 38.6	0.383	240.1	-4.2	G0 V	6.20	0.57	0.07		21.6	7.5	41.0	04. s	4.26	-23	-32	-21	100180	BD+15 2345
NN B	11 29 10	+14 38.6	0.383	240.1	-10.3	K6 IV	9.22	1.14	1.03		21.6	7.5	41.0	04. s	7.28	-22	-30	-26		
Gl 431	11 29 23	-40 46.3	0.717	290.1	-78	M3.5	11.52	1.54	0.97	1.16	94.3	12.1	94.3	12.1	11.39	-56	60	-25		
Gl 431.1A	11 29 32	+61 21.6	0.076	180.5	-47.9	F6 V	5.74	+0.50 J	-0.01 J		43.9	5.2	43.9	5.2	3.95	23	-26	-34	100203	BD+61 1246
Gl 431.1B	11 29 32	+61 21.6	0.076	180.5		G3 V	7.1 *				43.9	5.2	43.9	5.2	5.3 *					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Wo 9367	11 31 48	+03 20.3	0.214	239.6	3	F6 V	5.77	0.46	0.01		44.0	11.9	38.0	05. r	3.67	-14	-21	-10	100563	BD+03 2521
Gl 432 A	11 32 03	-32 34.0	1.061	320.8	-22.6	K0 V	5.98	0.81	0.39	0.29	101.7	11.5	101.7	11.5	6.02	-49	20	13	100623	CD-32 8179
Gl 432 B	11 32 04	-32 34.1	1.061	320.8		m	15. *				101.7	11.5	101.7	11.5	15. *					
NN	11 32 09	-23 35.6	0.681	245.9		M1	11.17	1.53		0.80	29.5	18.8	47.0	09. r	9.53					CD-23 10062
NN	11 32 33	-05 22.0	0.994	161.6		m	15.1 *			1.44			60.0	09. r	14.0 *					
NN	11 32 55	+39 12.3	0.701	252.3		m	13.11			1.19			59.0	11. r	11.96					
Gl 433	11 32 58	-32 15.1	0.831	185.1	28	M2 V	9.83	1.51	1.17	0.90	90.5	13.8	90.5	13.8	9.61	22	-40	-24		CD-31 9113
NN	11 34 00	+39 28.3	0.588	131.9	-42	K5	10.03	1.35	1.27	0.60	34.1	15.3	45.0	09. r	8.3	69	-22	-19		BD+40 2442
Gl 433.1	11 34 28	+30 04.6	0.150	262.0		DA3	12.50	-0.06	-0.98				45.0	05. w	10.77					
NN	11 34 43	+82 05.2	0.429	90.0		m	11.77	1.50					50.0	24. r	10.3					
NN	11 34 55	+58 59.5	0.370	240.0		m	12.57			1.01			42.0	08. r	10.69					
GJ 1147	11 36 03	-41 05.6	0.961	274.5	28	k	13.79	1.72	1.20	1.21			50.0	09. r	12.28	-74	-60	-9		
Gl 433.2A	11 36 07	+45 23.1	0.600	271.3	-17.3	G0 V	6.45	0.57	-0.02		49.9	9.0	40.0	04. r	4.46	-56	-29	-36	101177	BD+45 1947
Gl 433.2B	11 36 06	+45 23.1	0.581	268.8	-18.9	SB K2 V	8.40	0.96	0.72		49.9	9.0	40.0	04. r	6.41	-53	-31	-36		
NN A	11 36 08	-12 55.6	0.135	36.4	-23.8	F7 V	5.48	0.52					51.0	06. r	4.02	0	25	-9	101198	BD-12 3466
NN	11 36 21	+42 36.0	0.454	343.2	+14.8	SB K5 V	8.26	0.96	0.82		17.9	22.2	50.0	08. r	6.75	-30	34	1	101206	BD+43 2135
NN	11 36 29	-24 26.4	0.248	172.8	96.7	G6/8 V	6.41	0.82	0.32				75.0	10. r	5.79	26	-83	44	101259	CD-24 9867
Gl 434	11 38 25	+34 29.0	0.386	181.9	-5.9	G8 Ve	5.33	0.72	0.25	0.27	116.0	5.0	116.0	5.0	5.65	7	-15	-4	101501	BD+35 2270
Gl 435	11 38 37	-44 07.9	0.695	289.4	13.3	K5 Ve	7.77	1.06	0.90	0.42	79.8	8.5	79.8	8.5	7.28	-35	-25	6	101581	CD-43 7228
NN	11 38 39	-28 55.3	0.382	302.8	-12.1	G0 V	6.44	0.66	0.19		31.7	4.9	31.7	4.9	3.95	-58	3	6	101563	CD-28 9027
GJ 1148	11 39 09	+43 01.8	0.612	258.8		M3.5	11.90	1.52	1.13	1.23	89.1	4.8	89.1	4.8	11.65					
Gl 435.1	11 39 14	+05 25.5	0.446	152.3	19	K5	9.60	1.25	1.20	0.52	47.3	11.9	45.0	08. r	7.87	38	-33	7		BD+05 2529
NN	11 39 28	+15 03.0	0.370	312.0		M3.5	12.58	+1.48S	1.24				60.0	24. r	11.5					
Gl 436	11 39 31	+26 59.8	1.080	135.5	9.7	dM3.5	10.67	1.52	1.23	1.01	98.8	2.9	98.8	2.9	10.64	45	-20	18		
NN	11 40 48	+25 34.9	0.204	256.0		m	13.83			1.25			53.0	10. r	12.45					
Gl 438	11 40 49	-51 33.3	0.860	128.6	0.5	K0	10.36	1.53	1.19	+1.08C	119.0	10.2	119.0	10.2	10.74	30	9	-13		CP-51 4413
NN	11 41 04	-57 44.0	0.353	3.5		K1 V	8.21	0.91			29.2	13.6	41.0	05. r	6.27				101930	CP-57 4948
Gl 439	11 42 04	+31 14.5	0.386	184.2	28.6	dK8	8.96	1.13	1.06	0.42			44.0	05. r	7.18	7	-41	29		BD+31 2290
Gl 440	11 42 58	-64 33.5	2.667	97.2		DQ6	11.50:	0.19	-0.63	0.06	218.5	5.0	218.5	5.0	13.20:					
GJ 1149	11 43 03	+63 22.9	0.381	202.0		DC9	16.39	0.66	+0.20?				47.0	05. w	14.75					
Gl 441	11 43 08	+72 22.3	0.050	9.5	-25.1	dK8	9.02	1.17	1.12	0.46	47.7	13.8	48.0	06. r	7.43	12	-10	-21		BD+72 545
Gl 443	11 44 08	-13 43.6	1.035	132.6	-128	M3	11.69	1.48	1.05	1.07	82.0	11.9	82.0	11.9	11.26	42	82	-107		
Gl 442 A	11 44 08	-40 13.7	1.587	284.4	15.3	G5 V	4.90	0.66	0.10	0.22	97.1	9.0	97.1	9.0	4.84	-68	-40	4	102365	CD-39 7301
Gl 442 B	11 44 09	-40 13.4	1.592	284.4			15. *				97.1	9.0	97.1	9.0	15. *					
NN	11 44 23	+70 18.7	0.365	263.0		m	13.60			1.25			59.0	11. r	12.45					
GJ 1150	11 44 23	+51 15.4	0.120	138.0	1.8	dM0 p	9.62	1.26	1.19	0.52			45.0	06. r	7.89	10	-4	7		BD+51 1697
Gl 444 A	11 44 32	-11 32.7	0.210	254.8	23	dK8	9.02	1.12	1.09	0.45			45.0	05. r	7.29	-14	-28	8	102392	BD-11 3178
Gl 444 B	11 44 32	-11 32.7	0.210	254.8			14.2 *						45.0	05. r	12.5 *					
Gl 445	11 44 35	+78 57.7	0.863	55.5	-112.2	sdM4	10.80	1.60	+1.08?	1.19	191.5	5.3	191.5	5.3	12.21	67	-56	-74		
Gl 446	11 44 45	-30 00.3	0.353	229.4	11.8	G5 V	6.48	0.68	0.20	0.24	62.9	13.6	54.0	08. r	5.14	-9	-27	-16	102438	CD-29 9337
NN A	11 45 08	+00 32.0	0.303	253.0		m	13.25			1.23			64.0	12. r	12.28					
NN B	11 45 09	+00 31.8	0.303	253.0		m	17.6 P						64.0	12. r	16.6 P					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 447	11 45 09	+01 06.0	1.348	152.0	-31.1	dM4.5	11.12	1.75	+1.40:	1.33	301.1	1.9	301.1	1.9	13.51	18	6	-33		
NN	11 45 33	-34 56.8	0.165	247.5	-0.1	G5/6 V	7.09	0.77	0.23				49.0	07. r	5.54	-11	-8	-9	102540	CD-34 7692
NN	11 45 49	-11 00.5	0.836	268.9		k	12.90	1.46	1.16	1.10			44.0	09. r	11.12					
Gl 448	11 46 31	+14 51.1	0.511	256.5	-0.2	A3 V	2.14	0.09	0.07	0.00	78.9	9.1	78.9	9.1	1.63	-23	-19	-9	102647	BD+15 2383
Gl 449	11 48 05	+02 02.8	0.789	110.4	+4.3	SB? F9 V	3.61	0.55	0.11	0.16	98.8	4.3	98.8	4.3	3.58	37	3	6	102870	BD+02 2489
GJ 1151	11 48 29	+48 40.1	1.821	237.5	-34	m	13.25	1.84	1.30	1.38	121.8	3.0	121.8	3.0	13.68	-28	-66	-32		
Gl 450	11 48 33	+35 32.8	0.350	321.0	+0.5	SB? M1 Ve	9.73	1.51	1.20	0.88	123.5	13.3	123.5	13.3	10.19	-12	6	-3		BD+36 2219
GJ 1152	11 49 02	+35 28.1	0.110	255.7	-9.3	G7 IV	9.64	0.78			44.6	14.6	44.6	14.6	7.9	-6	-8	-11		BD+35 2288
NN A	11 49 48	+10 13.5	0.356	286.1	10.7	K0	7.54	1.06	0.90	0.36	18.2	20.5	63.0	11. r	6.54	-27	-9	6	103112	BD+10 2347
NN B	11 49 45	+10 17.6	0.340	289.0		m	15. *				18.2	20.5	63.0	11. r	14. *					
Gl 451 A	11 50 06	+38 04.7	7.053	145.4	-99.1	G8 VI	6.45	0.75	0.17	0.29	116.0	4.2	116.0	4.2	6.77	265	-149	-18	103095	BD+38 2285
Gl 451 B	11 50 06	+38 04.7	7.053	145.4			12. *				116.0	4.2	116.0	4.2	12. *					
NN	11 50 24	+24 45.3	0.298	282.0		m	14.60			1.34			54.0	08. r	13.26					
Gl 452 A	11 50 43	-07 05.3	0.538	198.3	26.7	M3	11.87	1.54		1.04	82.2	8.5	82.2	8.5	11.44	8	-40	2		
Gl 452 B	11 50 44	-07 05.4	0.538	198.3		f	19.4 P				82.2	8.5	82.2	8.5	19.0 P					
NN	11 50 45	-31 07.1	1.140	263.1		M4	13.61	1.70	1.11	1.24			60.0	14. r	12.5					
NN	11 51 18	+07 17.3	0.955	159.8	-60	M6 :	17.89	1.72			70.6	2.6	70.6	2.6	17.13	50	-14	-71		
Gl 452.1	11 51 34	+10 05.7	0.785	173.9		M3.5	12.77	1.69	1.25	1.15	96.1	19.3	96.1	19.3	12.68					
Wo 9376	11 51 54	-51 06.7	0.340	314.0		G5	10.97	0.92	0.66	0.34	39.0	8.5	39.0	8.5	8.93					CD-50 6462
Gl 452.2A	11 51 55	-37 28.3	0.316	280.8	-11.5	F7 V	6.75	+0.52 J	-0.04 J	+0.30CJ	50.9	13.6	28.0	03. r	3.99	-53	-10	-7	103437	CD-37 7536
Gl 452.2B	11 51 55	-37 28.3	0.316	280.8			8.1 *				50.9	13.6	28.0	03. r	5.3 *					
Gl 452.3A	11 51 59	+19 41.4	0.445	267.9	5.9	dG6	8.22	0.71	0.21		51.6	14.3	26.0	03. r	5.29	-70	-39	-12	103432	BD+20 2658
Gl 452.3B	11 52 02	+19 42.4	0.444	268.4	5.7	dG7	8.43	0.76	0.27		51.6	14.3	26.0	03. r	5.5	-70	-38	-12	103431	BD+20 2659
Gl 452.4	11 52 22	+29 01.2	0.361	145.0	-7	M0 Ve	10.52	1.39	1.32	0.64			42.0	08. r	8.64	37	-19	-1		BD+29 2228
Gl 452.5A	11 52 29	-55 48.9	0.299	131.8	51.1	G5 V	7.29	+0.64 J	+0.12:J	+0.36CJ	44.3	11.9	33.0	06. r	4.88	56	-32	-16	103493	CP-55 4711
Gl 452.5B	11 52 29	-55 48.9	0.299	131.8	55.7		7.7 *				44.3	11.9	33.0	06. r	5.3 *	58	-36	-15		
Wo 9381	11 52 36	+01 15.1	0.741	272.4		M1.5	11.50	1.44		0.89	38.4	15.3	48.0	10. r	9.91					
NN	11 53 09	-18 37.6	0.602	120.6		m	14.3 *			1.26			45.0	08. r	12.6 *					
NN	11 55 01	+12 06.2	0.729	288.0		M2.5	11.86	1.45	1.15	0.93	27.5	21.8	48.0	11. r	10.27					
Gl 453	11 55 27	-27 25.2	1.246	240.1	+49.9	SB K5 V	6.98	1.15	1.10	0.42	101.9	9.4	101.9	9.4	7.02	-19	-74	-6	103932	CD-26 8883
NN	11 55 43	+42 51.5	0.405	161.0		m	14.08			1.29			56.0	10. r	12.82					
NN	11 56 27	+42 56.3	0.326	285.0		m	12.07			0.93			42.0	08. r	10.19					
GJ 1153	11 56 36	-20 04.2	0.454	161.7	-12	K2 V	7.94	0.98	0.77	0.34			50.0	07. r	6.43	27	-7	-35	104067	BD-19 3382
NN A	11 58 09	-13 32.5	0.487	268.8		M3	12.74	1.55		1.17			58.0	14. r	11.6					
NN B	11 58 08	-13 32.5	0.487	268.8		m	15. *						58.0	14. r	14. *					
Gl 454	11 58 10	-10 09.7	0.501	168.1	0.1	K0 IV	5.55	0.77	0.44	0.25	78.2	6.6	78.2	6.6	5.02	19	-16	-17	104304	BD-09 3413
Gl 454.1	11 58 35	-01 27.4	0.508	295.2		K4	10.96	1.12	0.98	0.44	47.2	13.6	47.2	13.6	9.3					
NN	11 59 07	-11 57.0	0.253	199.0		M5-6	12.34	1.46		1.05			50.0	10. r	10.83					
Gl 454.2A	11 59 13	-34 22.3	0.191	272.1	-4	G0 V J	7.35	+0.59 J	+0.08 J	+0.30CJ	45.5	15.3	27.0	05. r	4.51	-31	-11	-7	104471	CD-33 8130
Gl 454.2B	11 59 13	-34 22.3	0.191	272.1			8.1 *				45.5	15.3	27.0	05. r	5.3 *					
Gl 454.3	11 59 47	+43 25.1	0.017	253.0	5.5	K0 V	8.38	1.15	1.10				46.0	15. r	6.7	-3	0	5	104526	BD+43 2180
Gl 455	11 59 48	+28 52.0	0.791	268.3		M3	12.84	1.75		1.12	49.3	3.7	49.3	3.7	11.3					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	12 01 04	-42 08.7	0.349	111.0	38.9	F6 V	5.15	0.41	-0.03		37.1	10.3	37.1	10.3	3	56	-18	6	104731	CD-41 6938
NN	12 01 27	-32 44.8	0.763	275.4		M4.5	14.0 *			1.30			62.0	10. r	13.0 *					
NN	12 02 40	+09 00.6	0.226	280.8	-32.2	G8 IIIa CN	4.13	0.98	0.63	0.49	40.4	6.5	40.4	6.5	2.16	-25	4	-33	104979	BD+09 2583
NN	12 03 03	+69 49.1	0.479	262.0		M4	13.07			1.25			76.0	14. r	12.47					
Gl 455.1	12 03 17	-18 35.4	0.297	163.0		K5 V	9.99	1.34	1.20	0.60			42.0	09. r	8.11				105065	BD-18 3319
Gl 455.2	12 04 15	-64 20.1	0.057	137.9	+9.0 SB	F2 III	4.15	0.34	0.02	+0.20CJ	51.6	10.2	51.6	10.2	2.71	8	-6	-4	105211	CP-63 2145
Gl 455.3	12 05 50	-24 27.0	0.099	116.4	+2.9 SB	F2 III-IV	4.02	0.32	-0.02	+0.20CJ	70.7	11.3	70.7	11.3	3.27	7	-1	0	105452	CD-24 10174
Gl 456	12 05 52	-00 12.2	0.969	265.0	4.9	dM2	11.24	1.41	1.18	0.70	69.1	11.6	69.1	11.6	10.44	-54	-37	-9		
Wo 9390 A	12 06 53	-11 34.6	0.355	118.8	+4. SB	G2 V	6.81	+0.66 J	+0.19 J		43.3	8.8	44.0	07. r	5.03	38	1	-3	105590	BD-11 3246
Wo 9390 B	12 06 55	-11 34.5	0.355	118.8	2.8	K5	9.2 *				43.3	8.8	44.0	07. r	7.4 *	38	2	-4		
NN	12 07 01	-03 16.5				DA4	13.5 :						47.0	09. w	11.9 :					
NN	12 07 07	+40 31.9	0.321	259.6	0.6	K0 V	7.47	0.79	0.43		32.9	11.0	46.0	07. r	5.78	-26	-20	-3	105631	BD+41 2276
Gl 456.1A	12 07 20	-45 55.7	0.382	255.9	-4.2	K5 V	8.45	1.14	1.07	+0.54C	48.3	15.3	52.0	07. r	7.03	-29	-14	-15	105671	CP-45 5806
Gl 456.1B	12 07 23	-45 54.8	0.390	258.0		m	13.25	1.56		+1.48C	48.3	15.3	52.0	07. r	11.83					
NN	12 07 31	-14 47.0	0.720	184.0		m	12.06	1.58	1.09	1.24			112.0	21. r	12.31					
Wo 9393	12 08 26	+41 20.0	0.229	355.7		M2 V	10.67	1.35		0.69			44.0	09. r	8.89					
NN A	12 08 38	-19 40.8	0.255	231.0		M2:	11.68	1.59		1.08			74.0	10. r	11.03					
NN B	12 08 43	-19 41.5	0.255	231.0		m	12.62	1.68		1.16			74.0	10. r	11.97					
NN	12 08 58	+57 41.1	0.540	130.4		DA9	15.79	0.58	-0.20		49.4	4.6	49.4	4.6	14.26					
NN A	12 08 59	+53 42.1	0.222	232.1	4.3	K2	8.03	0.88	0.56		19.3	9.8	44.0	06. r	6.25	-12	-20	7	105963	BD+54 1499
NN B	12 08 58	+53 41.9	0.220	231.9	-4	K3	8.23:				19.3	9.8	44.0	06. r	6.45:	-10	-22	0		
Wo 9394	12 09 29	+13 32.7	0.495	207.7	95	F6 V-VI	10.18	0.47	-0.18	0.20	41.4	20.5	41.4	20.5	8.3	1	-81	75	106038	BD+14 2481
Gl 457	12 09 36	+59 12.3	0.093	90.6	-15	dM0	10.04	1.28	1.23	0.56	44.7	6.0	44.7	6.0	8.29	14	-1	-11	238087	BD+59 1428
NN	12 09 40	+49 06.0	0.360	143.0		m	12.91			1.09			45.0	09. r	11.18					
Gl 458 A	12 09 50	+54 45.7	0.244	70.3	-17.6	dM1.5	9.79	1.43	1.16	0.73	75.1	10.2	75.1	10.2	9.17	17	5	-16	238090	BD+55 1519
Gl 458 B	12 09 51	+54 45.9	0.244	70.3		m	13.33	1.61		1.20	75.1	10.2	75.1	10.2	12.71					
Wo 9395	12 09 52	-06 04.7	0.410	221.0		K3	9.96	1.00	0.80	+0.52C	39.2	15.3	23.0	04. r	6.77				106092	BD-05 3450
NN	12 09 57	+39 57.3	0.239	130.0		M2 V	11.41	1.51		0.88			50.0	12. r	9.9					
Gl 458.1A	12 09 57	-02 48.7	0.725	303.7	14.3	G4 V	7.43	0.71	0.25	0.22	46.5	8.5	46.5	8.5	5.77	-71	-7	24	106116	BD-02 3481
NN	12 10 24	+10 19.2	0.412	149.4	-8.8	G8 V	7.92	0.79	0.45		40.6	46.0	36.0	06. r	5.7	47	-22	-18	106156	BD+10 2391
Wo 9397	12 10 50	+16 58.7	0.669	228.5		M1.5	11.96	1.45		0.83	40.1	13.1	35.0	07. r	9.68					
NN	12 10 53	+10 32.4	0.094	261.4	2.3	A2 m	5.85	0.27	0.11		147.5	69.9	147.5	69.9	6.7	-2	-3	2	106251	BD+11 2440
GJ 1154 A	12 11 46	+00 54.2	0.985	253.0		m	13.73	+1.77 J	+1.02 J	+1.42 J	118.2	3.9	118.2	3.9	14.09					
NN	12 11 54	+24 52.4	0.363	175.0		m	12.16	1.48	1.12	0.94			41.0	08. r	10.22					
Gl 458.2	12 12 41	+49 00.7	0.230	257.0	-16.4	M2 V	10.52	1.46		0.73			54.0	11. r	9.18	-10	-17	-16		BD+49 2126
Gl 459	12 12 58	+57 18.6	0.102	87.3	-13.4	A3 V	3.30	0.08	0.07		56.5	8.0	56.5	8.0	2.06	12	-1	-11	106591	BD+57 1363
NN	12 12 59	+39 27.9	0.319	280.0		m	11.89			0.88			40.0	07. r	9.9					
Gl 459.2	12 14 14	+44 40.8	0.032	187.6	-53	K4 V	9.18	1.50	1.76				44.0	21. r	7.4	15	-13	-49	106783	BD+45 2014
GJ 1155 A	12 14 20	+03 14.6	0.706	292.5	5	sdM3	13.28	1.62		1.14	46.0	3.4	46.0	3.4	11.59	-71	-13	7		
GJ 1155 B	12 14 20	+03 14.6	0.706	292.5		DA s	15.32	0.38			46.0	3.4	46.0	3.4	13.63					
NN	12 14 28	+31 26.1	0.090	251.0	-34	dM4-5e	14.15	1.62		1.28			51.0	09. r	12.69	-1	-6	-35		
Wo 9403	12 15 21	+46 54.1	0.456	257.3	16	dM1.5e	11.50	1.44		0.73	49.5	16.1	33.0	07. r	9.09	-54	-39	11		

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	12 16 15	+30 02.5	0.408	213.0		m	16.32	1.98					65.0	27. r	15.4					
GJ 1156	12 16 32	+11 24.0	1.301	279.1		dM e	13.81	1.88	+1.05:	1.59	152.9	3.0	152.9	3.0	14.73					
Gl 459.3	12 16 56	+28 39.5	0.655	274.6	-1	M2 V	10.63	1.44	1.26	0.73	49.8	10.9	49.8	10.9	9.12	-56	-26	-9		BD+29 2279
Gl 460	12 17 47	+26 16.7	0.147	275.8	+7.2 SB	F0 IV	6.15	0.30	0.08		59.4	13.6	59.4	13.6	5.02	-11	-5	6	107326	BD+26 2329
Gl 461 A	12 17 52	+00 51.7	0.090	103.0	4.1	M0 V	10.10	+1.47 J	+1.24 J	+0.81 J			63.0	13. r	9.1	7	0	4		BD+01 2684
Gl 462	12 19 25	+42 25.1	0.548	162.7	15.4	M0 Ve	9.45	1.36	1.22	0.60	79.5	10.2	79.5	10.2	8.95	19	-19	24	107596	BD+42 2296
NN	12 19 53	+25 27.0	0.715	254.7		M0	11.38	1.34	1.12	0.76	47.8	27.3	36.0	07. r	9.16					
GJ 1157	12 20 26	-46 20.7	0.798	245.5	42	k	13.62	1.61	1.04	1.30			69.0	11. r	12.81	-19	-65	-16		
Gl 463	12 20 45	+64 18.2	0.681	300.0	7.7	M3	11.58	1.45		1.05	55.5	3.8	55.5	3.8	10.3	-56	0	-17		
NN	12 21 13	+67 28.0	0.240	120.0		m	11.25			1.02			79.0	16. r	10.74					
Gl 464	12 21 21	+12 51.6	0.188	171.9	6.6	dM2	10.39	1.44	1.25	0.72	49.3	11.9	49.3	11.9	8.9	11	-15	2	107888	BD+13 2529
Gl 464.1	12 22 01	+31 33.4	0.207	276.1	-4.4	G6 IV	8.78	0.74	0.36		53.2	20.5	53.2	20.5	7.4	-16	-7	-6	108021	BD+32 2241
Gl 465	12 22 13	-17 56.0	2.532	154.7	58	dM4	11.28	1.60	1.13	0.98	112.1	5.2	112.1	5.2	11.53	96	-71	-23		
NN	12 22 25	-03 56.7	0.258	213.8	47	G5	8.1 *				54.7	17.0	54.7	17.0	6.8 *	7	-43	29	108081	BD-03 3280
NN	12 22 31	+23 40.1	0.327	201.0		m	16.58	1.88					39.0	16. r	14.5					
GJ 2092	12 23 48	-65 56.0	0.186	182.0	55	DA/F	13.97	0.40	-0.54				83.0	09. w	13.57	5	-8	-11		
NN A	12 24 44	+27 18.3	0.270	161.0	1	K3 V	8.89	+1.02 J	+0.92 J				42.0	04. r	7.01	23	-20	2	108421	BD+27 2135
NN C	12 24 27	+27 17.8	0.227	156.0		dM5 e	14.88	1.73		1.38			42.0	04. r	13					
Gl 468	12 25 55	-18 01.1	0.267	139.3	2.7	K4 V	9.22	1.24	1.20	0.48			46.0	08. r	7.53	25	-5	-11	108581	BD-17 3632
NN A	12 26 19	-10 23.3	0.281	273.0		M2	10.96	1.51		0.99			83.0	16. r	10.56					
NN B	12 26 18	-10 23.3	0.281	273.0		g	11. *						83.0	16. r	11. *					
Gl 469	12 26 27	+08 42.4	0.700	245.7		M3.5	12.06	1.60	1.28	1.20	78.0	17.0	78.0	17.0	11.52					
NN	12 26 37	+42 00.6	0.284	221.0		m	12.90			1.21			70.0	13. r	12.13					
Wo 9407	12 26 39	-30 33.6	0.410	142.1	16.2	K0 V	9.06	0.79	0.24	0.26	42.5	13.6	20.0	03. r	5.57	83	-14	-51	108682	CD-30 9942
GJ 1158	12 26 49	-55 42.8	1.250	231.9	-27	M4	13.27	1.62	1.24	1.24			65.0	12. r	12.33	-67	-16	-65		
GJ 1159 A	12 26 58	+53 49.2	1.232	275.1		m	14.21	1.55			45.9	4.7	45.9	4.7	12.52					
GJ 1159 B	12 26 58	+53 49.5	1.232	275.1	-89	M5.5-6	18.0 *				45.9	4.7	45.9	4.7	16.3 *	-88	-86	-95		
NN	12 26 58	+23 16.4	0.180	268.0		dM5	14.18	1.60		1.26			46.0	08. r	12.49					
Gl 469.1	12 27 10	-03 03.0	0.672	210.0	+0.1 SB	G8 V	9.03	0.70	0.13	0.26	50.3	13.6	50.3	13.6	7.5	-1	-56	-30	108754	BD-02 3528
NN A	12 27 22	-05 10.6	0.605	239.2		M3.5	13.0 *			1.20			60.0	07. r	11.9 *					
NN B	12 27 22	-05 10.6	0.605	239.2		M3.5:	14.25			1.32			60.0	07. r	13.14					
Gl 469.2A	12 27 30	-13 07.0	0.253	260.7	1.9	G0 V J	6.46	+0.58 J	+0.05 J	+0.34C	47.4	10.2	47.4	10.2	4.84	-19	-16	-3	108799	BD-12 3647
Gl 469.2B	12 27 30	-13 07.0	0.253	260.7			9.2 *				47.4	10.2	47.4	10.2	7.6 *					
Gl 471	12 28 46	+09 05.6	0.829	230.0	19	dM1	9.70	1.45	1.23	0.72	66.8	10.2	66.8	10.2	8.82	-18	-59	3		BD+09 2636
GJ 1160	12 28 57	+55 23.7	0.108	93.2	-5	K2 V	8.12	0.93	0.64				44.0	07. r	6.34	12	4	-3	109011	BD+55 1536
Gl 471.2	12 29 29	-15 55.2	0.432	261.9	-0.8 SB	F0 IV	4.30	0.37	0.01	+0.21C	54.8	10.8	54.8	10.8	2.99	-30	-22	-7	109085	BD-15 3489
NN	12 29 54	+31 52.3	0.477	294.3		m	13.22			1.10			41.0	08. r	11.28					
NN	12 29 56	+20 40.0				M4	12.90	1.56	1.12	1.10			47.0	10. r	11.26					
Gl 472	12 30 39	-68 28.5	0.629	240.5	0.3	K0 V	7.13	0.85	0.48	0.29	76.3	11.3	76.3	11.3	6.54	-29	-15	-22	109200	CP-68 1684
Gl 473 A	12 30 51	+09 17.6	1.811	277.4	-5	dM5.5eJ	13.04	+1.83 J	+1.20 J	+1.62 J	232.2	4.3	232.2	4.3	14.87	-91	152	-526		
Gl 473 B	12 30 51	+09 17.6	1.811	277.4		M7	13.3 *				232.2	4.3	232.2	4.3	15.1 *					
Gl 474	12 31 20	+33 39.6	0.009	195.5	-42.3	K0 III	6.24	1.05	0.90		53.8	11.9	53.8	11.9	4.89	5	-3	-42	109345	BD+34 2333

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 475	12 31 22	+41 37.7	0.764	292.2	+6.6 SB	G0 V	4.27	0.59	0.05	0.21	114.7	4.9	114.7	4.9	4.57	-32	-4	1	109358	BD+42 2321
NN	12 31 25	-14 21.8	0.531	265.6	9.7	K3/4 V	9.05	1.11	1.01	0.42	32.1	6.1	42.0	05. r	7.17	-46	-39	0	109333	BD-13 3557
Gl 476	12 32 30	+10 06.5	0.516	235.7	32.6	M3	11.42	1.42	1.01	0.99	69.4	8.3	69.4	8.3	10.63	-11	-40	23		
GJ 1161 A	12 32 54	-34 36.3	0.228	250.5		K4 V	7.91	1.04	0.83	0.40			62.0	07. r	6.87				109524	CD-34 8280
GJ 1161 B	12 32 58	-34 37.7	0.228	251.0			11.91	1.60	1.28	1.01			62.0	07. r	10.87					
Gl 477	12 33 15	-45 39.2	0.710	186.5	-12	M1	11.10	1.48	1.13	0.92	78.8	18.0	78.8	18.0	10.58	-1	-2	-44		CD-45 7872
Gl 478	12 33 45	-76 40.7	0.849	265.0	-106	m	11.00	1.30	1.10	0.60	53.8	11.9	29.0	04. r	8.31	-174	18	6		
NN	12 33 50	-04 06.1	0.504	254.3		M3: V	13.1 *	+1.6 *		1.10	39.0	15.7	43.0	09. r	11.3 *					
Gl 479	12 35 11	-51 43.6	1.035	271.4	3	M3	10.67	1.54	1.14	1.06	121.1	7.5	121.1	7.5	11.09	-33	-23	-1		CD-51 6859
Gl 479.1	12 35 44	+79 29.4	0.129	274.4	-18.4 SB	dG2 e	6.96	0.59	0.12		52.3	13.6	34.0	06. r	4.62	-8	-21	-13	110010	BD+80 389
GJ 2095	12 36 02	-49 32.5	0.573	257.0	-12	DA6	13.96	0.18	-0.70		60.4	8.4	60.4	8.4	12.87	-64	23	-25		
NN	12 36 10	-38 04.9	1.487	207.2		M4	12.74	1.69	1.25	1.38			139.0	27. r	13.46					
GJ 1162	12 36 15	-04 02.8	0.740	253.1		m	13.52	1.60	1.28	1.23	50.5	3.1	50.5	3.1	12.04					
Gl 480	12 36 25	+11 58.4	1.163	258.5	-4.4	dM4	11.52	1.48	1.19	1.08	80.2	4.8	80.2	4.8	11.04	-51	-45	-11		
GJ 2096	12 36 40	-77 34.4	0.900	293.1	24.3	K5 V	9.05	1.20	1.04	0.47	34.0	15.3	49.0	08. r	7.5	-52	-70	23	109952	CD-77 568
NN	12 36 41	+47 18.9	0.368	101.0		m	12.14			0.99			48.0	09. r	10.55					
NN	12 37 16	+25 47.4	0.224	229.0		m	14.81	1.63		1.34			47.0	07. r	13.17					
Gl 480.1	12 38 08	-43 18.4	1.047	311.7	-44	M3.5	12.24	1.73	1.39	1.14	46.2	22.2	81.0	20. r	11.8	-69	22	22		
Gl 481	12 38 35	+15 39.4	0.417	163.9	24.5	K4	7.96	1.12	1.02	0.44	66.7	5.0	66.7	5.0	7.08	24	-24	18	110315	BD+16 2404
Gl 482 A	12 39 07	-01 10.5	0.568	270.8	-19.9 VAR	F0 V	3.46	+0.36 J	-0.03 J	0.11	98.7	6.2	98.7	6.2	3.43	-28	-6	-18	110379	BD-00 2601
Gl 482 B	12 39 07	-01 10.5	0.568	270.7	-19.6	F0 V	3.52			0.09	98.7	6.2	98.7	6.2	3.49	-28	-6	-18	110380	
NN	12 39 15	-71 21.4	0.706	269.2		k-m	13.50			1.23			57.0	11. r	12.28					
NN A	12 39 16	+48 31.0	0.273	135.0		m	11.66			0.88			44.0	08. r	9.88					
NN B	12 39 17	+48 31.0	0.273	135.0		m	14.8 *						44.0	08. r	13.0 *					
NN	12 39 27	+55 59.9	0.119	91.4	-6.3	K3 V	8.29	0.95	0.71				44.0	07. r	6.51	13	4	-5	110463	BD+56 1618
NN	12 40 59	+78 09.4	0.803	304.5		m	15.84	1.86					51.0	20. r	14.4					
GJ 1163	12 41 09	+25 22.8	0.343	262.0		dM4	12.96	1.63		1.14			54.0	11. r	11.62					
Gl 483	12 41 59	+52 02.1	0.432	245.6	10.6	K3 V	7.04	0.94	0.72		63.1	6.8	63.1	6.8	6.04	-21	-23	14	110833	BD+52 1650
Gl 484	12 42 38	+39 33.0	0.392	291.6	80.7	G0 V	5.95	0.55	-0.03	0.22	63.5	7.6	63.5	7.6	4.96	-39	8	76	110897	BD+40 2570
NN	12 43 32	+53 11.7	0.252	281.0		m	14.42			1.28			46.0	08. r	12.73					
NN	12 43 55	-11 32.4	0.287	280.8	-16.8	G5 V	6.87	0.70	0.31		27.8	7.3	47.0	08. r	5.23	-32	-3	-10	111031	BD-11 3361
NN	12 44 37	-03 17.9	0.504	269.8		M3	12.63	1.54		1.11			52.0	13. r	11.2					
NN	12 44 45	+46 54.2	0.814	250.1		M2.5	11.76	1.50		1.03			61.0	14. r	10.69					
Gl 485	12 44 54	+31 29.4	0.247	177.3	-1.6	K4 V	9.84	1.29	1.24	0.50	56.7	19.5	37.0	06. r	7.68	18	-26	1		BD+32 2274
Gl 486	12 45 29	+10 01.9	1.077	246.8	18.8	dM4	11.38	1.57	1.18	1.22	115.6	10.5	115.6	10.5	11.69	-22	-41	12		
GJ 1164 A	12 45 32	-24 32.2	0.350	299.1		K4/5 V	9.02	1.12	0.98	0.47			48.0	05. r	7.43				111261	CD-24 10541
GJ 1164 B	12 45 31	-24 32.0	0.368	295.2		K7	10.04	1.38	1.12	0.61			48.0	05. r	8.45					
NN	12 45 50	+47 30.3	0.573	161.1		m	13.65			1.16			41.0	08. r	11.71					
GJ 1165	12 45 54	-15 26.9	0.093	60.9		K2 V	7.94	0.96	0.55	0.36			50.0	08. r	6.43				111312	BD-14 3581
NN	12 46 05	+58 36.8				DC8 :	15.56						54.0	06. w	14.22					
Gl 486.1	12 46 21	+25 06.8	0.358	251.9	-8.7	G7 V	6.31	0.70	0.26	0.23	40.3	14.5	60.0	09. r	5.2	-18	-22	-9	111395	BD+25 2568
Wo 9417	12 46 29	+60 35.5	0.109	95.8	-12	F6 V	5.85	0.46	-0.04		40.8	13.8	36.0	04. r	3.63	16	1	-9	111456	BD+61 1320

