

# *Waveshapping Circuits and Data Converters*

Lesson #19

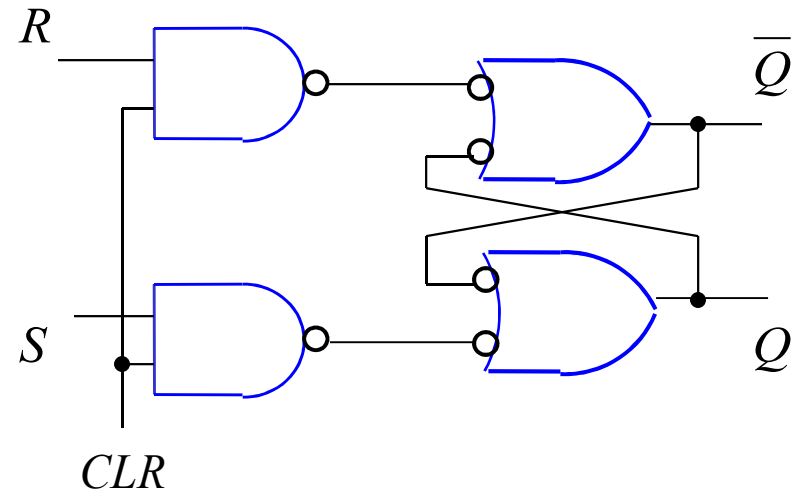
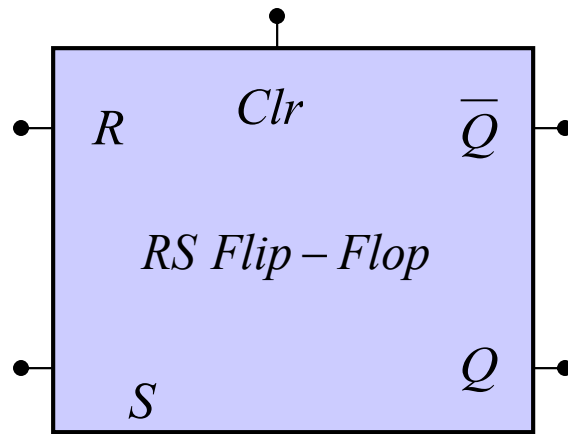
Timers

Section 12.3

## *555 Timer*

- An device introduced by Signetics in 1972
- An economical and convenient way to design multivibrator circuits.
- Consists of voltage divider string, two comparators, a RS flip-flop and a switching transistor
- RS flip-flop is a device which can attain one of two states based on the states of its inputs RS.