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 487	12 47 04	+66 23.0	0.437	258.0	-3.1	M3	10.90	1.64	1.21	1.16	116.2	10.5	116.2	10.5	11.23	-12	-14	0		
NN	12 47 04	+09 44.8	0.431	276.3		M3.5	13.07	1.56		1.16	39.7	11.7	39.7	11.7	11.1					
NN	12 47 12	+01 28.3	0.646	186.7	2.7	G8 V	8.16	0.69	0.12	0.26	40.2	12.3	26.0	04. r	5.23	46	-97	-49	111515	BD+02 2585
NN	12 47 52	+55 22.3	0.046	267.5		DA4	12.31	0.03	-0.93				66.0	12. w	11.41					
NN	12 47 56	+55 04.5	1.286	192.2		DC9+	17.82	+1.50:			40.2	0.7	40.2	0.7	15.84					
Wo 9418	12 48 05	+71 27.6	0.260	230.0	-76.5	K8	10.08	0.97	0.90		39.0	8.5	20.0	03. r	6.59	5	-94	-28		BD+71 632
NN	12 48 09	+27 11.9	0.263	227.0		m	14.14						40.0	06. p	12.15					
Gl 488	12 48 10	-00 29.4	0.402	185.6	+6.1 VAR	M0.5Ve	8.49	1.40	1.26	0.66	83.1	6.0	83.1	6.0	8.09	11	-21	-5	111631	BD+00 2989
GJ 1166 A	12 48 57	+22 22.5	0.187	294.0	19	dM4	12.97	1.60		1.11			40.0	06. r	10.98	-21	-5	20		
GJ 1166 B	12 49 02	+22 23.3	0.187	294.0	15	dM3-3.5	14.28	1.72		1.16			40.0	06. r	12.29	-21	-5	16		
Wo 9420	12 50 26	+34 00.5	0.187	267.9	10.8	K1 V	9.42	1.08	0.89	0.41	78.7	20.6	31.0	05. r	6.88	-24	-15	11	111996	BD+34 2366
Wo 9421	12 50 37	-03 16.9	0.265	268.4	-7.1	F5 V	6.11	0.50	0.04	0.16	40.7	10.2	36.0	06. r	3.89	-31	-17	-6	111998	BD-02 3593
Gl 488.1	12 50 40	-39 54.4	0.066	114.1	-2.5	A7 III	4.26	0.21	0.12	+0.13C	54.1	15.3	54.1	15.3	2.9	4	4	-3	111968	CD-39 7893
Wo 9423	12 52 11	-43 52.7	0.312	224.7	32	G1 V	5.88	0.64	0.25	0.18	42.8	10.2	42.8	10.2	4	1	-45	-13	112164	CD-43 7953
Gl 488.2A	12 52 22	-06 03.9	0.365	235.4		K5	10.42	1.18	1.09	0.47	45.5	13.6	27.0	04. r	7.58					BD-05 3596
Gl 488.2B	12 52 21	-06 03.7	0.292	238.0		m	17.0 P				45.5	13.6	27.0	04. r	14.2 P					
NN	12 53 41	+51 12.3	0.820	162.7		m	14.40	1.74			49.4	4.0	49.4	4.0	12.87					
Gl 489	12 55 07	-14 11.6	0.349	274.6	5.1	K4 V	9.12	1.12	+1.00:	0.43	61.7	10.2	61.7	10.2	8.07	-21	-16	6	112575	BD-13 3627
Gl 490 A	12 55 19	+35 29.8	0.260	244.0	-6.9 SB?	M0 Ve	10.68	1.44	1.13	0.84	47.4	4.1	47.4	4.1	9.06	-13	-23	-5		BD+36 2322
Gl 490 B	12 55 18	+35 29.6	0.260	244.0	-2.8	dM4 e	13.20	1.64	1.14	1.26	47.4	4.1	47.4	4.1	11.58	-13	-23	-1		
Gl 491 A	12 56 28	-09 34.0	0.851	283.5	8	K0 V	7.56	+0.79 J	+0.37 J	+0.29 J	60.4	20.8	42.0	06. r	5.68	-84	-41	23	112758	BD-09 3595
Gl 491 B	12 56 28	-09 34.0	0.851	283.5			12.5 *				60.4	20.8	42.0	06. r	10.6 *					
NN	12 56 55	+08 00.1	0.700	270.6		m+	16.0 *			1.53			52.0	09. r	14.6 *					
NN	12 57 30	-05 21.7	0.328	279.0		M3.5	12.54	1.56		1.13			61.0	15. r	11.5					
Gl 492	12 57 38	+03 45.5	0.963	207.5		DC9	15.79	0.64	-0.10		63.9	4.5	63.9	4.5	14.82					
Gl 493	12 57 45	-02 26.1	0.814	269.9	-14.5	dM0.5	9.78	1.20	1.15	0.50	59.4	10.3	59.4	10.3	8.65	-58	-31	-10	112943	BD-01 2754
Gl 493.1	12 58 05	+05 57.1	0.973	284.4	-40.0 SB	dM5 e	13.40	1.75	+1.1 :	1.43	122.8	4.6	122.8	4.6	13.85	-44	-2	-33		
NN	12 58 16	-62 55.3	0.556	221.5		dM2	10.95			0.84	28.6	13.6	55.0	09. r	9.65					
Gl 494	12 58 19	+12 38.7	0.714	268.3	-11.1	dM1.5e	9.75	1.47	1.10	0.87	89.9	12.6	89.9	12.6	9.52	-32	-20	-10		BD+13 2618
Gl 496 A	13 01 05	-20 18.9	0.141	84.3	26.7	F7 V J	6.27	+0.56 J	+0.07 J	+0.29C			42.0	07. r	4.39	24	-6	18	113415	BD-19 3629
Gl 496 B	13 01 05	-20 18.9	0.141	84.3	28		6.4 *						42.0	07. r	4.5 *	25	-7	19		
Gl 496.1	13 02 04	-52 09.8	1.151	224.9	37.8	K9 V	9.06	1.37	1.27	0.58	49.3	5.6	49.3	5.6	7.52	-38	-89	-66	113538	CP-51 5750
NN	13 03 12	+37 24.3	0.352	238.0		M4	11.72			0.99			59.0	11. r	10.57					
Gl 498	13 03 29	+49 44.2	0.142	24.1	-3.3	dK8	9.30	1.17	1.04	0.46			43.0	05. r	7.47	-2	13	-9	113827	BD+50 1979
Gl 499 A	13 03 49	+20 59.7	0.084	315.6	-1.8	dM0	9.44	+1.29 J	+1.22 J	+0.60 J	58.3	11.9	58.3	11.9	8.27	-7	1	-1		BD+21 2486
Gl 499 B	13 03 49	+20 59.7	0.084	315.6	-2.5		14.9 *				58.3	11.9	58.3	11.9	13.7 *	-7	1	-2		
Gl 499.1	13 03 57	+22 53.0	0.058	153.2	-5.1	M5 III	5.60	1.59	1.63	+1.31:	43.5	15.3	43.5	15.3	3.8	5	-3	-6	113866	BD+23 2538
NN	13 04 05	-77 02.5	0.063	141.2		K3 V	8.88	1.04	0.84	0.40			40.0	06. r	6.89				113693	CD-76 570
NN	13 04 24	+31 08.0	0.502	159.9		m	15.48:	1.86					60.0	24. r	14.4 :					
GJ 2097	13 04 36	+21 05.0	0.082	241.0	-7	m	12.58:	+1.62:	1.19	1.38			156.0	23. r	13.55:	-2	-2	-7		
Wo 9427	13 05 15	+34 40.1	0.125	267.2	-10.2	dK8	9.34	1.18	1.10	0.46			42.0	05. r	7.46	-11	-10	-9		BD+35 2406
Wo 9428	13 05 57	+17 14.3	0.103	255.5		M0	11.80	1.55	1.22	0.90			46.0	08. r	10.11					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Wo 9429	13 06 19	+05 29.0	0.685	173.2	28.1	G5 IV	6.80	0.67	0.18	0.20	45.6	10.9	45.6	10.9	5.1	51	-58	-1	114174	BD+06 2697
NN	13 06 24	+16 38.2	0.541	252.5		m	12.99			1.06			40.0	08. r	11					
NN	13 06 27	-39 52.3	1.196	142.4		M3.5	12.86	1.60	1.10	1.18			62.0	16. r	11.8					
NN	13 06 45	+49 20.8				M0	11.04	1.54	1.19	0.82			52.0	09. r	9.62					
Gl 500	13 07 00	-21 55.3	0.379	155.8	-12.4 SB	G6 V	7.36	0.73	0.27	+0.37C	76.3	13.6	76.3	13.6	6.77	9	1	-25	114260	BD-21 3660
GJ 1167 A	13 07 13	+29 15.2	0.379	240.0		dM5	14.18	1.72		1.33			63.0	10. r	13.18					
Gl 501 A	13 07 33	+17 47.6	0.450	288.8	-11.6 SB	F5 V	4.98	+0.45 J	-0.06 J		51.7	5.7	51.7	5.7	3.55	-41	-10	-6	114378	BD+18 2697
Gl 501 B	13 07 33	+17 47.6	0.450	288.8	-27.7	F5 V	5.17				51.7	5.7	51.7	5.7	3.74	-44	-9	-22	114379	
Gl 501.1	13 08 18	+36 12.0	0.057	288.3	-14.9 SB	F5 IV	8.16	0.58	0.07		46.9	22.2	46.9	22.2	6.5	-5	-4	-15	114519	BD+36 2344
NN	13 09 00	+28 50.0	0.643	221.9		m	15.89	1.86					50.0	20. r	14.4					
Gl 501.2	13 09 15	-37 32.3	0.390	276.3	-15.0 VAR	G3 V	4.85	0.70	0.31	0.24	57.1	9.9	57.1	9.9	3.63	-35	-6	-1	114613	CD-37 8437
NN	13 09 24	+25 36.5	0.487	248.9		m	15.75	1.79					41.0	15. r	13.8					
Gl 502	13 09 32	+28 07.9	1.189	317.7	5.1	G0 V	4.26	0.57	0.07	0.21	119.8	7.6	119.8	7.6	4.65	-46	10	7	114710	BD+28 2193
NN	13 09 59	+85 18.6	0.331	137.0		DC9	16.00	0.78	0.14		54.5	9.3	54.5	9.3	14.68					
Wo 9433	13 10 04	+74 07.2	0.305	279.3	-38.6	G2	9.34	0.58	0.02		41.9	18.8	41.9	18.8	7.5	-16	-41	-28		BD+74 526
NN	13 10 10	-02 00.0	0.166	275.2		K0	7.56						53.0	06. o	6.18				114783	BD- 1 2784
NN	13 10 11	-47 12.2	2.127	268.4		DC9+	17.05	1.40			67.6	3.3	67.6	3.3	16.2					
GJ 1168	13 10 41	+20 27.2	0.619	283.9		dM	13.02	1.58		1.17			56.0	11. r	11.76					
Gl 503 A	13 11 08	-58 50.2	0.296	237.7	-64.8	F7 IV	4.92	0.48	-0.03	+0.17C	52.2	7.8	52.2	7.8	3.51	-57	38	-16	114837	CD-58 4940
NN	13 11 26	+56 56.7	0.017	182.8	-18.7	K2 II	7.97	1.17	1.10		50.5	30.7	50.5	30.7	6.5	5	-9	-15	115019	BD+57 1424
Gl 503.2	13 11 34	+56 58.4	0.112	98.2	-8.9	G1 V	6.83	0.60	0.08	+0.19t	48.4	15.3	36.0	06. r	4.61	15	3	-8	115043	BD+57 1425
NN	13 11 36	+04 09.8	0.728	271.7		m	13.48	1.64		1.16			46.0	09. r	11.79					
NN	13 12 38	-72 52.0	0.500	249.7		m	13.05			1.09			43.0	09. r	11.22					
Gl 503.3	13 13 16	-19 40.7	0.326	110.9	34.2	K1 IV	5.22	1.03	0.87	+0.48C	46.9	10.9	46.9	10.9	3.6	45	-8	12	115202	BD-19 3653
GJ 1169	13 14 14	+28 08.0	0.749	285.8	-16	m	13.26	1.65	1.33	1.16	62.8	2.5	62.8	2.5	12.25	-54	-20	-11		
Gl 504	13 14 18	+09 41.1	0.388	299.8	-27.4	G0 V	5.20	0.58	0.10	0.20	74.2	9.0	74.2	9.0	4.55	-31	2	-20	115383	BD+10 2531
Gl 505 A	13 14 22	+17 17.0	0.658	113.3	6.7	K1 V	6.59	+0.94 J	+0.62 J	+0.35:	84.0	11.1	84.0	11.1	6.21	37	7	1	115404	BD+17 2611
Gl 505 B	13 14 22	+17 17.0	0.658	113.3	9	M1 V	9.6 *				84.0	11.1	84.0	11.1	9.2 *	37	7	3		
NN	13 14 28	+23 26.0	0.274	106.0		M2	11.69			0.88			44.0	08. r	9.91					
NN	13 15 30	+02 29.9	0.360	263.0		m	12.97			1.21			68.0	13. r	12.13					
GJ 1170	13 15 41	+36 34.0	0.300	196.0	23	dM2	11.29	1.41	1.14	0.83	42.7	17.0	46.0	10. r	9.6	11	-24	28		
Gl 506	13 15 47	-18 02.0	1.515	225.1	-8.4	G6 V	4.74	0.71	0.26	0.23	112.1	12.2	112.1	12.2	4.99	-25	-50	-33	115617	BD-17 3813
NN	13 16 33	+33 42.1	0.004	241.9		K1 V	8.13v	1.14	0.94				54.0	14. r	6.8 v				115781	BD+34 2411
Gl 506.2	13 16 45	+85 00.9	0.136	279.7	8.7	dF7	7.28	0.50	0.02		43.4	11.4	19.0	03. s	3.67	-33	-11	3	116459	BD+85 222
Gl 507 A	13 17 14	+35 23.0	0.873	154.6	-4.9	dM1.5	9.51	1.47	1.20	0.81	79.9	12.5	79.9	12.5	9.02	46	-25	-1		BD+35 2436
Gl 507 B	13 17 14	+35 23.0	0.873	154.6	-8.5	M3	12.10	1.58	+1.2 :	1.08	79.9	12.5	79.9	12.5	11.61	46	-25	-4		
NN	13 17 17	-35 08.0	0.961	241.9		M3.5	12.8 *			1.14			57.0	11. r	11.6 *					
Gl 507.1	13 17 22	+33 36.6	0.251	240.0	-11.8	dM2	10.62	1.51	1.20	0.90	50.6	10.9	50.6	10.9	9.14	-10	-23	-8		
Gl 508 A	13 17 36	+48 02.4	0.147	101.0	-3.3 SB?	dM1.5eJ	8.94	+1.48 J	+1.20 J	+0.83 J	103.0	8.0	103.0	8.0	9	6	2	-3	115953	BD+48 2108
Gl 508 B	13 17 36	+48 02.4	0.147	101.0			9.8 *				103.0	8.0	103.0	8.0	9.9 *					
Gl 508.1	13 17 47	-36 26.9	0.353	255.4	0.1	A2 V	2.75	0.04	0.03	+0.00C	60.6	8.2	60.6	8.2	1.66	-20	-19	-3	115892	CD-36 8497
Gl 508.2	13 18 38	+34 32.7	0.593	119.1	-23	dM1	10.62	1.44	1.20	0.85	51.1	15.3	61.0	14. r	9.55	45	2	-25		BD+35 2439

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B−V	U−B	R−I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	13 19 05	+04 01.7	0.504	265.9		m	11.9 *			0.92			44.0	08. r	10.1 *					
NN	13 20 36	+24 44.3	1.080	215.6		M3.5	12.93	1.62	1.12	1.24	72.5	2.6	72.5	2.6	12.23					
NN	13 20 55	-25 38.9	0.662	250.4		m	12.90			1.24			79.0	15. r	12.39					
NN A	13 21 06	+02 58.9	0.185	1.4	28	G5 V	7.06	0.77	0.38				49.0	06. r	5.51	1	6	33	116442	BD+ 3 2765
NN B	13 21 08	+02 59.0	0.190	359.5		G5 V	7.36	0.83	0.51				49.0	06. r	5.81				116443	BD+ 3 2766
Gl 508.3	13 21 07	-13 46.8	0.763	239.2		K7	11.79	1.40	1.08	0.77	46.6	13.1	29.0	06. r	9.1					
Gl 509 A	13 21 14	+29 29.7	0.539	295.7	-39	dM0	9.52	+1.33 J	+1.21 J	+0.60 J	53.2	5.5	53.2	5.5	8.15	-50	-13	-34	116495	BD+29 2405
Gl 509 B	13 21 14	+29 29.7	0.539	295.7		dK6	9.8 *				53.2	5.5	53.2	5.5	8.4 *					
Gl 509.1	13 21 26	+58 10.0	0.120	104.9	-6.6	M0 V	9.75	1.26	1.14	0.57			49.0	08. r	8.2	12	2	-6	238224	BD+58 1441
NN A	13 21 55	+55 11.2	0.121	102.0	-5.6 SB	dA1 p	2.25	+0.02 J	+0.03 J		41.4	6.1	41.4	6.1	0.34	13	4	-5	116656	BD+55 1598
NN B	13 21 56	+55 10.9	0.119	106.0	-9.3 SB	A1 m	3.95	+0.13 J	+0.09 J		41.4	6.1	41.4	6.1	2.04	14	1	-8	116657	
Gl 510	13 23 04	-28 06.8	0.471	257.4	-14	M2.5	11.02	1.53	1.16	+1.15C	69.6	49.2	71.0	17. r	10.3	-30	-13	-9		CD-27 9225
NN	13 23 14	+55 14.9	0.115	98.5	-8.9 SB	A5 V	4.01	0.16	0.08		41.0	7.5	41.0	7.5	2.07	13	3	-9	116842	BD+55 1603
Gl 511	13 23 56	-24 02.0	0.388	255.5	-10.9	K3 V	8.72	0.89	+0.63:	0.34	40.9	7.8	33.0	05. r	6.31	-45	-34	-10	116858	CD-23 11071
Gl 511.1	13 24 17	+63 31.0	0.457	299.3	-30.9	dG6	6.50	0.74	0.30		26.9	11.9	62.0	10. r	5.46	-25	-24	-31	117043	BD+64 949
NN	13 24 33	-30 55.0	0.614	256.6		M4	13.6 *			1.25			60.0	11. r	12.5 *					
Gl 511.2	13 24 47	-15 42.9	0.123	279.4	-12.4	K1 III	4.75	1.10	1.06	0.36	57.3	11.9	57.3	11.9	3.54	-15	1	-6	116976	BD-15 3668
Gl 512 A	13 25 46	-02 05.6	0.482	158.9	-41.6 VAR	dM4	11.32	1.52	+1.23 J	1.11	83.8	11.2	83.8	11.2	10.94	3	1	-50		
Gl 512 B	13 25 46	-02 05.6	0.482	158.9		M4	13.69	1.68		1.32	83.8	11.2	83.8	11.2	13.31					
Gl 512.1	13 25 59	+14 02.7	0.628	202.3	5.3	G2.5 Va	4.98	0.71	0.26	0.24	43.2	9.6	112.0	15. r	5.23	7	-26	1	117176	BD+14 2621
Gl 513	13 26 52	+11 42.9	1.228	165.0	40	M5	12.13	1.46	1.00	1.10	51.8	7.8	51.8	7.8	10.7	94	-73	4		
NN	13 27 23	-51 47.7	0.684	236.3		m	13.1 *			1.12			46.0	09. r	11.4 *					
Gl 514	13 27 27	+10 39.0	1.552	134.3	14.3	M1 V	9.05	1.50	1.24	0.81	138.7	2.9	138.7	2.9	9.76	54	-8	-3		BD+11 2576
Gl 514.1	13 27 29	-08 26.6	1.202	246.2		M4 :	14.25	1.65	1.23	1.35	67.4	4.9	67.4	4.9	13.39					
Gl 515	13 27 40	-08 18.6	1.188	247.7	37	DA5	12.31	0.08	-0.61		61.6	3.2	61.6	3.2	11.26	-55	-72	-14		BD-07 3632
GJ 1171	13 28 08	+19 26.0	1.397	200.5			14.73	1.80	+1.86:?	1.38	69.1	5.5	69.1	5.5	13.93					
NN	13 29 08	-02 03.8	0.880	287.5	-53.3	G9 V	7.36	0.78	0.32	0.29	38.5	14.9	47.0	07. r	5.72	-101	-15	-19	117635	BD-01 2832
NN	13 29 28	+29 32.0	0.278	235.0		M4 e	11.95	1.57		1.26			126.0	22. r	12.45					
NN	13 29 29	+23 38.7	0.282	279.0		m	12.26			1.02			50.0	10. r	10.75					
Wo 9448 A	13 29 41	+31 23.4	0.141	281.4		SB M0 V	11.11	+1.44 J		+0.70 J	48.3	7.8	48.3	7.8	9.53					+31 2500
Wo 9448 B	13 29 41	+31 23.4	0.141	281.4			11.3 *				48.3	7.8	48.3	7.8	9.7 *					
Gl 516 A	13 30 18	+17 04.2	0.338	127.0	-1.9	dM3.5e	12.01	+1.53 J	+1.25 J	+1.00 J	63.0	6.3	63.0	6.3	11.01	24	0	-8		
Gl 516 B	13 30 18	+17 04.2	0.338	127.0	-1.5	dM3.5e	12.3 *				63.0	6.3	63.0	6.3	11.3 *	24	0	-7		
GJ 2102	13 31 05	+08 50.5	0.515	280.1		K0	7.98	1.00	0.90	0.37	52.7	6.3	52.7	6.3	6.59				117936	BD+09 2776
Wo 9450	13 31 36	-38 38.8	0.594	132.3	83.6	G4 V	7.29	0.67	0.16	0.18	42.6	10.0	35.0	06. r	5.01	105	-43	-26	117939	CD-38 8635
NN	13 31 40	-26 06.6	0.788	242.9		m	14.0 *			1.28			56.0	10. r	12.7 *					
GJ 1172	13 31 49	+04 55.5	0.192	133.5	14	dM0.5	9.97	1.38	1.21	0.68	34.7	15.3	57.0	11. r	8.75	20	-4	7		BD+05 2767
Wo 9452	13 31 52	+75 15.7	0.452	276.1	-35	K7	10.27	1.29	1.25	0.52	41.1	13.6	35.0	06. r	7.99	-38	-57	-18		BD+75 510
Gl 517	13 32 07	-08 05.1	0.293	250.5	-24	K5	9.31	1.21	1.04	0.54	49.0	10.1	52.0	09. r	7.89	-27	-12	-20	118100	BD-07 3646
NN	13 32 10	-00 20.4	0.287	276.0	-13.2	A3 V	3.37	0.11	0.10	0.06	36.9	5.8	36.9	5.8	1.21	-36	-16	-4	118098	BD+00 3076
NN	13 32 25	+20 27.1	0.181	164.0		m	13.77			1.18			42.0	08. r	11.89					
GJ 1173	13 32 51	-00 08.2	0.235	14.1	10	K7 V	10.28	1.44	1.20	0.68			48.0	10. r	8.69	-2	17	18		BD+00 3077

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Wo 9453 A	13 34 01	+74 45.3	0.440	265.7	-3	dK5	9.79	1.12		0.42	42.4	11.9	31.0	03. r	7.25	-48	-45	13		BD+75 511
Wo 9453 B	13 34 01	+74 45.3	0.440	265.7		k	13.47	1.44		1.12	42.4	11.9	31.0	03. r	10.93					
Gl 518	13 34 13	+03 57.0	3.870	253.6		DZ9	14.65	0.95	0.37	0.33	122.2	3.9	122.2	3.9	15.09					
Gl 518.1	13 34 29	+08 01.6	0.837	245.7		K4	10.02	1.09	0.92	0.44	47.1	13.6	27.0	04. r	7.18					BD+08 2735
NN	13 34 33	+23 13.4	0.194	151.0		m	12.66			1.03			42.0	08. r	10.78					
Gl 518.2A	13 34 55	+30 20.3	0.166	282.2	3.6	G8 V	9.30	0.64	0.10		47.3	13.1	47.3	13.1	7.7	-14	-7	6	118576	BD+30 2428
Gl 518.2B	13 34 57	+30 20.4	0.171	281.1	3.8		10.51	0.83	0.56		47.3	13.1	47.3	13.1	8.9	-15	-7	7		
Gl 519	13 35 13	+35 58.4	0.315	101.0	-15.0 SB?	dM1	9.04	1.42	1.16	0.66	101.9	18.8	101.9	18.8	9.08	12	3	-17		BD+36 2393
Gl 520 A	13 35 49	+48 23.6	0.239	242.0	-28	dM0.5	10.17	+1.40 J	+1.18 J	+0.69 J-	12.3	19.4	44.0	06. r	8.39	-7	-33	-18		BD+48 2138
Gl 520 B	13 35 49	+48 23.6	0.239	242.0			11.0 *			-	12.3	19.4	44.0	06. r	9.2 *					
Gl 520 C	13 35 38	+48 23.6	0.239	242.0		m	14.46	1.66		+1.26 -	12.3	19.4	44.0	06. r	12.68					
NN	13 36 19	+26 04.9	0.601	278.4		M3	12.56	1.52		1.08			50.0	12. r	11.1					
NN	13 36 20	-02 00.5	0.290	255.0		M3	12.12	1.58		0.99			53.0	13. r	10.7					
Gl 521	13 37 20	+46 26.0	0.402	353.3	-65.3	dM2	10.23	1.42	1.08	0.85	82.9	5.3	82.9	5.3	9.82	-13	-9	-67		BD+46 1889
Gl 521.1	13 37 33	-03 56.4	0.627	322.2	+5.0 SB?	K7	9.59	1.40	1.20	0.65	72.2	14.4	72.2	14.4	8.88	-32	7	26	118926	BD-03 3508
GJ 1174	13 38 08	+44 01.3	1.144	285.2	-42	M3	12.76	1.64		1.20	62.1	4.4	62.1	4.4	11.73	-78	-49	-30		
GJ 1175	13 38 10	-34 12.6	0.265	130.7		K1 V	6.98	0.86	+0.45:	0.28			60.0	09. r	5.87				118972	CD-33 9242
NN	13 38 13	+47 28.1	0.585	148.1		m	15.30	1.73			45.1	7.9	45.1	7.9	13.57					
Gl 521.2A	13 38 24	+50 46.3	0.143	294.8	-12	F7 V	6.33	0.54	-0.03		49.4	17.0	38.0	04. r	4.23	-16	-10	-11	119124	BD+51 1859
Gl 521.2B	13 38 26	+50 46.1	0.150	292.0	-13.6		10.46	1.36	1.11	0.62	49.4	17.0	38.0	04. r	8.36	-16	-12	-12		
NN	13 39 00	+30 17.0	1.599	273.7		m	15.83	1.75			44.8	6.2	44.8	6.2	14.09					
NN	13 39 07	+15 04.5	0.253	284.0		k-m	12.09	1.50	1.23				43.0	21. r	10.3					
Gl 522	13 39 22	+00 07.7	0.455	199.8	45.9	M0 V	9.74	1.30	1.29	0.55	75.8	17.0	48.0	08. r	8.15	28	-53	23	119217	BD+00 3090
NN	13 39 30	-15 45.2	0.510	268.5		m	13.5 *			1.32			82.0	13. r	13.1 *					
GJ 1176	13 39 53	-01 25.9	0.330	240.8		K7 V	9.28	1.19	1.20	0.45			45.0	07. r	7.55				119291	BD-00 2725
NN	13 40 29	+33 33.1	0.708	188.6		M3	11.97	1.64		1.19			94.0	23. r	11.8					
NN	13 40 33	+09 19.6	0.348	250.0		m	13.09			1.15			51.0	10. r	11.63					
Gl 524	13 41 36	-53 51.	0.440	214.0		k	12.50	1.54	1.38	+1.27C	72.2	12.0	72.2	12.0	11.79					
Gl 524.1	13 42 30	-04 22.1	0.227	239.0	4.5	dM1	10.53	1.34	1.24	0.57	44.8	8.4	44.8	8.4	8.79	-8	-23	1		BD-03 3527
NN A	13 42 35	+51 56.1	0.742	269.0		M3	12.3 *				41.1	4.9	41.1	4.9	10.4 *					
Gl 525	13 42 39	+18 03.7	1.896	166.7	20.4	dM1	9.80	1.41	1.17	0.67	79.6	4.0	79.6	4.0	9.3	91	-70	-4		BD+18 2776
Gl 525.1	13 42 50	-32 47.5	0.486	252.1	-21.6 SB	F3 IV	4.23	0.38	0.00	+0.22C	47.0	9.7	47.0	9.7	2.59	-46	-23	-14	119756	CD-32 9603
NN	13 43 09	-17 42.6	0.623	210.2		M3.5	11.86	1.56		1.18			96.0	24. r	11.8					
Gl 526	13 43 12	+15 09.7	2.325	129.8	16.1	M4 Ve	8.46	1.44	1.09	0.86	184.0	1.3	184.0	1.3	9.78	62	-2	-3	119850	BD+15 2620
NN	13 44 15	+57 15.3	0.257	316.0		DA3	13.30						42.0	04. w	11.42					
GJ 1177 A	13 44 49	-32 10.9	0.102	105.9		K5 V	8.94	1.32	1.22	0.57			69.0	08. r	8.13				120036	CD-31 10649
GJ 1177 B	13 44 50	-32 10.9	0.121	120.8			9.12	1.36	1.24	0.60			69.0	08. r	8.31					
Gl 527 A	13 44 53	+17 42.3	0.483	274.4	-16.1 SB?	F7 V	4.50	0.48	0.04	+0.15t	60.4	12.4	74.0	10. r	3.85	-29	-17	-8	120136	BD+18 2782
Gl 527 B	13 44 53	+17 42.3	0.483	274.4		M2	11.0 *				60.4	12.4	74.0	10. r	10.3 *					
GJ 1178	13 44 59	+10 36.7	0.884	262.7		DA7	15.08	0.38	-0.48		50.3	3.6	50.3	3.6	13.59					
GJ 1179 A	13 45 58	+23 51.6	1.484	275.6		dM4 :	15.32	1.96		1.58	83.4	2.4	83.4	2.4	14.93					
GJ 1179 B	13 45 48	+23 49.6	1.484	275.6		DC9	15.65	1.10	0.47	0.42	83.4	2.4	83.4	2.4	15.26					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN A	13 46 02	-35 27.2	0.554	250.8	3.5	G3 IV-V	6.57	0.55	0.05	0.19	40.2	21.2	34.0	06. r	4.23	-49	-60	-5	120237	CD-35 9019
NN B	13 46 02	-35 27.2	0.554	250.8	3.5	K4 :	10.14	1.23	1.22	0.52	40.2	21.2	34.0	06. r	7.8	-49	-60	-5	120237	
NN	13 46 17	+04 21.1	0.183	179.0		m	14.34			1.34			61.0	10. r	13.27					
NN A	13 46 28	+03 02.6	0.298	145.0		M2:	11.19	1.57	1.21	0.94			68.0	13. r	10.35					
Gl 528 A	13 46 47	+27 13.7	0.461	258.5	-20.7	K4 V	7.61	+1.12 J	+1.04 J	+0.42 J	85.1	5.4	85.1	5.4	7.26	-19	-22	-15	120476	BD+27 2296
Gl 528 B	13 46 47	+27 13.7	0.461	258.5	-20.9	dK6	8.03*				85.1	5.4	85.1	5.4	7.68*	-19	-22	-15		
Gl 529	13 47 05	-21 51.4	1.826	254.0	-36.8	K6 V	8.17	1.26	+1.25:	0.49	77.1	10.0	77.1	10.0	7.61	-94	-68	-22	120467	BD-21 3781
NN	13 47 58	-21 26.3	0.373	183.0		M2.5	12.72	1.56		1.12			48.0	11. r	11.13					
NN	13 48 03	-53 17.1	0.552	139.8		m	12.9 *			1.12			50.0	10. r	11.4 *					
Gl 530	13 48 35	-24 08.4	0.647	243.3	2.1	G5 V	6.44	0.69	0.27	0.28	56.4	12.0	61.0	10. r	5.37	-26	-42	-6	120690	CD-23 11329
NN	13 48 43	+36 59.0	0.441	282.6		M3.5	13.65			1.26			57.0	10. r	12.43					
Gl 531	13 49 27	-50 40.5	0.595	265.4	-25	K1 V	7.38	0.90	0.56	0.35	74.1	14.5	60.0	09. r	6.27	-52	-12	3	120780	CD-50 8092
GJ 1180	13 49 42	+26 53.0	0.052	244.0	-20.1		10.83	0.75	0.32	0.21	76.0	16.3	76.0	16.3	10.23	-5	-6	-19		BD+27 2303
Gl 532	13 50 01	+50 11.9	0.448	109.1	-44.8	dM0 p	8.90	1.33	1.20	0.58	68.6	7.0	68.6	7.0	8.08	32	-7	-44	234078	BD+50 2030
NN	13 50 11	+14 40.2	0.311	171.0		M2	11.63	1.50		1.00			62.0	12. r	10.59					
NN	13 50 36	-09 01.6	0.451	134.0		DA6	14.60	0.21	-0.57				48.0	05. w	13.01					
Gl 533	13 51 02	+13 11.8	0.695	194.5	6	dM0	9.80	1.40	1.27	0.68	71.0	13.6	71.0	13.6	9.06	19	-42	-3		BD+13 2721
Gl 533.1	13 51 29	+65 52.5	0.565	255.9	-52.5	M1.5	11.83	1.50		0.89	45.5	13.6	42.0	09. r	9.95	-23	-78	-16		
NN	13 51 34	+67 04.2	0.667	216.8		m	15.69	1.90					64.0	26. r	14.7					
GJ 1181 A	13 52 12	-28 50.7	0.266	249.1		K7 V	9.59	+1.45 J	+1.22 J	+0.76 J			71.0	14. r	8.85				121271	CD-28 10318
Gl 534	13 52 18	+18 38.9	0.369	190.0	+1.0	SB G0 IV	2.68	0.58	0.20	0.20	104.7	7.6	104.7	7.6	2.78	8	-15	-1	121370	BD+19 2725
Gl 534.1A	13 53 14	-54 27.4	0.229	188.8	4.6	G8 V	6.00	0.78	0.25	0.30			87.0	14. r	5.7	0	-8	-11	121384	CD-54 5466
Gl 534.1B	13 53 14	-54 26.	0.230	190.0			13.8 P						87.0	14. r	13.5 P					
NN	13 53 32	-27 49.1	0.509	259.6		m	15.3 *			1.43			53.0	08. r	13.9 *					
Gl 534.2	13 54 01	+79 05.7	0.254	294.0	0	dM1	10.61	1.45		0.74	53.0	13.6	49.0	10. r	9.06	-22	-11	-2		
Gl 534.3	13 55 43	-33 45.2	0.516	231.5	60.3	G5 V	8.17	0.68	0.16	0.24	46.5	10.2	24.0	04. r	5.07	-9	-118	-7	121849	CD-33 9467
NN	13 55 49	+12 48.7	0.785	342.9		M3	12.26	1.66	1.28	1.16			76.0	18. r	11.7					
NN	13 56 11	+00 10.1	0.541	223.9		m	14.05			1.20			39.0	07. r	12.01					
NN	13 56 21	-23 18.9	0.344	261.0		f-g	14.93	0.32					48.0	06. w	13.34					
NN	13 56 27	-19 35.4	0.583	251.5		K2 :	13.0 *			1.38			112.0	78. r	13.2 *					
Gl 535	13 57 00	+23 06.7	0.170	273.7	-57.4	dM0 p	9.03	1.16	1.12	0.44	49.0	10.1	46.0	06. r	7.34	-28	-16	-51	122120	BD+23 2640
Gl 536	13 58 31	-02 25.3	0.994	307.9		M1	9.70	1.46	1.17	0.86	95.1	8.3	95.1	8.3	9.59				122303	BD-01 2892
Gl 536.1A	13 59 34	+15 44.1	0.120	99.0	-10.5	dM0.5 J	11.25:	+1.45 J		+0.72 J	45.7	18.8	34.0	08. r	8.9 :	10	8	-15		
Gl 536.1B	13 59 34	+15 44.1	0.120	99.0	6		11.45:				45.7	18.8	34.0	08. r	9.1 :	16	9	1		
NN	13 59 41	-20 45.9	0.628	125.3		M3.5	13.19	1.61		1.16			51.0	13. r	11.7					
NN	13 59 54	+13 55.9	0.140	131.5	-11	dM0.5	10.65	1.47		0.80	15.4	14.9	55.0	12. r	9.35	7	0	-15		
NN	13 59 59	-24 17.7	0.545	318.4		M0.5	12.15	1.70		0.96	39.5	20.5	42.0	18. r	10.3					
Gl 537 A	14 00 32	+46 34.9	0.585	94.5	-41.1	dM3 e	9.85	1.48	+1.1 :	0.83	89.1	4.3	89.1	4.3	9.6	24	2	-45		BD+47 2112
Gl 537 B	14 00 32	+46 34.9	0.585	94.5	-28	dM3 e	9.95*				89.1	4.3	89.1	4.3	9.70*	24	7	-33		
NN	14 00 32	+15 12.9	0.051	272.3		G5	7.12						45.0	05. o	5.39				122676	BD+15 2658
Gl 538	14 01 05	+11 01.8	0.322	163.8	-11.6	SB G8 V	6.30	0.74	0.29	0.26	65.8	6.7	65.8	6.7	5.39	13	-12	-19	122742	BD+11 2625
Gl 538.1	14 03 31	-26 26.5	0.150	162.9	27.3	K2 III	3.27	1.12	1.04	+0.40t	50.0	3.5	50.0	3.5	1.76	24	-19	3	123123	CD-26 10095

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 539	14 03 44	-36 07.5	0.736	224.9	1.3	K0- IIIb	2.06	1.01	0.87	0.36	58.5	17.7	58.5	17.7	0.9	-25	-48	-24	123139	CD-35 9260
Gl 539.1	14 03 48	-74 36.9	0.299	306.0	-22.1	G1 V	6.02	0.58	0.06	0.20	39.3	10.2	49.0	08. r	4.47	-24	2	27	122862	CP-74 1142
NN	14 04 49	+38 51.7	1.046	159.7		m	14.54	1.70	2.05		37.4	4.4	37.4	4.4	12.4					
Wo 9468	14 06 27	-61 16.6	0.817	215.2	40.7	G9 V	9.68	0.78	0.28	0.29	42.5	7.2	42.5	7.2	7.82	-26	-79	-56	123505	CP-60 5215
Gl 539.2	14 06 34	-30 41.5	0.523	244.2	-12	M0	11.81	1.50		0.79	44.5	8.8	44.5	8.8	10.05	-40	-39	-11		CD-30 11195
Wo 9470	14 08 07	+25 19.7	0.068	199.9	+10.8 SB	F8 IV	4.83	0.53	0.07		40.1	13.6	40.1	13.6	2.8	6	-6	11	123999	BD+25 2737
NN	14 08 15	+76 05.0	0.500	312.4		M1	11.6 *				48.3	8.0	48.3	8.0	10.0 *					
NN	14 09 05	-12 22.5	0.306	236.9	7.6	K1 V	7.93	0.86	0.58		9.1	10.2	43.0	07. r	6.1	-9	-33	2	124106	BD-11 3684
Gl 540	14 09 12	+80 50.4	0.577	157.7	7.4	M1 e	10.35	1.43	1.14	0.83	58.2	3.4	58.2	3.4	9.17	35	4	32		BD+81 465
NN A	14 09 39	-00 21.2	0.739	290.1	-44	M3.5	12.97	1.63	1.21	1.04	39.7	3.9	39.7	3.9	10.96	-96	-23	3		
NN B	14 09 40	-00 21.4	0.739	290.1		m+	21. P				39.7	3.9	39.7	3.9	19. P					
Gl 540.1	14 09 54	-27 01.6	0.042	196.7	27	K2 III	5.09	1.15	1.13	+0.54C	46.7	18.8	46.7	18.8	3.4	18	-16	12	124206	CD-26 10158
NN	14 10 10	-03 04.9	0.368	205.8		K1	7.03	0.74	0.24				51.0	08. r	5.57				124292	BD- 2 3804
Gl 540.2	14 10 26	-11 47.2	0.758	237.0		dM5.5e	13.86	1.53	0.83	1.38			86.0	18. r	13.53					
Wo 9472	14 10 53	-06 43.6	0.219	47.0		dM0	10.16	1.43	1.23	0.67			52.0	08. r	8.74					BD- 6 3950
NN A	14 11 38	-15 07.3	0.219	200.0		K4 V	10.40	+1.28 J	+0.96 J	+0.72 J			40.0	06. r	8.41				124498	BD-14 3902
NN C	14 11 34	-15 07.1	0.219	200.0		m	13.96	1.60	0.99	1.21			40.0	06. r	11.97					
NN	14 11 47	+30 26.9	0.433	294.1		K4	8.04	1.08	0.95	0.41	62.9	9.0	62.9	9.0	7.03				124642	BD+30 2494
NN	14 12 09	+23 41.9	0.483	203.4		m	13.50			1.15			42.0	08. r	11.62					
Gl 540.3	14 12 28	-44 46.0	0.196	139.0	3.4	G4 V	6.31	0.60	0.07	+0.32C			48.0	09. r	4.72	11	0	-16	124580	CD-44 9181
NN	14 12 32	+10 38.9	0.332	179.0		M2	12.37	1.52	1.21				43.0	20. r	10.5					
GJ 1182	14 13 04	+04 54.0	1.060	225.3	4	m	14.30	1.72	+1.3 :	1.47	71.8	3.4	71.8	3.4	13.58	-7	-70	0		
NN	14 13 23	+45 15.1	0.743	250.2		M2.5	11.6 *				61.3	4.6	61.3	4.6	10.5 *					
Gl 541	14 13 23	+19 26.5	2.281	208.8	-5	K2 III ep	-0.10	1.20	1.26	0.47	91.2	5.2	91.2	5.2	-0.3	25	-116	-3	124897	BD+19 2777
Wo 9473	14 13 23	-05 45.8	0.436	181.1	14.6	F6 III	4.08v	0.52	0.04	0.16	46.6	10.5	46.6	10.5	2.42v	27	-36	-12	124850	BD-05 3843
Wo 9474 A	14 14 24	+51 35.8	0.178	299.8	-18.7	A7 V	4.75	0.20	0.06		46.0	11.9	37.0	05. r	2.59	-21	-15	-14	125161	BD+52 1784
Wo 9474 B	14 14 26	+51 36.4	0.173	297.2	-20.8	K1 V	8.23	0.82	0.39		46.0	11.9	37.0	05. r	6.07	-20	-17	-15		
NN	14 14 29	+46 19.0	0.247	309.7	-8.1	A0 p	4.18	0.08	0.05		40.8	8.8	40.8	8.8	2.23	-29	-6	-5	125162	BD+46 1949
NN	14 14 39	+10 49.5	0.260	:253.		M2	11.52	1.52	1.27	0.93			55.0	10. r	10.22					
NN	14 14 55	+31 56.7	0.606	256.9		m	13.10			1.36			115.0	17. r	13.4					
Gl 541.1	14 15 21	-07 18.5	0.351	131.0	-12.8 SB?	G8 V	6.47	0.73	0.35	0.22			57.0	09. r	5.25	15	4	-28	125184	BD-06 3964
NN	14 15 26	-00 17.5	0.382	226.0		k-m	12.76	1.59	1.17				58.0	26. r	11.6					
Gl 541.2	14 15 29	+45 40.5	0.041	113.0		dM0 p	10.25	1.44	1.22	0.69			52.0	08. r	8.83					BD+46 1951
Gl 542	14 15 30	-59 08.3	0.947	209.5	-14.9	K3 V	6.66	1.03	0.94	0.34	104.9	9.4	104.9	9.4	6.76	-33	-12	-29	125072	CP-58 5467
Gl 542.1A	14 16 10	-25 35.4	0.507	313.2	-21	F5 V	5.87	0.50	-0.10	0.20	46.8	10.1	39.0	05. r	3.83	-54	6	36	125276	CD-25 10271
Gl 542.1B	14 16 10	-25 35.4	0.507	313.2			13.3 *				46.8	10.1	39.0	05. r	11.3 *					
Gl 542.2	14 16 20	-06 22.1	0.430	184.5	9.6	K5	9.10	1.30	1.18	0.56	41.8	6.9	41.8	6.9	7.21	24	-40	-18	125354	BD-05 3853
Gl 543	14 16 36	-07 03.8	1.355	235.5	-97	M3	13.40	1.64	1.09	1.04	54.1	8.6	54.1	8.6	12.07	-97	-88	-79		
NN	14 16 51	+13 14.0	0.110	108.2	-3. VAR	dF1	5.41	0.38	-0.03		40.4	10.3	40.4	10.3	3.4	10	5	-8	125451	BD+13 2782
Gl 544 A	14 17 00	-04 55.2	0.643	258.5	-9.1	K1 V	7.58	0.84	0.52	0.30	52.6	6.2	52.6	6.2	6.18	-39	-43	6	125455	BD-04 3665
Gl 544 B	14 17 00	-04 55.2	0.643	258.5		M4	15.1 *			1.30	52.6	6.2	52.6	6.2	13.7 *					
Gl 545	14 17 29	-09 22.8	1.062	215.2	75	M4	12.9 :	1.59	1.14	1.20	91.1	13.6	91.1	13.6	12.7 :	42	-73	39		

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	14 18 02	+39 16.7				M0:e:	12.31	1.51	1.00	1.03			49.0	10. r	10.76					
Gl 545.1	14 18 20	-40 09.9	0.510	257.6	3.1	K3/4 V	9.02	1.10	1.05	0.47	42.4	6.2	47.0	05. r	7.38	-32	-40	8	125595	CP-39 6278
NN	14 18 40	-00 53.1	0.625	163.6		M3	13.15	1.66		1.21			59.0	14. r	12					
NN	14 18 51	+27 49.1	0.293	292.0		m	12.62			1.03			43.0	09. r	10.79					
Gl 546	14 19 48	+29 51.7	0.711	243.3	-37.2	SB? K8 V	8.55	1.26	1.24	0.52	69.1	7.2	69.1	7.2	7.75	-23	-53	-20		BD+30 2512
NN	14 20 19	-22 03.2	0.536	210.2		m	15.0 *			1.33			43.0	07. r	13.2 *					
Gl 547	14 20 42	+01 28.5	0.528	155.1	-18.9	G1 V	6.27	0.63	0.09	0.23	57.9	5.8	57.9	5.8	5.08	21	-15	-39	126053	BD+01 2920
NN	14 22 27	+09 06.7	0.570	71.3		m	12.26	1.63	1.23	1.10			66.0	13. r	11.36					
NN	14 22 45	-20 02.4	0.570	286.9		m	14.7 *			1.29			42.0	07. r	12.8 *					
Gl 548 A	14 23 24	+23 51.4	1.376	145.0	8.6	dM1	9.75	1.44	1.26	0.73	63.7	6.4	63.7	6.4	8.77	98	-22	-21		BD+24 2733
Gl 548 B	14 23 27	+23 51.6	1.373	144.7	7.7	dM2	10.00	1.46	1.26	0.79	63.7	6.4	63.7	6.4	9.02	98	-21	-21		
Gl 549 A	14 23 30	+52 04.9	0.468	211.2	-11.4	F7 V	4.06	0.50	0.01	+0.16t	70.0	11.9	81.0	07. s	3.6	8	-28	4	126660	BD+52 1804
Gl 549 B	14 23 29	+52 03.7	0.471	210.8	-11.3	M3	11.50	1.50		1.02	70.0	11.9	81.0	07. s	11.04	9	-28	4		
Gl 550	14 24 10	-51 42.6	0.306	277.5	11.8	G5 V	7.83	0.70	0.21	+0.34C	56.6	13.6	30.0	05. r	5.22	-22	-37	25	126525	CD-51 8206
NN	14 24 44	+24 01.3				DC8	15.41						58.0	06. w	14.23					
GJ 1183 A	14 25 23	-00 09.2	0.412	283.0		m	13.95	1.65	1.32	1.36	61.8	3.7	61.8	3.7	12.9					
GJ 1183 B	14 25 24	-00 09.1	0.412	283.0		m	14.03	1.68	1.24	1.37	61.8	3.7	61.8	3.7	12.98					
GJ 2108	14 25 24	-81 07.0	0.450	208.0	58	DA6	13.75	0.25	-0.53				44.0	05. w	11.97	-29	-24	-33		
Gl 550.1	14 25 31	+24 03.8	0.502	279.4	-59	dM0	10.92	1.26	1.08	0.51	50.2	13.4	25.0	04. r	7.91	-92	-61	-19		BD+24 2735
Gl 550.2A	14 25 37	-02 00.3	0.142	267.9	-10.1	SB? G2 IV	4.83	+0.72 J	+0.21 J	+0.36CJ	44.6	8.8	44.6	8.8	3.08	-16	-9	-3	126868	BD-01 2957
Gl 550.2B	14 25 37	-02 00.3	0.142	267.9	-8.0	SB G4 V	9.0 *				44.6	8.8	44.6	8.8	7.2 *	-14	-9	-1		
Gl 550.3	14 26 03	-46 14.3	0.180	196.0		K5	10.35	1.44	1.26	+0.87C	46.1	10.2	48.0	08. r	8.76					CP-45 6863
Gl 551	14 26 19	-62 28.1	3.809	281.7	-16	dM5 e	11.05:	+1.83:	1.43	1.66	771.8	4.1	771.8	4.1	15.49:	-25	-2	13		
NN	14 26 37	+33 24.6	0.802	206.2	-21	dM9	19.74				95.0	5.7	95.0	5.7	19.63	10	-43	-11		
NN	14 26 37	+12 20.6	0.127	303.9		G5	8.38						46.0	05. o	6.69				127068	BD+12 2700
NN	14 26 40	+46 07.8	0.907	275.6	-68	M5.5:	16.99:	+2.22:			45.0	8.2	45.0	8.2	15.26:	-73	-87	-28		
Gl 552	14 27 11	+15 44.2	1.711	321.8	7.5	dM2.5	10.68	1.47	1.17	0.94	56.9	8.1	56.9	8.1	9.46	-125	27	64		BD+16 2658
Gl 552.1	14 27 30	-53 52.6	0.320	217.0		k-m	11.63	1.51	1.12	+1.27C	52.5	13.6	61.0	13. r	10.56					
NN	14 27 39	+42 01.2	0.272	144.9	0.4	G5 V	6.35	0.70	0.21		30.1	9.4	59.0	10. r	5.2	22	-3	-1	127334	BD+42 2508
NN	14 27 50	+29 47.7	0.516	206.3		m	14.66			1.33			50.0	08. r	13.15					
Gl 553	14 28 12	-08 25.3	1.283	259.9	-26.8	K7 V	9.40	1.40	1.22	0.66	66.1	4.0	66.1	4.0	8.5	-70	-65	5	127339	BD-07 3856
Gl 553.1	14 28 20	-12 04.1	0.538	227.0		M3	11.92	1.57	1.33	1.18	83.8	23.9	87.0	21. r	11.6					
NN A	14 28 34	-15 24.8	0.430	150.2	29.2	G5 V J	8.38	+0.71 J	+0.17 J		39.4	11.9	23.0	04. r	5.19	73	-33	-48	127356	BD-14 3970
Gl 554	14 28 42	+35 40.3	0.525	290.7	-12	dK5	8.70	1.04	0.91	0.40	54.8	20.5	44.0	06. r	6.92	-52	-25	7	127506	BD+36 2500
NN	14 29 21	+59 56.2	0.825	282.4	21	M6.5	17.88				103.3	1.3	103.3	1.3	17.95	-33	-8	27		
NN	14 29 48	+16 14.1	0.180	:108.		m	13.61			1.28			67.0	11. r	12.74					
GJ 1184	14 29 48	+11 34.2	0.219	21.3	-39.3	K5	9.69	1.21	1.17	0.57	41.5	4.0	41.5	4.0	7.78	-27	22	-31		BD+11 2687
NN	14 30 01	+05 59.6	0.322	343.0		dM0	10.64	1.23	1.14	0.60	47.7	5.3	47.7	5.3	9.03					
NN	14 30 32	+49 52.4	0.595	259.6		m	13.26			1.17			51.0	10. r	11.8					
Wo 9486	14 30 54	-09 42.5	0.561	206.9		K4	10.54	1.25	1.21	0.54	42.7	10.2	29.0	05. r	7.85					BD-09 3964
NN	14 31 05	+81 01.9	0.142	211.4		G5	6.91	0.76	0.34				54.0	07. r	5.57				128642	BD+81 482
Gl 555	14 31 35	-12 18.6	0.690	330.3	9	M3	11.31	1.64	1.20	1.28	159.0	6.6	159.0	6.6	12.32	-7	3	21		BD-11 3759