# RS Flip-Flop



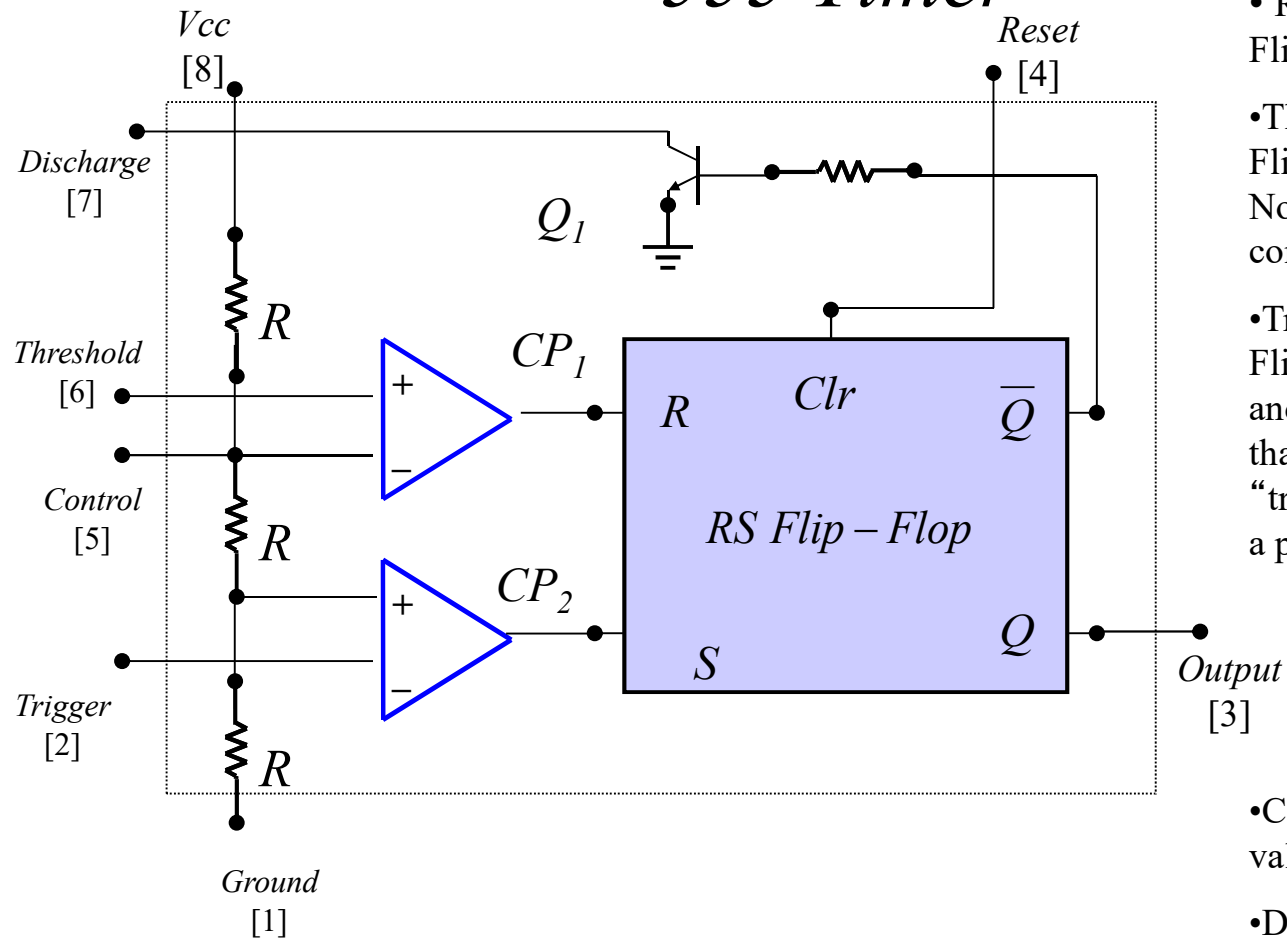
Clr	R	S	Q
0	x	x	0
1	0	0	NC
1	0	1	1
1	1	0	0
1	1	1	?

x - don't care

NC - No Change

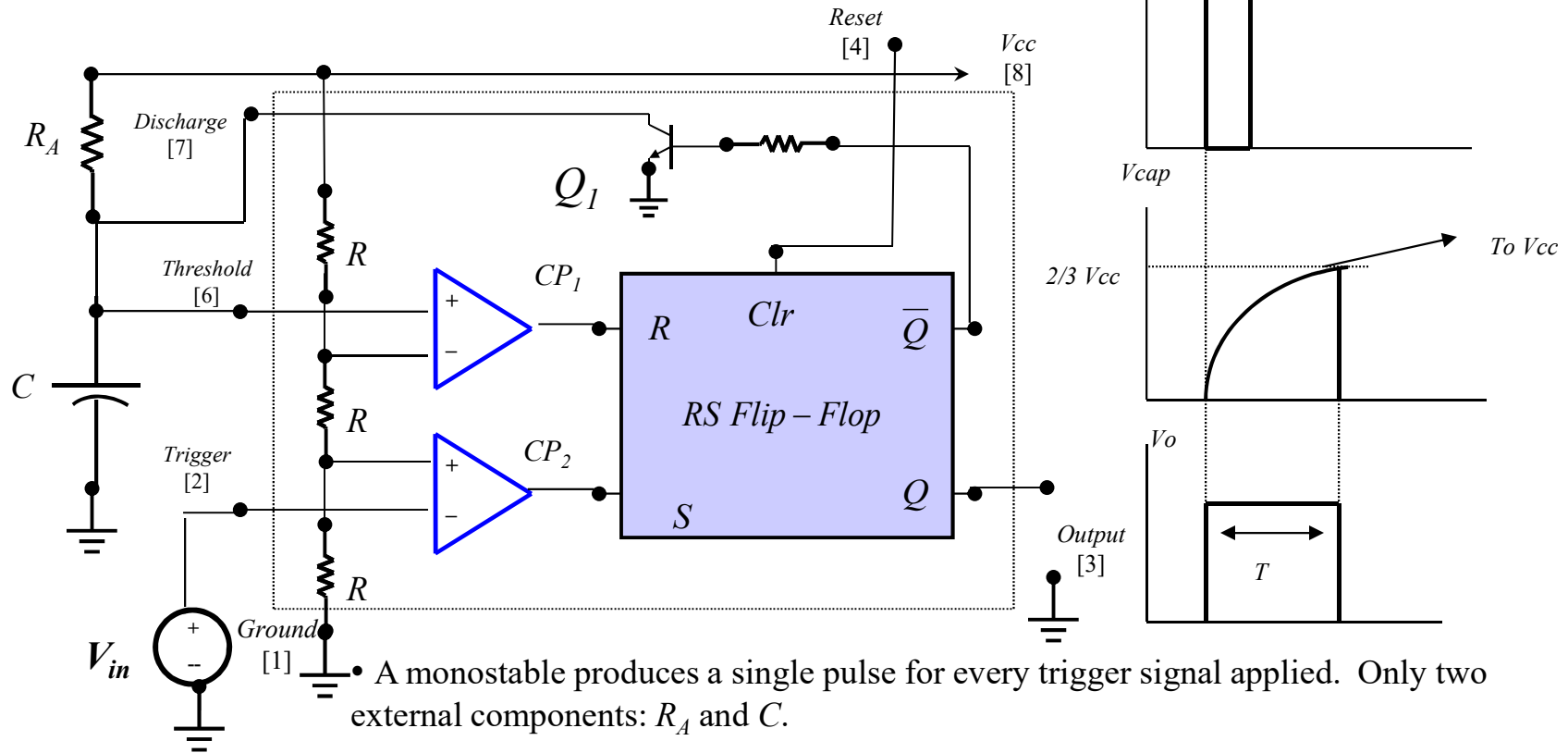
? - indeterminate

# 555 Timer



- Reset – will always reset the Flip-flop and usually set to Vcc
- Threshold – Value  $> 2/3 V_{cc}$  then Flip-flop is RESET,  $Q=0$  and  $\text{Not}Q=1$  and transistor  $Q_1$  conducts
- Trigger – Value  $< 1/3 V_{cc}$  then Flip-flop is SET,  $Q=1$  and  $\text{Not}Q=0$  and transistor  $Q_1$  is cutoff. Note that the Flip-flop will be “triggered” on the falling edge of a pulse applied to this input
- Control – probe to test threshold value
- Discharge – is the  $Q_1$  output and presents a short to ground when  $Q_1$  conducts