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 556	14 31 51	+53 07.4	0.310	321.7	11.5	K3 V	7.23	0.99	0.84		69.8	9.0	69.8	9.0	6.45	-21	6	9	128165	BD+53 1719
Gl 557	14 32 30	+29 57.7	0.227	55.6	+0.9 VAR	F2 V	4.46	0.36	-0.08		64.1	18.7	64.1	18.7	3.5	2	16	-5	128167	BD+30 2536
Gl 558	14 32 55	+33 57.7	0.788	287.1	-51.9	dM0.5	9.58	1.28	1.17	0.54	38.8	5.9	38.8	5.9	7.52	-91	-58	-14		BD+34 2541
Gl 558.1	14 33 32	-67 42.7	0.448	229.0	-30	F8 V	6.04	0.50	-0.02	0.16	49.2	7.2	39.0	03. s	4	-60	-12	-13	128020	CP-67 2616
NN	14 33 33	+09 58.0	0.317	141.3	-15	K0	7.50	0.99	0.78				67.0	11. r	6.63	12	-4	-24	128311	BD+10 2710
NN	14 35 24	+58 34.4	0.907	137.0		m	11.74			1.06			71.0	14. r	11					
NN	14 35 54	+18 30.9	0.078	202.5	-14.4	gK2	5.91	1.10	0.99		45.6	18.7	45.6	18.7	4.2	-3	-10	-13	128750	BD+18 2906
Gl 559 A	14 36 11	-60 37.8	3.689	281.1	-26.2	G2 V	0.01	0.64	0.23	0.22	749.0	4.7	749.0	4.7	4.38	-32	4	14	128620	CP-60 5483
Gl 559 B	14 36 11	-60 37.8	3.689	281.1	-18.1	K0 V	1.34	0.84	0.64	0.29	749.0	4.7	749.0	4.7	5.71	-26	-1	14	128621	
NN	14 36 37	-74 55.5	0.129	102.6		G5 V	6.73						45.0	05. o	5				128400	CP-74 1218
Gl 559.1	14 37 56	+64 30.4	0.149	255.6	-23.1 SB	dG0 e	7.54	0.61	0.03		47.5	12.1	26.0	04. r	4.61	-7	-35	-3	129333	BD+64 1017
Gl 560 A	14 38 26	-64 45.5	0.300	218.1	7.2	F0 Vp	3.19	0.24	0.11	0.02	54.2	9.0	54.2	9.0	1.86	-12	-21	-13	128898	CP-64 2977
Gl 560 B	14 38 26	-64 45.5	0.300	218.1	7	K5 V	8.47	1.15	1.24	0.42	54.2	9.0	54.2	9.0	7.14	-12	-21	-13		
Wo 9490 A	14 40 16	+19 41.5	0.324	235.1	-28.7	K5	9.74	+1.29 J	+1.27 J	+0.59 J	53.4	3.5	53.4	3.5	8.38	-16	-32	-19		BD+20 3010
Wo 9490 B	14 40 16	+19 41.5	0.324	235.1			10.0 *				53.4	3.5	53.4	3.5	8.6 *					
Wo 9490 C	14 40 09	+19 43.1	0.298	234.0	-28	K5	10.08	1.34	1.28	0.58	53.4	3.5	53.4	3.5	8.72	-15	-30	-19		BD+20 3009
Wo 9491	14 40 25	-05 26.5	0.337	161.9	4.7	F2 III	3.88	0.38	-0.02		45.5	9.4	45.5	9.4	2.17	24	-18	-19	129502	BD-05 3936
Gl 561	14 41 09	+26 57.7	0.330	270.0	-77.4	dK0	9.67	0.73	0.29		52.6	15.3	52.6	15.3	8.3	-44	-40	-58		BD+27 2411
Wo 9492	14 41 28	+66 16.1	0.332	261.0		M3	10.83	1.55		0.96			83.0	16. r	10.43					
NN A	14 41 44	-22 02.3	0.363	200.9		K2/3 V	9.32	1.17		0.44			40.0	05. r	7.33				129715	BD-21 3954
NN B	14 41 49	-22 01.8	0.346	198.0		k-m	16.3 P						40.0	05. r	14.3 P					
Wo 9493	14 42 54	+17 10.5	0.083	232.3	-9	K0 III	4.60	0.98	0.75		43.2	8.5	43.2	8.5	2.78	-5	-10	-6	129972	BD+17 2780
Gl 561.1A	14 43 06	-25 13.9	0.184	234.1	-19.7	F2 III-IV	5.10	+0.34 J	+0.09 J	+0.18CJ	47.5	13.6	31.0	04. s	2.56	-26	-18	-13	129926	CD-24 11661
Gl 561.1B	14 43 07	-25 14.0	0.160	238.8	-20.6	dF9	7.14*				47.5	13.6	31.0	04. s	4.60*	-27	-14	-11		
Gl 562	14 44 03	+16 43.1	0.938	187.4	44.9	K5 V	9.25	1.27	1.17	0.53	65.8	7.2	65.8	7.2	8.34	58	-49	29		BD+17 2785
NN	14 44 41	-17 29.5	1.177	252.6		DC9	16.48	0.94			69.0	4.0	69.0	4.0	15.67					
NN	14 44 45	+02 54.8	0.281	256.4		G8 V	7.78	0.90	0.57				45.0	07. r	6.05				130307	BD+03 2938
GJ 1185	14 45 21	-02 57.5	0.657	306.4		m	13.28	1.63	1.20	1.01	50.5	3.6	50.5	3.6	11.8					
Gl 563.1	14 46 03	+38 40.6	0.176	209.0	-13.5	dM2	9.71	1.32	1.14	0.55	19.1	6.3	47.0	07. r	8.07	4	-21	-6		BD+39 2801
Gl 563.2A	14 46 42	-25 53.8	1.217	260.7	22	M3	11.66	1.49	1.05	0.87	38.6	8.4	48.0	08. r	10.07	-52	-100	48		CD-25 10553
Gl 563.2B	14 46 40	-25 54.0	1.217	260.7	44	M3	12.06	1.52	1.05	0.93	38.6	8.4	48.0	08. r	10.47	-35	-108	59		
Gl 563.3	14 47 55	+07 01.3	0.603	265.3	-31.3	K2 V	9.08	0.96	0.76	0.36	51.9	13.6	31.0	04. r	6.54	-69	-68	12	130871	BD+07 2850
Gl 563.4	14 47 55	-15 47.4	0.123	235.2	-23.5 SB	F5 IV-V	5.15	0.41	-0.03	0.11	48.6	10.2	48.6	10.2	3.58	-21	-5	-15	130819	BD-15 3965
Gl 564	14 48 02	+24 07.0	0.146	78.1	-2.7	G2 V	5.85	0.56	0.02	0.20	69.7	8.5	69.7	8.5	5.07	3	7	-6	130948	BD+24 2786
Gl 564.1	14 48 06	-15 50.1	0.129	236.6	-46.7	A3 IV	2.75	0.15	0.09	-0.03	53.6	9.1	53.6	9.1	1.4	-39	2	-29	130841	BD-15 3966
NN A	14 48 37	+09 55.7	0.225	283.4	-35.6	dG5	7.40	0.76	0.34				43.0	06. r	5.57	-37	-14	-17	131023	BD+10 2752
NN B	14 48 37	+09 55.6	0.225	283.4		k	8.9 *						43.0	06. r	7.1 *					
Gl 565	14 48 50	-24 05.6	1.033	245.8	-65.4	K5 V	7.83	1.00	0.88	0.36	67.3	7.1	67.3	7.1	6.97	-85	-40	-26	130992	CD-23 11940
Gl 566 A	14 49 05	+19 18.4	0.171	127.2	2.2	G8 Ve	4.70	0.73	0.22	0.28	149.1	3.6	149.1	3.6	5.57	6	1	-1	131156	BD+19 2870
Gl 566 B	14 49 05	+19 18.4	0.171	127.2	3.1	K4 Ve	6.97	1.16	1.15	0.44	149.1	3.6	149.1	3.6	7.84	6	1	0		
NN	14 49 58	+00 22.6	0.320	163.0		M2	12.58	1.58	1.12	1.00			39.0	09. r	10.5					
NN	14 50 05	+12 36.0	0.233	194.0		k	11.61	1.52	1.21				61.0	29. r	10.5					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	14 51 03	+28 42.6	0.120	306.1	-43.7	K0 V	7.96	0.86	0.52				41.0	07. r	6.02	-27	-15	-34	131509	BD+29 2592
Gl 567	14 51 07	+19 21.2	0.497	295.9	-31.0 SB	K2 V	6.02	0.84	0.49	0.30	86.9	4.1	86.9	4.1	5.72	-36	-14	-14	131511	BD+19 2881
GJ 1186	14 51 13	+11 47.0	0.733	174.5		m	15.29	1.82		1.40	53.9	4.1	53.9	4.1	13.95					
Gl 568 A	14 51 41	+23 45.5	0.692	278.7	-35.7	M3.5 J	12.19	+1.61 J	+1.24 J	+1.22 J	93.9	8.1	93.9	8.1	12.05	-38	-28	-15		
Gl 568 B	14 51 41	+23 45.5	0.692	278.7			12.7 *				93.9	8.1	93.9	8.1	12.6 *					
Gl 569 A	14 52 08	+16 18.3	0.335	108.4	-8.4	dM0 e	10.20 J	1.48	1.15	0.96	95.6	11.4	95.6	11.4	10.10 J	9	5	-16		BD+16 2708
NN	14 52 26	+35 45.8	0.838	169.3		M3.5	12.31			1.20			86.0	16. r	11.98					
NN	14 52 29	+10 09.1	0.514	216.8		M0.5	11.30	1.40	1.11	0.80			42.0	08. r	9.42					
NN	14 53 03	+41 20.8	0.266	301.0		m	14.67			1.28			41.0	07. r	12.73					
NN	14 53 34	+82 43.2	0.284	144.3	-44	F9 V	5.64	0.68	0.17		12.2	6.2	65.0	06. s	4.7	36	-27	-18	133002	BD+83 431
NN	14 53 42	-27 57.1	0.965	210.1		dM8	17.05	1.34			161.0	6.0	161.0	6.0	18.08					
Gl 569.1	14 53 46	+53 52.5	1.079	296.1	-14.4	K1 V	7.78	0.78	0.33		44.9	10.8	39.0	06. r	5.74	-116	-59	23	132142	BD+54 1716
NN A	14 54 11	+18 06.6	0.993	299.5	8	M5	15.50						60.0	17. s	14.4	-62	-16	46		
NN B	14 54 12	+18 06.8	0.993	299.5	9	M7 :	18.60						60.0	17. s	17.5	-61	-16	47		
Gl 570 A	14 54 32	-21 11.5	2.025	149.1	29.1	K5 Ve	5.75	1.10	1.06	0.40	174.2	6.0	174.2	6.0	6.96	50	-22	-31	131977	BD-20 4125
Gl 570 B	14 54 31	-21 11.3	1.933	149.7	+27.9 SB	M2 V	8.00	1.50	1.22	0.89	174.2	6.0	174.2	6.0	9.21	47	-22	-29	131976	BD-20 4123
Wo 9503	14 54 34	-04 08.6	0.181	212.5	21.7	F0 V	4.49	0.32	0.05		43.2	6.9	43.2	6.9	2.67	16	-22	12	132052	BD-03 3696
Gl 570.1	14 54 42	-48 39.5	0.336	181.5	37.3	G5 V	6.35	0.71	0.27	0.26	49.2	11.9	62.0	10. r	5.31	25	-34	-16	131923	CD-48 9494
NN	14 54 43	+49 49.9	0.252	154.5	-16	F8 V	5.63	0.50	0.00		25.9	7.6	41.0	04. s	3.69	28	-14	-12	132254	BD+50 2126
NN A	14 54 59	+00 02.0	0.067	115.9	20.6	K1 III	5.53	1.13	1.11		39.7	9.2	39.7	9.2	3.5	19	1	11	132132	BD+00 3277
NN	14 55 01	+15 10.8	0.598	289.6		m	14.73	1.68		1.20	40.9	5.0	40.9	5.0	12.79					
Gl 570.2	14 55 30	+31 36.7	1.374	211.1	7.7	dM2	11.11	1.33	1.08	0.63	66.1	17.0	31.0	06. r	8.57	75	-188	58		
Gl 571	14 56 14	-43 53.5	0.370	223.0	-2.3	K7 V	10.15	1.31	1.09	0.56	56.4	11.9	56.4	11.9	8.91	-17	-24	-10		CP-43 6820
GJ 1187	14 56 29	+56 51.8	0.683	156.7	10	m	15.53	1.95		1.62	89.4	4.6	89.4	4.6	15.29	35	1	14		
NN	14 57 02	+59 46.9	0.090	309.0		dK5	10.16	1.38	1.27	0.61			45.0	07. r	8.43					BD+60 1577
Gl 571.1	14 58 01	-10 55.9	0.470	178.9	14	dM0.5	9.48	1.40	1.28	0.63	51.6	7.5	51.6	7.5	8.04	26	-33	-17	132683	BD-10 4011
NN	14 58 45	+07 21.7	0.502	259.6		M3.5	12.73	1.49		1.17			62.0	16. r	11.7					
NN	14 58 51	+05 45.0	0.410	165.1		M3	12.10	1.45	0.89	1.10			63.0	16. r	11.1					
Gl 572	14 59 09	+45 37.1	0.394	36.0	-10	dM0	9.13	1.43	1.18	0.72	74.3	9.8	74.3	9.8	8.48	-9	16	-20		BD+45 2247
NN	14 59 11	+35 39.3	0.322	147.0		M2	12.05			0.93			43.0	06. r	10.22					
Gl 574	14 59 42	-46 05.9	0.290	271.0	-65.2	K5 V	9.86	1.20	1.07	+0.62C	56.8	11.9	56.8	11.9	8.63	-66	20	0		CP-45 7173
GJ 1188	15 00 57	+03 58.1	1.136	308.3	-128	m	12.10	1.46	1.12	0.76	47.0	10.2	27.0	04. r	9.26	-235	-15	27		
NN	15 02 05	-18 23.7	0.191	226.8		K4 V	9.59	1.20	1.18	0.52			41.0	06. r	7.65				133412	BD-18 3965
Gl 575 A	15 02 08	+47 50.9	0.396	273.8	-29.7	F9 V n	5.19	+0.65 J	+0.11 J		85.1	5.1	85.1	5.1	4.84	-16	-30	-15	133640	BD+48 2259
Gl 575 B	15 02 08	+47 50.9	0.396	273.8	+3.4 SB	dG2	5.96				85.1	5.1	85.1	5.1	5.61	-13	-12	13		
NN	15 02 08	-20 55.2	0.696	250.5		m	14.7 *			1.33			49.0	08. r	13.2 *					
Gl 575.1	15 02 15	+29 40.4	0.295	125.0		k-m	12.75	1.53	1.23	0.98	45.3	8.5	45.3	8.5	11.03					
Gl 576	15 02 27	+05 50.3	0.746	229.7	-68. VAR	K5	9.82	1.31	1.12	0.58	56.4	10.3	56.4	10.3	8.58	-47	-66	-46		BD+06 2986
NN	15 03 10	-07 03.1	0.200	266.0		DA7	15.90	0.39	-0.43		39.1	5.5	39.1	5.5	13.86					
NN	15 03 14	+60 34.6	0.685	285.8		M2	11.00	1.50		0.89			65.0	14. r	10.06					
Wo 9510	15 03 58	+65 00.3	0.264	265.0	-72.6	G8	9.47	0.82	0.44		39.4	13.6	39.4	13.6	7.4	-4	-70	-36		BD+65 1033
NN	15 04 28	+55 16.1	0.481	288.1		m	13.35			1.20			54.0	10. r	12.01					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 577	15 04 57	+64 14.2	0.166	309.1	-6.4	dG5 e	8.42	0.68	0.11		52.5	15.3	22.0	04. r	5.13	-33	-15	-1	134319	BD+64 1046
Gl 578	15 05 06	+25 03.8	0.249	132.6	-9.8	F5 V	4.93	0.43	-0.02	0.17	61.3	9.3	50.0	05. s	3.42	17	-2	-19	134083	BD+25 2873
Gl 579	15 05 16	+25 07.2	1.003	299.5	-69.6	K7 V	10.09	1.41	+1.22:	0.64	62.2	4.9	62.2	4.9	9.06	-93	-40	-23		BD+25 2874
GJ 1189	15 06 54	+24 12.2	0.499	288.5	-51.3	dK8	9.31	1.06	0.98	0.40	58.4	20.4	34.0	04. r	6.97	-74	-44	-8		BD+24 2824
NN	15 07 07	+03 21.0	0.735	311.1		M3	11.46	1.50	+1.13:	1.05			78.0	19. r	10.9					
Gl 579.2A	15 07 28	-16 08.5	3.674	196.1	294.3	K0 VI	9.08	0.77	0.17	0.30	39.9	3.0	39.9	3.0	7.08	281	-443	-41	134439	BD-15 4042
Gl 579.2B	15 07 28	-16 13.5	3.677	196.0	308	K2 VI	9.45	0.86	0.37	0.34	39.9	3.0	39.9	3.0	7.45	292	-446	-34	134440	BD-15 4041
NN	15 07 48	+19 33.2	0.462	179.6		m	13.35			1.26			69.0	12. r	12.54					
Wo 9512 A	15 08 41	-51 54.6	0.132	235.7	-10	G8 III	3.41	0.92	0.66		41.6	10.2	26.0	03. s	0.48	-22	-14	-2	134505	CD-51 8830
Wo 9512 B	15 08 33	-51 55.1	0.123	232.6	-10.5	F9 V	6.69	0.50	-0.02		41.6	10.2	26.0	03. s	3.76	-21	-12	-4	134483	CD-51 8827
NN	15 09 12	-10 02.9	1.005	257.6		M4	14.26	1.66	1.02	1.33	68.0	3.1	68.0	3.1	13.42					
NN	15 09 40	+18 09.0	0.678	215.5	-58	m	13.45	1.51	1.08	1.12	42.3	3.1	42.3	3.1	11.58	-11	-87	-39		
Gl 579.3	15 10 14	-00 58.5	0.375	219.4	-60.1	K0	9.29	0.78	0.38	+0.42C	46.7	10.2	20.0	03. r	5.8	-40	-88	-47	134985	BD-00 2941
NN A	15 10 29	+19 28.1	0.656	296.0	-37.8	G5 V	6.68	0.68	0.25	0.33	22.6	7.1	50.0	09. r	5.17	-67	-28	2	135101	BD+19 2939
NN B	15 10 30	+19 28.5	0.666	294.9	-38.2	G7 V	7.53	0.73	0.33	0.35	22.6	7.1	50.0	09. r	6.02	-68	-29	3		
Gl 579.4	15 10 33	-25 07.3	0.402	259.4	5.5	G5 V	6.45	0.70	+0.33:	0.22	31.2	7.5	54.0	09. r	5.11	-13	-29	16	134987	CD-24 11928
NN	15 10 57	+45 54.6	0.539	311.0		m	13.35			1.27			72.0	13. r	12.64					
Gl 580 A	15 11 20	-01 09.5	1.373	249.0	-69.2	K0 V J	7.35	+0.77 J	+0.35 J	+0.27 J	58.9	2.6	58.9	2.6	6.2	-85	-98	-15	135204	BD-00 2944
Gl 580 B	15 11 20	-01 09.5	1.373	249.0			7.35*				58.9	2.6	58.9	2.6	6.20*					
GJ 1190	15 11 25	-03 36.9	0.767	282.7	-110.3	K5 V	9.84	1.13	1.01	0.47	47.5	8.7	33.0	05. r	7.43	-148	-49	-8		BD-03 3746
Gl 580.1	15 13 35	-58 37.0	0.169	214.6	9.6	A3 V	4.07	0.09	0.09	+0.05C	51.6	11.9	51.6	11.9	2.6	-2	-17	-6	135379	CP-58 5875
Gl 580.2	15 14 03	+67 32.2	0.448	151.8	-48.1	F8 V	5.13	0.53	0.08		48.3	7.4	48.3	7.4	3.55	52	-30	-26	136064	BD+67 876
NN	15 14 42	+03 21.4				DA wk	14.02						51.0	06. w	12.56					
Wo 9518	15 15 47	-18 26.4	0.567	131.8		K5 p	10.35	1.22	1.03	0.52	44.5	8.5	44.5	8.5	8.59					BD-18 4031
NN	15 16 29	-12 34.1	0.724	253.5		M3	12.58	1.52		1.24			75.0	23. r	12					
Gl 581	15 16 50	-07 32.4	1.224	256.3	-9.4	dM5	10.56	1.60	1.23	1.10	157.9	6.5	157.9	6.5	11.55	-22	-30	8		BD-07 4003
Gl 582	15 18 25	-48 08.1	1.648	260.4	-69.4	G2 V	5.65	0.65	0.06	0.22	63.1	7.8	63.1	7.8	4.65	-125	-55	40	136352	CD-47 9919
NN	15 18 39	-47 44.8	0.197	225.5	-11.2	F8 V	5.00	0.50	0.04		29.9	4.6	29.9	4.6	2.38	-25	-20	-8	136351	CD-47 9922
NN	15 18 53	+68 01.8	0.611	310.2		m	13.44			1.16			45.0	09. r	11.71					
Gl 582.1A	15 19 08	-47 44.4	0.453	235.3	-22.1 VAR	G5 V J	8.29	+0.70 J	+0.10 J	+0.46CJ	56.1	15.6	56.1	15.6	7	-39	-21	-4	136466	CD-47 9926
Gl 582.1B	15 19 08	-47 44.4	0.453	235.3			8.6 *				56.1	15.6	56.1	15.6	7.3 *					
GJ 2112 A	15 19 11	-27 39.5	0.745	35.4		M3 :	13.28	1.70		1.21			60.0	15. r	12.2					
Gl 583	15 19 27	-04 35.9	0.298	271.5	-17.8	K7 V	9.47	1.33	1.23	0.56	60.2	18.8	54.0	10. r	8.13	-27	-16	3		BD-04 3873
Wo 9520	15 19 38	+21 09.3	0.145	34.7		dM0 e	10.11	1.51		0.94	91.6	5.2	91.6	5.2	9.92					BD+21 2763
GJ 1191	15 19 54	-10 28.8	0.209	195.1	-5.3	K2 V	7.99	0.95	0.79	0.35			50.0	07. r	6.48	0	-17	-12	136713	BD-10 4088
GJ 1192	15 20 11	+01 36.1	0.519	224.6	-26.1	K3 V	8.30	1.00	0.86	0.32	43.5	8.1	42.0	06. r	6.42	-18	-60	-15	136834	BD+01 3071
Gl 584 A	15 21 08	+30 28.0	0.238	144.1	-7.3 SB	G2 V	5.62	+0.58 J	+0.04 J	+0.18tJ	59.6	5.1	59.6	5.1	4.5	15	-5	-13	137107	BD+30 2653
Gl 584 B	15 21 08	+30 28.0	0.238	144.1	-10.6 SB	G2 V	5.96*				59.6	5.1	59.6	5.1	4.84*	14	-6	-16	137108	
Gl 585	15 21 35	+17 39.6	1.302	196.8	84	M4	13.68	1.78	1.18	1.36	85.1	2.9	85.1	2.9	13.33	81	-41	63		
NN A	15 22 36	+37 33.1	0.171	299.4	-8.6 SB	F0 V	4.31	0.31	0.07		39.5	7.4	42.0	07. r	2.43	-19	-10	2	137391	BD+37 2636
NN B	15 22 36	+37 33.4	0.170	299.0	-8.6	G1 V	6.50	0.59	0.13		39.5	7.4	42.0	07. r	4.62	-18	-10	2	137392	BD+37 2637
NN	15 23 02	-26 31.9	0.811	269.6	-48	K3/4 V	8.84	1.05	0.92	0.40	12.7	24.1	42.0	05. r	6.96	-87	-47	30	137303	CD-26 10870

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 585.1	15 25 12	+02 46.3	0.050	259.0		dM0	10.21	1.34	1.23	0.57			40.0	06. r	8.22					BD+03 3032
NN	15 25 15	+10 46.3	0.454	238.0		K5	9.86	1.30		0.55			44.0	06. r	8.08					BD+11 2811
Gl 586 A	15 25 27	-09 10.2	0.365	168.5	+8.2 SB	K2 V	6.92	0.81	0.49	0.29	61.8	5.1	61.8	5.1	5.87	19	-17	-14	137763	BD-08 3981
Gl 586 B	15 25 30	-09 10.8	0.379	165.5	8	K2 V	7.58	0.92	0.65	0.30	61.8	5.1	61.8	5.1	6.53	20	-17	-15	137778	BD-08 3983
Gl 586 C	15 25 03	-08 51.0	0.318	172.0		k-m	15.41	1.84		1.42	48.0	5.0	48.0	5.0	13.82					
Gl 587	15 25 44	-49 46.8	0.238	246.8	-42.7	G5 V	7.69	0.77	0.25	0.32	56.0	13.6	40.0	07. r	5.7	-51	0	1	137676	CP-49 8137
Gl 587.1	15 25 53	+25 57.8	0.120	121.0		dM0	11.12	1.46		0.76			42.0	07. r	9.24					
NN	15 27 58	+43 03.5	0.698	146.4		m	14.17	1.73		1.33	51.1	4.4	51.1	4.4	12.71					
NN	15 28 39	-26 44.8	0.575	219.8		M3.5	13.7 *			1.18			43.0	08. r	11.9 *					
Gl 588	15 28 58	-41 05.6	1.539	228.5	15.4	M3	9.31	1.52	1.11	1.05	165.1	5.4	165.1	5.4	10.4	-6	-46	-1		CD-40 9712
NN	15 29 19	+14 25.7	0.033	200.6		G5	7.70						88.0	10. o	7.42				138441	BD+14 2889
NN	15 29 52	+29 01.2	0.579	274.7		m	14.30			1.34			62.0	10. r	13.26					
NN	15 32 02	+46 24.9	0.199	5.0		m	13.58			1.21			51.0	10. r	12.12					
Gl 588.1	15 32 03	+38 04.9	0.080	166.0		dM0	11.28	1.50	1.20	0.77			40.0	06. r	9.29					
GJ 1193	15 32 13	+14 26.3	0.697	257.7		M3.5	13.83	1.57	1.08	1.21	48.4	3.9	48.4	3.9	12.25					
NN	15 32 43	-14 37.5	0.062	86.2	-28.2	G8.5 III	3.90	1.00	0.74		39.5	15.3	39.5	15.3	1.9	-20	9	-19	138905	BD-14 4237
Gl 589 A	15 33 08	+17 52.9	1.219	263.0	-43.2	M4.5:	12.41	1.58	1.18	1.04	70.2	2.5	70.2	2.5	11.64	-55	-74	12		
Gl 589 B	15 33 08	+17 52.9	1.219	263.0		M6	14.99	1.81	+1.79:	1.40	70.2	2.5	70.2	2.5	14.22					
Gl 590	15 33 21	-37 43.4	0.892	201.7		M4	12.8 :	+1.6 :		0.83	81.6	11.9	81.6	11.9	12.4 :					
NN	15 33 37	+22 19.1	0.743	260.7		k-m	12.69	1.51		1.16	53.2	4.0	53.2	4.0	11.32					
Gl 591	15 34 10	+39 59.7	0.458	276.9	-65.6	K3 V	7.60	0.96	0.76	0.29	47.0	4.2	47.0	4.2	5.96	-43	-62	-26	139323	BD+40 2903
Gl 592	15 34 13	-13 57.5	0.774	216.2		M4	12.70	1.58	1.07	1.23	76.4	4.1	76.4	4.1	12.12					
Gl 593 A	15 34 15	+39 58.0	0.465	277.3	-67.7	K2 V	7.43	+0.91 J	+0.69 J	+0.28 J	47.0	4.2	47.0	4.2	5.79	-44	-64	-28	139341	BD+40 2905
Gl 593 B	15 34 15	+39 58.0	0.465	277.3			7.6 *				47.0	4.2	47.0	4.2	6.0 *					
Gl 594	15 37 45	-44 29.8	0.317	212.7	-5.4	F5 IV-V	4.64	0.40	-0.03	+0.24C	58.3	7.2	58.3	7.2	3.47	-15	-19	-10	139664	CD-44 10310
GJ 1194 A	15 38 16	+43 39.5	1.225	106.3	-108	m	12.48	+1.57 J		+1.11 J	73.3	4.8	73.3	4.8	11.81	31	-22	-128		
GJ 1194 B	15 38 17	+43 39.4	1.225	106.3		m	13.8 *				73.3	4.8	73.3	4.8	13.1 *					
Gl 595	15 39 20	-19 18.6	2.254	243.2	83	M3.5	11.87	1.60	1.05	1.14	111.0	11.8	111.0	11.8	12.1	43	-102	62		
NN	15 40 15	-30 46.1	0.504	226.5		m	13.1 *			1.08			40.0	08. r	11.1 *					
GJ 1195	15 40 22	-10 46.3	1.166	254.9	-171.4	F3 VI	7.22	0.49	-0.21	0.22	39.4	7.9	39.4	7.9	5.2	-190	-108	-34	140283	BD-10 4149
Gl 596 A	15 40 55	+26 26.2	0.166	128.6		K7	10.70	1.29	1.30		56.1	22.2	30.0	07. r	8.1					BD+26 2723
Gl 596 B	15 40 57	+26 25.5	0.186	125.0		m	13.5 P				56.1	22.2	30.0	07. r	10.9 P					
Gl 596.1A	15 41 31	+02 40.4	0.163	200.4	+19.4 SB	G5 V	5.86	0.68	0.24	0.24	50.6	8.1	50.6	8.1	4.38	19	-12	10	140538	BD+02 2989
Gl 596.1B	15 41 31	+02 40.4	0.163	200.4			12.0 *				50.6	8.1	50.6	8.1	10.5 *					
Gl 596.2	15 41 48	+06 34.9	0.142	72.0	2.7	K2 III	2.64	1.17	1.24	0.38	49.7	8.6	49.7	8.6	1.12	5	12	-4	140573	BD+06 3088
Gl 597	15 42 15	+76 09.6	1.141	133.8	-46.1	M3	12.22	1.65	1.18	+1.10:	75.2	3.2	75.2	3.2	11.6	78	-4	-34		
Gl 598	15 44 01	+07 30.5	0.241	250.9	-68.5 SB	G0 V	4.43	0.60	0.11	0.20	83.9	4.6	83.9	4.6	4.05	-50	-25	-41	141004	BD+07 3023
NN	15 44 01	-58 01.6	0.594	245.1		M2-3	11.65			0.88	30.5	11.3	45.0	08. r	9.92					
Gl 599 A	15 44 14	-37 45.6	0.468	241.9	-5.2	G6 V	6.01	0.72	0.31	0.25	73.5	9.4	73.5	9.4	5.34	-17	-25	4	140901	CD-37 10500
Gl 599 B	15 44 14	-37 45.6	0.468	241.9	1	DA7	12.78	0.33	-0.42		73.5	9.4	73.5	9.4	12.11	-52	-10	-4		
NN	15 44 42	-10 44.3	0.505	228.8		M2	11.25			1.02			79.0	16. r	10.74					
NN	15 45 38	+01 43.6	0.240	227.5	-28.4	G8 V	7.43	0.81	0.44		33.6	13.6	46.0	07. r	5.74	-21	-28	-15	141272	BD+ 2 3001

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 599.1	15 47 22	-50 32.2	0.260	102.0	47.9	k	10.72	1.19	1.13	+0.61C	50.0	10.2	23.0	03. r	7.53	60	4	-39		CP-50 8682
NN	15 47 38	+01 06.6	0.180	96.0		m	12.45			1.09			56.0	11. r	11.19					
NN	15 47 46	+34 57.5	0.937	317.4		m	13.16	1.64			56.6	3.9	56.6	3.9	11.92					
NN	15 48 14	+51 11.7	0.472	306.0		M3:	12.05	1.53		0.97			48.0	09. r	10.46					
NN	15 48 19	+04 37.6	0.140	64.6	-9.1	A2 m	3.71	0.15	0.11	0.06	38.4	6.9	38.4	6.9	1.63	-4	14	-13	141795	BD+04 3069
NN	15 48 57	+74 34.2	0.318	162.6	-27	K5	9.31	1.18		0.48	34.2	11.9	46.0	07. r	7.62	38	-17	-8	142474	BD+74 634
NN	15 49 21	+29 40.4	0.501	206.4		M7	13.01	1.58		1.18			58.0	11. r	11.83					
Gl 600	15 49 46	+11 01.6	0.358	228.4	-0.7	dM0	9.36	1.42	1.27	0.65	47.4	4.7	47.4	4.7	7.74	3	-35	8		BD+11 2874
Gl 601 A	15 50 43	-63 16.7	0.440	205.0	0.4	F2 IV	2.84	0.29	0.04	0.07	82.1	11.9	82.1	11.9	2.41	-15	-17	-11	141891	CP-63 3723
NN	15 50 52	+13 21.1	0.584	195.3	+35.1 SB	G1 V	6.10	0.60	0.00	0.22	41.7	19.4	53.0	07. r	4.72	50	-34	18	142267	BD+13 3024
Gl 602	15 50 57	+42 35.4	0.765	35.0	-56.4	F9 V	4.61	0.57	0.00	0.21	57.5	5.7	57.5	5.7	3.41	-44	15	-71	142373	BD+42 2648
NN A	15 51 11	+34 54.5	0.569	151.7		M3	11.75	1.51	1.21	1.07	53.4	3.4	48.7	6.3	10.19					
NN B	15 51 11	+34 54.0	0.569	151.7		m	13.18	1.53		1.20	40.4	4.5	48.7	6.3	11.62					
GJ 1196	15 51 38	-25 51.6	0.250	295.4		K5 V	9.28	1.24	1.23	0.49			47.0	08. r	7.64				142288	CD-25 11183
NN	15 53 08	+34 00.0	0.643	139.0		m	15.95	1.76			42.1	5.9	42.1	5.9	14.07					
NN	15 53 39	+35 20.6	0.261	307.0		m	13.68			1.37			92.0	14. r	13.5					
Wo 9531	15 53 58	+38 05.4	0.084	18.9	-11.6	F0 IV	5.45	0.33	0.03		43.2	8.5	43.2	8.5	3.63	-10	0	-11	142908	BD+38 2712
Gl 603	15 54 08	+15 49.4	1.322	166.6	6.6	F6 V	3.85	0.48	-0.03	0.14	84.1	9.6	84.1	9.6	3.47	60	-36	-26	142860	BD+16 2849
Gl 604	15 54 16	-42 28.7	0.323	233.3	35.6	K5 V	8.05	1.12	1.03	0.43	58.9	7.8	58.9	7.8	6.9	21	-38	7	142709	CD-42 10934
Wo 9532	15 55 44	+63 57.4	0.220	326.9	-0.6	G5	9.54	0.89	0.59		44.2	8.5	21.0	03. r	6.15	-49	-9	3	143433	BD+64 1102
NN	15 56 27	+35 32.7	0.353	333.0		M6 :	12.69	1.59		1.15			61.0	12. r	11.62					
Wo 9533	15 56 32	+27 52.7	0.828	291.5	-69.8	K0 V	8.01	0.77	0.30	0.27	44.4	7.8	44.4	7.8	6.25	-90	-67	5	143291	BD+28 2503
NN	15 56 38	+25 42.8	0.136	215.2	-4.5 SB	K2 V	8.33	1.00	0.72				44.0	07. r	6.55	4	-15	0	143313	BD+25 3003
Gl 604.1	15 56 52	-45 18.6	0.203	228.8	-23.6	G5 IV	7.54	0.74	0.38	+0.35C	44.2	15.3	44.2	15.3	5.8	-31	-9	-3	143120	CD-45 10373
Wo 9535	15 57 11	+65 32.4	0.238	136.2	-8.0 SB	dG5	9.04	0.86	0.56		42.3	13.6	26.0	03. r	6.11	41	8	-14	143665	BD+65 1092
Gl 606	15 57 11	-08 06.8	0.194	104.7		dM0	10.50	1.51	1.16	0.89	98.1	8.0	98.1	8.0	10.46					BD-07 4156
NN	15 57 31	-16 23.3	0.747	238.0	-25	F8 V	5.47	0.52	0.03	0.16	33.2	6.0	33.2	6.0	3.08	-44	-100	13	143333	BD-16 4196
NN	15 57 34	+15 08.9	0.846	209.5		m	13.99	1.58	1.13	1.15	40.0	5.9	40.0	5.9	12					
Gl 606.1A	15 58 21	-84 05.8	0.320	269.0	-10.5	K0 V	7.68	0.78	0.43	+0.41CJ	49.0	17.0	39.0	06. r	5.64	-21	-18	29	142022	CP-83 593
Gl 606.1B	15 58 21	-84 05.8	0.320	269.0		k-m	11.03	1.36	1.19		49.0	17.0	39.0	06. r	8.99					
NN	15 59 08	+40 28.3	0.394	227.0		m	13.12			1.13			47.0	09. r	11.48					
Gl 606.2	15 59 08	+33 27.2	0.798	194.8	18.4	G0 V	5.41	0.60	0.08		40.2	12.4	60.0	06. s	4.3	52	-34	21	143761	BD+33 2663
NN	15 59 24	-24 57.2	0.650	200.8		m	13.2 *			1.15			49.0	10. r	11.7 *					
Gl 607	15 59 45	+30 19.0	0.351	293.0	10.1	M3	12.51	1.56	1.20		61.2	5.1	61.2	5.1	11.44	-14	-5	25		
Gl 608	15 59 53	+61 48.0	0.462	274.6	-36.5	dM0	9.99	1.29	1.23	0.52	42.5	5.9	42.5	5.9	8.13	-21	-59	7		BD+62 1446
NN A	15 59 54	+30 35.8	0.189	316.0		m	13.37			1.11			45.0	05. r	11.64					
NN B	15 59 46	+30 35.9	0.189	316.0		m	15.17			1.39			45.0	05. r	13.44					
Gl 609	16 00 43	+20 44.6	1.571	217.6	25	M3	12.56	1.63	1.20	1.27	99.4	3.0	99.4	3.0	12.55	40	-58	35		
Gl 609.1	16 00 57	+58 41.9	0.467	316.0	-7.7 SB	F8 IV-V	4.01	0.52	0.10		48.7	8.5	48.7	8.5	2.45	-42	-17	7	144284	BD+58 1608
Wo 9540 A	16 01 37	-11 14.2	0.072	241.7	-32.2	F6 IV-V	4.84	+0.45 J	+0.03 J		41.1	4.2	41.1	4.2	2.91	-30	-8	-13	144070	BD-10 4237
Wo 9540 B	16 01 37	-11 14.2	0.072	241.7		F6 IV-V	5.0 *				41.1	4.2	41.1	4.2	3.1 *				144069	
Wo 9540 C	16 01 37	-11 14.1	0.070	254.3	-31.3	G8 V	7.30	0.75			41.1	4.2	41.1	4.2	5.37	-29	-7	-11		

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	16 01 40	-06 07.9	0.854	184.0		dM4.5-5	15.51	1.89			60.4	4.4	60.4	4.4	14.42					
Wo 9541 A	16 01 41	-11 18.8	0.075	248.0	-31.5	G8 V	7.46	0.74	0.29		43.0	4.5	43.0	4.5	5.63	-29	-7	-12	144087	BD-11 4057
Wo 9541 B	16 01 41	-11 18.8	0.070	248.1	-28.1	K2 V	8.03	0.84	0.51		43.0	4.5	43.0	4.5	6.2	-26	-7	-11	144088	BD-11 4058
Gl 609.2	16 01 59	+25 22.9	0.867	322.2	-48.2 SB	G8 V	7.10	0.77	0.33	0.28	54.6	8.0	54.6	8.0	5.79	-88	-16	5	144287	BD+25 3020
Wo 9543 A	16 02 29	-32 43.5	0.426	237.0	-26.4	G9 V	8.34	+0.82 J	+0.38 J		41.0	7.2	41.0	7.2	6.4	-40	-39	2	144179	CD-32 11405
Wo 9543 B	16 02 29	-32 43.5	0.426	237.0		K1 V	9.0 *				41.0	7.2	41.0	7.2	7.1 *					
Wo 9543 C	16 02 29	-32 43.5	0.426	237.0		K5	11.1 *				41.0	7.2	41.0	7.2	9.2 *					
Gl 610	16 02 44	-20 18.6	0.465	140.0	43.4	K3/4 V	7.40	1.04	0.94	0.38	58.5	4.4	58.5	4.4	6.24	54	-11	-17	144253	BD-20 4399
NN	16 02 57	-45 02.4	0.027	4.5	-15.5	A m	4.72	0.23	0.15	0.12	33.3	9.2	33.3	9.2	2.3	-13	9	1	144197	CD-44 10625
Gl 611 A	16 03 13	+39 17.4	0.579	275.0	-60	G8 V	6.66	0.73	0.21		80.1	7.6	80.1	7.6	6.18	-34	-56	-22	144579	BD+39 2947
Gl 611 B	16 03 07	+39 17.6	0.624	274.5		m	14.23	1.72		+1.25:	72.5	3.4	72.5	3.4	13.53					
Gl 611.1	16 03 51	-70 55.9	0.440	208.3	25.7	G8 V	7.22	0.72	0.31	+0.35C	47.9	8.0	47.9	8.0	5.62	-12	-45	-19	144009	CP-70 2163
Gl 611.2	16 03 58	+80 45.8	0.044	334.6	-21.1	K0	7.57	1.06	0.96		46.1	10.2	46.1	10.2	5.89	3	-17	-12	145742	BD+81 541
Gl 611.3	16 04 18	+08 31.2	0.503	279.4	-41.6	dM3 e	11.55	1.46		0.85	36.6	5.4	36.6	5.4	9.37	-59	-45	20		
Gl 612	16 04 42	+38 46.4	0.577	157.8	24.1	K3 V	8.61	0.96	0.71		56.6	13.2	38.0	06. r	6.51	76	0	0	144872	BD+39 2950
Gl 612.1	16 04 48	+34 45.9	0.622	153.6	8.2	dM0	10.45	1.24	1.25	0.50	49.8	9.8	49.8	9.8	8.94	58	-6	-14		BD+35 2774
NN	16 05 02	+06 06.1	0.377	233.0		m	13.46			1.15			43.0	09. r	11.63					
GJ 1197	16 05 09	+26 58.6	0.564	140.3		m	13.33	1.64	1.25	1.02	45.6	3.7	45.6	3.7	11.62					
NN	16 05 10	+47 38.1	0.123	3.0	-17.3	dK8	9.90	1.17	1.08	0.43	42.9	4.1	42.9	4.1	8.06	-15	-6	-15		BD+47 2298
GJ 1198	16 05 31	-10 17.3	1.354	195.1		M2	14.70:	+1.70:	+0.99:	1.30	46.9	2.7	46.9	2.7	13.06:					
Gl 613	16 05 41	-56 19.1	0.351	338.7	37.9	K3 V	7.11	0.85	0.48	0.38	75.3	11.9	75.3	11.9	6.49	37	-14	18	144628	CP-56 7345
NN	16 07 11	+77 02.9	0.309	281.0		M1.5	12.35			1.05			42.0	10. r	10.5					
NN	16 07 47	+53 04.4	0.230	71.0		dM0	10.19	1.45		0.76			64.0	10. r	9.22					
NN	16 07 56	-70 01.2	0.643	203.3		k-m	13.75			1.31			70.0	11. r	12.98					
Wo 9547	16 07 57	-52 47.0	0.440	216.0		g	10.50	1.16	1.12		39.4	5.9	39.4	5.9	8.48					CP-52 9317
Gl 614	16 08 47	+43 57.0	0.323	155.9	-13.3	K0 V	6.66	0.88	0.66		61.9	10.2	61.9	10.2	5.62	21	-11	-15	145675	BD+44 2549
GJ 1199	16 09 06	+13 30.4	0.541	181.1	131	DA6	15.09	0.23	-0.64		54.9	4.7	54.9	4.7	13.79	88	-3	43		
Gl 615	16 09 47	-57 25.5	1.647	212.0	10	K0 V	7.53	0.83	0.28	0.32	69.9	6.4	69.9	6.4	6.75	-52	-95	-29	145417	CP-57 7690
NN	16 10 44	-21 16.4	0.122	273.6	16.7	G3 V	6.69	0.61	0.08				40.0	06. r	4.7	10	-10	16	145809	BD-21 4305
Gl 615.1A	16 10 58	+13 39.6	0.456	156.7	18.1	G8 V	7.36	+0.76 J	+0.39 J		51.8	5.2	51.8	5.2	5.93	43	-9	-11	145958	BD+13 3091
Gl 615.1B	16 10 58	+13 39.6	0.456	156.7	20.8	G8 V	7.5 *				51.8	5.2	51.8	5.2	6.1 *	45	-8	-10		
NN	16 11 17	-28 22.6	0.520	224.7		M3.5	12.96			1.19			62.0	12. r	11.92					
NN	16 12 17	+04 59.6	0.427	280.8		m	13.53			1.18			47.0	09. r	11.89					
GJ 1200	16 12 27	+19 13.3	2.033	280.0	-82	m	12.92	1.54	1.10	1.12	56.5	3.9	56.5	3.9	11.68	-127	-123	67		
Gl 615.2A	16 12 48	+33 59.0	0.287	253.6	-12.2 SB	F8 V	5.64	0.51	0.00	0.21	44.4	5.4	44.4	5.4	3.88	-7	-30	11	146361	BD+34 2750
Gl 615.2B	16 12 48	+33 59.0	0.287	253.6	-14.5	G1 V	6.72			0.24	44.4	5.4	44.4	5.4	4.96	-8	-32	9	146362	
Gl 615.2C	16 12 03	+33 53.9	0.305	254.0		M3.5	12.31	1.40		1.04	44.4	5.4	44.4	5.4	10.55					
Gl 616	16 12 54	-08 14.3	0.554	155.6	12	G1 V	5.49	0.65	0.16	0.22	65.1	6.5	65.1	6.5	4.56	29	-16	-25	146233	BD-07 4242
NN	16 13 26	+24 35.0	0.252	344.0		M2	11.99	1.51		0.91			42.0	08. r	10.11					
NN	16 14 05	+35 56.5	0.252	307.0		K5	9.62	1.23	1.36				41.0	09. r	7.68					
Wo 9551	16 15 10	+71 03.4	0.286	181.6	-17.5	dG5	7.90	0.63	0.22		42.0	8.2	25.0	03. r	4.89	53	-18	11	147231	BD+71 775
NN	16 15 40	-04 34.3	0.091	65.2	-7.7 VAR	G9.5 IIIb	3.24	0.96	0.75		40.6	8.8	40.6	8.8	1.28	-5	9	-8	146791	BD-04 4086