# 555 Monostable



$$v_c(t) = K_1 + K_2 e^{-t/R_A C}$$

$$v_c(0) = 0 = K_1 + K_2$$

$$v_c(\infty) = +A = K_1$$

$$v_c(t) = A(1 - e^{-t/R_A C})$$

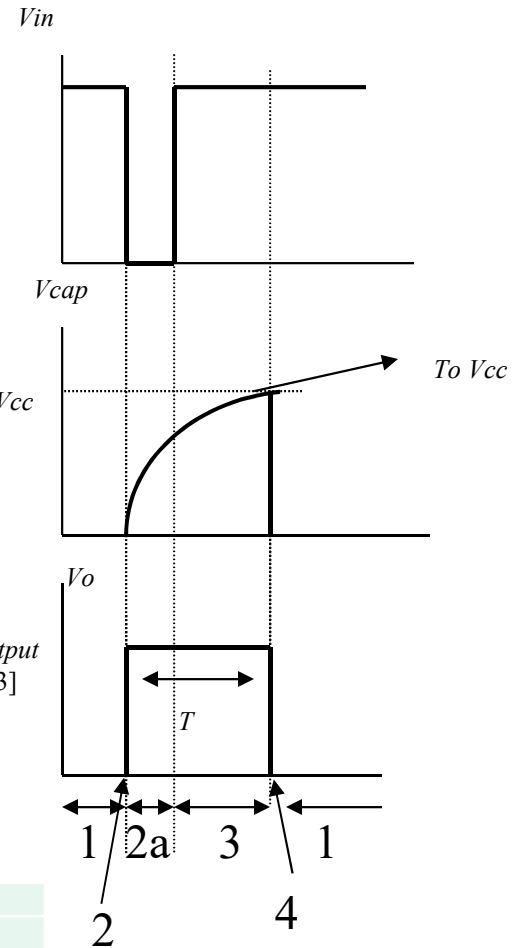
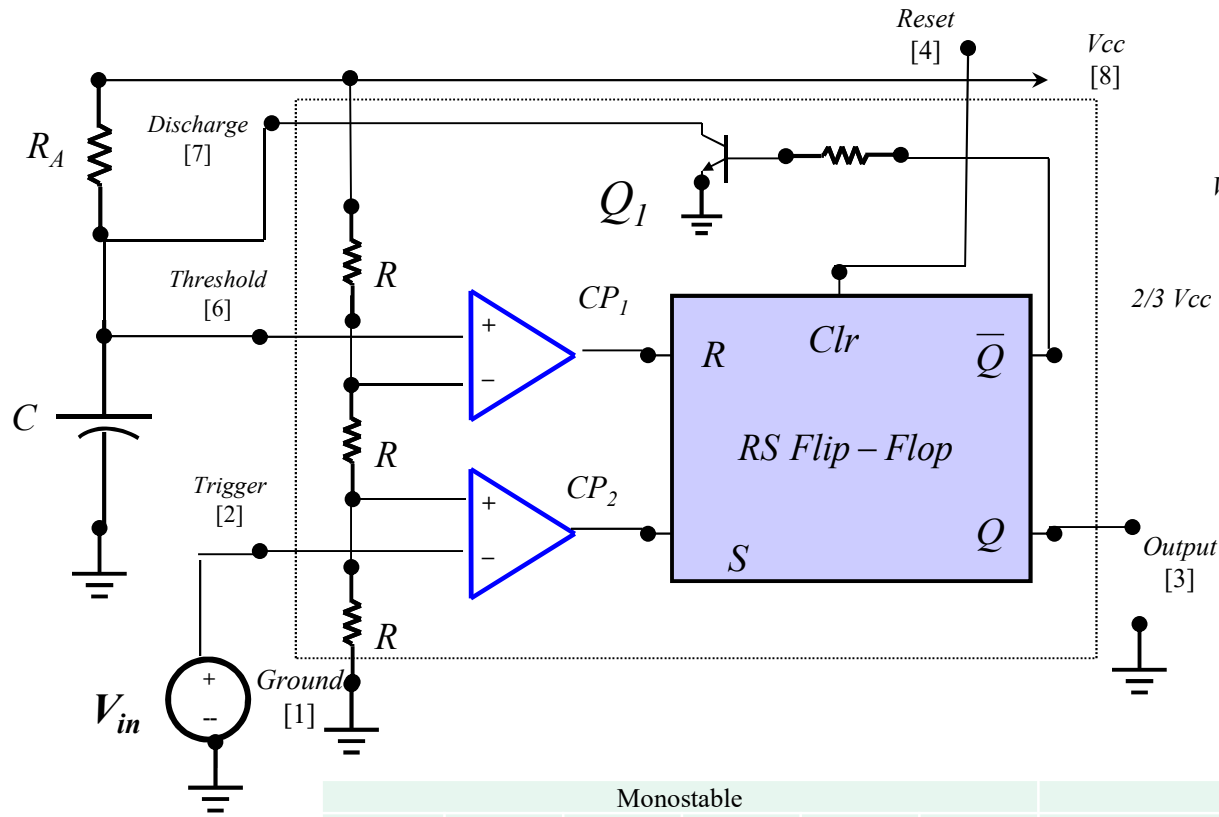
$$v_c(T) = \frac{2A}{3} = A(1 - e^{-T/R_A C})$$

$$\therefore T = R_A C \ln(3)$$

- When the trigger drops below  $1/3 V_{cc}$ , the comparator  $CP_2$  causes the flip-flop to be SET and  $Q_1$  opens and  $C$  begins to charge through  $R_A$ . When the voltage of the capacitor reaches  $2/3 V_{cc}$ , the comparator  $CP_1$  causes the flip-flop to be RESET and  $Q_1$  saturates presents a “zero” resistance to ground for the capacitor to discharge through.