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 616.2	16 15 59	+55 23.8	0.492	157.2	-32.6	dM1.5e	9.96	1.48	1.08	0.90	47.5	6.5	47.5	6.5	8.34	47	-23	-27		BD+55 1823
Wo 9553	16 16 02	-28 10.2	0.260	169.1	-31.1	G0 V	7.67	0.61	0.12		42.6	9.0	23.0	03. s	4.48	-24	-27	-50	146775	CD-27 10902
Wo 9554	16 16 05	-50 02.1	0.162	251.0	-28.9	G8 III	4.02	1.08	1.16	0.41	43.0	11.9	43.0	11.9	2.2	-33	-1	8	146686	CD-49 10536
Gl 617 A	16 16 37	+67 21.5	0.510	280.3	-19.9 VAR	M0 Ve	8.60	1.41	1.26	0.68	88.3	3.8	88.3	3.8	8.33	-11	-32	5	147379	BD+67 935
Gl 617 B	16 16 39	+67 22.6	0.522	278.6	-19.5	M2.5	10.72	1.49	1.13	1.08	88.3	3.8	88.3	3.8	10.45	-10	-32	6		
Gl 618 A	16 16 47	-37 25.4	1.222	324.5	20	M3	10.60	1.57	1.21	1.08	130.0	8.2	130.0	8.2	11.17	15	3	47		CD-37 10765
Gl 618 B	16 16 47	-37 25.4	1.222	324.5		M5 :	14.15	1.79		1.59	130.0	8.2	130.0	8.2	14.72					
Gl 618.1	16 17 48	-04 08.9	0.409	268.0	-118.1	dM2	10.70	1.40	1.28	0.68	27.2	3.9	27.2	3.9	7.87	-122	-64	-11		
Wo 9557 A	16 18 12	+39 49.6	0.137	270.8	-29	F3 IV-V	5.46	0.40	-0.08		40.9	10.2	40.9	10.2	3.5	-14	-28	-9	147365	BD+40 3005
Wo 9557 B	16 18 12	+39 49.6	0.137	270.8			11. *				40.9	10.2	40.9	10.2	9. *					
NN A	16 18 56	+75 52.3	0.267	341.0	-9.5 VAR	F3 V	4.95	0.37	0.08		40.7	7.5	40.7	7.5	3	-27	-14	-10	148048	BD+76 596
NN B	16 19 50	+75 50.1	0.264	341.0		m	14.51				40.7	7.5	40.7	7.5	12.56					
Gl 618.4	16 19 01	-48 31.9	0.763	231.6		M3	11.83	1.48		0.89	43.1	8.4	43.1	8.4	10					
Gl 619	16 19 12	+41 04.6	0.122	347.7	7.5	dM0 p	8.98	1.30	1.17	0.56	73.6	16.4	68.0	09. r	8.14	-6	7	7		BD+41 2695
NN	16 19 32	+01 08.7	0.165	287.2	-45.5 VAR	F0 V	4.82	0.34	0.04		45.3	7.6	45.3	7.6	3.1	-44	-16	-11	147449	BD+01 3215
Gl 620	16 20 07	-24 35.1	0.712	206.4		M1	10.23	1.47	1.18	0.75	49.1	17.0	66.0	13. r	9.33					CD-24 12677
Gl 620.1A	16 20 38	-39 04.7	0.074	91.1	17	G3/5 V	5.39	0.63	0.14	0.22	66.4	10.7	78.0	11. r	4.85	17	-3	-1	147513	CD-38 10983
Gl 620.1B	16 20 10	-39 06.8	0.080	90.0	52	DA2	11.00	-0.14	-0.96		65.5	5.4	78.0	11. r	10.46	8	1	-3		CD-38 10980
Gl 621	16 21 32	-13 31.5	0.316	227.6	9	K3 V	8.40	0.96	0.72	0.34	60.2	7.8	60.2	7.8	7.3	7	-24	7	147776	BD-13 4418
Gl 622	16 22 17	-21 49.1	0.640	240.7		K5	10.40	1.45	1.18	0.71	66.4	6.9	66.4	6.9	9.51					BD-21 4352
Gl 623	16 22 39	+48 28.4	1.231	111.6	-27.8 SB	dM3	10.28	1.48	1.09	1.02	131.7	3.9	131.7	3.9	10.88	22	1	-47		
Gl 624	16 23 04	-69 58.5	0.231	63.5	+7.6 SB	G0 V	4.91	0.55	0.04	0.19	92.4	10.2	92.4	10.2	4.74	12	4	-6	147584	CP-69 2558
Gl 624.1A	16 23 18	+61 37.6	0.080	338.0	-13.7	G8 III	2.74	0.91	0.70		46.2	18.7	46.2	18.7	1.1	-8	-11	-9	148387	
Gl 624.1B	16 23 18	+61 37.6	0.080	338.0		K2	8.8 *				46.2	18.7	46.2	18.7	7.1 *					BD+61 1591
NN	16 23 29	+26 08.4	0.184	271.0		m	12.24			1.11			66.0	13. r	11.34					
NN	16 23 56	-17 16.5	0.519	219.5		m	14.3 *			1.43			84.0	13. r	13.9 *					
Gl 625	16 24 14	+54 25.1	0.420	108.0	-12.6	dM2	10.12	1.61	1.23	0.96	159.3	4.6	159.3	4.6	11.13	6	-3	-16		
GJ 1201	16 25 30	+09 19.3	0.469	191.5		DA s	16.13	0.38	-0.45		44.3	4.5	44.3	4.5	14.36					
Gl 626	16 25 32	+07 25.2	0.346	224.5	-35	dK8	8.83	1.23	1.22	0.50	53.6	9.2	61.0	08. r	7.76	-21	-36	-14	148467	BD+07 3180
Gl 626.1	16 25 43	-78 47.3	0.141	239.6	+5.4 VAR	K0 IV	3.89	0.91	0.62	+0.44C	54.1	15.3	54.1	15.3	2.6	-4	-13	2	147675	CP-78 1103
NN	16 25 46	+15 40.8	0.304	177.0		m	13.18			1.10			41.0	08. r	11.24					
NN	16 25 52	+25 18.3	0.057	171.7		G5	8.19						41.0	05. o	6.25				148555	BD+25 3086
Gl 626.2	16 26 40	+36 52.2	0.864	326.4	24	DZA6	13.85	0.17	-0.67		64.0	3.5	64.0	3.5	12.88	-65	-11	14		
Gl 627 A	16 26 41	+18 31.1	0.514	318.0	-36.2	K3 V	7.68	+0.85 J	+0.45 J	+0.32 J	58.4	9.8	50.0	06. r	6.17	-58	-14	10	148653	BD+18 3182
Gl 627 B	16 26 41	+18 31.1	0.514	318.0		K3 V	7.85*				58.4	9.8	50.0	06. r	6.34*					
GJ 2121	16 27 24	-14 33.3	0.539	243.5		M3	12.32:	+1.52:	+1.43:	1.09			58.0	15. r	11.1 :					
Gl 628	16 27 31	-12 32.3	1.175	183.4	-13.0 SB	M3.5	10.08	1.58	1.18	1.20	244.7	6.3	244.7	6.3	12.02	-6	-19	-17		BD-12 4523
NN	16 28 06	-03 52.9	0.159	262.4		K5	9.58	1.25	1.22	0.50			44.0	06. r	7.8					BD- 3 3952
Gl 629	16 28 08	-38 54.1	0.543	232.5	-50.6 SB	K0 V	7.24	0.86	0.48	0.34	56.1	8.5	56.1	8.5	5.98	-62	-28	2	148704	CD-38 11019
NN	16 28 48	-87 19.0	0.066	170.0		DA6	14.58	0.22	-0.63				41.0	08. w	12.64					
GJ 1202	16 29 22	+17 40.9	0.886	202.7		k-m	12.78	1.57	1.14	1.10	53.0	2.9	53.0	2.9	11.4					
NN	16 29 39	+40 58.0	0.358	330.0		m+	14.79	1.72		1.60			100.0	29. r	14.8					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Wo 9566	16 30 23	+03 21.2	0.420	243.0	-58.0 SB	K1	8.85	0.88	0.54	0.34	40.8	7.5	29.0	05. r	6.16	-47	-77	0	149162	BD+03 3215
GJ 1203	16 30 28	+12 43.1	0.788	260.2		k-m	12.18:	1.46	1.14	1.06	50.7	3.6	50.7	3.6	10.71:					
NN	16 30 29	+09 56.6	0.287	57.0		m	13.05	1.66		1.18			60.0	11. r	11.94					
NN	16 30 50	-53 28.7	0.671	195.4		m	12.0 *			1.02			56.0	11. r	10.7 *					
Gl 629.2A	16 32 05	-04 07.0	0.704	193.3	-171.6 SB	G5 Ve	9.62	0.74	0.11	0.32	50.9	9.6	50.9	9.6	8.15	-126	-89	-100	149414	BD-03 3968
NN	16 32 10	+03 24.2	0.240	132.0		k	11.57	1.48	1.24				48.0	23. r	10					
NN	16 32 19	-27 11.3	0.924	179.7		m	14.2 *			1.31			57.0	09. r	13.0 *					
Gl 629.3	16 32 33	-49 11.2	0.599	184.8		M1 :	12.38	1.48	1.15	0.96	51.6	13.6	51.6	13.6	10.9					
NN	16 32 35	-30 44.5	1.189	225.3		M3.5	12.68	1.54	1.02	1.05			46.0	12. r	11					
Gl 630	16 33 17	+33 24.3	0.263	252.0		dM0	11.06	1.34	1.27	0.60	45.0	8.1	29.0	04. r	8.37					
NN	16 33 25	+43 24.0	0.356	143.6		DA8	14.82	0.42	-0.42		66.5	3.0	66.5	3.0	13.93					
Gl 630.1A	16 33 29	+57 14.8	1.620	316.0	-118.6 SB	dM4 e	12.90	1.60	1.05	1.32	69.0	2.9	69.0	2.9	12.09	-103	-121	-34		
Gl 630.1B	16 33 31	+57 15.2	1.620	316.0		DQ8	15.00	0.49	-0.36		69.0	2.9	69.0	2.9	14.19					
NN	16 33 37	+35 07.2	0.197	137.0		m	12.95			1.27			87.0	15. r	12.65					
GJ 1204	16 33 43	+08 54.9	0.557	254.1		m	13.80	1.65		1.29	65.2	4.2	65.2	4.2	12.87					
Gl 631	16 33 44	-02 13.2	0.552	124.6	-12.1	K0 Ve	5.75	0.82	0.42	0.28	95.1	8.1	95.1	8.1	5.64	3	0	-30	149661	BD-01 3220
Gl 632	16 34 28	+79 53.7	0.126	135.7	-16.9	dG3	7.06	0.62	0.06		44.8	22.9	34.0	06. r	4.72	20	-4	-13	150706	BD+80 519
Gl 632.1	16 34 52	+31 12.2	0.553	142.4	-10.3	dK6	9.49	1.20	1.16	0.46	60.5	10.7	60.5	10.7	8.4	31	-7	-31	149957	BD+31 2875
Gl 632.2A	16 35 48	+76 04.9	0.180	41.0	-7.1	K7	10.02	+1.15 J		+0.47 J	50.9	13.6	29.0	05. r	7.33	-14	5	-26		BD+76 614
Gl 632.2B	16 35 47	+76 04.9	0.160	38.0		DA	13. *				50.9	13.6	29.0	05. r	10. *					
Gl 632.3	16 36 13	+05 31.4	0.180	267.0		G	10.22	0.99			46.4	10.2	19.0	03. r	6.61					
Gl 633	16 37 09	-45 54.2	0.536	137.9	30	M3	12.68	1.61	1.20	1.07	104.6	11.9	104.6	11.9	12.78	27	-13	-24		
Wo 9572	16 37 22	+05 36.5	0.336	162.4	51	K2	8.67	0.89	0.60		39.6	30.8	32.0	05. r	6.2	71	-8	-4	150281	BD+05 3246
NN	16 37 32	+00 48.3	0.217	135.0		m	13.69	1.70		1.33	89.3	4.6	89.3	4.6	13.44					
Gl 634	16 37 56	-43 53.0	0.614	219.4	-42	M3	11.57	1.55		0.92	54.8	10.7	54.8	10.7	10.26	-57	-36	-3		CD-43 11010
Gl 634.1	16 38 31	-02 45.3	0.440	183.1	-40.1	dG2	7.22	0.64	0.07	+0.35C	45.8	6.0	45.8	6.0	5.52	-15	-44	-38	150433	BD-02 4230
Wo 9574	16 38 41	-17 38.8	0.022	260.3	-22.1	G7.5 II CN	4.96	1.11	0.87		43.7	12.2	43.7	12.2	3.2	-21	-2	-5	150416	BD-17 4618
NN	16 39 02	+36 24.6	0.222	324.0		M2	11.50	1.50		0.93			55.0	10. r	10.2					
NN	16 39 06	-05 43.5	0.225	175.0		g-k	12.06	1.50	1.25				43.0	21. r	10.2					
Gl 635 A	16 39 24	+31 41.5	0.614	309.9	-70.4 SB	G0 IV	2.91	+0.65 J	+0.21 J	+0.23 J	99.0	2.8	99.0	2.8	2.89	-54	-47	-26	150680	BD+31 2884
Gl 635 B	16 39 24	+31 41.5	0.614	309.9	SB?	K0 V	5.4 *				99.0	2.8	99.0	2.8	5.4 *					
NN	16 39 25	-37 14.8	0.093	176.3		G8 V	7.13	0.77					50.0	07. r	5.62				150474	CD-37 10931
GJ 1205	16 39 50	+53 47.0	0.236	212.0		DC7	15.06	0.33	-0.52		48.1	3.5	48.1	3.5	13.47					
NN	16 40 22	+67 41.5	0.451	325.6		m	15.65	1.95			75.2	4.3	75.2	4.3	15.03					
Gl 635.1	16 40 41	+79 00.8	0.060	334.3	-20.9	gG9	6.32	1.14	1.20		46.0	18.8	46.0	18.8	4.6	1	-19	-11	151623	BD+79 511
Gl 637	16 42 30	-72 52.8	0.701	226.7	-27	m	11.35	1.57	1.22	0.86	67.0	12.4	67.0	12.4	10.48	-50	-21	16		
Gl 637.1	16 42 44	+68 11.3	0.522	325.8	10.4	K1 V	7.56	0.79	0.36		48.4	11.6	44.0	07. r	5.78	-53	-10	18	151541	BD+68 883
Gl 638	16 43 15	+33 35.7	0.389	352.6	-30.6	K7 V	8.11	1.37	1.29	0.57	103.2	3.0	103.2	3.0	8.18	-29	-12	-16	151288	BD+33 2777
Wo 9577	16 43 35	-30 31.6	0.168	228.4	43	K5	10.59	1.41	1.26		40.8	15.3	34.0	10. r	8.2	38	-29	11		CD-30 13458
NN	16 44 00	+16 34.4	0.585	206.4		m	11.65			1.05			72.0	14. r	10.94					
Wo 9578	16 44 21	+56 52.2	0.065	10.7	-3.6 SB	F2 V	4.85	0.38	-0.06		44.1	11.9	44.1	11.9	3.1	-7	-1	-4	151613	BD+57 1702
Gl 638.1	16 45 16	-47 37.9	0.096	246.6	29.4	K0 V	7.38	0.91	0.59	0.32	18.1	10.2	57.0	09. r	6.16	25	-18	3	151337	CD-47 11068

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	16 45 54	-15 39.0	0.248	180.0		M2	10.94	1.50		0.88			63.0	11. r	9.94					
Gl 639	16 46 50	+37 06.3	0.369	192.0	2.7	K7 V	8.41	0.82	0.44		52.3	11.4	52.3	11.4	7	29	-16	4	151877	BD+37 2804
Gl 639.2	16 47 00	-64 21.2	0.530	256.1		g	11.00	0.72	0.04	0.29	51.0	13.6	51.0	13.6	9.5					
GJ 1206	16 47 38	+59 08.8	0.317	154.0		DAV4	12.23	0.18	-0.64		81.2	4.6	81.2	4.6	11.78					
NN	16 47 43	+39 21.8	0.296	162.7	26	K4	9.75	1.27		0.54	14.3	13.6	44.0	06. r	7.97	39	11	7		BD+39 3048
Gl 640	16 47 54	+18 59.2	0.087	200.0	-4.8	dK5	8.90	1.02	0.89	0.40	36.2	6.8	40.0	04. r	6.91	3	-11	-3	151995	BD+19 3174
NN	16 48 17	-04 45.4	0.762	249.9		k	13.4 *			1.17			48.0	09. r	11.8 *					
NN	16 48 50	+22 31.8	0.410	3.0		m	14.08	1.75		1.46			100.0	15. r	14.08					
NN	16 48 59	+47 48.9	0.110	249.0	-0.4	dK8	9.42	1.19	1.12	0.42	42.6	12.4	37.0	04. r	7.26	2	-10	10		BD+47 2391
NN	16 49 11	+38 14.0	0.078	19.3	6	dK8	10.55	1.59	1.14	0.98	27.4	13.6	102.0	20. r	10.59	-1	6	3		BD+38 2847
Gl 641	16 50 27	+00 04.5	1.658	205.8	45.4	G8 V	6.64	0.76	0.32	0.24	60.5	8.9	60.5	8.9	5.55	84	-108	10	152391	BD+00 3593
NN	16 51 15	+40 10.2	0.219	192.0		m	13.44			1.16			45.0	09. r	11.71					
Gl 642	16 51 54	+11 59.5	0.670	299.6	-67.3	dM1.5	10.74	1.45	1.24	0.71	58.1	18.8	45.0	09. r	9.01	-84	-43	25		
Gl 643	16 52 45	-08 13.9	1.190	222.5	-14.1 SB	sdM4	11.80	1.69	1.35	1.21	171.9	7.3	171.9	7.3	12.98	-8	-35	0		
Gl 644 A	16 52 48	-08 14.7	1.183	222.2	12.1	M3 J	9.69	+1.57 J	+1.08 J	+1.08 J	153.9	2.6	153.9	2.6	10.63	16	-34	9	152751	BD-08 4352
Gl 644 B	16 52 48	-08 14.7	1.183	222.2			9.9 *				153.9	2.6	153.9	2.6	10.8 *					
Gl 644 C	16 52 55	-08 18.2	1.190	222.5	20	M7	16.78	+1.99:		1.92	153.9	2.6	153.9	2.6	17.72	23	-32	12		
Gl 645	16 53 24	-36 58.7	0.469	198.0		M1	11.44	1.51		+1.12C	59.6	8.4	59.6	8.4	10.32					
GJ 1207	16 54 26	-04 16.0	0.636	126.3		dM3.5	12.28	1.60	1.11	1.24	104.4	8.0	104.4	8.0	12.37					
Wo 9581	16 54 28	-55 54.8	0.038	201.2	-6	K5 III	3.12	1.60	1.97	0.64	41.8	15.3	41.8	15.3	1.2	-7	-1	0	152786	CP-55 7766
GJ 1208	16 55 01	+21 31.8	0.578	176.9	46	DA6	14.06	0.25	-0.56		43.0	3.1	43.0	3.1	12.23	50	-35	-19		
NN	16 55 04	+13 32.9	0.211	134.0		m	14.35			1.25			42.0	08. r	12.47					
Gl 646 A	16 55 26	-39 29.2	0.331	55.6	42.5	K5 V	8.50	+1.16 J	+1.08:J	+0.64CJ	73.0	10.2	73.0	10.2	7.82	46	9	-5	153026	CD-39 10940
Gl 646 B	16 55 26	-39 29.2	0.331	55.6			10.4 *				73.0	10.2	73.0	10.2	9.7 *					
Gl 647	16 55 28	+13 22.0	0.100	29.0		dM0	10.66	1.36	1.31	0.67	26.2	4.1	26.2	4.1	7.75					
Gl 648	16 55 45	+65 12.7	0.229	76.6	-20.9 SB	F6 V	4.89	0.48	-0.03	+0.17t	52.9	9.7	59.0	07. r	3.74	1	-6	-27	153597	BD+65 1157
Gl 649	16 56 07	+25 49.6	0.527	191.9	+4.3 VAR	dM2	9.65	1.50	1.20	0.85	105.0	4.5	105.0	4.5	9.76	20	-13	1		BD+25 3173
NN	16 56 09	+14 02.6	0.380	271.0		m	13.13			1.26			77.0	13. r	12.56					
Gl 649.1A	16 56 30	+47 26.3	0.317	330.1	-6.6	dK8 J	7.83	0.98	0.80	0.34	57.0	4.4	57.0	4.4	6.61	-26	-6	6	153557	BD+47 2415
Gl 649.1B	16 56 30	+47 26.3	0.317	330.1			11.19	1.47	1.04	0.81	57.0	4.4	57.0	4.4	9.97					
Gl 649.1C	16 56 19	+47 26.0	0.303	332.5	-7	dK8	7.90	1.00	0.82	0.34	57.0	4.4	57.0	4.4	6.68	-25	-6	5	153525	BD+47 2411
NN	16 57 44	-61 29.6	0.204	195.9		K3 V	8.84	1.04	0.92	0.39			40.0	06. r	6.85					CD-61 5703
NN	16 58 18	+25 25.3	0.186	328.0		m	13.22			1.09			39.0	08. r	11.18					
Gl 650	16 58 22	-13 29.4	0.320	184.1	+83.4 SB	G2 V	7.12	0.58	0.10	+0.33C	58.5	13.6	32.0	06. r	4.65	91	-29	1	153631	BD-13 4528
NN	16 58 39	+08 16.9	0.290	236.0		m	13.43			1.17			47.0	09. r	11.79					
NN	16 59 09	-53 09.9	0.150	178.6	7	F6 V	5.29	0.50	0.01		31.5	4.6	40.0	04. s	3.3	-1	-15	-12	153580	CP-53 8316
NN	16 59 50	+77 47.2	0.259	56.0		m	12.67			1.05			45.0	09. r	10.94					
NN	17 00 09	-05 59.8				dM2	10.85	1.50	1.22	0.78			50.0	08. r	9.34					BD- 5 4394
Gl 651	17 01 12	+47 08.4	0.874	7.9	-47.3	G8 V	6.77	0.73	0.27		61.8	6.0	61.8	6.0	5.72	-73	-12	-35	154345	BD+47 2420
Gl 652	17 01 19	-28 30.6	0.277	160.5	15.3	G8 IV-V	6.58	0.83	0.54	+0.38C	69.8	8.2	69.8	8.2	5.8	16	-12	-14	154088	CD-28 12769
GJ 1209	17 02 08	+17 00.9	1.136	174.5	75	m	12.28	1.55	+1.18:	1.04	57.9	3.0	57.9	3.0	11.09	119	-13	2		
NN	17 02 11	+51 28.0	0.646	13.0		k-m	13.56	1.75			105.2	2.5	105.2	2.5	13.67					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 653	17 02 27	-04 59.0	1.471	218.5	34.2	K5 V	7.73	1.16	1.06	0.49	88.7	5.7	88.7	5.7	7.47	48	-68	21	154363	BD-04 4225
Wo 9582 A	17 02 37	+59 39.0	0.446	303.4	-73.1	K4 V	8.65	1.04	0.94	0.38	47.6	7.6	43.0	05. r	6.82	-34	-80	-14	154712	BD+59 1783
Wo 9582 B	17 02 38	+59 39.2	0.458	304.7	-72.7	K4	10.31	1.40	1.33	0.64	47.6	7.6	43.0	05. r	8.48	-36	-80	-14		
Gl 654	17 02 37	-05 00.7	1.461	219.2	34.6	M3.5V	10.08	1.44	1.07	0.91	104.7	10.6	104.7	10.6	10.18	46	-55	20		BD-04 4226
Gl 654.1	17 02 44	+00 46.5	0.335	183.1	-15.8	F9 V	6.00	0.58	0.05	+0.31C	46.9	11.9	51.0	09. r	4.54	2	-29	-19	154417	BD+00 3629
Gl 654.2	17 04 00	+15 17.8	0.127	224.9	-30.9	K0 V	7.09	0.94	0.67				69.0	11. r	6.28	-18	-23	-13	154653	BD+15 3108
Wo 9584 A	17 04 17	+54 32.1	0.113	316.3	-14.3	F7 V	5.63	+0.47 J	+0.03 J		46.8	8.3	43.0	06. r	3.8	-12	-15	-2	154906	BD+54 1857
Wo 9584 B	17 04 17	+54 32.1	0.113	316.3	-16.5 SB	F7 V	5.73*				46.8	8.3	43.0	06. r	3.90*	-12	-17	-4	154905	
Wo 9584 C	17 04 17	+54 32.1	0.113	316.3		M3 :	13.5 *				46.8	8.3	43.0	06. r	11.7 *					
Gl 654.3	17 04 36	-41 39.3	0.385	213.2	-19.1	K5 V	8.29	1.05	0.90	0.40	53.0	11.9	55.0	08. r	6.99	-27	-27	-2	154590	CP-41 7862
Gl 654.4	17 04 50	+88 41.8	0.029	0.0	-10.3	K0	8.32	0.87	0.54		47.5	10.2	36.0	05. r	6.1	1	-9	-6	163545	BD+88 105
Gl 655	17 05 01	+21 37.1	0.481	268.6	-49.9	M3	11.61	1.56	1.30	+1.06:	65.5	7.2	65.5	7.2	10.69	-35	-49	1		
GJ 1210	17 05 17	+07 26.3	0.653	233.2		m	14.01	1.88	1.44	1.41	78.0	5.3	78.0	5.3	13.47					
GJ 1211	17 05 37	+03 01.7	0.336	176.0		DZ7	15.19	0.46	-0.25		57.3	6.2	57.3	6.2	13.98					
Gl 656	17 05 40	-60 40.4	0.612	8.9	8.8	K0 V	7.41	0.89	0.53	0.33	67.8	8.1	67.8	8.1	6.57	30	27	17	154577	CP-60 6718
NN	17 07 05	+03 59.7	0.066	208.4		G5	7.95						48.0	05. o	6.36				155121	BD+ 4 3342
Gl 656.1A	17 07 30	-15 39.9	0.102	21.6	-2.4	A1 V	3.02	+0.06 J	+0.08 J	+0.03CJ	51.1	9.6	51.1	9.6	1.56	-4	9	1	155125	BD-15 4467
Gl 656.1B	17 07 30	-15 39.9	0.102	21.6		A3 V	3.4 *				51.1	9.6	51.1	9.6	1.9 *					
NN	17 07 34	+11 59.3	0.380	256.0		m	13.99			1.26			52.0	09. r	12.57					
NN	17 07 56	+43 45.3	0.428	129.0		M3	11.80	1.48	0.89	1.25	131.8	3.1	125.0	36. r	12.3					
Gl 657	17 08 34	-43 10.5	0.288	175.4	-27	F0 IVn	3.33	0.41	0.09	0.23	57.5	8.5	57.5	8.5	2.13	-31	-10	-14	155203	CD-43 11485
Gl 659 A	17 09 08	+54 33.4	0.137	147.8	4.2	dK8	8.85	1.16	1.08	0.44	49.5	6.4	49.5	6.4	7.32	12	6	-3	155674	BD+54 1861
Gl 659 B	17 09 10	+54 33.1	0.140	141.1	2.9	dK8	9.34	1.25	1.21	0.50	49.5	6.4	49.5	6.4	7.81	12	6	-5		BD+54 1862
Gl 660 A	17 09 18	-01 47.3	0.549	234.7		M3.5 J	12.05	+1.60 J	+1.26 J	+1.11 J	85.3	4.5	85.3	4.5	11.7					
Gl 660 B	17 09 18	-01 47.3	0.549	234.7			12.2 *				85.3	4.5	85.3	4.5	11.9 *					
NN	17 09 52	+38 30.1	0.233	96.0		m	11.61			1.15			101.0	20. r	11.63					
Gl 660.1	17 10 11	-05 03.4	0.708	164.7		M0	11.62	1.46	1.06	0.76	49.6	6.5	49.6	6.5	10.1					
NN	17 10 14	+56 43.2	0.082	185.2		G5	6.98	0.70	0.22				45.0	06. r	5.25				155902	BD+56 1954
Gl 661 A	17 10 40	+45 44.8	1.582	171.3	-30	M3 J	9.96	+1.49 J	+1.01 J	+1.08 J	159.5	3.1	159.5	3.1	10.97	38	-32	-26	155876	BD+45 2505
Gl 661 B	17 10 40	+45 44.8	1.582	171.3		M3.5	10.4 *				159.5	3.1	159.5	3.1	11.4 *					
GJ 1212	17 10 59	-08 21.4	0.604	223.6	-15	dM1	12.05	1.61	1.18	1.10	63.1	9.5	63.1	9.5	11.05	-6	-47	4		
GJ 1213	17 11 26	+42 23.7	1.083	250.1	10.7	dM1	10.10	1.27	1.13	0.63	37.2	4.0	37.2	4.0	7.95	32	-82	107		BD+42 2810
Gl 663 A	17 12 16	-26 31.8	1.235	203.6	0.5	K1 Ve	5.07	0.85	0.53	+0.32 J	187.6	7.8	187.6	7.8	6.44	0	-31	-6	155886	CD-26 12026
Gl 663 B	17 12 16	-26 31.9	1.231	202.0	0.9	K1 Ve	5.11	0.86	0.63		187.6	7.8	187.6	7.8	6.48	1	-30	-7	155885	
NN	17 12 41	+26 58.9	0.321	300.0		m	12.35	1.52	1.24	0.95			40.0	07. r	10.36					
GJ 1214	17 12 49	+05 01.7	0.890	142.6		m	14.67	1.74	1.17	1.39	77.4	5.4	77.4	5.4	14.11					
NN A	17 12 57	+24 53.5	0.160	189.0	-40. SB	A3 IV	3.14	0.08	0.08	0.03	39.3	6.7	39.3	6.7	1.11	-8	-37	-23	156164	BD+25 3221
Gl 664	17 13 09	-26 28.6	1.222	203.1	-0.1 VAR	K5 Ve	6.33	1.16	1.07	0.44	182.0	12.4	182.0	12.4	7.63	0	-31	-7	156026	CD-26 12036
NN	17 13 31	-12 07.4	0.170	96.0	21	dM0	10.33	1.37		0.61	30.1	15.3	42.0	06. r	8.45	23	13	-11		BD-12 4699
NN	17 13 39	+19 03.3				M2	10.36	1.55	1.20	0.81			69.0	12. r	9.55					BD+19 3268
NN	17 13 40	+11 07.0	0.369	201.0		M2.5	10.84	1.38	1.27	0.86			59.0	10. r	9.69					BD+11 3149
GJ 2128	17 14 17	+08 06.8	0.277	256.0		M3.5	11.49	1.55	1.23	1.00			68.0	13. r	10.65					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN A	17 14 57	-11 46.6	0.298	180.0		M3	12.83	1.49		1.15			48.0	08. r	11.24					
NN B	17 14 56	-11 46.1	0.298	180.0		M3	12.91	1.49		1.12			48.0	08. r	11.32					
Gl 665.1	17 15 04	-24 01.2	0.130	126.6	-14.7	G3 V	6.59	0.62					43.0	05. r	4.76	-13	-1	-16	156365	CD-23 13297
Gl 666 A	17 15 15	-46 35.1	1.053	80.5	23	G8 V	5.53	0.77	0.35	0.28	131.9	6.1	131.9	6.1	6.13	28	19	-29	156274	CD-46 11370
Gl 666 B	17 15 15	-46 35.1	1.053	80.5	25.1	M0 V	8.69	1.41	0.89	0.81	131.9	6.1	131.9	6.1	9.29	30	18	-29		
GJ 1215	17 15 25	+11 43.7	0.539	218.7		m	15.10	+1.88:		1.50	78.8	4.9	78.8	4.9	14.58					
Gl 667 A	17 15 33	-34 56.2	1.167	99.2	0	K3 V	6.29	+1.04 J	+0.82 J	+0.42 J	140.0	6.0	140.0	6.0	7.02	3	17	-35	156384	CD-34 11626
Gl 667 B	17 15 33	-34 56.2	1.167	99.2	1	K5 V	7.2 *				140.0	6.0	140.0	6.0	7.9 *	4	17	-35		
Gl 667 C	17 15 34	-34 56.5	1.180	98.3	0.6	M2.5	10.24	1.57	1.16	0.96	140.0	6.0	140.0	6.0	10.97	4	18	-36		
Gl 667.1	17 15 40	-75 17.7	0.978	256.5	58.9	G2 V	7.00	0.60	-0.03	0.22	42.0	8.9	35.0	05. r	4.72	5	-127	70	155918	CP-75 1368
NN	17 15 45	-01 43.7	0.138	141.0		K7	10.59	1.44		0.75			51.0	08. r	9.13					
NN	17 16 10	+18 12.2	0.231	182.0		m	13.02			1.15			53.0	10. r	11.64					
Gl 668.1	17 17 19	-05 51.9	0.186	168.9	-33.1	G9 V	6.32	0.85	0.47	0.31	23.5	8.1	85.0	13. r	5.97	-26	-16	-16	156826	BD-05 4426
Gl 669 A	17 17 54	+26 32.8	0.430	330.0	-33.7	dM4 e	11.42	1.55	1.15	1.18	93.3	1.9	93.3	1.9	11.27	-36	-18	-3		
Gl 669 B	17 17 53	+26 32.8	0.430	330.0	-34	dM5 e	12.97	1.64	0.73	1.39	93.3	1.9	93.3	1.9	12.82	-36	-19	-4		
Gl 670 A	17 18 00	-21 03.7	0.313	132.0	-8.8	F2 V	4.41	+0.39 J	-0.05 J	+0.24CJ	59.8	6.5	59.8	6.5	3.29	-5	-4	-26	156897	BD-20 4731
Gl 670 B	17 18 00	-21 03.7	0.313	132.0		K3	8.9 *				59.8	6.5	59.8	6.5	7.8 *					
Gl 671	17 18 17	+41 46.5	0.863	159.8	-18.9	M3	11.37	1.56		1.04	77.4	4.8	77.4	4.8	10.81	42	-20	-31		
Gl 672	17 18 47	+32 31.9	1.050	173.0	-79.1	G2 V	5.39	0.62	0.07	0.24	73.7	5.5	73.7	5.5	4.73	22	-80	-63	157214	BD+32 2896
GJ 1216	17 19 26	+49 19.2	1.304	155.5		m	14.48:	+1.66:			58.7	5.6	58.7	5.6	13.32:					
NN	17 19 47	+21 28.4	0.304	327.0		m	13.84			1.28			60.0	10. r	12.73					
GJ 1217	17 19 52	-14 54.4	0.206	207.0	-56	K5 V	10.84	1.41	1.34	0.62	42.7	7.0	42.7	7.0	8.99	-50	-31	-14		BD-14 4622
Gl 672.1	17 20 35	-32 11.8	0.596	198.0		M2	11.64:	1.50		0.87	48.4	10.2	48.4	10.2	10.06:					
NN	17 20 40	-80 08.1	0.681	314.7		m	12.1 *			1.15			81.0	16. r	11.6 *					
NN	17 21 39	-04 19.1	0.265	245.0		M2	12.19	1.51		1.04			53.0	11. r	10.81					
Gl 673	17 23 16	+02 10.2	1.315	206.1	-23.3	K7 V	7.53	1.36	1.27	0.60	128.9	3.5	128.9	3.5	8.08	1	-53	-10	157881	BD+02 3312
Gl 673.1	17 23 19	-24 07.9	0.118	180.0	-37.2	A9 V	4.17	0.28	0.12	+0.14C	44.2	8.2	44.2	8.2	2.4	-36	-12	-11	157792	CD-24 13337
GJ 1218	17 23 33	-62 24.1	0.996	197.3	28	m	12.68:	+1.48:	1.10	1.22			78.0	15. r	12.14:	-10	-62	-21		
NN	17 23 39	+01 50.9	0.040	0.0			10.90	0.67		0.30	73.7	19.8	73.7	19.8	10.2					
NN	17 24 11	-25 06.7	0.645	137.9		M3.5	13.35			1.20			53.0	10. r	11.97					
Gl 674	17 24 53	-46 50.6	1.044	147.0	-10.2	M3	9.37	1.53	1.21	1.03	219.7	12.1	219.7	12.1	11.08	-15	-5	-19		CP-46 8664
Gl 675	17 25 09	+67 20.9	0.534	271.7	-38.3	SB K0 V	6.43	0.76	0.29		75.7	6.2	75.7	6.2	5.83	1	-50	7	158633	BD+67 1014
GJ 1219	17 25 27	+14 31.8	1.142	254.4		m	13.69	1.76	1.21	1.18	50.8	7.0	50.8	7.0	12.22					
NN	17 26 05	-23 47.7	0.310	258.3		K5 V	9.66	1.29		0.55			45.0	07. r	7.93				158233	CD-23 13396
Gl 676 A	17 26 15	-51 35.7	0.300	238.0	-27.2	M0	9.58	1.46	1.31	+0.94C	83.3	7.5	83.3	7.5	9.18	-29	-5	12		CP-51 10396
Gl 676 B	17 26 20	-51 35.6	0.290	240.0		m	13.31	1.51			83.3	7.5	83.3	7.5	12.91					
NN	17 26 47	+37 29.6	0.190	173.0		m	13.35			1.16			47.0	09. r	11.71					
Gl 677 A	17 27 24	+29 26.0	0.341	214.5	-8.6	dM0 J	9.55	+1.15 J	+1.03 J	+0.48 J	48.2	4.5	48.2	4.5	7.97	18	-29	5		BD+29 3029
Gl 677 B	17 27 24	+29 26.0	0.341	214.5			9.93*				48.2	4.5	48.2	4.5	8.35*					
Gl 678 A	17 27 49	-01 01.4	0.213	214.3	-77.3	SB G8 IV-V	5.98	+0.72 J	+0.31 J	+0.24 J	50.5	5.0	50.5	5.0	4.5	-61	-47	-21	158614	BD-00 3300
Gl 678 B	17 27 49	-01 01.4	0.213	214.3	-73.8	G8 IV-V	6.2 *				50.5	5.0	50.5	5.0	4.7 *	-58	-45	-20		
Gl 678.1A	17 27 55	+05 35.4	0.262	174.4	-3.8	M1 V	9.30	1.49	1.23	0.76	70.8	27.3	100.0	21. r	9.3	4	-10	-8		BD+05 3409

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	17 28 54	+47 26.3	0.194	66.6		G5	7.21						50.0	06. o	5.7				159062	BD+47 2491
Gl 679	17 30 13	+34 18.3	0.256	284.7	-52	G5 V	6.56	0.65	0.17		54.8	6.2	54.8	6.2	5.25	-29	-48	-7	159222	BD+34 2989
NN	17 30 54	+50 27.4	0.535	178.8		m	12.74	1.47	1.02	1.06	47.0	8.1	47.0	8.1	11.1					
Gl 680	17 31 24	-48 39.3	0.460	7.0		M0	10.15	1.56	1.21	+1.24C	81.9	13.6	81.9	13.6	9.72					CP-48 9312
Gl 681	17 32 37	+12 35.7	0.257	152.6	+12.6 SB	A5 III	2.08	0.15	0.10	0.00	64.6	3.9	64.6	3.9	1.13	21	1	-9	159561	BD+12 3252
NN	17 33 12	-54 24.0	0.446	193.0		DA8	15.8 *	0.46	-0.45				48.0	09. w	14.2 *					
Gl 682	17 33 28	-44 16.6	1.155	216.3	-60	M3.5	10.95	1.65	1.20	1.26	211.6	5.9	211.6	5.9	12.58	-64	-11	9		CD-44 11909
Wo 9593 A	17 33 36	-49 22.6	0.214	185.2	6.7	G2 V	9.40	+0.63 J			39.4	12.8	39.4	12.8	7.4	-3	-23	-12	159462	CD-49 11579
Wo 9593 B	17 33 36	-49 22.5	0.221	187.1		G5	10.2 *				39.4	12.8	39.4	12.8	8.2 *					
Gl 683	17 33 59	-54 28.2	0.157	195.5	-3.3	A7 V	5.25	0.20	0.08	+0.10C	55.1	11.9	55.1	11.9	3.96	-9	-10	-3	159492	CP-54 8403
Gl 683.1	17 34 18	-42 32.0	0.403	154.3	+3.8 SB	G5 V	7.17	0.65	0.18	+0.34C	44.9	7.2	44.9	7.2	5.43	-5	-22	-36	159656	CD-42 12320
Gl 683.2A	17 34 26	-37 49.8	0.115	185.3	2.8	G8 V	6.80	+0.77 J	+0.31:J	+0.38CJ	19.9	6.8	54.0	10. r	5.46	1	-9	-5	159704	CD-37 11734
Gl 683.2B	17 34 26	-37 49.8	0.115	185.3			9.1 *				19.9	6.8	54.0	10. r	7.8 *					
Gl 684 A	17 34 28	+61 54.8	0.568	154.1	-16.3 SB	G0 Va	5.34	0.56	0.07	+0.24 J	67.9	5.8	67.9	5.8	4.5	36	-5	-22	160269	BD+61 1678
Gl 684 B	17 34 28	+61 54.8	0.568	154.1		K3 V	8.06	1.10	1.00		67.9	5.8	67.9	5.8	7.22					
NN	17 34 52	-29 59.1	0.240	236.0		k-m	10.94	1.47	1.22				60.0	29. r	9.8					
Gl 685	17 35 02	+61 43.1	0.573	153.3	-16.3	M1 Ve	9.97	1.47	1.18	0.79	71.1	2.8	71.1	2.8	9.23	35	-5	-22		
NN	17 35 25	-43 06.9	0.291	234.5	-23.8	G5 V	7.24	0.72	0.24	0.24	5.1	8.5	39.0	06. r	5.2	-29	-27	16	159868	CD-43 11901
NN	17 35 30	+22 07.8	0.287	175.0		m	14.08			1.25			47.0	09. r	12.44					
Gl 686	17 35 39	+18 36.4	1.361	43.2	-9.5	dM1	9.62	1.53	1.08	0.86	128.9	2.6	128.9	2.6	10.17	-32	34	-20		BD+18 3421
Gl 686.1A	17 35 44	+22 59.1	0.237	220.8	4.1	dM0 eJ	10.00	1.33	1.24	0.60	40.6	3.5	40.6	3.5	8.04	19	-18	10		BD+23 3151
Gl 686.1B	17 35 44	+22 59.1	0.237	220.8	1.3		10.22	1.38	1.30	0.64	40.6	3.5	40.6	3.5	8.26	17	-20	9		
NN	17 36 27	+08 03.3	0.240	201.0		M4	12.28	1.57		1.00			48.0	09. r	10.69					
Gl 686.2	17 36 32	-49 23.2	0.209	148.2	3.7	F2 V	4.77	0.40	-0.04	+0.25C	42.7	8.5	42.7	8.5	2.92	-3	-10	-21	160032	CD-49 11616
Gl 687	17 36 42	+68 23.1	1.304	194.8	-23.2 SB?	M3.5 V	9.18	1.50	1.06	1.10	212.7	2.0	212.7	2.0	10.82	31	-21	-4		BD+68 946
Gl 688	17 36 48	+03 35.0	0.199	242.5	+22.4 SB	K3 V	6.52	0.96	0.77	+0.50C	81.0	7.8	81.0	7.8	6.06	22	1	13	160346	BD+03 3465
GJ 1220	17 36 50	+82 06.8	0.566	329.9		m	14.18	1.76			70.9	3.4	70.9	3.4	13.43					
Gl 689	17 37 02	+71 54.4	0.104	111.4	-23.9	dK8	8.62	1.10	1.04	0.43	46.9	11.9	51.0	06. r	7.16	8	-15	-20	160964	BD+71 850
NN	17 37 14	+68 46.9	0.323	359.9	-14.4 SB	F5 V	4.80	0.43	-0.01		42.1	9.0	51.0	05. s	3.34	-28	-15	-10	160922	BD+68 949
NN A	17 37 32	+27 47.5	0.195	179.0		M1	11.12	1.45		0.77			45.0	06. r	9.39					
NN B	17 37 33	+27 48.3	0.195	179.0		M5	12.72	1.53		1.12			45.0	06. r	10.99					
NN A	17 38 07	+61 15.8	0.069	319.1		dK8	10.28	1.23		0.63			41.0	05. r	8.34					
NN B	17 38 08	+61 15.6					14.70			1.29			41.0	05. r	12.76					
NN	17 39 13	-40 59.9	0.536	194.4		M3	12.55			1.10	21.2	18.8	54.0	10. r	11.21					
Gl 690 A	17 39 18	+71 21.2	0.338	341.0	-0.8	dM0	9.20	1.10	1.01	0.44	53.7	7.3	53.7	7.3	7.85	-28	-10	5		BD+71 851
NN	17 39 30	-08 47.3	0.965	240.2	-92	M3	13.52	+1.61:	+1.22:	1.06	43.1	3.5	43.1	3.5	11.69	-69	-117	34		
Gl 690.1	17 39 39	-16 36.5	0.656	191.4		M2.5	13.05	+1.55:		1.03	51.3	5.2	51.3	5.2	11.6					
Wo 9599	17 39 45	+65 01.5	0.119	344.9	-8.1	K0	8.37	0.93	0.69		41.6	17.0	40.0	05. r	6.38	-13	-10	-2	161284	BD+65 1203
Gl 691	17 40 10	-51 48.6	0.192	183.9	-9	G5 V	5.14	0.70	0.24	0.20	77.2	16.3	103.0	17. r	5.2	-12	-4	-2	160691	CD-51 11094
Wo 9600	17 40 22	-18 29.7	0.535	192.1		M2	12.15	1.43		0.88	40.2	9.0	40.2	9.0	10.17					
Gl 692	17 40 26	-21 39.6	0.105	245.4	10.2	F5 V	4.87	0.47	-0.03	+0.26C	59.8	8.5	59.8	8.5	3.75	10	-6	5	160915	BD-21 4712
NN	17 40 33	+05 48.7	0.240	105.0		M2	10.67			0.85			64.0	11. r	9.7					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 692.1	17 41 09	+21 38.4	0.655	191.4	24.4	K0 V	7.49	0.77	0.30	0.29	47.0	8.5	47.0	8.5	5.85	65	-26	0	161198	BD+21 3198
Gl 693	17 42 24	-57 16.9	1.739	219.2	-115	M3.5	10.75	1.65	1.21	1.11	165.5	8.4	165.5	8.4	11.84	-120	1	38		
Gl 694	17 42 25	+43 24.4	0.636	179.1	-14.5	dM3.5	10.47	1.53	1.23	1.02	101.7	3.4	101.7	3.4	10.51	24	-19	-12		BD+43 2796
NN	17 42 25	-07 59.4	0.338	217.0		g	11.48	1.45	1.24				41.0	20. r	9.5					
Gl 694.1A	17 42 49	+72 10.4	0.268	177.0	-13.7	F5 IV-V	4.58	0.42	0.01		54.9	5.2	54.9	5.2	3.28	25	-7	-6	162003	BD+72 804
Gl 694.1B	17 42 51	+72 10.9	0.277	175.1	-10.9	F8 V	5.79	0.53	0.02		54.9	5.2	54.9	5.2	4.49	25	-4	-5	162004	BD+72 805
NN	17 44 04	+24 39.7	0.600	326.8		m	12.67	1.51	1.04	1.12	69.2	2.4	69.2	2.4	11.87					
Gl 694.2	17 44 11	+46 52.4	0.030	225.0	5.7	dM1.5	10.72	1.49	1.27	0.78	46.4	3.9	46.4	3.9	9.05	4	3	4		BD+46 2361
Gl 695 A	17 44 30	+27 44.9	0.814	202.9	-16.7	G5 IV	3.42	0.75	0.39	0.24	115.1	5.4	115.1	5.4	3.73	17	-33	-5	161797	BD+27 2888
Gl 695 B	17 44 28	+27 44.7	0.827	204.2	-13.9	M3 J	10.35	+1.49 J	+1.03 J	+1.10 J	115.1	5.4	115.1	5.4	10.66	18	-32	-3		
Gl 695 C	17 44 28	+27 44.7	0.827	204.2		M4 K	10.8 *				115.1	5.4	115.1	5.4	11.1 *					
Gl 695.1	17 44 39	-33 59.7	0.603	199.2	2.4	G8 V	7.19	0.71	+0.33:	0.24	49.3	6.2	49.3	6.2	5.65	-2	-57	-12	161612	CD-33 12476
Wo 9605	17 45 16	+04 57.5	0.581	248.3	-93.1	K1 V	8.92	0.84	0.47	0.31	39.4	7.2	39.4	7.2	6.9	-62	-97	18	161848	BD+04 3509
NN	17 46 13	+36 07.9	0.080	23.1		G5	7.62						54.0	06. o	6.28				162160	BD+36 2941
NN	17 46 45	-56 33.4	1.256	237.6	-6	M2	12.13	1.46	1.15	0.80	39.1	10.1	29.0	05. r	9.44	-53	-171	100		
Gl 696	17 47 53	-06 02.1	0.153	190.0	-26.2 SB?	dM1.5	10.17	1.43	1.26	0.69	55.4	19.4	56.0	11. r	8.91	-19	-20	-9	162283	BD-06 4663
NN	17 47 56	+22 42.0	0.780	259.4		m	20.1 P				67.2	6.4	67.2	6.4	19.2 P					
NN	17 48 12	+23 46.2	0.585	320.6	-80	M4.5-5	13.50	1.61		1.19	46.6	4.3	46.6	4.3	11.84	-84	-51	16		
GJ 1221	17 48 58	+70 52.4	1.651	311.0		DXP9	14.15	0.40	-0.30		162.8	2.1	162.8	2.1	15.21					
NN	17 49 15	+14 46.0	0.269	297.0		m	13.71			1.18			43.0	08. r	11.88					
NN	17 50 48	+16 55.8	0.347	232.0		m	12.69			1.13			57.0	11. r	11.47					
GJ 2133	17 50 48	-34 39.0	0.409	235.0		k	13.52	1.64					56.0	24. r	12.3					
Gl 697	17 51 22	+21 20.0	0.089	299.8	-12.5	dK5	8.48	0.95	0.70	0.36	55.0	7.4	55.0	7.4	7.18	-11	-10	2		BD+21 3245
NN	17 51 22	-65 42.6	0.333	165.1	-22.2	F8 V	6.36	0.45			44.9	17.6	29.0	04. r	3.67	-50	-19	-25	162521	CP-65 3528
GJ 1222	17 51 55	+07 23.5	0.668	241.7	-20	m	13.11	1.55	1.11	1.23	59.8	3.7	59.8	3.7	11.99	0	-51	24		
Gl 697.1	17 52 56	+03 45.7	0.092	278.7	3	dM0 e	10.13	1.34	1.23	0.58	38.4	3.6	38.4	3.6	8.05	2	-3	11		BD+03 3531
Gl 698	17 53 34	+18 30.4	0.065	228.4	-28.8	dK8	9.22	1.18	1.16	0.48	32.3	11.2	47.0	06. r	7.58	-16	-24	-7		BD+18 3497
NN	17 53 40	+36 11.7	0.118	262.7		G5	7.84						50.0	06. o	6.33				163621	BD+36 2975
NN	17 53 44	+04 50.4	0.010	8.5		dK8	8.0 *				46.0	12.5	46.0	12.5	6.3 *				163489	BD+04 3553
NN	17 53 48	-41 59.0	0.392	194.0		M3	11.36	1.51		+0.89t			53.0	11. r	9.98					CP-41 8405
NN	17 54 48	+58 24.0	0.879	16.4		m	17.98			1.85	46.5	1.0	46.5	1.0	16.32					
NN	17 54 49	+15 47.2	0.279	221.0		m	12.21			1.13			71.0	14. r	11.47					
Gl 698.1	17 54 59	-51 37.1	0.240	161.0	-10.4	K3 V	9.64	0.92	0.72	+0.47C	46.3	15.3	23.0	04. r	6.45	-28	-26	-32	163436	CP-51 10685
NN A	17 55 10	+24 00.0	0.073	343.6	-28.1 SB	G2 V	6.30	0.64	0.20		50.0	8.9	50.0	8.9	4.79	-22	-17	-7	163840	BD+24 3283
Gl 699	17 55 23	+04 33.3	10.310	355.8	-111	M5 V	9.55	1.74	1.29	1.25	545.3	1.0	545.3	1.0	13.23	-141	5	18		BD+04 3561
Wo 9608	17 55 40	-30 09.6	0.609	165.1	-109	K0 V	9.37	0.79	0.35	0.30	42.9	11.9	19.0	03. r	5.76	-114	-108	-101		CD-30 15026
NN	17 56 28	+46 35.2	0.594	357.2		m	11.79	1.56	1.41	1.12	71.3	4.7	71.3	4.7	11.06					
Gl 699.1	17 56 40	+82 44.1	3.587	337.3	-154	DA7	14.30	0.35	-0.52		61.5	3.2	61.5	3.2	13.24	-157	-300	-40		
Gl 699.2	17 57 50	-03 41.3	0.160	107.5	-42.9	F3 V	4.62	0.38	0.00	+0.22C	46.7	13.6	46.7	13.6	3	-38	-13	-23	164259	BD-03 4217
Gl 700.1A	18 00 21	-08 10.9	0.046	147.1	-38.4 SB	dF3 J	5.24	+0.38 J	+0.04 J	+0.22CJ	58.3	9.1	58.3	9.1	4.07	-35	-15	-8	164765	BD-08 4549
Gl 700.1B	18 00 21	-08 10.9	0.046	147.1	-35.1		5.93*				58.3	9.1	58.3	9.1	4.76*	-32	-13	-7	164764	
Gl 700.1C	18 00 27	-08 11.9	0.050	147.0	-14		9.4 *				58.3	9.1	58.3	9.1	8.2 *	-12	-6	-5		

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 700.2	18 00 29	+26 19.2	0.715	148.1	20.7	K0 V	6.99	0.80	0.47	0.24	60.4	13.3	53.0	08. r	5.61	54	6	-40	164922	BD+26 3151
GJ 1223	18 01 03	+37 31.8	1.158	171.9		m	14.85	1.77		1.47	83.5	4.0	83.5	4.0	14.46					
Gl 701	18 02 28	-03 01.9	0.644	121.1	32.5	dM2	9.38	1.52	1.20	0.85	125.9	4.7	125.9	4.7	9.88	33	14	-19	165222	BD-03 4233
NN	18 02 32	+35 57.4	0.257	170.0		M0	10.83	1.48		0.82			56.0	10. r	9.57					BD+35 3145
Gl 702 A	18 02 56	+02 30.6	1.135	167.1	-6.9 SB	K0 Ve	4.21	+0.86 J	+0.51 J	0.26	199.0	3.6	199.0	3.6	5.7	7	-20	-19	165341	+02 3482
Gl 702 B	18 02 56	+02 30.6	1.135	167.1	-10.0 SB	K5 Ve	6.00	1.15		0.45	199.0	3.6	199.0	3.6	7.49	5	-21	-19		
Gl 702.1	18 03 01	-36 01.5	0.110	81.1	13.2	G5 V	5.95	0.62	0.07	0.20	57.7	6.8	57.7	6.8	4.76	13	5	-9	165185	CD-36 12214
Gl 702.2	18 03 09	+04 39.4	0.314	182.5	-120.4	G2 V	6.80	0.62	0.04	0.22	50.0	2.7	50.0	2.7	5.29	-83	-84	-38	165401	BD+04 3589
GJ 1224	18 04 42	-15 58.0	0.664	238.2		m	13.63	1.79		1.42	132.7	3.7	132.7	3.7	14.24					
Wo 9615 A	18 04 59	+09 33.3	0.102	322.4	-23.9	A4 V	3.73	0.12	0.10	-0.04 J	48.6	7.5	48.6	7.5	2.16	-23	-12	3	165777	BD+09 3564
Wo 9615 B	18 04 59	+09 33.3	0.102	322.4			14. *			0.40	48.6	7.5	48.6	7.5	12. *					
Gl 703	18 05 04	+15 56.5	0.210	198.4	25.5	G6	8.68	0.65	0.16		71.7	11.9	71.7	11.9	7.96	28	7	6		BD+15 3364
Gl 704 A	18 05 08	+30 33.2	0.116	311.7	+1.6 SB?	F7 V	5.09	0.50	-0.10:		59.2	3.9	59.2	3.9	3.95	-4	0	9	165908	BD+30 3128
Gl 704 B	18 05 08	+30 33.2	0.116	311.7		K5 V	8.45	1.10	+1.0 :		59.2	3.9	59.2	3.9	7.31					
Gl 705.1	18 05 47	-62 00.9	0.222	339.4	+29.7 SB	G3 IV-V	5.48	0.58	0.09	+0.32C	51.6	10.2	51.6	10.2	4.04	36	-2	3	165499	CP-62 5797
NN	18 06 45	-12 02.8	0.208	171.9	-2.2	K7 V	10.47	1.38	1.17	0.66	18.1	10.4	42.0	08. r	8.59	4	-18	-14		BD-12 4935
Gl 705.2	18 06 48	+52 47.4	0.403	261.0		K5	12.51	1.50		0.73	50.8	11.9	50.8	11.9	11					
Gl 706	18 07 58	+38 27.2	0.557	215.3	-19.1	K2 V	6.40	0.87	0.59	0.34	88.7	2.5	88.7	2.5	6.14	17	-31	1	166620	BD+38 3095
Gl 707	18 08 44	-43 27.1	0.442	162.8	-2	K7 Ve	8.37	1.31	1.22	0.54	68.0	9.1	68.0	9.1	7.53	-10	-21	-21	166348	CD-43 12343
NN	18 09 42	+49 57.8	0.228	185.0		K7	9.96	1.29	1.25				41.0	10. r	8					BD+49 2743
NN	18 11 05	+26 01.0	0.210	100.0		m	13.32			1.28			76.0	13. r	12.72					
NN	18 12 05	-77 03.6	0.626	202.2		m	14.1 *			1.26			49.0	09. r	12.6 *					
Gl 708	18 13 07	+18 28.9	0.110	34.0	1.7	dM1	10.07	1.33	1.31	0.56	38.4	3.9	38.4	3.9	7.99	-8	11	-2	348282	BD+18 3606
NN	18 13 33	+18 55.5	0.440	186.0		M0	10.84	1.50		0.77			48.0	10. r	9.25					BD+18 3609
Gl 708.1	18 13 36	+64 22.8	0.344	84.7	-36.1	F5 V	5.03	0.38	-0.04		50.3	8.8	50.3	8.8	3.54	-5	-17	-45	168151	BD+64 1252
Gl 708.2	18 13 45	+13 54.1	0.501	170.3	11	dM0	10.20	1.44	1.24	0.69	53.2	4.2	53.2	4.2	8.83	37	-16	-22		BD+13 3578
Gl 708.3	18 13 48	+01 30.8	0.771	211.2		M5	12.52	1.61	1.32	1.08	63.0	5.2	63.0	5.2	11.52					
Gl 708.4	18 14 06	+45 11.6	0.138	217.2	-64.9	G2 V	6.29	0.62	0.12		46.0	10.2	49.0	08. r	4.74	-6	-62	-23	168009	BD+45 2684
Gl 709	18 15 05	+45 32.0	0.300	354.0	-36.8	dM0	10.28	1.47	1.20	0.75	46.4	5.5	46.4	5.5	8.61	-38	-28	-6		BD+45 2688
NN	18 15 48	+26 39.0	0.343	72.5	-49	K3	9.59	1.02	0.84	0.41	43.8	4.8	43.8	4.8	7.8	-41	-16	-43	335828	BD+26 3215
Wo 9624	18 16 00	-45 43.1	0.154	208.5	25	F7 V	6.85	0.54	0.07		43.2	8.5	22.0	03. s	3.56	18	-37	-4	167954	CD-45 12390
NN A	18 16 25	+38 46.2	1.091	197.8		m	11.87	1.58		1.07	88.0	3.6	88.0	3.6	11.59					
NN B	18 16 24	+38 46.2	1.091	197.8		m	13.53	1.77		1.24	88.0	3.6	88.0	3.6	13.25					
NN	18 16 29	-45 56.5	0.153	172.6	-18	G5 V	7.32	0.76			28.8	11.9	43.0	06. r	5.49	-22	-10	-4	168060	CD-45 12402
NN	18 16 40	-05 47.6	0.530	137.2		M2.5	12.57	1.45		0.90	40.2	10.7	33.0	07. r	10.16					
Gl 710	18 17 15	-01 57.7	0.014	249.7	-13.3	dM1	9.66	1.37	1.22	0.61	71.7	9.0	71.7	9.0	8.94	-11	-7	-1	168442	BD-01 3474
NN	18 17 19	-09 36.9	0.267	201.5		G8 V	6.92	0.70	0.31		31.8	11.9	48.0	08. r	5.33				168443	BD- 9 4692
GJ 1225	18 17 33	+68 32.8	1.740	203.5		m	15.39	1.88		1.34	54.3	7.8	54.3	7.8	14.06					
GJ 1226	18 18 24	-01 03.8	1.082	207.9	50	M3.5	12.71	1.66	1.12	1.14			62.0	15. r	11.7	83	-49	6		
Gl 711	18 18 43	-02 54.8	0.890	218.4	6.9	K0 III-IV	3.26	0.94	0.66	0.33	54.9	9.7	54.9	9.7	1.96	39	-65	15	168723	BD-02 4599
NN	18 18 51	+66 10.5	0.623	131.3		m	13.48	1.83		1.35	137.3	5.3	137.3	5.3	14.17					
Gl 712	18 19 44	+06 18.9	1.158	272.7	-48	M3	12.58	1.48	1.07	1.11	69.1	3.2	69.1	3.2	11.78	-30	-61	64		

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	18 20 45	+60 59.9	0.688	172.2		DC:9	15.65	0.97	0.98		78.1	4.1	78.1	4.1	15.11					
GJ 2135	18 21 15	-13 09.9	0.637	195.9		DA7	15.60	0.42	-0.60				50.0	10. w	14.09					
NN	18 21 31	+28 08.6	0.190	201.0		M3	12.49	1.61		1.19			72.0	17. r	11.8					
NN	18 21 33	+01 39.6	0.269	139.0		g	11.84	1.56	1.29				72.0	34. r	11.1					
Gl 713 A	18 21 57	+72 42.7	0.632	124.4	+32.0 SB	F7 V	3.57	0.49	-0.06	0.20	132.6	3.7	132.6	3.7	4.18	3	39	-2	170153	BD+72 839
GJ 1227	18 22 05	+62 02.3	1.544	217.1		m	13.41	1.76		1.36	121.3	1.6	121.3	1.6	13.83					
NN	18 23 01	+24 36.6	0.429	190.0		M0	10.79			0.73			45.0	06. r	9.06				336196	BD+24 3411
NN	18 23 51	+38 20.1	0.712	185.8		M1	11.27	1.48	1.19	0.76			39.0	06. r	9.23					
NN	18 24 04	+11 19.3	0.279	183.0		m	12.85			1.12			52.0	10. r	11.43					
Gl 713.1	18 24 53	-25 27.1	0.190	193.1	-43.2	K1+ IIIb	2.82	1.04	0.89	+0.50C	59.7	9.7	59.7	9.7	1.7	-41	-20	1	169916	CD-25 13149
Gl 714	18 25 51	-58 18.1	0.430	184.0	-3.4	M1	9.85	1.48	1.20	+0.95C	69.2	11.9	69.2	11.9	9.05	-17	-24	-6		CP-58 7399
Gl 715	18 27 16	-01 51.0	0.256	139.5	-54.3	dK5	8.05	1.10	1.06	0.38	50.1	6.5	50.1	6.5	6.55	-42	-33	-26	170493	BD-01 3500
Gl 716	18 28 23	-18 56.5	0.239	215.2	-41.6	K3 V	6.81	0.85	0.56	0.30	83.7	15.4	71.0	11. r	6.07	-36	-25	5	170657	BD-18 4986
GJ 1228	18 29 22	+54 45.0	0.372	318.0		DXP8	15.50	0.49	-0.44		67.2	5.6	67.2	5.6	14.64					
NN	18 29 24	-62 47.0				K7	9.52	1.45		0.67			70.0	11. r	8.75					CP-62 5888
NN	18 29 49	+79 23.0	0.355	3.9	-27	K5	9.28	1.18		0.47	32.0	13.6	45.0	07. r	7.55	-27	-35	-14		BD+79 590
GJ 1229	18 29 52	+13 41.8	0.164	45.1	-45.3	G8 V	7.20	0.68	0.24				40.0	06. r	5.21	-44	-16	-14	171067	BD+13 3677
NN	18 30 22	+40 38.5	0.419	348.0		m	11.99			1.13			79.0	16. r	11.48					
Gl 717	18 30 42	-11 40.3	0.406	232.5	-83.7	K7 V	10.00	1.28	1.20	0.53	48.3	4.7	48.3	4.7	8.42	-65	-63	19		BD-11 4672
Gl 718	18 31 12	+22 16.9	0.510	200.9	38.8	K4 V	8.89	1.12	1.05	0.42	49.7	9.2	45.0	07. r	7.16	66	-4	6	171314	BD+22 3406
Gl 719	18 32 45	+51 41.0	0.376	151.0	-24.5 SB	K6 Ve	8.1 v	1.22	+1.04:		58.0	5.6	58.0	5.6	6.9 v	20	-17	-29	234677	BD+51 2402
Wo 9629	18 32 50	-44 20.7	0.220	225.0	-10.6	G0	10.23	0.62	0.00	+0.36C	40.3	11.9	40.3	11.9	8.3	-11	-22	12		CD-44 12736
NN	18 32 58	+40 05.1	0.223	168.0		M3 p	11.42	1.42		1.21			124.0	45. r	11.9					
NN	18 33 41	+41 26.8	0.387	95.0		M2	11.78			0.90			44.0	08. r	10					
Gl 720 A	18 33 50	+45 41.8	0.566	53.0	-31.2	dM2	9.85	1.42	1.15	0.73	67.8	2.1	67.8	2.1	9.01	-37	-11	-33		BD+45 2743
Gl 720 B	18 33 59	+45 42.9	0.566	53.0		m	13.02	1.60		1.18	67.8	2.1	67.8	2.1	12.18					
NN	18 34 01	+13 33.7	0.347	34.0		M3.5	12.46			1.23			89.0	16. r	12.21					
Wo 9630	18 34 07	-25 42.6	0.333	148.5	-24.3	G5 V	7.44	0.69	0.21		41.4	7.5	41.4	7.5	5.53	-26	-24	-28	171665	CD-25 13291
Gl 721	18 35 15	+38 44.2	0.348	35.2	-12.1	A0 V	0.03	0.00	-0.01	-0.09	129.6	5.5	129.6	5.5	0.59	-15	-5	-7	172167	BD+38 3238
GJ 2138	18 35 54	-14 31.7	0.544	166.9		dM1	11.26	1.56	1.23	0.98			72.0	14. r	10.55					
Gl 722	18 35 54	-21 05.7	0.171	206.0	38.6	G5 V	5.86	0.68	0.14	0.24	71.8	5.0	71.8	5.0	5.14	40	-3	-5	172051	BD-21 5081
NN	18 36 26	+20 35.1	0.215	189.8	29	F9	9.34	0.65	0.08		42.7	10.1	42.7	10.1	7.5	37	8	0	349063	BD+20 3876
Gl 722.1	18 36 28	+42 37.2	0.289	78.0	33.1	dK0 e	8.34	0.82	0.39		43.9	10.3	32.0	05. r	5.87	-7	49	-23	172393	BD+42 3123
Gl 723	18 37 32	-10 30.3	0.539	193.9		M0.5	11.49	1.55		0.86	66.0	6.4	66.0	6.4	10.59					
Gl 724	18 38 08	-13 25.1	0.671	186.7		M0	10.63	1.50	1.21	0.84	56.2	6.1	56.2	6.1	9.38					BD-13 5069
NN	18 38 09	+33 21.8	0.301	3.0		m	13.12			1.14			49.0	10. r	11.57					
GJ 1230 A	18 39 04	+24 44.2	0.501	85.3		k-m	12.4 *	+1.71 J	+1.19 J	+1.38 J	130.2	28.3	136.0	22. r	13.1 *					
GJ 1230 B	18 39 04	+24 44.3	0.501	85.3		m	14. :				130.2	28.3	136.0	22. r	15. :					
NN	18 39 36	+80 02.5	0.237	35.0		M4 e	13.22	1.72		1.16			55.0	13. r	11.9					
Gl 724.1	18 39 48	-50 12.8	0.183	202.5	-32.5	G5 V	9.32	0.68	0.14	+0.37C	52.7	8.5	52.7	8.5	7.93	-34	-8	11	172582	CP-50 10804
NN	18 39 59	+39 39.4	0.309	236.0		m	13.42			1.25			64.0	12. r	12.45					
NN	18 40 07	+31 46.8	0.307	272.0		M3	11.27			1.04			85.0	15. r	10.92					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
GJ 2139	18 40 12	-11 11.7	0.354	224.0	53	DA5	14.18	0.15	-0.61				53.0	06. w	12.8	19	-25	9		
NN	18 40 27	+13 51.0	0.313	352.0		m	12.81			1.28			96.0	16. r	12.72					
NN	18 40 57	+04 17.3	0.140	302.0	46	DA6	14.92	0.14	-0.59		40.4	3.4	40.4	3.4	12.95	-1	1	16		
NN	18 41 45	+40 36.8	0.619	348.7		m	18.23				70.8	0.8	70.8	0.8	17.48					
Gl 725 A	18 42 12	+59 33.3	2.273	323.3	-0.8	dM4	8.90	1.52	1.11	1.06	286.1	1.8	286.1	1.8	11.18	-24	-12	26	173739	BD+59 1915
Gl 725 B	18 42 13	+59 33.0	2.272	323.1	+1.2 VAR	dM5	9.71	1.59	1.14	1.15	286.1	1.8	286.1	1.8	11.99	-24	-10	27	173740	
NN	18 42 48	-28 59.0	0.435	137.0		k	12.65	1.53	1.12				41.0	19. r	10.7					
Gl 725.1	18 43 05	+43 46.8	0.107	266.8	-44.6	K0	7.54	0.84	0.58		50.2	10.2	50.0	06. r	6.03	-9	-44	-6	173701	BD+43 3058
Gl 725.2	18 43 31	+20 29.8	0.335	181.9	22.3	F6 V	4.19	0.46	0.01	+0.17t	50.1	5.3	50.1	5.3	2.69	38	0	-8	173667	BD+20 3926
NN	18 44 11	-61 40.1	0.544	196.7		m	12.8 *			1.05			42.0	08. r	10.9 *					
Gl 725.3	18 44 39	-50 45.4	0.221	177.5	-5.5	G3 V	8.70	0.65	0.14	+0.35C	53.8	6.8	53.8	6.8	7.35	-12	-16	-5	173560	CP-50 10835
NN	18 44 47	+52 24.1	0.843	298.4		M1	15.11	1.85			50.1	2.5	50.1	2.5	13.61					
Gl 726	18 44 50	-03 41.5	0.275	206.1	16	K7	8.81	1.29	1.21	0.54	68.3	14.9	71.0	12. r	8.07	23	-8	-1	173818	BD-03 4380
NN	18 45 11	-14 38.1	0.337	223.0		k	12.13	1.51	1.18				45.0	22. r	10.4					
NN	18 45 22	-57 29.0	0.675	249.7		m	12.7 *			1.25			90.0	16. r	12.5 *					
NN	18 45 48	-62 07.	0.141	48.0		M3	10.72	1.46		+0.82t			58.0	11. r	9.54					
Gl 727	18 46 07	+10 41.7	0.447	163.9	-8.4	dK4	7.97	1.07	0.98	0.40	64.1	5.1	64.1	5.1	7	12	-22	-23	174080	BD+10 3665
Gl 728	18 46 40	+17 23.2	0.593	224.2	-21.3	dM1.5	9.22	1.28	1.22	0.60	64.3	5.3	64.3	5.3	8.26	16	-45	10	229590	BD+17 3729
NN	18 46 42	-20 23.0	0.037	8.6	-17.7 SB	K2 III	5.24	1.41	+2.42C		42.8	15.3	42.8	15.3	3.4	-18	-1	4	174116	BD-20 5277
Gl 729	18 46 45	-23 53.5	0.720	106.7	-12.1	dM4.5e	10.46	1.72	+1.3 ?	1.30	341.1	8.1	341.1	8.1	13.12	-14	-1	-8		
Gl 730	18 47 31	+03 02.1	0.473	203.0	-1.4	dM1.5	10.74	1.47		0.79	58.9	6.4	58.9	6.4	9.59	21	-32	-3		
NN	18 47 35	-60 49.6	0.698	298.9		m	13.4 *			1.18			49.0	10. r	11.9 *					
NN	18 48 35	-57 09.8	0.805	196.9		M2	12.14	1.47	1.13	0.97	30.6	10.7	45.0	09. r	10.41					
NN	18 49 23	+47 54.8	0.277	115.0		m	12.53			1.11			58.0	12. r	11.35					
NN	18 49 37	+24 23.8	0.374	263.0		m	12.76			1.08			47.0	10. r	11.12					
Gl 731	18 49 38	+16 31.8	0.537	207.9	-14.9	dM1.5	10.15	1.47	1.14	0.73	74.8	3.3	74.8	3.3	9.52	15	-34	-1	229793	
NN A	18 50 01	-54 25.1	0.208	108.8		K3 V	9.18	1.13	1.02	0.44			40.0	06. r	7.19				174564	CD-54 8050
NN B	18 50 01	-54 25.1	0.208	108.8		m	12.3 P						40.0	06. r	10.3 P					
Gl 732 A	18 50 15	-38 39.8	1.011	161.1		sdG0	12.70	1.53	1.12	1.23	75.2	12.1	75.2	12.1	12.08					
Gl 732 B	18 50 15	-38 39.8	1.011	162.0			16. *				75.2	12.1	75.2	12.1	15. *					
Gl 732.1	18 50 28	+52 54.6	0.259	354.6	-1.6 SB?	G9 IVa	5.50	0.84	0.51		41.5	5.5	41.5	5.5	3.59	-28	-2	10	175225	BD+52 2294
NN	18 51 54	-37 33.5	0.378	159.6	-24.6	K1 V	8.11	0.88	0.47	0.34	36.9	8.5	41.0	06. r	6.17	-33	-32	-21	175073	CD-37 12969
Wo 9637	18 52 06	-22 44.1	0.105	103.7	+104.2 SB	K3 IIIa:	4.99	1.33	1.51	0.48	40.0	13.6	40.0	13.6	3	97	25	-32	175190	BD-22 4915
Gl 734 A	18 52 33	+10 54.6	0.120	95.0	-26.8 VAR	dM0	9.44	1.36	1.30	+0.66 J	62.1	7.3	62.1	7.3	8.41	-21	-15	-10	230017	BD+10 3724
Gl 734 B	18 52 33	+10 54.6	0.120	95.0			12.3 *				62.1	7.3	62.1	7.3	11.3 *					
Gl 735	18 53 03	+08 20.3	0.130	129.0	-13.5 SB	dM3 e	10.11	1.53	+1.1 :	1.08	88.6	4.3	88.6	4.3	9.85	-9	-10	-7		
Gl 736	18 53 12	+04 12.1	0.099	181.7	20.1	G8 V	8.03	0.90	0.56	0.33	68.8	20.5	42.0	06. r	6.15	22	4	-4	175541	BD+04 3911
Gl 737 A	18 53 21	-56 03.1	0.412	186.2	-13.5	K7 V	9.45	+1.42 J	+1.1 :J	+0.75 J	73.1	8.0	73.1	8.0	8.77	-22	-20	1	175224	CP-56 9037
Gl 737 B	18 53 21	-56 03.1	0.412	186.2	-15.8	K5 V	10.00			0.84	73.1	8.0	73.1	8.0	9.32	-24	-19	2		
Wo 9638	18 53 47	+23 29.7	0.314	155.4	+10.3 SB	K2	8.09	0.91	0.55		40.9	7.2	40.9	7.2	6.15	27	-1	-26	175742	BD+23 3500
NN	18 54 45	+07 30.5	0.182	227.0		m	11.20			0.83			48.0	08. r	9.61					
NN	18 55 00	+46 18.6	0.323	13.0		m	13.95			1.23			47.0	09. r	12.31					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 738 A	18 55 09	+32 50.2	0.224	135.3	-45.8 SB	F9 V	5.34	+0.59 J	+0.03 J		56.5	4.2	56.5	4.2	4.1	-12	-39	-28	176051	BD+32 3267
Gl 738 B	18 55 09	+32 50.2	0.224	135.3		K1 V	7.7 *				56.5	4.2	56.5	4.2	6.5 *					
NN A	18 55 13	+54 28.1	0.320	178.0		dM0	10.44	1.38	1.33	0.62	20.0	7.7	42.0	05. r	8.56					
NN B	18 55 15	+54 26.1	0.320	178.0		m	12.04	1.56		0.93	20.0	7.7	42.0	05. r	10.16					
Gl 739	18 55 20	-48 20.2	0.509	163.0		M3	11.15	1.46		1.02	87.1	5.6	87.1	5.6	10.85					CD-48 12818
Gl 740	18 55 34	+05 51.4	1.245	189.6	10.4	M2 V	9.22	1.46	1.17	0.76	94.6	6.4	94.6	6.4	9.1	46	-39	-19	176029	BD+05 3993
Wo 9639	18 56 55	+30 06.5	0.200	15.4	-39.5	G2 V	6.79	0.58	0.00		40.6	6.6	35.0	04. r	4.51	-43	-22	-4	176377	BD+29 3423
NN	18 57 13	+07 55.1	0.408	115.0		M2	10.86	1.42	1.26	0.73			43.0	07. r	9.03					BD+ 7 3922
Gl 740.1	19 00 10	-00 47.0	0.130	198.1	-7.2	dG5	8.43	0.73	0.29	+0.39C	54.3	10.2	54.3	10.2	7.1	0	-13	-1	176982	BD-00 3631
Gl 741	19 00 29	-13 38.1	0.780	225.8		M4 :	14.85v	+1.56v		+1.29v	53.1	3.9	53.1	3.9	13.48v					
Gl 742	19 00 39	+70 35.1	0.536	9.6		DXP5	13.20	0.05	-0.86		74.8	3.7	74.8	3.7	12.57					
Wo 9641	19 01 41	-21 49.0	0.100	127.1	27.2	K0 III	3.77	1.01	0.85		43.1	11.9	43.1	11.9	1.9	24	4	-16	177241	BD-21 5237
NN	19 02 54	+70 21.0	0.205	7.0		m	12.54			1.01			42.0	08. r	10.66					
NN A	19 02 55	+63 55.0				M0	10.60	+1.42 J	+1.24 J	+0.69 J			40.0	06. r	8.6					
Gl 743	19 03 00	+22 59.8	0.325	43.2	-16.9	G9	8.55	0.81	0.42		57.1	13.6	28.0	04. r	5.79	-52	18	-18	177745	BD+22 3579
Gl 743.1A	19 03 02	-37 08.2	0.289	160.9	-53.2	F8 V	4.87	+0.52 J	+0.00 J	+0.29CJ	52.8	8.4	68.0	08. r	4.03	-54	-16	5	177474	CD-37 13048
Gl 743.1B	19 03 02	-37 08.2	0.289	160.9	-51.3	F8 V	5.00*				52.8	8.4	68.0	08. r	4.16*	-53	-16	4	177475	
NN A	19 03 06	+13 47.5	0.100	185.0	-25. SB	A0 Vn	2.99	0.01	-0.01	-0.07	39.8	10.7	39.8	10.7	1	-9	-26	-6	177724	BD+13 3899
Gl 743.2	19 03 18	+25 50.7	0.059	225.6	-71.5	dK2	7.22	1.03	1.10		20.0	2.9	20.0	2.9	3.73	-27	-67	-6	177830	BD+25 3719
Gl 744	19 03 30	-37 53.0	0.417	208.3	58.5	G5 IV	6.15	0.71	0.27	+0.35C	61.2	6.5	61.2	6.5	5.08	56	-33	-15	177565	CD-37 13049
Wo 9643	19 03 49	-27 44.7	0.255	192.0	+45.4 SB	K1 III	3.32	1.19	1.15		43.1	10.2	43.1	10.2	1.5	46	-20	-17	177716	CD-27 13564
Gl 745 A	19 04 58	+20 48.8	0.578	234.7	32.1	sdM2	10.76	1.58		0.93	112.2	3.5	112.2	3.5	11.01	36	12	15		
Gl 745 B	19 05 05	+20 48.1	0.578	234.7	31.7	sdM2	10.75	1.58		0.93	112.2	3.5	112.2	3.5	11	35	11	15	349726	
NN	19 05 18	-42 30.4	0.127	166.4	-32	K1 V	7.88	0.86	0.53				43.0	07. r	6.05	-33	-9	4	177996	CD-42 13922
NN	19 05 19	-31 03.1	0.096	134.0		K0 V	7.82						39.0	05. o	5.78				178076	CD-31 16381
Gl 746	19 05 43	+16 46.6	0.310	169.0	+14.8 SB	G5 V	6.07	0.70	0.27		59.5	8.5	59.5	8.5	4.94	25	0	-14	178428	BD+16 3752
Gl 747 A	19 05 45	+32 27.0	1.635	48.9	-47	M3.5 J	11.86	+1.70 J		+1.14 J	122.6	1.9	122.6	1.9	12.3	-70	-12	-34		BD+32 3326
Gl 747 B	19 05 45	+32 27.0	1.635	48.9		M5 K	12.16*				122.6	1.9	122.6	1.9	12.60*					
GJ 1231	19 06 15	+26 30.6	0.539	202.6		m	15.16	1.91		1.38	58.0	3.8	58.0	3.8	13.98					
Gl 747.1	19 06 29	-14 49.4	0.549	158.5		M3	12.02	1.50	1.08	+1.26C	46.9	9.6	46.9	9.6	10.38					
NN	19 06 37	+32 12.1	0.311	225.0		m	11.80			1.11			81.0	16. r	11.34					
Gl 747.2	19 07 04	+33 58.8	0.101	306.6	+11.2 SB?	dK6	9.43	1.24	1.17	0.50	35.0	11.6	46.0	08. r	7.74	2	9	12		BD+33 3339
Gl 747.3	19 07 10	-47 14.0	0.632	183.9	2	K7 V	9.36	1.32	1.26	0.58	47.5	12.7	59.0	11. r	8.21	-11	-48	-11	178445	CP-47 9196
NN	19 07 39	+39 07.5				M0	11.33	1.53	1.21	0.89			55.0	10. r	10.03					
GJ 1232	19 07 40	+17 35.5	0.740	227.0	-12	k-m	13.52	1.85	1.44	1.35	93.6	2.8	93.6	2.8	13.38	19	-32	12		
NN	19 08 07	+01 27.4	0.260	220.0		g	12.18	1.50	1.22				41.0	20. r	10.2					
NN	19 08 14	+79 40.4	0.198	355.6	-32.2	dK8	9.72	1.10	0.96	0.46	46.3	15.4	33.0	04. r	7.31	-14	-40	-8		BD+79 615
Gl 747.4	19 08 19	-55 57.0	0.330	238.0		k-m	11.31	1.45	1.11	+0.99C	54.0	8.5	54.0	8.5	9.97					CD-56 7638
NN	19 09 13	-82 37.8	1.261	165.0		M3.5	12.7 *			1.16			63.0	13. r	11.7 *					
NN	19 09 18	+32 35.0	0.244	225.0		m	10.48			0.70			48.0	07. r	8.89					
NN	19 09 32	-39 07.2	0.503	106.3		M3	12.7 *			1.11			52.0	10. r	11.3 *					
Gl 748	19 09 38	+02 48.6	1.801	105.8	-42.6	dM4	11.10	1.51	1.04	1.15	99.4	2.2	99.4	2.2	11.09	-48	-15	-81		