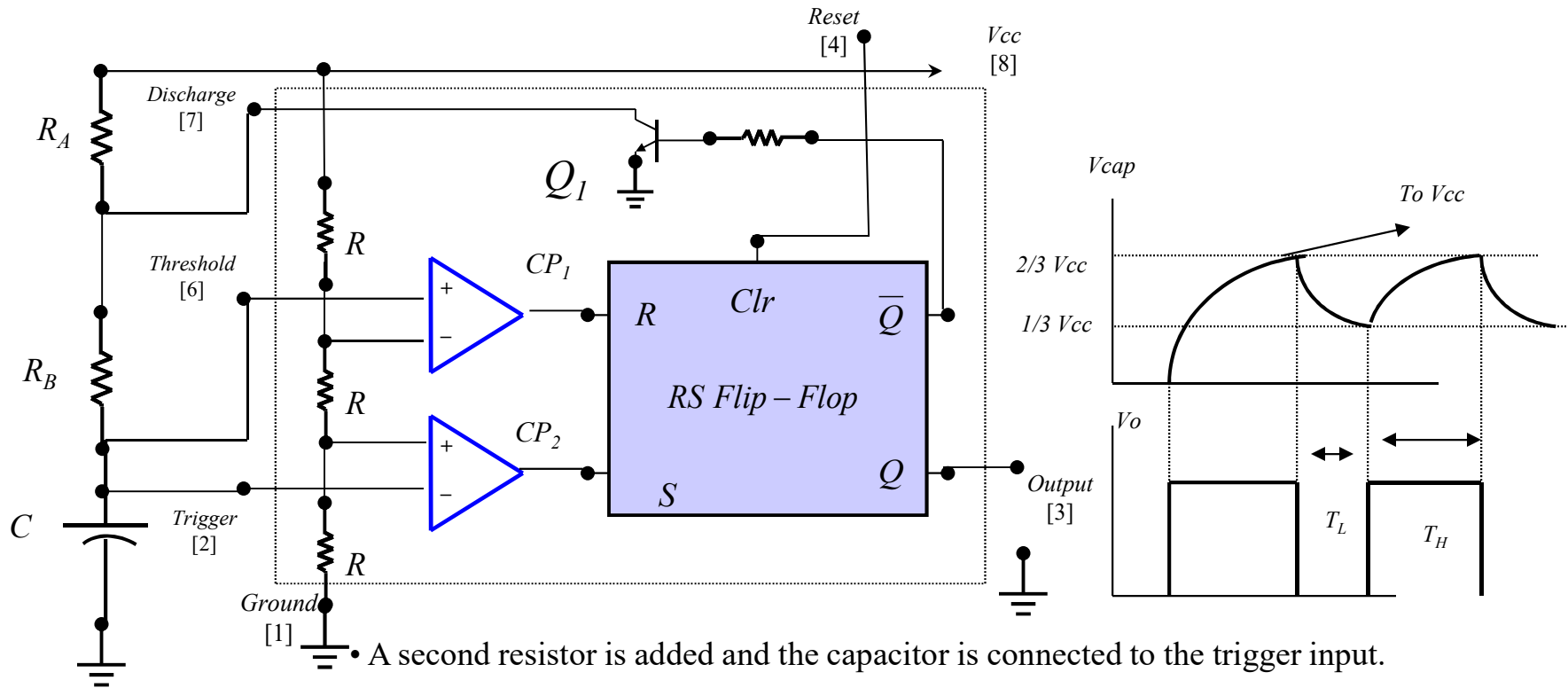
- As a result a single pulse of width  $T = R_A C \ln(3)$  is produced.

# 555 Monostable



Monostable						
State	1	2	2a	3	4	1
Vin	High	Low	Low	High	High	High
S	0	1	1	0	0	0
R	0	0	0	0	1	0
Q	0	1	1	1	0	0
Qnot	1	0	0	0	1	1
Transistor	ON	OFF	OFF	OFF	ON	ON
Vcap	0	0	<2/3 Vcc	<2/3 Vcc	=2/3Vcc	0

# 555 Astable



- At startup the capacitor voltage is less than  $1/3 V_{cc}$ , the flip-flop is SET (via the trigger comparator), Q1 opens and C begins to charge through  $R_A$  and  $R_B$ .
- As the capacitor voltage reaches  $2/3 V_{cc}$ , the flip-flop is RESET (via the threshold comparator), Q1 saturates, and the capacitor starts to discharge through  $R_B$ .
- When the capacitor voltage drops below  $1/3 V_{cc}$ , the flip-flop is SET again, Q1 reopens, and the process restarts again.