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	19 10 40	+35 28.8	0.250	124.0		m	12.01	1.56	1.23	1.00	58.0	2.9	58.0	2.9	10.83					
Wo 9648 A	19 10 48	+49 45.7	0.667	340.0	-39.8	G6 V	6.57	0.65	0.21		43.5	2.9	43.5	2.9	4.76	-62	-43	35	179958	BD+49 2959
Wo 9648 B	19 10 47	+49 45.6	0.668	343.7	-41.2	G6 V	6.75	0.65	0.19		43.5	2.9	43.5	2.9	4.94	-65	-43	31	179957	
Gl 748.1	19 11 01	+76 28.7	0.128	161.7	+0.8 SB?	F2 V	5.13	0.31	0.00		47.3	8.5	47.3	8.5	3.5	9	7	-6	180777	BD+76 717
GJ 1233	19 11 16	+57 34.8	0.451	26.7	-26.3	G8 V	7.04	0.79	0.43		39.1	9.0	54.0	09. r	5.7	-40	-22	-13	180161	BD+57 1961
Gl 748.2A	19 12 26	+02 04.3	0.513	41.9		K4	10.20	1.19		0.51	45.9	6.3	45.9	6.3	8.51					BD+01 3942
Gl 748.2B	19 12 26	+02 04.3	0.513	41.9		k-m	11.17	1.36		0.63	45.9	6.3	45.9	6.3	9.48					
Wo 9652 A	19 12 30	+19 13.4	0.726	305.3		M3	11.55			1.13	47.9	4.9	47.9	4.9	9.95					
Wo 9652 B	19 12 30	+19 12.7	0.726	305.3		M3.5	13.27			1.21	47.9	4.9	47.9	4.9	11.67					
Gl 750 A	19 13 03	-45 58.4	0.450	154.0	-36.8	K9 V J	10.12	+1.42 J	+1.08:J	+0.97CJ	72.6	8.1	72.6	8.1	9.42	-44	-16	-3	179930	CP-46 9672
Gl 750 B	19 13 03	-45 58.4	0.450	154.0			10.1 *				72.6	8.1	72.6	8.1	9.4 *					
Gl 751	19 13 14	+24 48.3	0.305	51.0	-70.1	dM0	9.72	1.35	1.24	0.58	26.9	7.1	51.0	10. r	8.26	-58	-44	-19	338030	BD+24 3692
Gl 752 A	19 14 29	+05 05.8	1.466	204.2	36.3	M3.5Ve	9.11	1.50	1.15	1.02	176.7	2.4	176.7	2.4	10.35	53	-6	-5	180617	BD+04 4048
Gl 752 B	19 14 32	+05 04.7	1.461	203.1		dM5 e	17.52v	+2.2 :		+1.83:	176.7	2.4	176.7	2.4	18.76v					
NN	19 15 48	-53 48.	0.102	164.0		M2	10.82	1.58		+0.95t			84.0	17. r	10.44					
Gl 754	19 17 07	-45 36.7	2.945	167.3	16	M4.5	12.23	1.68	1.22	1.33	175.7	8.4	175.7	8.4	13.45	-10	-69	-41		
GJ 1234	19 17 15	+38 38.0	0.250	179.0		DC7	14.57	0.44	-0.36		85.6	3.9	85.6	3.9	14.23					
Gl 754.2	19 17 53	+37 14.4	0.169	196.0	1.8	G8 V	6.31	0.68	0.21		40.7	10.2	60.0	10. r	5.2	13	-3	-2	181655	BD+37 3417
Gl 754.1A	19 17 53	-07 45.6	0.199	198.0		DQ5	12.28	0.06	-0.83	+0.04C	98.8	3.1	98.8	3.1	12.25					
Gl 754.1B	19 17 51	-07 45.3	0.199	198.0	10	dM5	12.12	1.63	1.42	1.09	98.8	3.1	98.8	3.1	12.09	13	-4	-3		
Gl 755	19 18 12	-35 04.6	0.123	131.7	-10.2	G5 V	6.48	0.62	0.19	0.22			48.0	07. r	4.89	-13	-5	-7	181321	CD-35 13422
NN	19 18 46	-17 56.6	0.035	313.1	1.2	F0 IV	3.93	0.23	0.13		39.1	8.7	39.1	8.7	1.89	2	2	4	181577	BD-18 5322
Gl 755.1	19 19 23	+14 34.9	0.090	180.0	35	DA5	13.01	0.06	-0.66		50.9	5.3	50.9	5.3	11.54	-1	-12	-4		
GJ 1235	19 19 32	+20 47.5	1.751	212.6	93	k-m	13.38	1.71		1.31	98.4	4.5	98.4	4.5	13.34	122	27	11		
GJ 1236	19 19 39	+06 57.2	0.836	242.3	32	m	12.35	1.69	1.33	1.09	91.5	2.4	91.5	2.4	12.16	49	-4	22		
Gl 756	19 19 49	+28 34.0	0.900	73.7	-30.6	M1	11.53	1.41	1.05	0.86	44.6	4.2	44.6	4.2	9.78	-69	12	-72		
Gl 756.1	19 20 14	-66 34.3	0.324	316.5	37.9	K5 V	8.40	1.04	0.96	0.32	38.8	10.2	43.0	09. r	6.57	52	-3	6	181433	CP-66 3431
NN	19 20 42	+29 20.6	0.704	179.7		m	15.37	1.82			47.6	4.1	47.6	4.1	13.76					
Gl 757	19 21 36	-22 09.3	0.494	206.3		K4	10.92	1.41	1.15	+0.80C	47.4	8.0	47.4	8.0	9.3					CD-22 13916
Gl 758	19 21 41	+33 07.3	0.190	24.2	-20.6	K0 V	6.37	0.81	0.46		56.7	5.1	56.7	5.1	5.14	-23	-12	-2	182488	BD+32 3411
Gl 759	19 22 35	+11 50.2	0.966	48.4	-100.6 SB?	G8 IV	5.16	0.77	0.42	0.24	64.3	4.3	64.3	4.3	4.2	-118	-29	-21	182572	BD+11 3833
Gl 760	19 22 59	+03 00.8	0.268	72.0	-29.9 SB	F0 IV	3.36	0.32	0.04		72.5	5.6	72.5	5.6	2.66	-32	-10	-9	182640	BD+02 3879
NN	19 23 08	+28 15.0	0.410	24.9		M3.5	12.48	1.56		1.15			67.0	17. r	11.6					
NN	19 24 36	+16 37.0	0.212	163.0		m	13.09			1.18			57.0	11. r	11.87					
GJ 1237	19 25 02	+49 21.2	0.843	32.8	-65.3	K3 V	8.01	0.93	0.64		40.7	10.4	48.0	08. r	6.42	-91	-47	-28	183255	BD+49 3009
GJ 1238	19 25 40	+75 26.7	0.681	33.8		m+	15.37	1.94		1.60	90.7	5.1	90.7	5.1	15.16					
NN	19 26 38	+07 03.2	0.348	50.0		K7	10.71	1.41	1.21				47.0	22. r	9.1					
Wo 9657 A	19 26 47	-27 05.4	0.053	139.0	-31.4	K3 III	5.52	1.12	1.35	0.36	43.8	10.2	21.0	05. r	2.1	-31	-12	1	183275	CD-27 14004
Wo 9657 B	19 26 47	-27 05.4	0.053	139.0	-31.8		8.69	0.86	0.32		43.8	10.2	21.0	05. r	5.3	-32	-12	1		
Gl 761.1	19 27 26	+31 30.6	0.400	183.3	-10	G7 IV	6.96	0.71	0.34		48.4	10.2	48.4	10.2	5.38	29	-22	-18	183650	BD+31 3618
Wo 9659	19 28 12	-06 37.1	0.194	223.0	58.4	G0	7.29	0.64	0.19		41.9	8.5	33.0	04. r	4.88	64	8	-4	183658	BD-06 5170
GJ 1239	19 29 14	-35 33.7	0.329	298.3		K5 V	8.71	1.11	0.98	0.43			50.0	08. r	7.2				183783	CD-35 13554

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
GJ 1240	19 29 20	-11 23.0	0.233	85.5	-48.1	K2 V	7.57	0.92	0.64	0.34			57.0	09. r	6.35	-50	-15	-5	183870	BD-11 5030
Gl 761.2	19 30 04	+00 28.2	0.250	79.0	-47.9	dM0.5	10.43	1.45	1.26	0.68	44.6	3.9	44.6	3.9	8.68	-50	-18	-13		BD+00 4241
NN	19 30 06	-52 32.	0.255	181.0		M4	12.80	1.55		+1.02t			39.0	08. r	10.76					
Gl 762	19 30 10	-62 56.9	0.500	226.4		m+	12.17	1.48		0.98	60.2	13.6	60.2	13.6	11.07					
Gl 762.1	19 30 18	+58 29.0	0.648	232.8	+11.4	SB K1 V	6.59	0.87	0.52		48.6	8.8	48.6	8.8	5.02	55	1	33	184467	BD+58 1929
Wo 9661	19 31 39	+07 16.3	0.264	126.1	-25.1	K3 IIIb	4.45	1.17	1.26		46.1	8.4	46.1	8.4	2.77	-17	-22	-24	184406	BD+07 4132
NN	19 31 56	+39 25.3	0.465	151.0		M2.5	11.70			0.99			60.0	10. r	10.59					
Gl 763	19 32 09	+04 28.1	0.605	59.9	-57.4	dM0.5	9.36	1.39	1.23	0.61	73.7	6.7	73.7	6.7	8.7	-66	-15	-13	184489	BD+04 4157
Gl 764	19 32 28	+69 34.6	1.822	162.0	28.2	K0 V	4.68	0.79	0.38	0.29	178.2	3.4	178.2	3.4	5.93	30	44	-17	185144	BD+69 1053
NN A	19 32 41	+08 21.0	0.054	222.0	-20.5	dM1	10.38	1.46	1.22	0.77	28.3	11.3	48.0	06. r	8.79	-11	-18	3		
NN B	19 32 41	+08 21.0	0.054	222.0			12.52	1.52		0.99	28.3	11.3	48.0	06. r	10.93					
NN	19 33 02	+51 07.7	0.185	173.6	0.4	F7 V	5.73	0.48	0.00	0.17	35.3	10.2	41.0	05. r	3.79	18	1	-11	184960	BD+50 2815
NN	19 33 41	+53 08.3	0.572	29.0		M3	12.20	1.64		1.03			57.0	14. r	11					
Gl 764.1A	19 34 02	-10 33.1	0.385	225.7	68	K2 V	8.58	+1.01 J	+0.82 J	+0.52CJ	52.5	6.4	52.5	6.4	7.18	76	4	-6	184860	BD-10 5130
Gl 764.1B	19 34 02	-10 33.1	0.385	225.7	68.6	K7	10.2 *				52.5	6.4	52.5	6.4	8.8 *	77	4	-6		
Gl 764.2	19 34 45	-14 24.8	0.179	215.7	-15.4	F7 V	5.47	0.50	0.04	+0.28C	45.0	11.9	50.0	08. r	3.96	-5	-21	7	184985	BD-14 5479
Gl 765 A	19 35 06	+50 06.3	0.260	355.5	-27.3	F4 V	4.48	0.38	-0.03		54.0	7.7	54.0	7.7	3.14	-23	-27	5	185395	BD+49 3062
Gl 765 B	19 35 06	+50 06.3	0.260	355.5			13.0 *				54.0	7.7	54.0	7.7	11.7 *					
GJ 1241	19 35 10	+27 36.4	0.405	85.0		DAV5	12.98	0.17	-0.56		55.6	2.9	55.6	2.9	11.71					
NN	19 36 07	+33 46.7	0.107	297.3		G5	7.47						41.0	05. o	5.53				185501	BD+33 3529
Wo 9664 A	19 38 18	-59 07.5	0.256	137.9	19.5	G5 V	7.48D	0.71	0.28		39.7	10.2	36.0	06. r	5.26D	-4	-23	-31	185454	CP-59 7505
Wo 9664 B	19 38 18	-59 07.5	0.256	137.9			8.7 *				39.7	10.2	36.0	06. r	6.5 *					
NN	19 39 19	-45 11.8	0.242	188.0		M1	10.01	1.34		+0.64t	34.0	11.0	51.0	08. r	8.55					CD-45 13383
GJ 1242	19 39 24	+03 02.5	0.536	209.5		m	12.88	1.60	1.23	0.97	42.7	2.6	42.7	2.6	11.03					
NN	19 40 06	+71 45.5	0.454	205.0		M0.5	10.96	1.48	1.25	0.76	48.1	7.3	48.1	7.3	9.37					
Gl 765.1A	19 40 29	+50 24.5	0.214	225.9	-27.4	G2 V	5.96	0.64	0.19		35.2	5.0	43.0	04. s	4.13	19	-31	1	186408	BD+50 2847
Gl 765.1B	19 40 32	+50 24.0	0.211	221.5	-28.1	G5 V	6.20	0.66	0.20		35.2	5.0	43.0	04. s	4.37	19	-31	-1	186427	BD+50 2848
Gl 765.2	19 40 40	+76 18.2	0.211	46.6	-3.8	dK0	8.08	0.88	0.55		43.9	11.2	40.0	06. r	6.09	-21	-6	-12	186922	BD+76 750
Wo 9666	19 40 42	-15 35.3	0.235	139.9	12.8	F5 IV	5.49	0.46	0.02		43.6	13.6	43.6	13.6	3.7	9	-8	-26	186185	BD-15 5444
NN	19 41 45	-71 12.2	0.673	176.3		m	13.9 *			1.19			41.0	08. r	12.0 *					
Gl 765.3	19 42 16	+57 53.8	0.129	114.2	-29.8	F8	6.23	0.55	0.05		45.6	8.5	42.0	05. r	4.35	0	-25	-22	186760	BD+57 2057
Gl 765.4A	19 43 39	+33 29.1	0.431	177.7	4.4	K3 V	8.35	+0.99 J	+0.78 J	+0.37 J	43.9	3.9	43.9	3.9	6.56	39	-8	-24	186858	BD+33 3582
Gl 765.4B	19 43 39	+33 29.1	0.431	177.7		K3 V	8.54*				43.9	3.9	43.9	3.9	6.75*					
Gl 766 A	19 43 43	+27 01.2	1.226	181.5		dM4.5 J	12.91	+1.72 J		+1.28 J	93.1	5.6	93.1	5.6	12.75					
Gl 766 B	19 43 43	+27 01.2	1.226	181.5			13.4 *				93.1	5.6	93.1	5.6	13.2 *					
NN	19 43 52	+32 15.7	0.457	63.0		M0	10.86			0.88			58.0	09. r	9.68					
Gl 767 A	19 44 26	+31 53.9	0.623	131.0	-4.4	M0.5	10.15	1.48	1.17	0.85	74.1	2.0	74.1	2.0	9.5	6	-5	-39	331161	BD+31 3767
Gl 767 B	19 44 26	+31 53.9	0.623	131.0	-3.5	M2 :	11.10	1.52			74.1	2.0	74.1	2.0	10.45	6	-4	-39		
Gl 767.1A	19 44 32	+33 36.6	0.444	178.9	4.2	F5 IV-V	4.99	0.47	0.00		44.4	2.5	44.4	2.5	3.23	40	-9	-24	187013	BD+33 3587
Gl 767.1B	19 44 34	+33 36.8	0.443	177.6	4.5	dK6	8.56	1.04	0.95	0.38	44.4	2.5	44.4	2.5	6.8	39	-8	-25	225732	BD+33 3589
NN	19 47 13	+08 04.9	0.249	243.0		k	15.21	1.72	1.25				39.0	16. r	13.2					
NN	19 48 05	+32 27.2	0.526	61.7		M3	12.41	1.62		1.06	58.5	3.4	58.5	3.4	11.25					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	19 48 19	+31 39.0	0.365	27.0		m	12.88			1.06			42.0	08. r	11					
Gl 768	19 48 21	+08 44.1	0.662	54.3	-26.1	A7 IV-V	0.77	0.22	0.08	0.02	201.0	3.8	201.0	3.8	2.29	-29	-10	-2	187642	BD+08 4236
Gl 768.1A	19 48 38	+10 17.4	0.274	120.0	-0.2	F8 V	5.11	0.55	0.07		46.3	13.1	59.0	07. r	3.96	-2	-3	-22	187691	BD+10 4073
Gl 768.1B	19 48 38	+10 17.4	0.274	120.0	-1.2	M3	13.10			1.18	46.3	13.1	59.0	07. r	11.95	-3	-3	-22		
GJ 1243	19 49 37	+46 21.0	0.290	32.0		m	12.83	1.64		1.22	83.9	2.4	83.9	2.4	12.45					
NN	19 49 43	+11 30.2	0.484	226.3	-19.5	G0 V	6.13	0.65	0.13		23.4	17.0	51.0	05. s	4.67	22	-41	15	187923	BD+11 4019
Gl 769	19 50 22	-47 55.6	1.072	186.2	25	M3	12.53	1.56	1.12	0.96	38.4	9.3	38.4	9.3	10.5	-2	-133	-18		
GJ 1244	19 50 37	-72 29.5	0.299	182.5		K5 V	8.45	1.06	0.98	0.38			49.0	07. r	6.9				187456	CD-72 1570
Gl 770	19 51 18	-24 04.0	0.426	197.4	-5.1	SB K3/4 V	6.17	1.02	0.94	0.34	71.7	8.3	71.7	8.3	5.45	3	-28	1	188088	CD-24 15668
NN	19 51 39	+34 00.4	0.241	2.0		m	11.63			0.89			46.0	08. r	9.94					
NN	19 52 06	+32 25.8	0.251	51.0		m	12.43			0.98			41.0	08. r	10.49					
GJ 1245 A	19 52 16	+44 17.5	0.731	143.1		M5.5 V e	13.41	1.90		1.65	212.0	4.3	212.0	4.3	15.04					
GJ 1245 B	19 52 17	+44 17.5	0.731	143.1		m	14.01	1.98		1.71	212.0	4.3	212.0	4.3	15.64					
Wo 9672	19 52 33	+03 56.0	0.383	229.6	50	K3	9.40	0.99	0.80	0.40	40.7	11.9	30.0	04. r	6.79	78	-4	10	188427	BD+03 4191
Gl 771 A	19 52 51	+06 16.8	0.481	174.8	-40.7	G8 IV	3.72	0.86	0.48	0.31	74.3	8.1	74.3	8.1	3.07	-12	-49	-9	188512	BD+06 4357
Gl 771 B	19 52 51	+06 16.8	0.481	174.8		M3	11.4 *				74.3	8.1	74.3	8.1	10.8 *					
GJ 1246	19 53 26	-31 28.2	0.418	86.8		K4 V	8.43	0.98					46.0	06. r	6.74				188474	CD-31 17179
Gl 772	19 53 56	-01 10.0	0.790	211.9	76	DA6	13.70	0.28	-0.60	-0.06	86.1	3.1	86.1	3.1	13.38	51	-14	-5		
Wo 9674	19 54 30	+51 08.1	0.586	52.6		M2	12.0 *				45.6	4.1	45.6	4.1	10.3 *					
Gl 773 A	19 54 33	-12 41.7	0.516	189.1	-10.6	VAR K4 V	9.30	1.33	1.21	0.56	47.4	5.4	47.4	5.4	7.68	11	-51	-9	188807	BD-12 5594
Gl 773 B	19 54 37	-12 41.5	0.520	188.1		m	15.36			1.54	47.4	5.4	47.4	5.4	13.74					
GJ 1247	19 54 35	-55 04.3	0.177	138.1		K3 V	8.60	1.08	0.88	0.38			44.0	07. r	6.82				188559	CD-55 8349
Gl 773.2	19 55 13	+29 41.1	0.262	19.7	-29.6	K0 Ve	7.90	0.80	0.38		47.4	10.8	38.0	06. r	5.8	-41	-15	7	189087	BD+29 3820
Wo 9677 A	19 55 39	+59 01.7	0.421	255.0		dM0 p	9.96	1.22		0.59			40.0	05. r	7.97					BD+58 2015
Wo 9677 B	19 55 30	+59 01.3	0.421	255.0		m	13.50	1.48		1.12			40.0	05. r	11.51					
NN	19 55 45	+01 54.6	0.864	201.3		k	11.95	1.55	1.33	1.02	63.1	3.8	63.1	3.8	10.95					
Gl 773.3	19 57 04	-10 05.4	0.483	214.5	+30.2	SB G0 V	5.88	0.58	0.05	0.21	40.6	7.2	40.6	7.2	3.92	56	-31	-2	189340	BD-10 5238
Gl 773.4	19 57 07	-33 50.3	0.315	155.6	-8.2	VAR F8 V	5.66	0.49	-0.02	0.15	51.6	7.2	51.6	7.2	4.22	-13	-24	-13	189245	CD-34 14082
NN	19 58 34	+22 34.6	0.238	179.7		G5	7.67						52.0	06. o	6.25				189733	BD+22 3887
Gl 773.6	19 58 50	-50 11.2	0.532	135.4	19.3	K5 V	8.66	1.12	1.09	0.42	47.8	10.2	51.0	08. r	7.2	-10	-30	-43	189484	CP-50 11256
Gl 774 A	19 59 20	-65 43.7	0.863	172.5	72	m	11.35	1.48	0.98	0.96	74.6	7.4	74.6	7.4	10.71	25	-77	-41		
Gl 774 B	19 59 20	-65 43.7	0.863	172.5	33	m	12.82	1.56	1.01	1.11	74.6	7.4	74.6	7.4	12.18	-4	-60	-21		
Gl 775.1	20 00 17	+15 27.6	0.598	195.9	20	G8 V	7.16	0.71	0.23	0.27	66.7	24.0	45.0	07. r	5.43	60	-20	-19	190067	BD+15 4026
Gl 775	20 00 17	+03 11.0	0.150	326.6	-29.7	K4 V	7.46	1.14	1.08	0.42	70.6	10.2	70.6	10.2	6.7	-22	-15	16	190007	BD+02 4076
Gl 776	20 00 34	-67 27.2	1.081	129.8	-12.2	G2 V	6.08	0.65	0.07	0.23	53.0	7.2	53.0	7.2	4.7	-75	-34	-52	189567	CP-67 3703
Gl 776.1	20 00 41	-45 47.7	0.584	270.7		K4 :	12.15	1.40		0.72	47.1	13.6	23.0	05. r	8.96					
NN	20 00 56	-31 49.7	0.813	156.6		m	14.5 *			1.31			50.0	08. r	13.0 *					
NN	20 01 19	-08 16.1	0.570	243.3		k-m	13.4 *			1.23			60.0	11. r	12.3 *					
GJ 1248	20 01 24	+05 51.9	0.922	212.0		k-m	12.09	1.60	1.14	0.96	78.9	4.3	78.9	4.3	11.58					
Gl 777 A	20 01 34	+29 45.7	0.864	127.7	-45.9	G8 IV-V	5.71	0.73	0.37	0.27	58.1	2.6	59.8	6.5	4.59	-12	-46	-68	190360	BD+29 3872
Gl 777 B	20 01 23	+29 43.9	0.857	127.9	-5	M4 :	14.37	1.67	1.12	1.37	85.4	10.2	59.8	6.5	13.25	4	-8	-68		
Gl 778	20 01 47	+23 12.7	1.353	228.3	-1.8	K1 V	7.26	0.82	0.40	0.31	54.7	18.3	55.0	08. r	5.96	99	-52	32	190404	BD+22 3908

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 779	20 01 51	+16 56.0	0.571	224.3	4.8	G1 V	5.80	0.61	0.09	0.19	60.2	5.6	60.2	5.6	4.7	40	-19	9	190406	BD+16 4121
Gl 779.1	20 02 04	+25 38.9	0.085	241.1	-6.4	K3 V	7.88	0.91	0.71				51.0	08. r	6.42	4	-9	4	190470	BD+25 4085
NN	20 02 46	-11 05.4	1.081	94.9		DC9	16.87	1.04			57.2	5.5	57.2	5.5	15.66					
NN	20 02 53	+54 19.5	0.124	157.7	-9	dK0	7.72	0.94	0.65		14.4	20.5	54.0	07. r	6.38	6	-7	-10	190780	BD+54 2281
GJ 1249	20 03 20	+38 20.0	0.278	68.5	-22.5	G5 IV	6.17	0.65	0.18		43.8	8.5	43.8	8.5	4.38	-29	-14	-19	190771	BD+38 3896
Gl 780	20 03 50	-66 18.7	1.660	133.5	-21.7	G8 V	3.56	0.76	0.45	0.23	175.2	8.2	175.2	8.2	4.78	-47	-12	-13	190248	CP-66 3474
Gl 781	20 03 55	+54 18.2	1.455	232.7	-148.0 SB	dM3 e	11.99	1.54		0.82	59.9	2.0	59.9	2.0	10.88	103	-156	11		
NN	20 04 25	+52 49.4	0.264	44.0		m	13.16			1.18			55.0	11. r	11.86					
Gl 781.1A	20 04 38	-31 53.6	0.796	158.8		M3	12.25	1.55	1.11	1.06	50.7	10.2	50.7	10.2	10.78					
Gl 781.1B	20 04 35	-31 53.3	0.796	158.8		M3.5	12.50	1.63	1.07	1.18	50.7	10.2	50.7	10.2	11.03					
NN	20 05 21	-01 41.2	0.407	129.0		k-m	13.55	1.62	1.20				49.0	22. r	12					
GJ 1250	20 06 21	+33 09.0	0.488	39.4		m	14.88	1.82	1.14		46.8	6.2	46.8	6.2	13.23					
Gl 781.2	20 06 48	-14 26.0	0.120	113.5	-14.5	K3/4 V	9.76	1.15	1.05	0.48	47.9	11.9	36.0	04. r	7.54	-17	-9	-9	191285	BD-14 5652
Gl 781.3	20 07 21	-21 55.4	0.311	158.0	35	DA6	14.44	0.19	-0.70				59.0	16. w	13.3	-9	-23	-11		
Gl 782	20 07 26	-20 38.2	0.565	231.0	+19.4 SB?	K4 Vp	8.92	1.29	1.21	0.55	63.2	6.8	63.2	6.8	7.92	39	-24	10	191391	BD-20 5833
GJ 2147	20 07 51	-30 21.9	0.423	236.0		DA4	12.18	0.07	-0.66				79.0	16. w	11.67					
NN	20 07 54	-25 43.4	0.848	166.6		m	14.98			1.34			45.0	07. r	13.25					
Gl 783 A	20 07 55	-36 13.7	1.633	163.8	-129.8	K3 V	5.32	0.87	0.46	0.34	177.1	9.4	177.1	9.4	6.56	-118	-49	48	191408	CD-36 13940
Gl 783 B	20 07 55	-36 13.7	1.633	163.8		M3.5	11.5 *				177.1	9.4	177.1	9.4	12.7 *					
Gl 783.2A	20 08 50	+16 02.0	0.574	314.7	-48.3	K1 V	7.33	0.85	0.49	0.30	35.5	10.3	51.0	06. r	5.87	-31	-26	59	191785	BD+15 4074
Gl 783.2B	20 08 57	+16 01.8	0.572	312.9		dM	13.94	1.62	1.14	1.24	35.5	10.3	51.0	06. r	12.48					
NN	20 09 36	+38 14.9	0.122	16.3	-6	G8 V	7.95	0.86	0.57				41.0	04. o	6.01	-15	-3	4	192020	BD+37 3812
NN	20 09 39	-12 45.9	0.275	134.6	22.6	F7 V	5.85	0.48	-0.07		38.1	7.1	39.0	05. r	3.81	13	-6	-38	191862	BD-13 5608
Gl 784	20 10 19	-45 18.8	0.796	102.5	-31.1	M0 V	7.97	1.43	1.18	0.73	163.9	8.5	163.9	8.5	9.04	-39	1	-2	191849	CD-45 13677
Gl 784.2A	20 11 32	+06 32.5	0.633	202.8		dM5	13.19	1.54	1.22	1.20	44.4	2.0	44.4	2.0	11.43					
Gl 784.2B	20 11 29	+06 34.0	0.633	202.8		DA7	15.72	0.37	-0.40	0.29	44.4	2.0	44.4	2.0	13.96					
NN	20 11 47	-07 25.8	0.269	178.0		K7 V	10.20	1.34	1.22	0.61			43.0	08. r	8.37					BD- 7 5223
Gl 785	20 12 10	-27 11.0	1.259	98.5	-54.4 SB?	K0 V	5.73	0.88	0.64	0.32	108.8	13.5	108.8	13.5	5.91	-74	-11	-20	192310	CD-27 14659
Gl 786	20 12 24	+77 04.8	0.517	6.7	-1.1	dM0	8.88	1.33	1.28		60.4	3.1	60.4	3.1	7.79	-34	-19	12	193202	BD+76 785
NN	20 12 37	-39 38.5	0.251	149.3		K1 V	7.77c	+0.86c					47.0	07. r	6.13c				192354	CD-39 13701
Gl 786.1	20 14 11	+42 49.5	0.060	170.0		dM0 p	9.97	1.34	1.30	0.60	34.6	3.8	34.6	3.8	7.67					
NN	20 14 28	+06 46.0	0.161	86.4	-57.3	dK8	9.72	1.14	1.08	0.44	47.2	17.0	33.0	04. r	7.31	-49	-37	-3		BD+06 4489
Gl 787	20 16 07	-46 35.1	0.387	255.7	29.9	K5 V	8.72	1.16	1.14	0.48	62.6	6.8	62.6	6.8	7.7	39	-14	6	192961	CP-46 9951
NN	20 16 30	+15 41.0	0.207	108.0		m	11.79			1.00			58.0	11. r	10.61					
Gl 788	20 17 02	+66 41.6	0.549	57.6	-4.6	G5 V	5.93	0.58	0.06		72.9	8.2	72.9	8.2	5.24	-31	-5	-17	193664	BD+66 1281
NN	20 17 13	+07 51.0	0.182	152.0		m	12.92			1.09			45.0	09. r	11.19					
NN	20 17 27	-51 57.0	0.110	336.0		M0	10.20	1.41		+0.71t			56.0	10. r	8.94					CD-52 9466
Wo 9691	20 18 04	-50 09.3	0.432	235.6	17.9	G2 IV-V	6.27	0.55	-0.02	0.20	43.5	7.8	43.5	7.8	4.46	30	-35	21	193307	CD-50 12929
Gl 788.1	20 18 35	-58 26.4	0.845	114.8	-66	m	10.59	1.46	1.16	0.68	51.2	8.5	51.2	8.5	9.14	-101	-1	-19		CD-58 7734
GJ 1251	20 21 33	-76 49.9	1.430	152.9	122	M4.5	13.82	1.74	1.13	1.26			59.0	10. r	12.67	-9	-145	-83		
GJ 1252	20 23 46	-56 35.7	1.283	161.4	6	m	12.23	1.45	1.07	0.97			42.0	08. r	10.35	-61	-127	-35		
Gl 790	20 24 38	-31 01.6	0.519	181.6	-1	G5 V	6.61	0.73	0.28	0.24	56.3	4.7	56.3	4.7	5.36	3	-43	-8	194640	CD-31 17597

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 791	20 24 40	-27 54.1	0.892	192.9	-16	M3	11.41	1.52	1.12	1.04	79.6	9.0	79.6	9.0	10.91	0	-55	6		CD-28 16676
NN	20 24 50	+27 20.9	0.288	0.0		m	12.27			0.97			43.0	08. r	10.44					
GJ 1253	20 24 58	+58 24.0	0.606	24.1		M5	14.04	1.79		1.42	107.6	3.6	107.6	3.6	14.2					
Gl 791.1A	20 26 01	-17 58.8	0.029	215.5	18.4	F2 IV	4.78	+0.38 J	+0.03 J	+0.36CJ	52.1	7.9	52.1	7.9	3.36	16	5	-8	194943	BD-18 5689
Gl 791.1B	20 26 01	-17 58.8	0.029	215.5			10.0 *				52.1	7.9	52.1	7.9	8.6 *					
Gl 791.2	20 27 21	+09 31.2	0.685	79.8	-15	dM6 e	13.05	1.65	1.28	1.32	114.2	1.9	114.2	1.9	13.34	-28	-5	-16		
Wo 9697 A	20 28 04	+26 40.6	0.197	224.8	15.4	dM1	10.28	+1.34 J	+1.24:J	+0.60 J	28.4	4.6	28.4	4.6	7.55	36	3	3		BD+26 3915
Wo 9697 B	20 28 04	+26 40.6	0.195	228.0			10.7 *				28.4	4.6	28.4	4.6	8.0 *					
Gl 791.3	20 29 33	+33 36.3	0.151	90.0	-26.8	dK8	9.23	1.13	1.08	0.42	49.2	10.2	39.0	05. r	7.19	-18	-24	-13		BD+33 3936
Gl 792	20 29 34	+38 22.9	0.743	16.8		M4	13.48	1.76		1.24	66.4	2.7	66.4	2.7	12.59					
Gl 793	20 29 50	+65 16.6	0.533	57.9	10.1	dM3	10.56	1.56	+1.21?	1.08	120.4	7.0	120.4	7.0	10.96	-21	9	-6		
Gl 793.1	20 31 06	+41 43.2	0.486	340.6	-6.1	SB G9 V	7.09	0.79	0.38	0.31	51.1	4.9	51.1	4.9	5.63	-26	-3	37	195987	BD+41 3799
NN	20 31 25	-13 53.7	0.097	43.3	-42.7	F6 V	6.13	0.54	-0.02	0.19			39.0	05. r	4.09	-39	-11	17	195838	BD-14 5781
NN	20 31 31	+23 11.8	0.287	73.0		m	12.93			1.09			45.0	09. r	11.2					
NN	20 32 11	+03 10.8	0.564	155.8		m	12.00	1.43	0.97	1.00	48.0	2.5	50.0	10. r	10.49					
Gl 794	20 32 14	+24 54.0	0.662	214.2	+71.0	VAR DA3	11.52	-0.07	-0.87		69.4	2.3	69.4	2.3	10.73	52	6	-5		
GJ 1254	20 32 40	+61 34.0	1.052	30.5	-29	m	12.52	1.52		1.23	62.5	2.8	62.5	2.8	11.5	-75	-39	0		
NN	20 33 18	+64 08.9	0.436	254.0		m	13.08			1.10			43.0	09. r	11.25					
NN	20 33 51	+59 07.1	0.262	260.0		m	13.43			1.19			51.0	10. r	11.97					
Gl 794.1	20 34 04	-47 28.0	0.088	38.6	-1.3	K0 III	3.11	1.00	0.80	+0.46C	44.8	13.6	44.8	13.6	1.4	-3	8	-4	196171	CD-47 13477
NN	20 34 54	+38 40.1	0.237	134.0		m	13.35			1.17			49.0	09. r	11.8					
NN	20 35 08	+21 46.5	0.288	190.0		M2	11.44	1.50		0.83			43.0	07. r	9.61					
Gl 794.2	20 35 55	-60 43.1	0.650	151.8	-31.6	F8 V	5.12	0.53	0.01	0.20	46.6	9.8	55.0	05. s	3.82	-55	-33	4	196378	CP-60 7419
Gl 794.3	20 36 47	+38 27.7	0.290	133.9	-21.4	G2 V	6.75	0.62	0.12		48.4	10.2	40.0	06. r	4.76	-1	-23	-34	196850	BD+38 4172
Gl 795 A	20 37 05	+04 47.6	0.882	84.1	-39.2	SB K4 V	8.18	+1.22 J	+1.17 J	+0.54 J	63.5	3.1	63.5	3.1	7.19	-66	-17	-34	196795	BD+04 4510
Gl 795 B	20 37 05	+04 47.6	0.882	84.1		K8 V	9.4 *				63.5	3.1	63.5	3.1	8.4 *					
Gl 796	20 37 13	-23 57.5	0.678	46.8	-45.3	G8 V	6.36	0.72	0.22	0.26	70.1	8.8	70.1	8.8	5.59	-61	19	7	196761	CD-24 16193
GJ 1255 -	20 52 04	+74 34.9	0.705	35.1	-29.9	G8 V	7.80	0.70	0.15		44.7	9.5	44.7	9.5	6.05	-61	-52	-8	199476	BD+74 889
GJ 1255 A	20 38 03	+75 25.0	0.650	30.7		SB K0 V	8.0 *	+0.86 J	+0.44 J	+0.35 J	40.4	2.4	40.4	2.4	6.0 *				197433	BD+75 752
GJ 1255 C	20 38 03	+75 25.0	0.650	30.7			10.4 *				40.4	2.4	40.4	2.4	8.4 *					
NN	20 38 07	-81 53.8	0.745	136.6		m	11.5 *			1.06			79.0	16. r	11.0 *					
GJ 1256	20 38 10	+15 18.7	1.487	63.3	-76	dM4-5	13.43	1.72	1.29	1.37	101.6	2.3	101.6	2.3	13.46	-94	-41	-11		
NN	20 38 13	-10 17.5				M0 e	11.94	1.51	1.17	0.92			44.0	08. r	10.16					
Gl 797 A	20 38 29	+19 45.2	0.338	21.8	-35.8	G5 V	6.45	0.63	0.09	0.22	49.8	2.1	49.8	2.1	4.94	-43	-16	16	197076	BD+19 4484
Gl 797 B	20 38 29	+19 43.1	0.330	22.0	-35.4	m	11.88	1.55	1.26		49.8	2.1	49.8	2.1	10.37	-42	-16	15		
Gl 798	20 38 37	-52 51.8	1.069	176.4	-42.9	K7 V	8.82	1.31	1.13	0.61	82.0	7.9	82.0	7.9	8.39	-48	-52	26	196877	CP-53 9928
Gl 799 A	20 38 44	-32 36.6	0.429	140.5	-4	dM4.5e	10.99	+1.57 J	+0.88 J	+1.33 J	122.8	6.1	122.8	6.1	11.44	-9	-12	-8	196982	CD-32 16135
Gl 799 B	20 38 44	-32 36.6	0.429	140.5	-3	dM4.5e	11.0 *				122.8	6.1	122.8	6.1	11.4 *	-8	-12	-9		
GJ 1257	20 38 45	-22 29.4	0.833	130.6	-60.3	K5 V	9.70	1.11	0.87	0.54	49.4	3.9	49.4	3.9	8.17	-72	-63	-28	196998	CD-22 14919
GJ 2149	20 39 36	-68 16.0	0.247	138.0		DA3	13.4 :	+0.1 :	-0.80				39.0	09. w	11.4 :					
Gl 799.1	20 39 41	-20 15.3	0.347	105.0		DA3	12.38	-0.08	-0.83		41.8	4.6	41.8	4.6	10.49					
Gl 800 A	20 40 04	-19 05.2	1.100	144.0	5	dM2	10.84	+1.43 J	+1.0 :J	+0.85 J	67.2	7.2	67.2	7.2	9.98	-8	-52	-57		BD-19 5899

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 800 B	20 40 04	-19 05.2	1.100	144.0			14.0 *				67.2	7.2	67.2	7.2	13.1 *					
NN	20 40 12	+57 14.5	0.291	18.0	-24	K7	10.29	1.36	+1.26:	0.60	44.9	11.2	42.0	08. r	8.41	-29	-28	7		BD+56 2471
NN	20 40 14	-29 36.1	0.206	190.5	-19.8	G5 V	6.95	0.67		0.24			43.0	06. r	5.12	-10	-26	11	197214	CD-29 17282
NN	20 40 23	-52 06.1	0.169	109.0	-1.6	A7 III-IV	4.51	0.27	0.09		47.3	11.5	47.3	11.5	2.9	-12	-4	-11	197157	CP-52 11752
NN	20 41 06	-00 21.8	0.448	54.0		K0	11.47	1.48	1.24				50.0	24. r	10					
Gl 802	20 41 53	+55 08.8	1.915	27.6	-23	dM5 e	14.68	1.79		+1.53:	63.3	5.4	63.3	5.4	13.69	-140	-32	22		
Gl 803	20 42 04	-31 31.1	0.441	142.1	-7.1	M0 Ve	8.81	1.42	0.95	0.85	106.9	5.3	106.9	5.3	8.95	-12	-15	-8	197481	CD-31 17815
NN A	20 42 05	+08 43.0	0.253	50.0		k-m	11.27			0.84			52.0	07. r	9.85					
NN B	20 42 04	+08 43.2	0.253	50.0		m	12.54			1.15			52.0	07. r	11.12					
Gl 804	20 42 06	+19 34.5	0.560	177.7	3	dM1.5e	10.31	1.45	1.15	0.75	48.8	4.7	48.8	4.7	8.75	36	-23	-34	352860	BD+19 4499
NN	20 42 44	-29 38.1	0.546	218.0		m	13.4 *			1.17			48.0	09. r	11.8 *					
Gl 805	20 43 08	-25 27.1	0.162	197.7	25.8	F5 V	4.13	0.43	0.02	0.14	73.5	18.8	77.0	12. r	3.56	23	-2	-15	197692	CD-25 15018
Gl 806	20 43 18	+44 18.7	0.506	56.7	-24.4	dM3	10.77	1.53	1.19	0.93	85.4	1.4	85.4	1.4	10.43	-29	-21	-9		
Wo 9706	20 44 07	+57 24.0	0.243	196.4	-32.4	F8 IV-V	4.51	0.54	0.10		43.8	7.6	43.8	7.6	2.72	27	-28	-15	198084	BD+57 2240
Gl 806.1A	20 44 11	+33 46.9	0.484	47.2	-10.9	SB K0- III	2.45	1.03	0.87		52.0	8.9	52.0	8.9	1.03	-45	-1	-6	197989	BD+33 4018
Gl 806.1B	20 44 05	+33 46.8	0.480	47.5		M4	13.40	1.66		1.11	52.0	8.9	52.0	8.9	11.98					
Gl 807	20 44 16	+61 38.6	0.826	6.3	-86.8	K0 IVe	3.43	0.92	0.62	0.33	76.1	6.3	76.1	6.3	2.84	-31	-96	9	198149	BD+61 2050
Gl 808	20 44 30	-79 29.0	1.216	144.6	35	M2.5	11.85	1.50	1.03	0.95	64.3	10.1	64.3	10.1	10.89	-49	-75	-34		
Gl 808.1	20 45 06	-44 10.3	0.211	119.3	-14.9	F1 IV	5.10	0.35	0.05	+0.20C	49.4	8.5	49.4	8.5	3.57	-23	-8	-5	197937	CD-44 14145
NN	20 46 37	+19 32.1	0.249	220.0		m	13.38	1.54		1.19			50.0	10. r	11.87					
NN	20 47 04	-00 32.2	0.395	123.6		M3.5	13.06	1.53		1.13			48.0	12. r	11.5					
NN	20 47 10	+37 16.9	0.229	48.0	71	DA4	12.93	0.14	-0.67				55.0	06. w	11.63	-14	29	-5		
Gl 808.2	20 48 04	+29 11.9	0.041	149.1	-8.3	K5 V	8.41	1.06	0.93				53.0	08. r	7.03	-1	-9	-2	198550	BD+28 3900
NN	20 48 13	+26 19.6	0.523	232.9		DC9	15.58	0.95	0.40		50.0	3.4	50.0	3.4	14.07					
NN	20 49 02	+52 42.4	0.536	32.2		K5	9.74	1.32		0.56	32.7	18.8	47.0	09. r	8.1					BD+52 2815
NN	20 49 59	+26 54.5	0.095	231.8	+1.0	SB G7 III CN	4.58	0.83	0.47		40.3	19.7	40.3	19.7	2.6	11	-2	2	198809	BD+26 4017
NN	20 51 10	+10 26.0	0.665	226.2		m	13.97	1.73		1.32	72.2	2.9	72.2	2.9	13.26					
NN	20 51 32	+68 58.7	0.232	77.0		M3	11.70	1.54		0.86			43.0	07. r	9.87					
Gl 809	20 52 18	+61 58.5	0.772	180.5	-17.0	SB M2 Ve	8.55	1.48	1.24	0.82	133.5	2.6	133.5	2.6	9.18	23	-10	-20	199305	BD+61 2068
GJ 1259	20 52 42	+12 58.8	0.676	55.2	-40	K3 V	8.81	1.05	1.05	0.42	43.5	10.2	43.0	06. r	6.98	-84	-5	-10		BD+12 4499
Gl 810 A	20 52 48	-14 13.2	1.486	107.5		M3.5 J	12.45	1.59		1.26	78.9	7.8	78.9	7.8	11.94					
Gl 810 B	20 52 47	-14 15.0	1.486	107.5			14.55	1.72		1.42	78.9	7.8	78.9	7.8	14.04					
Gl 811	20 53 49	-26 29.3	0.115	121.1	-16.1	F8 V	5.70	0.50	-0.04	0.17	38.0	6.0	45.0	05. r	3.97	-18	-10	1	199260	CD-26 15344
Gl 811.1	20 54 04	-10 37.6	1.155	182.8	51	dM4	11.47	1.51	1.07	1.04	56.3	5.7	56.3	5.7	10.22	73	-57	-60		
Gl 812 A	20 54 07	-05 02.2	0.816	106.1	-44.5	M3	11.91	1.51	1.06	1.14	63.5	4.4	63.5	4.4	10.92	-59	-37	-29		
Gl 812 B	20 54 06	-05 02.0	0.816	106.1		DC9+	16.60	1.16	0.64	0.45	63.5	4.4	63.5	4.4	15.61					
Gl 812.1	20 54 22	-44 18.5	1.101	207.9	-9.6	G0 V	6.53	0.58	-0.02	0.21	53.0	9.0	50.0	05. s	5.02	19	-94	43	199288	CD-44 14214
NN	20 55 03	+42 44.2	0.016	208.8		A2	9.0 *				42.4	22.2	42.4	22.2	7.1 *					BD+42 3917
Gl 813	20 55 09	+22 10.4	0.779	103.0	-31.1	M3	12.01	1.61	1.22	0.99	76.2	5.6	76.2	5.6	11.42	-35	-31	-34		
NN	20 56 23	-33 48.6	0.183	146.9		K0 V	7.35	0.84	0.49				52.0	08. r	5.93				199620	CD-34 14779
NN	20 56 40	+34 04.8	0.329	116.0		M2	11.06	1.46		0.75			42.0	07. r	9.18					
NN	20 57 17	+37 44.1	0.018	147.7		K5	8.00	1.67	2.03		44.3	13.0	44.3	13.0	6.2				199957	BD+37 4131

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Wo 9713	20 57 35	-42 13.4	0.417	87.0		K4	12.3 *				43.5	13.6	43.5	13.6	10.5 *					
Gl 815 A	20 58 09	+39 52.7	0.668	114.6	-33.7 SB	dM3 eJ	10.34	+1.52 J	+1.07 J	+0.92 J	66.1	4.5	66.1	4.5	9.44	-18	-35	-43		
Gl 815 B	20 58 09	+39 52.7	0.668	114.6			11.9 *				66.1	4.5	66.1	4.5	11.0 *					
Wo 9714	20 58 35	-32 43.2	0.200	:114.		K5 V	9.40	1.24	1.21	0.54	26.1	17.0	48.0	08. r	7.81				199981	CD-33 15343
NN	20 59 10	+20 32.1	0.538	223.8		m	14.1 *			1.21			40.0	08. r	12.1 *					
NN A	20 59 13	+33 02.8	0.356	113.0		m	12.29			1.08			59.0	08. r	11.14					
NN B	20 59 17	+33 02.7	0.356	113.0		m	13.12			1.19			59.0	08. r	11.97					
Gl 816	20 59 20	-06 30.6	0.515	201.9		M2.5	11.23	1.49		1.04	80.3	8.5	80.3	8.5	10.75					
Wo 9716	20 59 30	-57 09.3	0.499	317.3		M4	12.85	1.65	1.36	+1.17t	44.5	17.0	64.0	14. r	11.88					
NN	20 59 43	-50 34.4	0.500	141.6		m	13.1 *			1.18			57.0	11. r	11.9 *					
Gl 816.1A	21 00 53	+45 41.1	0.422	69.5	-13.6	K25 V	7.68	0.97	0.78		45.8	4.8	45.8	4.8	5.98	-39	-12	-20	200560	BD+45 3371
Gl 816.1B	21 00 53	+45 41.1	0.422	69.5			13.0 *				45.8	4.8	45.8	4.8	11.3 *					
Gl 816.2A	21 01 34	-20 03.2	0.050	225.2	23.8	A5 V	5.10	+0.17 J	+0.08 J	+0.10CJ	53.5	12.6	53.5	12.6	3.7	19	6	-13	200499	BD-20 6115
Gl 816.2B	21 01 34	-20 03.2	0.050	225.2			6.5 *				53.5	12.6	53.5	12.6	5.1 *					
Gl 817	21 02 09	-17 07.8	2.251	206.3	-47	M2	11.46	1.47	1.08	0.84	57.5	7.8	57.5	7.8	10.26	72	-173	40		
Gl 818	21 02 51	+06 52.6	0.572	172.5	-65.7	K6 V	8.30	1.22	1.16	0.50	58.6	8.3	58.6	8.3	7.14	-12	-79	0	200779	BD+06 4741
NN	21 02 56	-17 06.8				K7	10.33	1.42	1.17	0.66			47.0	07. r	8.69					BD-17 6172
NN	21 03 26	+04 13.8	0.217	140.0		m	12.18	1.49	1.14	1.03	43.1	4.2	43.1	4.2	10.35					
Gl 818.1A	21 04 11	-73 22.3	0.550	127.6	-10.1	G3 IV J	6.4 *	+0.59 J	+0.10 J	+0.22 J	41.7	14.1	41.7	14.1	4.5 *	-55	-26	-18	200525	CP-73 2192
Gl 818.1B	21 04 11	-73 22.3	0.550	127.6			6.4 *				41.7	14.1	41.7	14.1	4.5 *					
Gl 818.1C	21 04 11	-73 22.3	0.550	127.6			13.5 *				41.7	14.1	41.7	14.1	11.6 *					
Gl 819 A	21 04 24	-14 07.4	0.392	93.9	-34	K1 Ve	7.15	+0.90 J	+0.58 J	+0.32 J	68.1	11.2	68.1	11.2	6.32	-40	-17	-1	200968	BD-14 5936
Gl 819 B	21 04 24	-14 07.4	0.392	93.9		M0	10.2 *				68.1	11.2	68.1	11.2	9.4 *					
Gl 820 A	21 04 40	+38 30.0	5.220	52.4	-64.8	K5 Ve	5.21	1.18	1.11	0.47	288.7	1.9	288.7	1.9	7.51	-92	-54	-9	201091	BD+38 4343
Gl 820 B	21 04 40	+38 30.0	5.220	52.4	-64.3	K7 Ve	6.03	1.37	1.23	0.60	288.7	1.9	288.7	1.9	8.33	-92	-54	-9	201092	BD+38 4344
Gl 820.1	21 05 12	-82 01.	0.370	167.0	-57	DA6	13.56	0.25	-0.60		57.9	6.3	57.9	6.3	12.37	-75	44	61		
Wo 9720	21 05 42	-21 23.7	0.061	160.1	-12	A0 V	5.30	0.00	-0.03		44.7	11.9	44.7	11.9	3.6	-8	-10	4	201184	BD-21 5933
NN	21 05 49	+24 58.5	0.157	187.6	-4.1	dK8	9.88	1.16	1.05	0.46	41.7	7.7	32.0	04. r	7.41	16	-13	-11		BD+24 4329
Wo 9721 A	21 06 08	-04 37.8	0.058	281.0	11	dM2	9.44	1.13	1.00	0.50	44.6	7.6	44.6	7.6	7.69	10	8	-1		BD- 5 5480
Wo 9721 B	21 06 08	-04 37.8	0.058	281.0			13.40	1.63		1.11	44.6	7.6	44.6	7.6	11.65					
Gl 821	21 06 30	-13 28.7	2.096	160.1	-61	M3	10.87	1.50	1.10	0.86	91.7	10.3	91.7	10.3	10.68	-30	-118	-24		
Wo 9722	21 06 44	+59 32.1	2.098	208.7	-260.0 SB	sdM1	13.30	1.55			41.7	2.6	41.7	2.6	11.4	264	-215	-92		
Wo 9723	21 07 01	+46 57.3	0.497	119.6		K3	10.78	0.95	0.70		39.7	20.5	39.7	20.5	8.8					
Wo 9724	21 08 29	-43 48.0	0.713	163.6		M1	12.01	1.56		0.96	42.4	8.2	42.4	8.2	10.15					CD-44 14334
Wo 9725	21 08 34	+80 35.3	0.310	62.0		K5	10.84	1.26	1.27	+0.57t	40.4	13.6	28.0	05. r	8.08					
NN	21 08 47	+29 13.3	0.361	220.0		M1	11.05	1.34	1.22	0.87			53.0	11. r	9.67					
Wo 9726	21 09 01	-40 28.3	0.228	163.1	6.3	F7 V	5.83	0.45	0.01		40.6	6.9	36.0	04. r	3.61	-1	-29	-11	201647	CD-40 14216
NN	21 09 24	+45 15.3	0.399	220.1		K2	7.83	0.78	0.42		29.6	8.8	39.0	07. r	5.79				201924	BD+44 3728
GJ 2152	21 11 00	+07 13.7	0.363	70.0		f	16.17	0.45	-0.36		41.6	5.6	41.6	5.6	14.27					
Gl 822 A	21 12 03	+09 48.2	0.307	175.3	-15.8 SB	F7 V	5.11	+0.50 J	-0.01 J	+0.18tJ	53.3	5.3	53.3	5.3	3.74	7	-29	-10	202275	BD+09 4746
Gl 822 B	21 12 03	+09 48.2	0.307	175.3		F7 V	5.4 *				53.3	5.3	53.3	5.3	4.0 *					
Gl 822.1A	21 12 48	+37 49.9	0.465	20.0	-23.1 VAR	F0 IV	3.82	0.38	0.03	+0.14 J	51.4	4.1	51.4	4.1	2.37	-42	-16	20	202444	BD+37 4240

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 822.1B	21 12 48	+37 49.9	0.465	20.0		G0 V	6.42	0.60	0.09		51.4	4.1	51.4	4.1	4.97					
Gl 822.1C	21 12 47	+37 48.4	0.463	19.8		M3	12.00	1.53	1.14	1.04	51.4	4.1	51.4	4.1	10.55					
NN	21 13 00	+25 35.4	0.314	147.0		m	12.13			1.06			59.0	12. r	10.98					
Gl 822.2	21 13 45	+25 13.5	0.077	242.0	-26.6	G5 V	6.99	0.89	0.49	0.36			69.0	15. r	6.18	-2	-25	9	202573	BD+24 4357
NN A	21 13 56	+29 39.3	0.217	77.0		m	12.68			1.22			65.0	09. r	11.74					
NN B	21 13 54	+29 39.2	0.217	77.0		m	13.49			1.23			65.0	09. r	12.55					
Gl 824	21 14 05	+09 11.1	0.184	130.2	-18.3	dK8	7.95	1.02	0.84	0.40	68.4	10.9	61.0	07. r	6.88	-11	-20	-5	202575	BD+08 4638
Gl 825	21 14 20	-39 03.7	3.453	250.8	28.2	M0 Ve	6.67	1.41	1.21	0.69	258.6	10.4	258.6	10.4	8.73	63	-19	23	202560	CD-39 14192
Gl 825.1	21 14 47	-61 33.4	0.659	133.6	-19.6	G5 V	6.60	0.68	0.25	0.24	46.6	8.4	46.6	8.4	4.94	-58	-38	-11	202457	CP-61 6537
NN A	21 14 55	-09 06.7				M1	12.11	1.52	1.19	1.02			42.0	06. r	10.23					
NN B	21 14 58	-09 07.4					13.33			1.08			42.0	06. r	11.45					
NN A	21 15 05	+20 41.0	0.420	47.0		M3	12.47			+1.09 J			49.0	09. r	10.92					
NN B	21 15 05	+20 41.0	0.420	47.0		M4	14. *						49.0	09. r	12. *					
Gl 825.2	21 15 11	-43 32.7	0.246	86.0	10.7	G5 V	6.75	0.63	0.14	+0.33C	45.9	10.2	43.0	08. r	4.92	-11	1	-27	202628	CD-43 14464
Gl 825.3	21 15 28	-00 02.8	0.496	111.4	-26.9	dK6	8.22	0.98	0.83	0.40	47.5	5.0	47.5	5.0	6.6	-38	-32	-27	202751	BD-00 4195
NN	21 15 48	-56 03.0	0.450	114.0		DA6	14.28	0.26	-0.59				45.0	05. w	12.55					
Wo 9732	21 15 54	-67 51.9	0.411	284.8		m	10.90	1.45		+0.83t	49.1	23.9	55.0	10. r	9.6					
Wo 9733 A	21 16 19	-53 39.6	0.114	123.1	-14.5	A5 V	4.50	+0.19 J	+0.12 J		41.9	11.9	41.9	11.9	2.6	-19	-4	3	202730	CP-53 10037
Wo 9733 B	21 16 18	-53 39.6	0.121	127.0	-7.2	A7 V	6.9 *				41.9	11.9	41.9	11.9	5.0 *	-14	-7	-2		
Gl 825.4A	21 16 52	-26 33.6	0.643	236.8	-17.2	SB G5 V	6.63	+0.73 J	+0.23 J	+0.29 J	56.5	6.5	56.5	6.5	5.39	26	-32	39	202940	CD-26 15541
Gl 825.4B	21 16 52	-26 33.6	0.643	236.8	-21.2	dG6	9.6 *				56.5	6.5	56.5	6.5	8.4 *	23	-33	41		
Gl 826	21 17 23	+62 22.4	0.158	70.5	-11.5	A7 IV-V	2.44	0.22	0.11	0.02	67.0	8.0	67.0	8.0	1.57	-8	-12	-7	203280	BD+61 2111
GJ 1261	21 17 23	+53 59.8	0.240	333.0		DA	12.33	0.07	-0.67		50.9	6.2	50.9	6.2	10.86					
Wo 9735	21 17 23	-51 15.4	0.240	126.0	22.2	G5	10.64	0.81	0.36	+0.42C	44.1	10.2	44.1	10.2	8.9	-1	-19	-28		CD-51 12903
Gl 826.1	21 17 25	-20 03.3	0.744	193.6	15.6	K5 V	9.12	1.35	1.26	0.61	47.6	7.1	47.6	7.1	7.51	42	-61	-16	203040	BD-20 6185
GJ 1262	21 20 19	-68 26.7	0.221	43.2	11.5	G5 V	6.97	0.73	+1.79c				48.0	06. r	5.38	1	9	-23	203244	CD-68 2223
Gl 826.2	21 20 52	-46 55.2	0.738	96.7		M2	12.46	1.56		0.96	52.6	13.6	38.0	08. r	10.36					
NN	21 21 52	+08 17.3	0.257	228.0		m	13.64			1.15			40.0	08. r	11.65					
Gl 827	21 22 20	-65 35.6	0.805	6.7	-29.4	F8 V	4.22	0.49	-0.12	0.20	115.5	13.1	115.5	13.1	4.53	-13	42	6	203608	CP-65 3918
NN	21 23 00	-42 39.	0.087	340.0		M7	12.67	1.53		+1.09t			49.0	11. r	11.12					
Gl 827.1	21 23 18	-56 20.7	0.693	79.0	-40.5	K3 V	8.66	0.92	0.62	0.36	43.1	10.9	36.0	06. r	6.44	-89	24	-38	203850	CP-56 9645
Gl 828 A	21 23 45	-45 01.7	0.314	55.7	8.2	K0 V	7.48	0.91	0.71	+0.42C	67.0	10.2	67.0	10.2	6.61	-7	11	-19	203985	CP-45 10150
Gl 828 B	21 23 36	-45 01.	0.310	54.0		m	14.1 P				67.0	10.2	67.0	10.2	13.2 P					
Gl 828.1	21 24 11	+03 31.2	0.090	229.0	-4.7	dM1	10.52:	+1.38:	+1.2 :	0.67	52.6	10.1	52.6	10.1	9.12:	5	-7	4		
Gl 828.2	21 24 38	-07 03.4	0.411	180.0		M0	11.10	1.55	1.17	0.78	53.6	10.2	53.6	10.2	9.75					
NN	21 24 40	+70 15.6	0.034	35.2		G5	7.28						41.0	05. o	5.34				204521	BD+69 1169
NN	21 25 19	+07 05.4	0.653	199.2		M0.5	11.60	1.56	1.22	0.85	40.3	5.9	40.3	5.9	9.63					
NN	21 25 28	+33 48.5	0.322	233.0		m	11.15			0.82			47.0	08. r	9.51					
NN	21 25 28	-22 31.4	0.312	219.0		M4	12.21	1.56		1.03			53.0	10. r	10.83					
Gl 828.4	21 25 45	+10 23.5	0.119	78.4	-14.1	K2	8.73	0.86	0.60		50.7	11.9	30.0	05. r	6.12	-21	-10	-4	204417	BD+09 4821
Gl 828.5	21 26 43	+73 25.9	0.300	170.0	8	DA4	12.80	0.02	-0.66		48.8	2.2	48.8	2.2	11.24	26	-21	-33		
Gl 829	21 27 12	+17 25.1	1.058	69.8	-24.9	dM4 e	10.30	1.63	1.28	1.15	147.8	2.6	147.8	2.6	11.15	-38	-17	-5		

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 830	21 27 16	-12 43.6	1.059	104.5	-84.1	M0 V	9.10	1.28	1.24	0.55	63.6	9.2	63.6	9.2	8.12	-97	-62	-4	204587	BD-13 5945
NN	21 27 36	-40 55.4	1.730	143.7		M3	13.19	1.62	1.12	1.25			62.0	15. r	12.2					
Gl 831 A	21 28 34	-10 00.6	1.194	90.8	-56.7	dM4.5e	12.05	+1.67 J	+1.18 J	+1.33 J	125.6	4.5	125.6	4.5	12.54	-64	-33	5		
Gl 831 B	21 28 34	-10 00.6	1.194	90.8			14.9 *				125.6	4.5	125.6	4.5	15.4 *					
NN	21 28 45	+23 07.0	0.205	140.8	-23	dK8	9.25	1.05	0.80	0.50	40.7	6.2	40.7	6.2	7.3	-5	-29	-14		BD+22 4409
NN	21 28 54	-09 57.9	0.171	225.5		G0	7.41						58.0	06. o	6.23				204848	BD-10 5696
NN	21 30 06	+24 20.4	0.233	95.0		m	12.66			1.22			81.0	15. r	12.2					
Gl 832	21 30 14	-49 13.2	0.828	184.8	4.1	M1 V	8.67	1.47	1.05	0.93	215.0	6.1	215.0	6.1	10.33	3	-18	1	204961	CP-49 11439
NN	21 31 10	-07 04.2	0.519	167.7		M3.5	14.01	1.58		1.33			60.0	16. r	12.9					
NN A	21 31 16	+01 34.3	0.669	180.5		dM	13.35	1.68		1.22	68.6	8.0	68.6	8.0	12.53					
NN B	21 31 16	+01 34.3	0.669	180.5		m	14.5 *			1.29	68.6	8.0	68.6	8.0	13.7 *					
NN	21 33 05	+51 18.4	0.587	59.7		M3.5	11.78	1.46		1.06			70.0	17. r	11					
Gl 833	21 33 17	-51 04.1	0.473	115.0	28.1	K2 V	7.14	0.88	0.57	0.30	76.6	11.1	76.6	11.1	6.56	-2	-19	-36	205390	CD-51 12998
NN	21 34 00	-63 57.0	0.157	261.0		M2	10.62	1.44		+0.85t			65.0	13. r	9.68					
Gl 834 A	21 34 38	+39 14.0	0.263	233.0		dM0	10.34	+1.42 J	+1.1 :J	+0.77 J	49.8	4.2	49.8	4.2	8.83					
Gl 834 B	21 34 38	+39 14.0	0.263	233.0			12.3 *				49.8	4.2	49.8	4.2	10.8 *					
NN	21 35 38	-33 52.8	1.190	116.5		M2	12.57	1.62	1.33	1.18			57.0	21. r	11.3					
Gl 835	21 35 45	+27 29.9	0.430	93.0	-13.3	M0 e	9.88	1.50	1.26	0.81	80.8	2.6	80.8	2.6	9.42	-20	-15	-13		BD+27 4120
Gl 835.1	21 36 00	-77 36.8	0.243	167.5	+34.4 SB	K0 III	3.75	1.00	0.89	+0.46C	51.5	10.2	51.5	10.2	2.31	9	-38	-13	205478	CP-77 1510
NN	21 36 06	+52 51.3	0.296	70.0		M0	10.60	1.41		0.70			47.0	09. r	8.96					BD+52 2996
Gl 836	21 36 06	-24 22.5	1.208	124.4	36	M3.5	13.43	1.56	1.04	1.24	71.7	11.2	71.7	11.2	12.71	-16	-37	-78		
Gl 836.1	21 36 15	-27 31.9	0.397	101.2	-17.6	G4 IV-V	6.73	0.62	0.16	+0.32C	45.4	7.8	45.4	7.8	5.02	-40	-15	-15	205905	CD-27 15550
NN	21 37 19	-16 53.4	0.189	96.5	-31.2 SB	F0 p	3.68	0.32	0.20		28.2	7.4	28.2	7.4	0.9	-40	-19	0	206088	BD-17 6340
NN	21 37 40	+27 23.3	0.350	130.0		M3:	11.62			0.94			53.0	10. r	10.24					
NN	21 38 41	-01 00.2	0.262	81.0		m	12.57	1.56	1.19				52.0	24. r	11.2					
Wo 9747	21 38 47	+53 46.6	0.414	75.4		M3.5	14.1 *				42.9	13.6	42.9	13.6	12.3 *					
Gl 836.3	21 39 02	-41 21.0	0.353	145.6	57.8	K5 V	8.82	1.04	0.90	0.42	51.1	13.6	45.0	07. r	7.09	24	-32	-56	206276	CP-41 9682
Gl 836.4	21 39 25	-12 23.0	0.695	173.7		M1.5:	12.80	1.48		1.07	32.0	4.9	32.0	4.9	10.33					
NN	21 39 46	+27 27.6	0.307	259.0		m	13.97			1.21			43.0	08. r	12.14					
Gl 836.5	21 40 22	+20 46.7	0.677	200.0		DQ6	13.24	0.17	-0.71		79.6	8.0	79.6	8.0	12.74					
NN	21 41 45	+06 24.8	0.350	245.0		dM3	12.07	1.53	1.21				53.0	25. r	10.7					
NN A	21 41 46	+16 49.7	0.259	90.0		m	13.65			1.25			57.0	06. r	12.43					
NN B	21 41 45	+16 50.8	0.259	90.0		m	14.81			1.38			57.0	06. r	13.59					
Gl 836.6A	21 41 54	+28 31.0	0.376	129.3	+15.8 SB?	F4 V	4.78	+0.48 J	+0.01 J	+0.18tJ	43.2	5.3	43.2	5.3	2.96	-5	3	-44	206826	BD+28 4169
Gl 836.6B	21 41 54	+28 31.0	0.315	133.0	+23.5 SB?	G2 V	6.09*				43.2	5.3	43.2	5.3	4.27*	-1	12	-40	206827	
Gl 836.7	21 42 07	+14 32.6	0.261	116.5	-17	G0 V	5.94	0.59	0.04		66.1	10.2	66.1	10.2	5.04	-13	-20	-8	206860	BD+14 4668
NN	21 42 24	-06 00.7	0.438	204.0		M3.5	12.81	1.64	1.30		33.5	20.5	66.0	23. r	11.9					
Gl 836.8	21 42 30	+41 22.0	0.080	320.0	9.5	dK6	9.63	1.34	1.20	0.59	52.3	5.4	52.3	5.4	8.22	0	11	6		BD+40 4631
NN	21 42 48	-06 07.7	0.360	205.0		M3.5	13.54	1.65	1.01				49.0	17. r	12					
Gl 836.9A	21 43 02	-57 55.3	0.906	174.6	-7	K7 V	9.47	+1.32 J	+1.15 J	+0.59 J	52.1	8.5	52.1	8.5	8.05	-20	-77	22	206804	CP-58 7893
Gl 836.9B	21 43 02	-57 55.3	0.906	174.6		K7 V	9.6 *				52.1	8.5	52.1	8.5	8.2 *					
NN	21 43 24	+20 33.0	0.248	97.0		m	14.39	1.68		1.28			47.0	08. r	12.75					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
GJ 1263	21 44 04	-00 24.0	0.919	124.2	39	M3.5	12.65	1.61	1.27	1.22	81.8	5.5	81.8	5.5	12.21	-2	-1	-66		
Gl 837	21 44 17	-16 21.3	0.394	138.5	-6.3 SB	A6 m	2.87	0.29	0.09	+0.16C	68.1	16.0	68.1	16.0	2	-10	-23	-13	207098	BD-16 5943
GJ 1264	21 44 34	-72 19.9	0.464	132.0		M2 Ve	9.80	1.46	1.16	0.86			98.0	23. r	9.8					CD-72 1700
Wo 9754	21 44 55	-40 29.0	0.372	162.7	-6.8	K3 V	8.62	0.97	0.77	0.36	41.9	8.8	39.0	06. r	6.58	-11	-44	-1	207144	CD-40 14498
NN	21 45 00	+46 24.2	0.295	89.1		M3.5	13.36			1.23			59.0	11. r	12.21					
Gl 838	21 45 01	-47 31.9	0.337	150.6	-6.5	G2 V	5.58	0.60	0.08	0.20	71.8	6.5	71.8	6.5	4.86	-12	-20	1	207129	CD-47 13928
NN	21 45 26	+05 35.7	0.420	130.0		M1.5	11.79	1.43	1.15	0.86			40.0	08. r	9.8					
NN	21 45 37	+01 12.8	0.232	94.0		m	13.87			1.19			41.0	08. r	11.93					
NN	21 45 44	-63 21.3	0.545	32.8		m+	12.5 *			1.08			53.0	11. r	11.1 *					
NN	21 45 58	+50 00.3	0.823	57.6		M4	13.0 *				46.0	6.8	46.0	6.8	11.3 *					
NN A	21 46 00	-41 46.0	0.342	121.0		M6	12.2 *	+1.59 J		+1.10tJ			66.0	15. r	11.3 *					
NN	21 46 02	+27 42.3	0.708	196.2		m	11.99	1.62	1.21	0.95	54.2	5.1	54.2	5.1	10.66					
Gl 838.1A	21 46 40	+05 29.4	0.550	92.4	-10.3	K3 V	8.65	1.04	0.92	0.39	48.0	7.8	41.0	3.5	6.71	-51	-16	-36	207491	BD+05 4874
Gl 838.1B	21 47 04	+05 25.0	0.504	90.7		m	14.90	1.75	+1.19?	1.28	39.2	3.9	41.0	3.5	12.96					
Wo 9757	21 47 06	-11 54.9	0.425	230.0	37	K5	10.83	1.41	1.25		39.0	6.8	39.0	6.8	8.79	62	-6	-12		
NN	21 48 25	-10 16.4	0.054	76.7		G0	7.50						60.0	07. o	6.39				207687	BD-10 5774
Wo 9758	21 48 40	+74 45.9	0.173	39.4	20.7	K0	8.99	0.86	0.53		41.3	9.0	26.0	03. r	6.06	-36	6	11	208002	BD+74 938
NN	21 48 49	+12 36.4	0.653	73.1		m	13.42	1.50	1.10	1.17	38.1	3.6	38.1	3.6	11.32					
Gl 838.2	21 49 05	+00 36.9	0.348	100.6	-29.1	K1	8.60	0.83	0.51	+0.40C	49.2	14.0	30.0	05. r	5.99	-49	-33	-21	207795	BD+00 4788
NN	21 49 23	+13 22.3	0.224	123.0		m	13.93			1.32			68.0	11. r	13.09					
NN A	21 49 35	-77 34.3	0.288	129.0	-10.6	K3/4 V	8.24	1.00	0.89		34.7	11.9	49.0	08. r	6.69	-28	-10	2	207496	CP-77 1522
NN B	21 49 35	-77 34.3	0.288	129.0			10.5 *				34.7	11.9	49.0	08. r	9.0 *					
NN	21 49 40	+05 23.5	0.171	131.0		dM2	12.11	1.53	1.09	1.09			64.0	13. r	11.14					
Gl 838.3A	21 49 52	+42 06.8	0.343	208.5	-25.6	G8	7.86	0.78	0.32		46.1	8.5	36.0	04. r	5.64	42	-27	-13	207966	BD+41 4291
Gl 838.3B	21 49 52	+42 06.8	0.343	208.5		M1	11.45	1.43		0.73	46.1	8.5	36.0	04. r	9.23					
Gl 838.4	21 49 53	+02 09.4	0.331	178.0		DA3	12.75	0.01	-0.77		40.4	2.5	40.4	2.5	10.78					
NN	21 49 55	+27 11.5	0.806	159.4		m	14.06			1.20			39.0	07. r	12.02					
NN	21 50 14	+39 34.0	0.442	90.5	-51.7	K2	8.23	0.73	0.28		39.3	13.6	29.0	05. r	5.54	-56	-59	-36	207992	BD+39 4694
NN	21 50 16	+28 33.5	0.079	223.0	+19.0 VAR	F5 VI-V	5.53	0.42	-0.13		39.2	6.8	37.0	05. r	3.37	12	16	-7	207978	BD+28 4215
Gl 838.5	21 50 34	-13 47.3	0.311	87.4	-21.5	F1 III	5.08	0.37	-0.05	+0.22C	45.7	10.2	45.7	10.2	3.38	-37	-12	-4	207958	BD-14 6149
NN	21 51 06	-43 50.3	0.607	89.2			15.35			1.36			41.0	06. r	13.41					
NN	21 51 32	-01 31.2	0.260	177.0	113	DA6	14.41	0.26	-0.51				51.0	06. w	12.95	39	25	-55		
Gl 838.6	21 51 37	-47 14.1	0.497	219.6	59	M1	11.98	1.56	1.17	0.97	88.7	17.0	88.7	17.0	11.72	51	-24	-32		
Gl 839	21 51 55	+41 32.8	0.533	133.4	-48	dM1	10.35	1.36	1.20	0.66	45.5	11.4	46.0	09. r	8.66	-6	-57	-45		
Gl 840	21 52 32	+32 05.7	0.310	136.2	-13.8	dK0 e	7.78	0.92	0.64		41.8	11.7	49.0	08. r	6.23	-4	-22	-25	208313	BD+31 4574
NN A	21 53 27	+32 48.0	0.010	315.0			10.0 *				49.6	6.9	49.6	6.9	8.5 *					BD+32 4292
NN B	21 53 27	+32 48.0	0.010	315.0			10.2 *				49.6	6.9	49.6	6.9	8.7 *					
Gl 841 A	21 53 35	-51 14.4	0.390	189.0	-9	M0	10.4 :	+1.5 :	+0.9 :	+1.31C	68.4	9.4	68.4	9.4	9.6 :	-3	-24	15		CD-51 13128
Gl 841 B	21 53 35	-51 14.4	0.390	189.0		DQ7	14.68	0.16	-0.80		68.4	9.4	68.4	9.4	13.86					
NN	21 54 16	-02 08.9	1.426	64.2		dM5	14.64	1.76		1.42	75.0	3.2	75.0	3.2	14.02					
NN	21 54 17	+19 32.3	0.477	194.3		M3.5	12.90	1.58		1.13			52.0	14. r	11.5					
NN	21 54 56	+07 53.8	0.382	76.4		M1	11.01	1.50	1.12	0.92	55.7	5.8	55.7	5.8	9.74					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN A	21 55 56	-32 42.3	0.536	226.8		m	14.65			1.25			42.0	05. r	12.77					
NN B	21 55 55	-32 40.5	0.536	226.8		m	15.8 *			1.50			42.0	05. r	13.9 *					
Gl 842	21 55 56	-59 59.4	0.886	96.1	13.4	M2	9.75	1.49	1.18	0.81	77.2	11.5	77.2	11.5	9.19	-35	-17	-41		CP-60 7528
NN	21 55 57	-61 10.3	0.102	181.7		K7	9.55	1.25		+0.51t			45.0	06. r	7.82					CD-61 6651
NN	21 55 58	-47 00.1				M4	11.80	1.47		+0.88t			42.0	08. r	9.92					CD-47 14002
Wo 9763	21 56 42	-04 19.6	0.446	175.4		M2 :	14.17	1.59	1.45		42.1	15.3	42.1	15.3	12.3					
NN	21 57 18	+41 37.4	0.395	162.0		m	12.76			1.06			44.0	09. r	10.98					
Gl 842.2	21 57 58	+75 20.9	0.226	84.0	-18.6	dM1	10.56	1.45		0.76	53.1	4.4	53.1	4.4	9.19	-10	-20	-16		
NN	21 58 56	+28 03.9	0.394	85.0		m+	12.01	1.63	1.08	1.26	112.0	2.1	112.0	2.1	12.26					
Gl 843	21 59 12	-19 43.5	0.928	85.1		M3	12.03	1.59	1.15	1.10	80.1	6.4	80.1	6.4	11.55					
Gl 844	21 59 24	+16 13.4	0.430	70.0	-14.8	M2 V	10.62	1.58	1.28	1.01	70.9	10.2	70.9	10.2	9.87	-30	-11	-3		
NN	21 59 27	-37 19.2	0.836	105.6		M3.5	11.80	1.65	1.36	1.17			100.0	25. r	11.8					
Gl 845	21 59 33	-56 59.6	4.700	122.9	-40.4	K5 Ve	4.69	1.06	0.99	0.40	288.9	6.1	288.9	6.1	6.99	-78	-38	4	209100	CP-57 10015
Gl 846	21 59 39	+01 09.7	0.532	241.0	18.5	M0.5 V	9.18	1.48	1.21	0.75	98.9	3.8	98.9	3.8	9.16	31	6	-4	209290	BD+00 4810
NN	21 59 52	-50 52.8	0.581	147.7		M4	12.09	1.57		0.96			47.0	09. r	10.45					
Gl 847 A	21 59 55	-70 09.9	0.632	97.2	-9.1	m	10.97	1.38		0.60	51.1	21.6	29.0	03. r	8.28	-89	-22	-49		
Gl 847 B	21 59 55	-70 09.9	0.632	97.2		m	13.70	1.61		1.02	51.1	21.6	29.0	03. r	11.01					
NN	22 01 00	+01 21.8	0.032	129.0			10.34	0.73	0.29		43.2	8.9	43.2	8.9	8.52					
NN	22 02 01	+67 15.6	0.568	121.0		m	13.41			1.15			44.0	09. r	11.63					
NN	22 02 34	+04 53.5	0.488	74.4		M3	13.60	1.51	0.98	1.20			41.0	10. r	11.7					
NN	22 02 53	-38 30.3	0.784	131.0		M3.5	12.45			1.02			49.0	09. r	10.9					
NN	22 03 13	-12 08.9	0.293	242.0		K7	10.15	1.45		0.72			57.0	12. r	8.93					BD-12 6174
NN	22 03 28	+78 02.1	0.265	75.0		m	15.87	1.80	1.64				40.0	15. r	13.9					
Gl 847.1	22 03 38	-45 38.0	0.477	123.6	-23.4	K2 V	8.43	0.85	0.55	0.30	46.8	19.7	33.0	05. r	6.02	-57	-44	-9	209742	CD-45 14576
NN	22 03 53	+39 03.7	0.471	173.4		m	12.69			1.05			44.0	09. r	10.91					
NN	22 04 13	+03 10.7	0.601	125.7		M4	13.60	1.60	1.35	1.22			53.0	12. r	12.22					
NN A	22 04 25	+65 23.9	0.393	308.0		M1.5	11.62	1.55		0.90			48.0	10. r	10.03					
Gl 848	22 04 41	+25 06.0	0.300	84.5	-5.5	SB F5 V	3.76	0.44	-0.04		79.9	6.0	79.9	6.0	3.27	-16	-7	-7	210027	BD+24 4533
Gl 848.1A	22 04 55	-51 27.7	0.360	112.0	-38	K7	10.51	1.21		+0.59C	47.4	11.9	27.0	03. r	7.67	-69	-25	1		CD-51 13182
Gl 848.1B	22 04 34	-51 21.7	0.360	112.0		m	12.51	1.51		+1.14C	47.4	11.9	27.0	03. r	9.67					
Gl 848.1C	22 04 33	-51 21.9	0.360	112.0		m	13.42	1.49		+1.29C	47.4	11.9	27.0	03. r	10.58					
Gl 848.2	22 05 05	-47 12.2	0.197	138.2	10.9	B5 V	1.74	-0.13	-0.47	-0.07C	39.8	10.0	39.8	10.0	-0.3	-5	-21	-15	209952	CD-47 14063
Gl 848.4	22 06 52	-07 47.3	0.455	169.5	-21.4	G8 IV	6.55	0.75	0.36	0.25	53.9	22.2	53.9	22.2	5.2	2	-45	-3	210277	BD-08 5818
Gl 849	22 07 00	-04 53.2	1.037	91.5	-14.8	dM3.5	10.37	1.51	1.13	1.10	114.4	3.7	114.4	3.7	10.66	-40	-17	-15		BD-05 5715
Gl 849.1	22 07 13	-32 47.7	0.431	88.0	-14.6	F6 V	4.92	0.48	0.01	+0.26C	52.3	16.2	59.0	07. r	3.77	-36	-7	-8	210302	CD-33 15941
NN	22 07 21	+14 14.8	0.351	46.0		DA6	15.66	0.23	-0.54		39.7	4.4	39.7	4.4	13.65					
NN	22 07 34	+40 47.1	0.452	59.3		k-m	12.57	1.49			44.4	3.3	44.4	3.3	10.81					
Wo 9771	22 07 41	+05 57.1	0.276	83.4	-7.9	A2 V	3.53	0.08	0.10		48.1	8.0	48.1	8.0	1.94	-26	-8	-9	210418	BD+05 4961
NN	22 07 56	+19 22.3	0.128	135.9	21.3	G0 V	6.18	0.69	0.17				58.0	09. r	5	2	13	-19	210460	BD+18 4946
NN	22 08 37	-02 47.4	0.408	101.0		k-m	12.14	1.56	1.25				63.0	29. r	11.1					
Gl 850	22 09 01	+36 00.8	0.249	173.6	-18.3	K0	7.24	0.79	0.46		49.9	10.2	51.0	07. r	5.78	12	-23	-14	210667	BD+35 4725
Gl 851	22 09 05	+18 10.6	0.383	58.9	-51.4	dM2 e	10.22	1.50	1.15	0.96	82.5	2.8	82.5	2.8	9.8	-31	-41	22		

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Wo 9773	22 10 06	+08 18.8	0.681	172.2		M3	12.00	1.56	1.22	1.04	42.5	13.8	61.0	15. r	10.9					
NN	22 10 48	-14 59.6	0.409	231.0		M3.5	13.34	1.51		1.12			41.0	10. r	11.4					
GJ 1265	22 10 56	-17 55.8	0.887	111.7	24	m	13.57	1.73	+1.48:	1.33	95.8	4.4	95.8	4.4	13.48	-16	-13	-46		
NN	22 11 16	+25 43.3	0.260	:136.		m	13.62			1.20			48.0	09. r	12.03					
NN	22 11 22	+05 01.7	0.246	105.0		dM2	11.79	1.49		0.87			41.0	07. r	9.85					
Gl 851.2	22 11 36	-41 37.2	0.981	144.0	-18.8	G5 V	6.23	0.65	0.14	0.22	42.1	8.5	55.0	09. r	4.93	-42	-76	-5	210918	CD-41 14804
Wo 9775	22 11 46	-08 59.1	0.608	188.9	-18	K2	11.85			0.37	51.3	22.9	51.3	22.9	10.4	23	-54	-1		
Gl 851.3	22 11 56	-16 03.7	0.354	180.7	11.9	G8 V	6.54	0.90	0.57	0.33	34.3	7.5	83.0	13. r	6.14	13	-13	-14	211038	BD-16 6046
Gl 851.4	22 12 13	+56 52.3	0.120	70.0	-0.6	K0	9.83	0.72	0.23		48.0	15.3	48.0	15.3	8.2	-11	-3	-3		BD+56 2737
Gl 851.5	22 12 14	+27 35.9	0.569	333.4	17	dM0.5	10.35	1.46		0.66	36.7	11.9	46.0	09. r	8.66	-8	39	46		
NN	22 13 12	+56 47.9	0.443	83.0	-1.4	F0 IV	4.19	0.28	0.04		41.4	5.9	41.4	5.9	2.28	-44	-11	-23	211336	BD+56 2741
NN	22 13 59	+65 58.3	0.229	1.0		m	12.90			1.17			60.0	12. r	11.79					
NN A	22 14 01	+54 25.3	0.221	67.1	-7	K1 V	7.51	0.81	0.39				47.0	07. r	5.87	-20	-11	-4	211472	BD+53 2831
NN B	22 14 10	+54 24.9	0.222	76.0		m	14. *						47.0	07. r	12. *					
NN	22 14 31	-48 54.0	0.230	116.9		K3 V	8.42				32.1	13.6	32.1	13.6	6				211369	CD-49 13794
Gl 852 A	22 14 42	-09 03.0	0.537	239.1	54	dM4.5e	13.40	1.70	1.20	1.27	98.1	3.3	98.1	3.3	13.4	45	21	-33		
Gl 852 B	22 14 42	-09 03.0	0.537	239.1		dM5 e	14.40	1.90	1.80	1.46	98.1	3.3	98.1	3.3	14.4					
Gl 852.1	22 14 53	+15 06.6	0.226	105.0		m	13.55	1.54	1.24		51.9	13.6	51.9	13.6	12.1					
NN	22 14 58	-36 25.9	0.554	167.6			14.2 *			1.24			43.0	08. r	12.4 *					
Gl 853 A	22 15 00	-53 52.1	0.778	145.9	-13.5	G1 V	5.39	+0.60 J	+0.08 J	+0.22 J	82.4	10.9	82.4	10.9	4.97	-27	-37	7	211415	CP-54 10055
Gl 853 B	22 15 00	-53 52.1	0.778	145.9			9.9 *				82.4	10.9	82.4	10.9	9.5 *					
GJ 1266	22 15 04	+70 41.5	0.929	92.9		k	12.12	1.47		0.92	44.5	2.3	44.5	2.3	10.36					
Gl 854	22 15 08	+68 05.4	0.372	88.6	-3.8	dK6	9.23	1.15	1.07		47.7	7.3	47.7	7.3	7.62	-29	-11	-20		BD+67 1424
NN	22 16 31	-28 38.2	0.896	106.1		m	14.80			1.32			45.0	07. r	13.07					
NN	22 18 00	-65 46.	0.236	339.0		M5	11.98	1.56		+0.99t			53.0	11. r	10.6					
Wo 9779	22 19 04	-01 38.4	0.130	84.9	-25.6	SB A0 V	3.84	-0.05	-0.12		44.3	7.7	44.3	7.7	2.07	-20	-18	11	212061	BD-02 5741
GJ 1267	22 19 04	-54 49.0	0.293	322.6		M0 V	9.06	1.35	1.17	0.60			75.0	14. r	8.44				211970	CD-55 9073
Gl 855	22 20 13	-57 28.1	0.694	116.7	-20	M3	10.74	1.50	1.16	0.81	56.8	6.5	56.8	6.5	9.51	-54	-29	-3		CD-57 8545
Gl 855.1A	22 20 22	-72 30.0	1.477	117.6	25.2	G0 V J	5.98	+0.65 J	-0.06 J	+0.28 J	33.5	7.4	70.0	11. r	5.21	-66	-69	-39	211998	CP-72 2690
Gl 855.1B	22 20 22	-72 30.0	1.477	117.6			6.1 *				33.5	7.4	70.0	11. r	5.3 *					
NN	22 20 23	-17 51.0	0.778	158.3		M4	13.25	1.84		1.42	134.1	5.6	134.1	5.6	13.89					
NN	22 20 30	+27 46.7	0.376	96.0		m	14.06			1.24			46.0	09. r	12.37					
Gl 856 A	22 21 12	+32 12.5	0.327	133.0		dM0 eJ	11.41	+1.57 J		+1.10 J			91.0	18. r	11.21					
Gl 856 B	22 21 12	+32 12.5	0.327	133.0			11.6 *						91.0	18. r	11.4 *					
Gl 857	22 21 38	-58 02.8	0.365	158.3	7.8	G4 V	5.32	0.67	0.13	0.24	56.2	9.0	56.2	9.0	4.07	-5	-31	-2	212330	CP-58 7954
Wo 9780	22 21 59	-48 06.8	0.782	143.3		M3.5	12.51			1.22	43.8	22.2	84.0	15. r	12.13					
Gl 857.1A	22 22 24	+22 17.9	0.200	244.3	-6.3	dK7 e	8.86	+1.19 J	+1.10 J	+0.54 J	47.6	6.8	47.6	6.8	7.25	19	-6	7		BD+21 4747
Gl 857.1B	22 22 24	+22 17.9	0.200	244.3	-2.5		12.4 *				47.6	6.8	47.6	6.8	10.8 *	19	-2	5		
GJ 1268	22 22 56	+51 44.8	0.495	31.4		m+	14.94	1.81		1.39	63.0	3.6	63.0	3.6	13.94					
NN	22 23 28	+59 09.8	0.340	157.0		m	12.91			1.20			67.0	13. r	12.04					
NN A	22 23 43	+02 45.3	0.663	228.4		dM	13.68	1.59	1.06	1.22	39.1	3.3	39.1	3.3	11.64					
NN B	22 23 43	+02 45.1	0.663	228.4		m	17.7 P				39.1	3.3	39.1	3.3	15.7 P					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 859 A	22 23 52	-16 59.8	0.222	90.0	-0.3	G3 V	6.21	+0.62 J	+0.07 J	+0.22 J	60.8	8.1	60.8	8.1	5.13	-14	-4	-9	212698	BD-17 6521
Gl 859 B	22 23 51	-16 59.8	0.261	92.2	2	G3 V	6.4 *				60.8	8.1	60.8	8.1	5.3 *	-16	-4	-13	212697	BD-17 6520
Wo 9782 A	22 24 05	+04 08.3	0.309	79.0	-17.8	F7 V	5.75	0.52	0.04		41.1	7.6	41.1	7.6	3.82	-37	-15	-3	212754	BD+03 4705
Wo 9782 B	22 24 05	+04 08.3	0.309	79.0		K4:	11.7 *				41.1	7.6	41.1	7.6	9.8 *					
NN	22 24 32	+06 34.3	0.218	92.0		dM3 :	13.22	1.66					72.0	30. r	12.5					
NN	22 24 52	+63 37.3	0.288	44.0		K7	9.51	1.18	1.17	0.47			40.0	05. r	7.52					
GJ 1269 A	22 25 39	+11 59.6	0.200	92.0	3.8	K0 V	7.15	+0.90 J	+0.56 J		41.5	22.2	62.0	10. r	6.11	-12	-1	-11	212989	BD+11 4804
GJ 1269 B	22 25 39	+11 59.6	0.200	92.0			10.1 *				41.5	22.2	62.0	10. r	9.1 *					
Gl 860 A	22 26 13	+57 26.8	0.943	245.4	-33.3	M2 V	9.85	1.62	1.23	+1.15 J	251.9	2.3	251.9	2.3	11.86	26	-28	2	239960	BD+56 2783
Gl 860 B	22 26 13	+57 26.8	0.943	245.4	-31.7	M6 V	11.3 v	+1.8 :	+1.3 :		251.9	2.3	251.9	2.3	13.3 v	25	-26	2		
NN	22 26 15	-13 39.8	1.083	196.5	-21	M6.5	17.14	2.16			91.9	5.4	91.9	5.4	16.96	26	-52	10		
Wo 9784	22 26 21	+18 40.6	0.210	127.0		dM0	10.75	1.48	+1.31:	0.73			46.0	07. r	9.06					
Gl 862	22 26 25	-30 15.8	0.843	164.7	7.4	K5 V	7.65	1.10	1.00	0.38	75.2	9.4	75.2	9.4	7.03	6	-51	-15	213042	CD-30 19175
GJ 1270	22 27 32	+41 13.1	1.293	68.5		m	13.25	1.65		1.27	72.3	2.9	72.3	2.9	12.55					
Gl 862.1	22 28 41	-06 48.6	0.200	121.0	-9.6	SB F7 V	6.14	0.56	0.04	+0.31C	45.8	11.9	45.0	08. r	4.41	-13	-18	-6	213429	BD-07 5797
Gl 863	22 30 31	+09 07.1	0.547	74.5	-6.5	M0	10.37	1.51	1.16	0.83	66.0	4.3	66.0	4.3	9.47	-38	-7	-9		BD+08 4887
Wo 9787	22 30 38	-35 42.1	0.355	111.2	-51.3	G8 V	7.79	0.72	0.29		43.8	6.9	43.8	6.9	6	-52	-26	27	213628	CD-36 15445
NN	22 30 44	-09 52.3				M3	12.41	1.57	1.16	1.10			59.0	12. r	11.26					
Gl 863.1A	22 30 50	+53 32.1	1.318	86.1	-2	dM1 J	10.84	+1.36 J	+1.13 J	+0.62 J	45.8	3.0	45.8	3.0	9.14	-118	-34	-60		BD+53 2911
Gl 863.1B	22 30 50	+53 32.1	1.318	86.1			10.84*				45.8	3.0	45.8	3.0	9.14*					
Gl 863.2	22 31 58	-20 57.9	0.263	122.6	-4.2	F3 V	5.20	0.44	0.00	+0.24C	44.6	13.6	44.0	06. r	3.42	-16	-21	-11	213845	BD-21 6251
NN	22 32 14	+03 47.0	0.195	325.0		dM4 :	12.68			1.05			45.0	09. r	10.95					
NN	22 32 17	-01 20.8	1.135	78.3		dM4	14.83	1.70		1.32	42.8	3.7	42.8	3.7	12.99					
Gl 863.3	22 32 57	-54 52.0	0.465	124.0	66.9	G5 V	7.58	0.66	0.12	+0.36C	42.8	11.0	32.0	06. r	5.11	-9	-66	-69	213941	CP-55 9866
Gl 864	22 33 35	-01 05.6	0.607	175.0	10.9	dM1	10.01	1.44	1.18	0.77	65.8	6.4	65.8	6.4	9.1	21	-27	-29	214100	BD-01 4323
NN	22 34 27	-66 04.6	0.711	119.5		m	11.45			1.23			147.0	27. r	12.29					
NN	22 34 34	-00 53.2	0.140	96.0			10.5 *				47.3	18.7	47.3	18.7	8.9 *					
Gl 865	22 34 57	-65 38.2	0.853	101.4	-26	k-m	11.48	1.61	1.23	1.17	89.9	11.3	89.9	11.3	11.25	-51	-7	2		
Wo 9791	22 34 59	-65 38.5					14. P				43.6	20.5	43.6	20.5	12. P					
NN	22 35 16	+39 07.6	0.329	184.9		M2	9.41			0.66			71.0	11. r	8.67					BD+38 4818
NN A	22 35 36	-29 36.4	0.260	183.0		m	10.92			0.97			71.0	10. r	10.18					
NN B	22 35 37	-29 36.5	0.260	183.0		m	12.64			1.16			71.0	10. r	11.9					
Gl 866 A	22 35 45	-15 35.6	3.254	46.6	-60	M5 e	12.66	+1.98 J	+1.6 :J	+1.67 J	294.3	3.5	294.3	3.5	15	-69	-1	41		
Gl 867 A	22 36 01	-20 52.8	0.459	97.0	-8.7	SB dM2 e	9.10	1.51	1.09	0.93	115.4	4.0	115.4	4.0	9.41	-18	-9	-2	214479	BD-21 6267
Gl 867 B	22 36 01	-20 52.8	0.459	97.0		dM4 e	11.45	1.60	1.12	1.20	115.4	4.0	115.4	4.0	11.76					
Gl 867.1A	22 36 55	-12 52.4	0.281	122.7	-12.7	SB? G8/K0 V J	8.51	+0.78 J	+0.37 J	+0.39CJ	46.9	8.1	27.0	03. r	5.67	-28	-39	-17	214615	BD-13 6235
Gl 867.1B	22 36 55	-12 52.4	0.281	122.7	-13.8	dG9 e	8.6 *				46.9	8.1	27.0	03. r	5.8 *	-29	-39	-16		
Gl 867.1C	22 37 02	-12 50.9	0.270	126.0		k-m	14.65	1.61	1.45		46.9	8.1	27.0	03. r	11.81					
Gl 868	22 37 55	-29 56.1	0.401	94.3	1	K5 Ve	7.82	1.13	1.00	0.44	69.1	10.2	69.1	10.2	7.02	-22	-9	-14	214749	CD-30 19255
Gl 869	22 38 06	-32 15.1	0.356	87.3	-21	G8 V	7.39	0.80	0.44	0.25	60.6	13.6	43.0	07. r	5.56	-43	-11	0	214759	CD-32 17191
NN	22 38 28	+44 20.2	0.474	94.2		m	13.20			1.16			50.0	10. r	11.69					
Wo 9793	22 39 08	+18 33.7	0.273	72.6		M0	10.75	1.42		0.68			40.0	06. r	8.76					BD+18 5029

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 871 A	22 39 39	-47 28.1	0.334	175.1	17.3	G1 V	6.00	0.57	0.06	0.20	57.5	24.4	49.0	06. r	4.45	12	-34	-8	214953	CD-47 14307
Gl 871 B	22 39 39	-47 28.1	0.334	175.1		M1	11.10	1.41			57.5	24.4	49.0	06. r	9.55					
GJ 1271	22 40 08	+17 24.0	1.240	63.9		M3	11.78	1.56	1.16	1.03	52.6	4.4	52.6	4.4	10.38					
NN	22 40 46	-06 39.6	0.326	205.7	-18	K0	8.12	0.97	0.79				49.0	08. r	6.57	19	-29	10	215152	BD- 7 5839
NN	22 40 57	+21 52.6	0.409	92.7		m	15.00			1.44			63.0	10. r	14					
GJ 1272 A	22 42 58	+10 55.9	0.163	175.3	-0.6	dK6	9.98	+1.13 J	+1.02 J	+0.51 J	53.0	23.7	29.0	03. r	7.29	12	-17	-16		BD+10 4812
GJ 1272 B	22 42 58	+10 55.9	0.163	175.3	-0.6		12. *				53.0	23.7	29.0	03. r	9. *	12	-17	-16		
NN	22 43 18	-63 34.0	0.222	115.0		M3	11.40	1.46		+0.81t			41.0	08. r	9.46					
NN	22 43 47	-06 54.8	0.865	128.0		m	15.98	1.83			53.7	6.8	53.7	6.8	14.63					
NN	22 44 07	+23 18.1	0.058	94.8	-4.3	G8 IIIa CN	3.96	1.07	0.93		40.9	11.9	40.9	11.9	2	-5	-6	-1	215665	BD+22 4709
Gl 871.2	22 44 11	+49 56.8	0.239	90.5	-50.8	K0	7.86	0.80	0.49		48.0	15.3	39.0	05. r	5.82	-13	-57	-7	215704	BD+49 3937
Gl 872 A	22 44 12	+11 55.0	0.538	155.0	-6	F6 IV-V	4.19	0.50	-0.03	0.19	50.0	11.9	50.0	11.9	2.7	5	-38	-34	215648	BD+11 4875
Gl 872 B	22 44 12	+11 55.0	0.538	155.0	-7.2	M1	11.7 *				50.0	11.9	50.0	11.9	10.2 *	5	-39	-33		
Gl 873	22 44 40	+44 04.6	0.901	238.7	-0.5	SB dM4.5e	10.26v	1.61		1.19	197.0	2.5	197.0	2.5	11.73v	21	3	-1		BD+43 4305
NN	22 45 19	+44 17.4	0.095	222.6	2.2	F8	9.6 *				56.0	24.0	56.0	24.0	8.3 *	7	3	-3	215857	BD+43 4306
Gl 874	22 45 25	-37 03.0	0.807	109.4		M3	11.92	1.48		0.95	51.3	10.7	51.3	10.7	10.47					
NN	22 45 32	+31 36.2	0.500	69.0		m	12.91			1.10			47.0	10. r	11.27					
Wo 9796	22 45 33	-51 34.8	0.129	121.1	-3	A2 V	3.48	0.08	0.10		42.9	9.2	42.9	9.2	1.64	-11	-10	-1	215789	CD-51 13389
GJ 1273	22 46 39	+22 20.5	0.506	86.2	94	DA5	14.36	0.19	-0.68		52.6	4.1	52.6	4.1	12.96	-40	30	-44		
Wo 9797	22 47 20	-41 45.1	0.415	239.6	21.6	G5 V	7.77	0.74	0.24	0.26	43.7	9.6	33.0	05. r	5.36	61	-16	9	216054	CD-42 16092
NN	22 47 36	+24 19.8	0.150	104.0	15.3	G8+ III	3.48	0.93	0.68	0.47	39.2	20.4	39.2	20.4	1.4	-13	6	-19	216131	BD+23 4615
Gl 875	22 47 43	-07 21.4	0.152	316.8	-5.7	dM1 e	9.85	1.48	1.24	0.73	71.1	10.6	71.1	10.6	9.11	1	5	10	216133	BD-07 5871
GJ 1274	22 48 14	+34 35.2	0.889	71.3		m	11.72	1.53			48.1	5.2	48.1	5.2	10.13					
NN 1	22 48 17	+35 55.7	0.196	253.0		m	12. *				47.0	9.4	47.0	9.4	10. *					
NN	22 48 22	+28 20.3	0.223	103.0		m	12.55			1.08			52.0	11. r	11.13					
GJ 1275	22 48 56	+29 23.7	1.269	83.2		DA9	15.52	0.63	-0.10		48.3	4.3	48.3	4.3	13.94					
Wo 9798	22 48 56	+13 42.1	0.462	62.5	-1.7	dK4	8.30	0.84	0.44		42.7	12.1	35.0	06. r	6.02	-62	0	-5	216259	BD+13 5006
Gl 875.1	22 49 30	+31 29.4	0.513	95.6	-3.7	dM3.5e	11.63	1.55	1.07	1.11	65.0	4.4	65.0	4.4	10.69	-30	-15	-18		
NN	22 49 37	+23 09.0	0.202	139.1	-4.2	dK8	9.78	1.20	1.14	0.54			42.0	05. r	7.9	-4	-15	-17		BD+22 4725
Wo 9800 A	22 49 45	-33 08.5	0.034	239.5	16.5	A0 III	4.50	-0.04 J	-0.14 J		42.4	17.0	42.4	17.0	2.6	10	1	-13	216336	CD-33 16270
Wo 9800 B	22 49 45	-33 08.5	0.034	239.5	17		8.6 *				42.4	17.0	42.4	17.0	6.7 *	11	1	-14		
Wo 9801 A	22 49 52	+09 34.1	0.523	84.6	10.2	F7 IV	5.16	0.48	-0.01	0.17	49.7	9.8	41.0	05. s	3.22	-53	-6	-30	216385	BD+09 5122
Wo 9801 B	22 49 58	+09 38.1	0.520	84.7		M3:	13.52	1.66	1.32	1.10	49.7	9.8	41.0	05. s	11.58					
Gl 876	22 50 35	-14 31.2	1.143	123.5	-1.5	dM5	10.17	1.58	1.15	1.22	211.3	4.8	211.3	4.8	11.79	-13	-19	-12		BD-15 6290
Wo 9802	22 50 41	-48 51.8	0.236	110.0	-1	G3 IV	6.03	0.62	0.19		46.0	15.4	46.0	15.4	4.3	-19	-14	-7	216435	CD-49 13988
GJ 1276	22 51 09	-07 02.3	2.570	106.0		DZ9+	15.65	1.90			124.2	4.3	124.2	4.3	16.12					
NN	22 52 09	-05 44.7	0.693	62.2		m	13.9 *			1.24			50.0	09. r	12.4 *					
Gl 877	22 52 12	-75 42.7	1.420	225.6	-86	k	10.40	1.49	1.05	1.06	119.9	9.1	119.9	9.1	10.79	-13	31	97		
Gl 878	22 52 26	+60 43.7	0.690	259.8		M3	12.76	1.60		1.12	71.0	6.8	71.0	6.8	12.02					
NN	22 52 30	-52 34.	0.175	128.0		M4	11.49	1.45		+0.83t			42.0	08. r	9.61					
NN A	22 53 24	+05 29.5	0.448	128.0		dM0	11.26	1.45	1.19	0.82			45.0	08. r	9.53					
NN B	22 53 23	+05 29.6	0.448	128.0		DB	15.7 P						45.0	08. r	14.0 P					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
GJ 1277	22 53 25	-60 18.3	1.060	209.0	68	M4	14.08	1.79	1.45	1.42			90.0	13. r	13.85	62	-59	-20		
NN	22 53 32	+17 32.7				M0	10.50	1.49	1.19	0.82			65.0	11. r	9.56					
Gl 879	22 53 37	-31 49.8	0.360	114.6	9	K5 Ve	6.48	1.10	1.02	0.41	128.1	9.0	128.1	9.0	7.02	-5	-8	-13	216803	CD-32 17321
Gl 880	22 54 10	+16 17.4	1.071	254.8	-27.9 SB	dM2 e	8.67	1.50	1.18	0.88	148.2	2.5	148.2	2.5	9.52	32	-17	25	216899	BD+15 4733
NN	22 54 19	+67 59.2	0.748	63.2		m	14.68	1.70			40.2	5.0	40.2	5.0	12.7					
Gl 881	22 54 54	-29 53.3	0.372	115.6	6.1	A3 V	1.16	0.09	0.08	-0.06	153.7	7.7	153.7	7.7	2.09	-5	-7	-10	216956	CD-30 19370
Gl 882	22 55 00	+20 30.0	0.208	76.9	-33.7	G4 V	5.50	0.67	0.21	0.22	58.4	8.2	58.4	8.2	4.33	-16	-31	15	217014	BD+19 5036
Gl 883	22 57 16	-11 38.9	0.229	92.0	-20	dM1	10.60	1.42		0.64			41.0	08. r	8.66	-28	-17	6		BD-12 6393
Gl 884	22 57 38	-22 47.6	0.911	274.1	15.4	K5/M0 V	7.88	1.39	1.24	0.60	128.4	6.8	128.4	6.8	8.42	33	16	0	217357	CD-23 17699
NN A	22 57 51	-24 13.0	0.389	148.0		M1:	11.57	1.53		0.87			47.0	06. r	9.93					CD-24 17443
NN B	22 57 54	-24 14.0	0.389	148.0		M2	11.61	1.55		0.88			47.0	06. r	9.97					CD-24 17445
Gl 886	22 59 15	-04 06.9	0.446	117.2	-43.1 SB	K4 V	7.46	0.95	0.77	0.32	58.6	9.0	58.6	9.0	6.3	-28	-46	16	217580	BD-04 5804
Gl 886.1A	23 00 18	+42 29.3	0.046	81.2	+2.0 SB	A3 Vn	5.14	+0.09 J	+0.11 J		18.5	9.5	18.5	9.5	1.5	-11	-1	-4	217782	BD+41 4665
Gl 886.1B	23 00 18	+42 29.3	0.046	81.2			8.8 *				18.5	9.5	18.5	9.5	5.1 *					
NN	23 00 27	-49 59.7	0.116	201.0		M3	10.64	1.41		+0.76t			51.0	09. r	9.18					CD-50 13863
Gl 886.2	23 00 44	-35 01.2	0.113	41.5	-6.0 SB	F0 IV	5.11	0.29	0.00	+0.19C	50.2	11.9	50.2	11.9	3.6	-11	5	2	217792	CD-35 15630
GJ 1278	23 02 32	+66 29.7	0.332	107.0	7.4	dM1	9.89	1.40	1.26	0.66	33.8	13.6	58.0	12. r	8.71	-23	1	-17		BD+65 1846
Gl 887	23 02 39	-36 08.5	6.896	79.1	9.5	M2 Ve	7.34	1.49	1.18	0.84	284.3	14.9	284.3	14.9	9.61	-100	-15	-56	217987	CD-36 15693
Wo 9808	23 03 08	+68 08.7	0.606	73.5	-18.2	G6 V	7.48	0.65	0.09		47.5	15.9	31.0	05. r	4.94	-78	-52	-14	218209	BD+67 1498
Wo 9809	23 04 00	+63 39.0	0.174	109.8		dM0	10.82	1.42		0.73			44.0	07. r	9.04					
Gl 889 A	23 04 26	-23 25.6	0.340	152.5	19	K5 V	9.62	1.30	1.38	0.54	48.7	7.7	44.0	06. r	7.84	4	-31	-27	218294	CD-23 17748
Gl 889 B	23 04 34	-23 23.8	0.303	149.0		k-m	13.65	1.65		1.16	48.7	7.7	44.0	06. r	11.87					
NN	23 04 36	+71 26.8	1.320	71.5		M2	11.78	1.48		0.95			50.0	10. r	10.27					
NN	23 05 25	+68 23.8	1.125	88.5		m	12.45	1.54		1.10	63.5	4.2	63.5	4.2	11.46					
Gl 889.1	23 05 32	+03 03.3	0.533	60.0	32	dM0	10.91	1.52	1.21	0.77	61.3	3.3	61.3	3.3	9.85	-37	23	-28		
Gl 890	23 05 41	-15 40.8	0.050	79.0	2	dM2.5e	10.88	1.42	1.12	0.73	40.7	6.3	40.7	6.3	8.93	-5	0	-4		BD-16 6218
GJ 1279	23 06 33	-68 00.1	0.387	235.0		K5 V	8.39	1.20	1.14	0.50			70.0	11. r	7.62				218511	CD-68 2331
NN	23 06 34	-02 31.8	0.643	98.4	-40.9	K3 V	8.59	1.01	0.95	0.34	29.0	9.2	39.0	06. r	6.55	-68	-56	-1	218566	BD- 3 5577
NN	23 07 04	-02 14.5	0.449	143.0		k-m	12.66	1.54	1.18				43.0	20. r	10.8					
GJ 1280	23 07 08	-69 06.9	0.332	14.4		K4 V	8.78	1.02	0.76	0.42			44.0	06. r	7				218572	CD-69 2083
Wo 9812 A	23 07 15	-22 43.7	0.026	103.5	-1	G2 V	5.11	+0.65 J	+0.39 J		39.0	13.6	21.0	03. s	1.72	-5	-3	-1	218640	CD-23 17771
Wo 9812 B	23 07 15	-22 43.7	0.026	103.5	-6	A3 (IV)	5.9 *				39.0	13.6	21.0	03. s	2.5 *	-6	-5	3	218641	
Gl 891	23 07 32	-26 12.2	0.710	88.4		M2.5	11.27	1.52	+1.2 :	+0.94t	77.7	19.0	77.7	19.0	10.7					CD-26 16501
NN A	23 07 39	+47 41.2	0.150	89.6	-6.8 SB	G5	7.91	0.90	0.57		28.7	3.4	28.7	3.4	5.2	-20	-14	-8	218738	BD+47 4058
GJ 1281	23 08 03	-19 28.7	1.421	178.4	55	M3	12.47	1.49	1.05	0.96			40.0	10. r	10.5	81	-136	-80		
NN	23 09 35	-14 21.9	0.748	197.3		m	13.0 *			1.13			50.0	10. r	11.5 *					
Gl 891.1	23 10 15	+49 08.0	0.130	37.3	+11.2 SB	F0 V	4.52	0.29	0.04		49.1	6.1	49.1	6.1	2.98	-14	9	4	219080	BD+48 3964
NN	23 10 51	-81 36.7	0.531	82.6		k-m	10.1 *			0.71			58.0	09. r	8.9 *					
Gl 892	23 10 52	+56 53.5	2.094	81.8	-18.2	K3 V	5.56	1.01	0.89	0.35	146.4	4.7	146.4	4.7	6.39	-56	-40	-15	219134	BD+56 2966
NN	23 10 54	-70 19.9	0.200	68.3		G5 V	6.90						54.0	06. o	5.56				219048	CP-70 2999
GJ 2154 A	23 11 32	-19 55.1	0.454	84.0		K7 V	10.62	1.46	1.22	0.78			44.0	06. r	8.84					BD-20 6558
GJ 2154 B	23 11 32	-19 55.2	0.454	84.0		m	13.80	1.60	1.14	1.18			44.0	06. r	12.02					

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 893.1	23 11 51	-06 49.1	0.376	245.0		DQ6	15.42	0.22	-0.63		40.9	6.9	40.9	6.9	13.48					
Gl 893.2A	23 13 16	-09 21.6	0.368	92.0	-25.2	K0 III	4.22	1.11	1.00	0.38	43.3	6.2	43.3	6.2	2.4	-39	-26	7	219449	BD-09 6156
Gl 893.2B	23 13 14	-09 21.1	0.382	90.9	-26.1	K3 V J	9.62	+1.05 J	+0.90 J	+0.38 J	43.3	6.2	43.3	6.2	7.8	-41	-26	8	219430	BD-09 6155
Gl 893.2C	23 13 14	-09 21.1	0.382	90.9			10.3 *				43.3	6.2	43.3	6.2	8.5 *					
NN	23 13 36	+06 28.4	0.285	147.0		k	13.14	1.63	1.26				63.0	27. r	12.1					
NN	23 13 51	+30 23.8	0.377	74.9	9	K2 V	8.09	0.88	0.58		17.1	18.8	42.0	07. r	6.21	-42	-2	-10	219538	BD+29 4890
GJ 1282	23 13 58	-62 16.4	0.180	97.4	-1.8	F7 V	5.66	0.51	+1.61c				46.0	06. r	3.97	-17	-8	-4	219482	CD-62 1444
Gl 893.3A	23 14 00	-41 03.6	0.255	182.0		g-k	11.57	0.90		+0.54C	48.3	15.3	48.3	15.3	10					CD-41 15204
Gl 893.3B	23 14 01	-41 03.9	0.255	182.0			17.4 R				48.3	15.3	48.3	15.3	15.8 R					
Gl 893.4	23 14 11	+19 21.0	0.253	227.0		dM0	11.16	1.49	1.18	0.78			43.0	07. r	9.33					
NN A	23 14 14	-67 11.2	0.559	138.1	67.8	K5 V	8.73	1.05	0.96	0.39	37.5	6.0	43.0	04. r	6.9	1	-83	-39	219509	CP-67 3960
NN B	23 14 10	-67 12.3	0.542	138.3	66.4	K5 V	9.04	1.11	1.06	0.42	37.5	6.0	43.0	04. r	7.21	2	-81	-38	219495	CP-67 3959
NN	23 14 19	+05 25.4	0.009	159.5	-11	dM0.5	10.52	1.41	1.25	0.62	34.7	13.6	40.0	08. r	8.53	-1	-8	8		BD+ 4 4988
NN	23 14 25	+52 56.6	0.255	153.9	-25.3	F7 V	5.54	0.52	0.02		43.3	11.9	51.0	08. r	4.08	7	-27	-20	219623	BD+52 3410
Wo 9818	23 14 31	-58 30.6	0.087	343.7	18.4	F1 III	3.99	0.40	-0.04		41.0	10.2	41.0	10.2	2.1	9	3	-18	219571	CP-58 8062
Gl 894	23 14 51	-42 27.9	0.290	98.0	8	K3/5 V	10.38	1.32	1.25	0.58	61.6	8.5	61.6	8.5	9.33	-15	-11	-14	219630	CP-42 9551
NN	23 14 57	-48 35.0	0.799	157.7		m	13.7 *			1.20			46.0	09. r	12.0 *					
NN	23 14 58	+19 20.5	0.269	105.0		M4	12.10	1.59	1.20				78.0	36. r	11.6					
NN	23 15 00	+37 56.6	0.531	196.4		m	11.46	1.54	1.20	1.04	56.1	3.4	56.1	3.4	10.2					
NN	23 15 00	+09 25.2	0.125	111.0	24.8	dK8	9.72	1.13	0.98	0.50	51.4	6.8	51.4	6.8	8.27	-7	11	-24		BD+08 5036
NN	23 15 01	+06 07.3	0.298	142.0		dM4	12.53	1.55	1.28				49.0	23. r	11					
NN	23 15 25	-41 05.8	0.178	131.5	28.6	F5 V	5.53	0.44	-0.05				39.0	05. r	3.49	1	-21	-29	219693	CD-41 15211
Wo 9819	23 15 41	-58 34.7	0.263	125.8	17.2	G2 V	7.52	0.65	0.04		39.5	13.6	29.0	05. r	4.83	-18	-40	-15	219709	CP-58 8064
NN	23 15 50	-61 31.7	0.080	326.0		M3	11.20	1.41		+0.80t			43.0	08. r	9.37					CD-61 6801
Gl 894.1	23 15 56	+46 00.8	0.333	70.0	-5.7	M0.5	10.90	1.45		0.76	47.8	15.3	47.0	09. r	9.26	-31	-15	1		BD+45 4188
Wo 9821	23 16 08	-32 48.3	0.068	164.2	15.6	G8 III	4.41	1.13	1.06		42.1	10.2	42.1	10.2	2.5	6	-6	-15	219784	CD-33 16476
GJ 1283	23 16 10	-60 47.6	0.087	247.7		K4 V	8.97	1.15	1.05	0.48			49.0	07. r	7.42				219764	CD-61 6802
Gl 894.2A	23 16 29	-13 43.9	0.312	108.5	+10.3	SB G5 IV	5.20	0.79	0.41	0.26	40.9	8.6	51.0	08. r	3.7	-18	-14	-21	219834	BD-14 6448
Gl 894.2B	23 16 29	-13 43.6	0.321	106.1	10.3	K2 V	7.61	0.91	0.67	0.29	40.9	8.6	51.0	08. r	6.15	-19	-13	-21		
NN	23 17 24	-60 20.0	0.300	254.0		M2	10.99	1.45		+0.78t			46.0	08. r	9.3					
Wo 9822	23 17 28	+28 35.7	0.747	97.0	-53	K1 V	8.89	0.81	0.37	0.33	43.9	15.5	27.0	04. r	6.05	-98	-97	-31	219953	BD+28 4562
NN	23 19 09	+17 02.1	1.483	201.0		m	11.72	1.51	1.09	1.24	92.8	3.8	92.8	3.8	11.56					
Gl 894.4	23 19 11	+43 49.2	0.669	70.3	4.4	K1 V	7.36	0.80	0.41		50.6	16.0	50.0	08. r	5.85	-62	-14	-2	220182	BD+43 4445
Gl 894.5	23 20 27	-11 02.5	0.522	59.4	35.9	K2 V	7.80	0.89	0.59	0.32	59.7	10.0	59.7	10.0	6.68	-34	20	-38	220339	BD-11 6064
Gl 895	23 22 14	+57 35.0	0.287	185.0	-33.8	dM2 e	10.04	1.50	1.18	0.86	71.6	2.3	71.6	2.3	9.31	20	-29	-15		BD+57 2735
Gl 895.1	23 22 55	-45 53.1	0.482	96.0		M0	11.26	1.42			43.9	17.0	38.0	10. r	9.2					CD-46 14649
NN	23 23 16	+52 51.3	1.071	71.2		m	14.59	1.66			40.3	3.1	40.3	3.1	12.62					
Wo 9826	23 23 26	+28 55.5	0.578	125.3		K3	11.05	0.94	0.72	0.38	42.0	10.9	42.0	10.9	9.2					
GJ 2155	23 23 39	+08 37.0	0.537	68.7		K7	10.54	1.50	1.20	+0.70t	51.0	5.2	51.0	5.2	9.08					
NN	23 23 54	-47 07.0	0.521	136.4		m	15.75			1.42			42.0	06. r	13.87					
NN	23 23 59	+11 52.8	0.707	70.0		m	12.63			1.06			47.0	09. r	10.99					
Wo 9827	23 24 30	-01 33.9	0.439	62.0	27	dM0.5	10.39	1.28		0.53	47.6	10.6	34.0	06. r	8.05	-59	16	-27		BD-02 5958

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 895.2	23 26 16	+04 58.5	0.492	238.1	34	DAV4	13.04	0.16	-0.64	+0.02C	72.7	4.8	72.7	4.8	12.35	32	-8	8		
Gl 895.3	23 26 49	-47 18.6	0.210	105.0	-4	K7 V	10.21	1.31	+1.23:	+0.69C	48.6	10.2	48.6	10.2	8.64	-17	-12	-1		CP-47 9997
NN A	23 26 56	+41 11.9	0.404	95.0		M2	11.87	1.52	1.09	1.14	67.2	2.5	67.2	2.5	11.01					
NN B	23 26 55	+41 11.7	0.404	95.0		M3 :	12.44	1.61	1.06	1.28	67.5	2.5	67.5	2.5	11.59					
GJ 1284	23 27 35	-20 39.8	0.355	121.0		M2 Ve	11.16	1.51	1.03	1.10			92.0	25. r	11					
NN	23 27 45	+31 25.9	0.235	123.0	-14.6	K0	8.31	0.93	0.58				39.0	05. r	6.27	-11	-27	-13	221239	BD+30 4961
Gl 895.4	23 28 56	+58 53.3	1.108	84.3	-24.3	K0 V	6.74	0.83	0.51	0.28	56.1	4.3	56.1	4.3	5.48	-75	-59	-19	221354	BD+58 2605
Wo 9829	23 28 56	-04 21.6	0.259	137.1	-13.1	F8 V	6.49	0.54	-0.01		42.9	6.5	39.0	04. s	4.45	-9	-33	-4	221356	BD-04 5896
Gl 896 A	23 29 20	+19 39.7	0.560	91.7	1.1	dM4 e	10.38	1.54	1.08	1.13	151.9	3.7	151.9	3.7	11.29	-15	-6	-6		BD+19 5116
Gl 896 B	23 29 20	+19 39.7	0.560	91.7	-1.2	dM6 e	12.4 *	1.65	1.12	1.62	151.9	3.7	151.9	3.7	13.3 *	-15	-8	-5		
NN	23 30 08	-77 39.7	0.018	74.9	26	G2 V	5.81	0.68	0.31				72.0	12. r	5.1	12	-16	-17	221420	CP-78 1473
Gl 897 A	23 30 09	-17 01.5	0.400	126.0	-1.9	M3.5 J	10.95	+1.51 J	+0.95 J	+1.03 J	77.5	9.0	77.5	9.0	10.4	-11	-21	-7		BD-17 6768
Gl 897 B	23 30 09	-17 01.5	0.400	126.0			11.4 *				77.5	9.0	77.5	9.0	10.8 *					
Gl 898	23 30 12	-17 07.1	0.390	126.8	0.5	K5/M0 V	8.60	1.28	1.22	0.53	77.5	9.0	77.5	9.0	8.05	-10	-20	-9	221503	BD-17 6769
Wo 9830	23 30 57	+42 34.1	0.305	52.9	6.1	G0	7.14	0.58	0.04		41.0	10.2	31.0	04. s	4.6	-45	-4	13	221613	BD+42 4700
Gl 899	23 31 33	-00 05.1	1.388	227.8	20	M4	11.17	1.45	1.08	0.98	70.9	12.2	70.9	12.2	10.42	91	-9	-25		
Gl 900	23 32 26	+01 19.7	0.347	82.0	-10.9	dM0.5	9.56	1.35	1.20	0.64	58.4	10.8	58.4	10.8	8.39	-27	-14	3		BD+00 5017
NN	23 32 34	+24 58.2	0.208	16.0		M3	12.92			1.09			44.0	08. r	11.14					
GJ 1286	23 32 34	-02 39.3	1.157	137.4		M5	14.69	1.96		1.65	138.6	3.5	138.6	3.5	15.4					
Gl 900.1	23 32 52	-47 13.1	0.349	145.9	-5	G8 V	8.54	0.79	+0.35:	0.27	45.6	15.3	26.0	04. r	5.61	-17	-61	10	221818	CD-47 14628
NN	23 32 56	+29 47.4	0.348	217.0		m	13.21			1.14			47.0	09. r	11.57					
NN	23 32 57	+30 53.3	0.334	213.1	-17.9	K0	7.91	0.84	0.50				40.0	06. r	5.92	37	-19	-12	221851	BD+30 4983
NN	23 33 00	-16 34.3	0.152	151.0		DA	13.34	0.13	-0.57				45.0	07. w	11.61					
NN	23 33 07	+05 54.3	0.628	62.8		m	16.10	1.78			42.2	3.2	42.2	3.2	14.23					
NN	23 33 14	+41 41.3	0.714	77.2		M0	11.20	+1.43:	1.26	+0.82t	35.4	13.6	44.0	10. r	9.42					
NN	23 33 37	-48 51.9	0.142	259.9		M0	10.09	1.37		+0.64t			51.0	07. r	8.63					CP-49 11759
NN	23 33 37	-48 51.9	0.127	272.0			12.37	1.44		+1.09t			51.0	07. r	10.91					
NN	23 33 59	+55 13.2	0.479	101.1		M1	11.70	1.46	1.19	0.87			41.0	08. r	9.76					
NN	23 34 08	-36 45.5	1.155	87.9		M4	13.72	1.62	1.36	1.36			81.0	16. r	13.26					
Gl 901	23 34 14	+00 53.4	1.205	94.9	44	M3.5:	13.08	+1.56:	+1.13:	0.91	45.9	23.3	26.0	07. r	10.2	-181	-75	-108		
Wo 9832	23 35 06	+46 11.2	0.446	159.0	+6.8 SB	G8 III-IV	3.82v	1.01	0.69		48.1	7.4	48.1	7.4	2.23v	-1	-5	-44	222107	BD+45 4283
NN	23 35 30	+45 55.4	0.339	91.5	-0.6	G5	6.58	0.66	0.16		28.9	13.6	48.0	06. r	4.99	-29	-14	-10	222143	BD+45 4288
NN	23 35 33	-16 30.8	0.279	257.0		M2	11.34	1.57		0.96			67.0	13. r	10.47					BD-17 6785
NN	23 35 37	-41 47.6	0.282	131.0		M3	11.93	1.46		+0.98t			50.0	11. r	10.42					CD-42 16413
NN	23 36 14	+38 53.2	0.579	204.4		m	13.58			1.16			42.0	08. r	11.7					
NN	23 36 16	-07 58.1	0.050	:140.		DA	13.26	0.18	-0.47				63.0	11. w	12.26					
NN A	23 36 23	+20 44.6	0.329	58.0		m	14.24			1.23			41.0	08. r	12.3					
NN B	23 36 24	+20 44.5	0.329	58.0		g	17.9 P						41.0	08. r	16.0 P					
Gl 902	23 36 41	-72 59.3	0.749	169.1	71.7	K3 V	7.07	0.99	0.84	0.39	107.4	10.5	107.4	10.5	7.23	32	-66	-29	222237	CP-73 2299
GJ 2157	23 37 12	+58 41.6	0.037	27.5	-43	K0 V	7.45	0.86					53.0	07. r	6.07	15	-40	4	222366	BD+58 2627
Gl 902.1	23 37 13	-33 01.0	0.329	156.6	-8	K1 V	7.19	0.81	0.42	0.28	41.0	22.2	53.0	08. r	5.81	-2	-30	6	222335	CD-33 16646
Gl 903	23 37 17	+77 21.2	0.171	337.4	-43.1	K1 IVe	3.21	1.03	0.94	0.34	66.5	5.6	66.5	5.6	2.32	23	-39	0	222404	BD+76 928

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
Gl 904	23 37 23	+05 21.3	0.573	139.0	+5.5 SB?	F7 V	4.13	0.51	0.00	0.19	72.5	5.6	72.5	5.6	3.43	-8	-26	-26	222368	BD+04 5035
NN	23 37 44	+60 24.9	0.240	162.0		M2	11.41	1.57	1.20	0.89			54.0	10. r	10.07					
Gl 904.1A	23 38 19	+20 05.3	0.231	73.4	-18.6	K2	8.32	+1.11 J	+1.08 J		45.0	17.0	56.0	10. r	7.06	-16	-19	11	222474	BD+19 5135
Gl 904.1B	23 38 19	+20 05.3	0.231	73.4			11.7 *				45.0	17.0	56.0	10. r	10.4 *					
Gl 905	23 39 26	+43 55.2	1.617	177.0	-77.7	dM6 e	12.29	1.90	1.48	1.55	315.6	1.6	315.6	1.6	14.79	33	-74	0		
Wo 9835	23 39 38	-02 50.9	0.422	210.0	25	dM0	10.32	1.38		0.62			43.0	08. r	8.49	41	-9	-32		BD- 3 5691
Wo 9836 A	23 40 08	-14 49.3	0.116	122.6	-2.1 SB	B9 V	4.48	-0.04	-0.12		39.7	10.2	39.7	10.2	2.5	-7	-12	-3	222661	BD-15 6476
Wo 9836 B	23 40 08	-14 49.3	0.116	122.6			11. *				39.7	10.2	39.7	10.2	9. *					
GJ 1288	23 40 23	+30 32.9	0.438	231.4		m	14.36	1.77		1.38	81.9	2.6	81.9	2.6	13.93					
GJ 1289	23 40 33	+36 15.7	0.936	98.3	-6	k	12.57	1.60	1.64	1.29	123.0	2.9	123.0	2.9	13.02	-28	-21	-11		
Gl 905.2A	23 41 23	+32 19.0	0.233	256.0	-24.3	dM5	11.67	1.56	1.18	1.09	55.6	1.7	55.6	1.7	10.4	25	-14	12		
Gl 905.2B	23 41 21	+32 16.2	0.233	256.0	17	DA4	12.90	0.15	-0.61		55.6	1.7	55.6	1.7	11.63	26	-17	14		
NN	23 41 32	+64 27.8	0.548	81.7		M1.5	11.30	1.40	1.12		22.5	9.0	49.0	11. r	9.75					
GJ 1290	23 41 48	+21 19.3	0.428	79.0		m	13.30	1.59		1.20	45.1	4.0	45.1	4.0	11.57					
NN	23 42 58	-16 26.5	0.684	215.3		m	14.5 *			1.55			111.0	19. r	14.7 *					
Gl 906	23 43 18	+35 58.6	0.300	79.0	-21.8	dM0	9.90	1.35	1.20	0.58	55.5	11.9	55.5	11.9	8.62	-18	-28	7		
NN	23 43 52	-50 59.5	0.502	203.7		m	14.6 *			1.32			50.0	08. r	13.1 *					
Gl 907	23 45 31	+48 44.2	0.652	83.5	27	M1.5	12.07	1.66	1.34		65.6	9.7	65.6	9.7	11.15	-53	5	-12		
Gl 907.1A	23 45 50	-13 15.9	0.188	88.0	-3.4	dM0	9.86	+1.26 J	+1.13 J	+0.62 J			44.0	08. r	8.08	-18	-9	-2		BD-13 6464
NN	23 46 02	-27 56.1	0.593	244.0		M3.5:	12.4 *			1.06			53.0	11. r	11.0 *					
Gl 908	23 46 36	+02 08.2	1.370	133.4	-71.3	M2 Ve	8.98	1.48	1.09	0.85	177.9	5.6	177.9	5.6	10.23	-9	-68	41		BD+01 4774
NN	23 46 42	+09 49.3	0.345	172.0		dM4 :	13.57			1.19			47.0	09. r	11.93					
NN	23 47 04	+08 04.8				M1	11.39	1.45	1.14	0.80			40.0	07. r	9.4					
NN	23 47 23	+29 17.8	0.531	190.8		DA9	15.72	0.58	-0.24		47.0	4.1	47.0	4.1	14.08					
NN	23 47 31	+02 35.8	0.501	67.6	-26.8	G7 V	8.36	0.74	0.35	0.24	39.1	9.3	25.0	04. r	5.35	-93	-26	20	223498	BD+02 4723
GJ 1291 A	23 47 39	-29 40.8	0.192	83.4		K1 V	7.94	0.84	0.43	0.30			40.0	06. r	5.95				223515	CD-30 19702
Gl 908.1	23 47 55	+30 04.5	0.260	87.1	-3.1	dK8	9.34	1.26	1.19	0.49	42.8	8.3	48.0	06. r	7.75	-22	-13	-3		BD+29 5007
NN	23 47 55	-09 49.9	0.756	124.0		m	13.45			1.26			66.0	12. r	12.55					
NN	23 48 01	+09 40.0	0.668	60.9		M1	11.50	1.45	1.13	1.07			77.0	16. r	10.93					
NN	23 48 23	+38 13.1	0.236	204.0		m	14.18			1.25			45.0	08. r	12.45					
NN	23 49 12	+06 41.8	0.297	189.0		m	12.73			1.12			54.0	11. r	11.39					
Wo 9843	23 49 32	+77 19.4	0.278	107.9	0.8	F5 V	6.56	0.43	-0.12		40.8	13.6	24.0	03. s	3.46	-45	-16	-28	223731	BD+76 934
NN	23 49 48	-14 57.9	0.523	120.1		m	15.5 *			1.45			52.0	08. r	14.1 *					
Gl 909 A	23 49 57	+75 15.9	0.309	79.6	+1.7 SB	K3 V	6.40	0.98	0.71	0.38	96.5	2.9	96.5	2.9	6.32	-14	-6	0	223778	BD+74 1047
Gl 909 B	23 49 57	+75 15.9	0.309	79.6		M2	11.7 *				96.5	2.9	96.5	2.9	11.6 *					
Gl 909.1	23 50 05	-06 16.3	0.460	92.0	-28.8	K4	9.53	1.08	1.02	+0.53C	45.1	13.6	31.0	06. r	6.99	-61	-44	9	223782	BD-06 6308
Gl 910	23 50 36	+28 44.4	0.150	290.0	1.3	dM0 e	9.74	1.39	1.25	0.59	60.4	15.3	52.0	08. r	8.32	9	8	6		BD+28 4660
NN	23 51 28	-41 49.4	0.536	112.3		M4	13.3 *			1.07			39.0	10. r	11.3 *					
NN	23 51 38	+51 24.4	0.260	76.0		m	13.52			1.17			45.0	09. r	11.79					
NN	23 51 54	+07 53.0	0.297	261.0		M3:	13.01	1.50		1.10			43.0	09. r	11.18					
Gl 911	23 52 12	-22 03.3	0.132	344.8	18	dM0.5	10.87	1.47	1.22	0.72	39.7	7.9	39.7	7.9	8.86	-1	19	-15		BD-22 6219
NN	23 52 29	+28 21.3	0.578	86.3	-18.1 SB	K1 V	7.38	1.01	0.66	0.48	34.0	8.6	34.0	8.6	5	-68	-47	-3	224085	BD+27 4642

Name	RA(1950)	Dec(1950)	pm	angle	v_{rad}	Sp Type	m_V	B–V	U–B	R–I	π_{trig}	σ	π_{res}	σ	M_V	U	V	W	HD	DM
NN	23 52 50	-04 15.8	0.520	88.2		m	13.95			1.19			40.0	08. r	11.96					
Gl 912	23 53 07	-06 24.9	0.580	232.4		M2	11.15	1.48	1.14	0.98	62.3	18.9	69.0	16. r	10.3					BD-06 6318
NN	23 53 35	-39 19.7	0.285	131.1		K3 V	8.21	0.96					47.0	06. r	6.57				224228	CD-39 15200
NN A	23 54 46	-13 15.5	0.193	84.0		M4	12.93			1.23			56.0	08. r	11.67					
NN B	23 54 45	-13 15.4	0.193	84.0		M4	12.98			1.11			56.0	08. r	11.72					
GJ 1292	23 55 07	+23 02.4	1.460	135.0		k-m	11.72	1.54	1.05	1.14	72.1	2.6	72.1	2.6	11.01					
NN	23 55 11	+19 29.9	0.486	164.0		m	13.01			1.16			55.0	11. r	11.71					
NN	23 55 18	+38 21.2	0.237	225.0		m	12.64			1.13			59.0	12. r	11.49					
NN	23 55 34	+50 10.0	0.251	347.4	-3.2	dG2	6.64	0.66	0.19				47.0	06. r	5	-1	2	25	224465	BD+49 4291
NN	23 55 59	+07 23.1	0.367	166.3		M3	11.74	1.51	1.18	1.10	56.6	2.9	56.6	2.9	10.5					
Gl 913	23 56 07	+46 27.0	0.642	90.3	3.6	dM0.5	9.62	1.44	1.19	0.74	60.0	8.0	60.0	8.0	8.51	-46	-19	-11		BD+45 4378
NN A	23 56 56	+33 26.8	0.107	211.8	-7.6	F8 V	6.47	+0.55 J	-0.06 J		42.1	7.6	36.0	04. r	4.25	13	-7	-5	224635	BD+32 4747
NN	23 57 12	+47 29.2	0.893	103.7		m	16.10	1.87			59.8	8.2	59.8	8.2	14.98					
NN	23 57 12	-44 21.0	0.276	356.0		M7	12.82	1.64		+1.11t			54.0	12. r	11.48					
NN	23 57 14	-34 22.9	0.952	131.1		M4	12.8 *			1.22			78.0	14. r	12.3 *					
GJ 1293	23 58 51	-17 13.4	0.359	132.8	8	dM1.5	10.80	1.40		0.66			39.0	08. r	8.76	-13	-38	-19		BD-17 6862
NN	23 59 21	-37 30.5	0.050	209.5		K1 III	7.06	1.06	0.90		45.5	44.3	45.5	44.3	5.4				224936	CD-37 15469
Wo 9848	23 59 22	+25 44.0	0.696	206.1		K3	11.30	0.94	0.52	0.38	40.8	18.8	40.8	18.8	9.4					
Gl 914 A	23 59 33	+26 49.0	1.305	139.7	-37.6	SB G3 V	5.81	+0.67 J	+0.05 J	+0.31 J	79.6	3.2	79.6	3.2	5.31	-10	-78	-36	224930	BD+26 4734
Gl 914 B	23 59 33	+26 49.0	1.305	139.7		K6 V	9.0 *				79.6	3.2	79.6	3.2	8.5 *					
Gl 915	23 59 34	-43 26.1	0.915	137.7		DA5	13.05	0.07	-0.87	0.16	128.2	6.4	128.2	6.4	13.59					
GJ 1294 A	23 59 34	-68 33.4	0.287	134.7		M0 V	9.66	+1.39 J	+1.18 J	+0.68 J			60.0	12. r	8.55				224953	CD-68 2373
GJ 1294 B	23 59 34	-68 33.4	0.340	140.0			10.6 *						60.0	12. r	9.5 *					