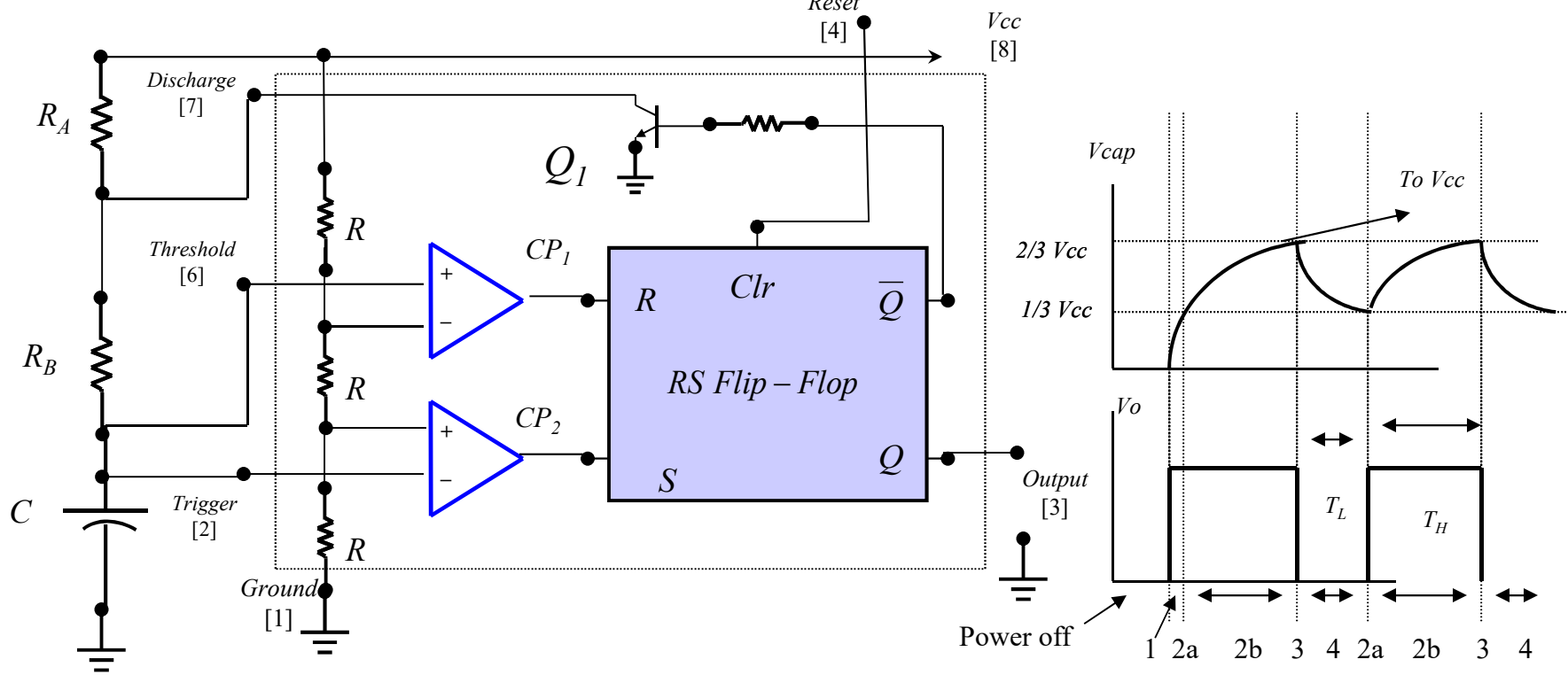
$$T_H = (R_A + R_B)C \ln(2)$$

$$T_L = R_B C \ln(2)$$

$$T = T_H + T_L$$

$$= (R_A + 2R_B)C \ln(2)$$

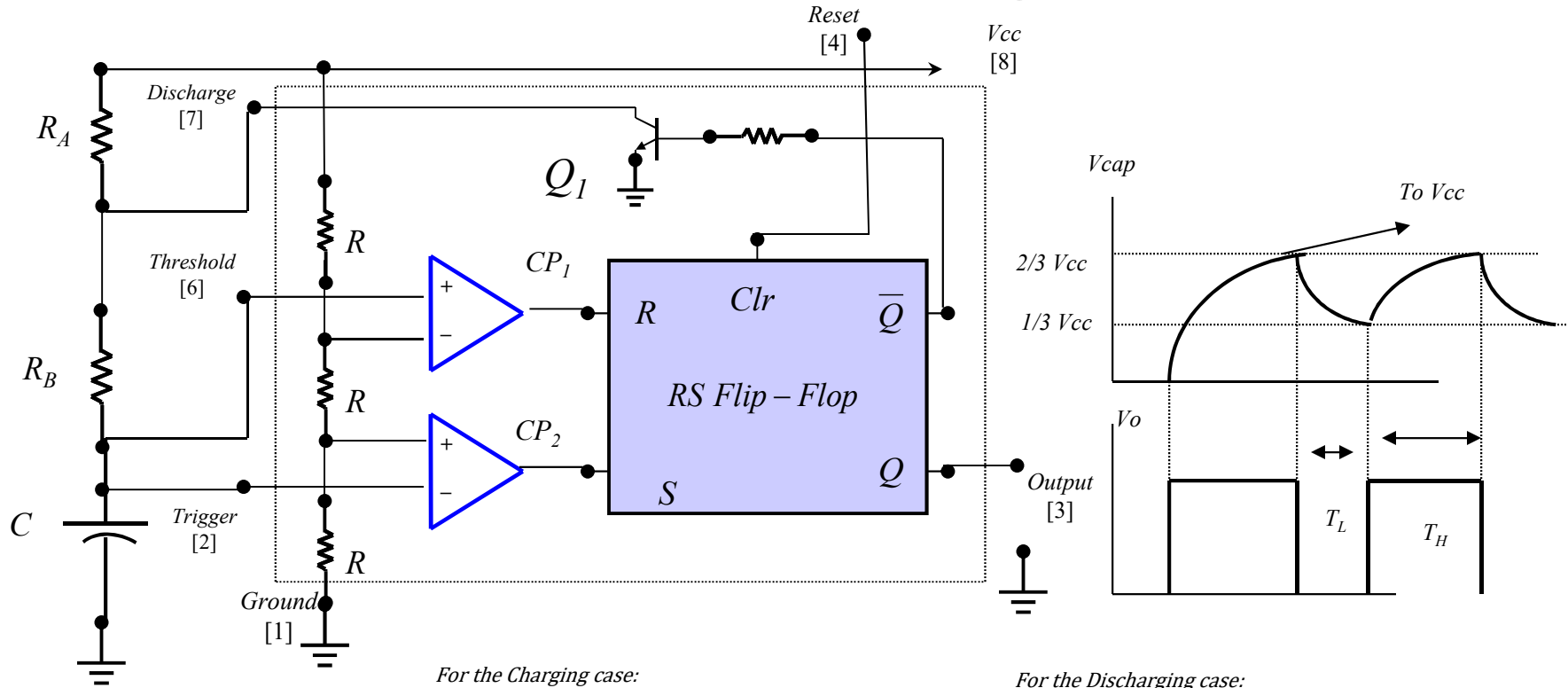
# 555 Astable



Astable									
State	1	2a	2b	3	4	2a	2b	3	4
Vcap	$<1/3V_{cc}$	$=1/3V_{cc}$	$<2/3V_{cc}$	$=2/3V_{cc}$	$<2/3V_{cc}$	$=1/3V_{cc}$	$<2/3V_{cc}$	$=2/3V_{cc}$	$<2/3V_{cc}$
S	1	0	0	0	0	1	0	0	0
R	0	0	0	1	0	0	0	1	0
Q	1	1	1	0	0	1	1	0	0
Qnot	0	0	0	1	1	0	0	1	1
Transistor	OFF	OFF	OFF	ON	ON	OFF	OFF	ON	ON
RC	$(R_A+R_B)C$	$(R_A+R_B)C$	$(R_A+R_B)C$		$R_B C$		$(R_A+R_B)C$		$R_B C$



# 555 Astable Timing



$$T_H = (R_A + R_B)C \ln(2)$$

$$T_L = R_B C \ln(2)$$

$$T = T_H + T_L$$

$$= (R_A + 2R_B)C \ln(2)$$

For the Charging case:

$$V_c(t) = K_1 + K_2 e^{-\frac{t}{(R_A+R_B)C}}$$

$$V_c(0) = \frac{1}{3}V_{CC} = K_1 + K_2$$

$$V_c(\infty) = V_{CC} = K_1$$

$$K_2 = \frac{1}{3}V_{CC} - K_1 = -\frac{2}{3}V_{CC}$$

$$V_c(t) = V_{CC} - \frac{2}{3}V_{CC} e^{-\frac{t}{(R_A+R_B)C}}$$

$$V_c(T_H) = \frac{2}{3}V_{CC} = V_{CC} - \frac{2}{3}V_{CC} e^{-\frac{T_H}{(R_A+R_B)C}}$$

$$\frac{1}{2} = e^{-\frac{T_H}{(R_A+R_B)C}}$$

For the Discharging case:

$$V_c(t) = K_1 + K_2 e^{-\frac{t}{R_B C}}$$

$$V_c(0) = \frac{2}{3}V_{CC} = K_1 + K_2$$

$$V_c(\infty) = 0 = K_1$$

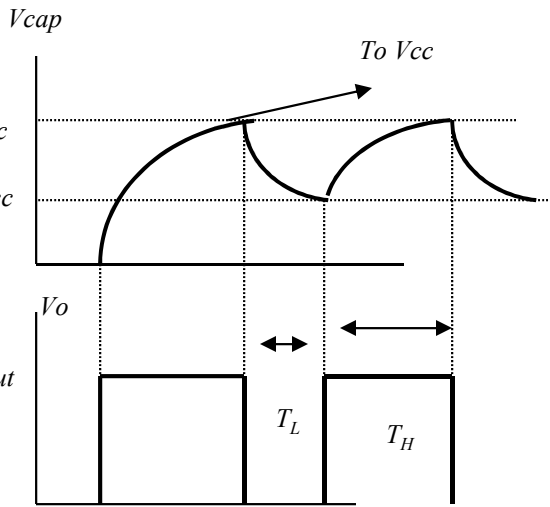
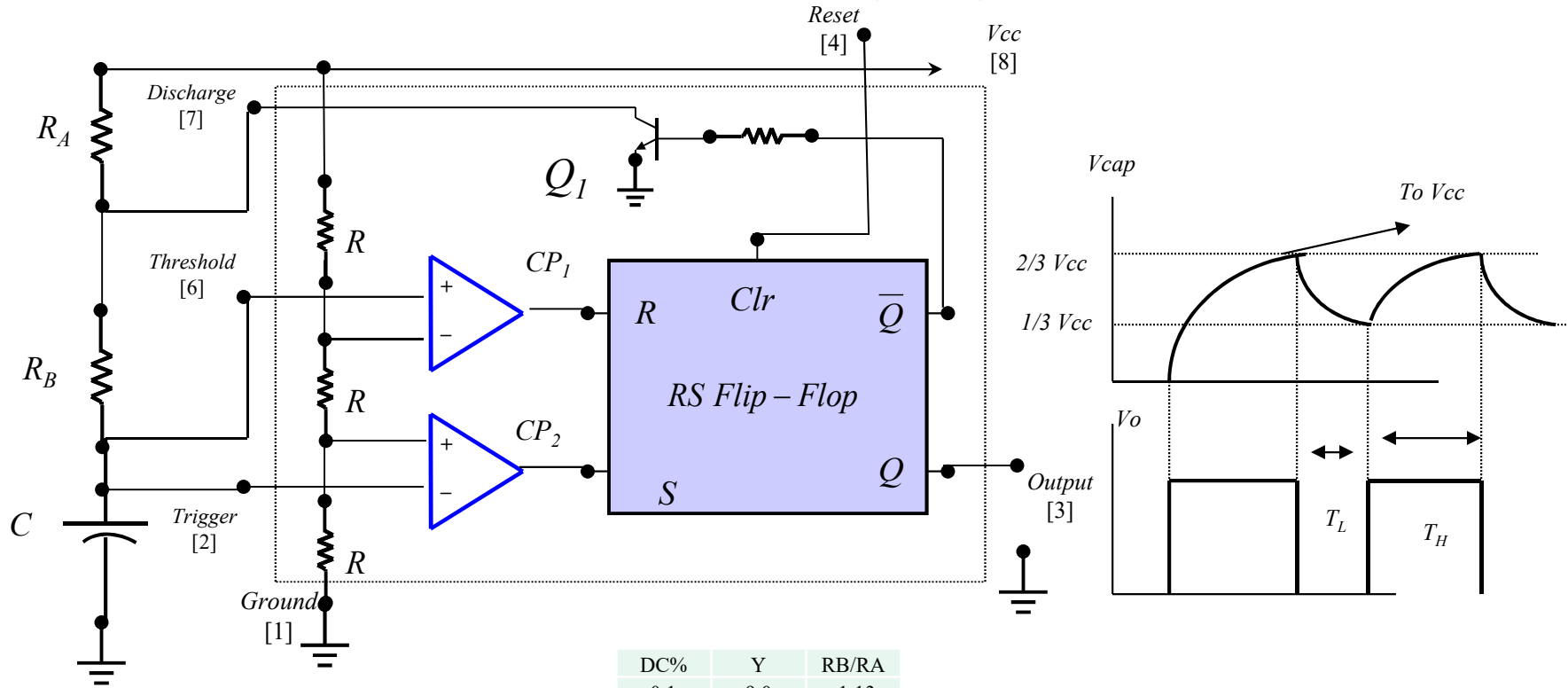
$$K_2 = \frac{2}{3}V_{CC}$$

$$V_c(t) = \frac{2}{3}V_{CC} e^{-\frac{t}{R_B C}}$$

$$V_c(T_L) = \frac{1}{3}V_{CC} = \frac{2}{3}V_{CC} e^{-\frac{T_L}{R_B C}}$$

$$\frac{1}{2} = e^{-\frac{T_L}{R_B C}}$$

# 555 Astable Duty Cycle



The Duty Cycle:

$$DC\% = \frac{R_A + R_B}{R_A + 2R_B} = \frac{R_A + R_B}{R_A + R_B + R_B} = \frac{1}{1 + \frac{R_B}{R_A + R_B}}$$

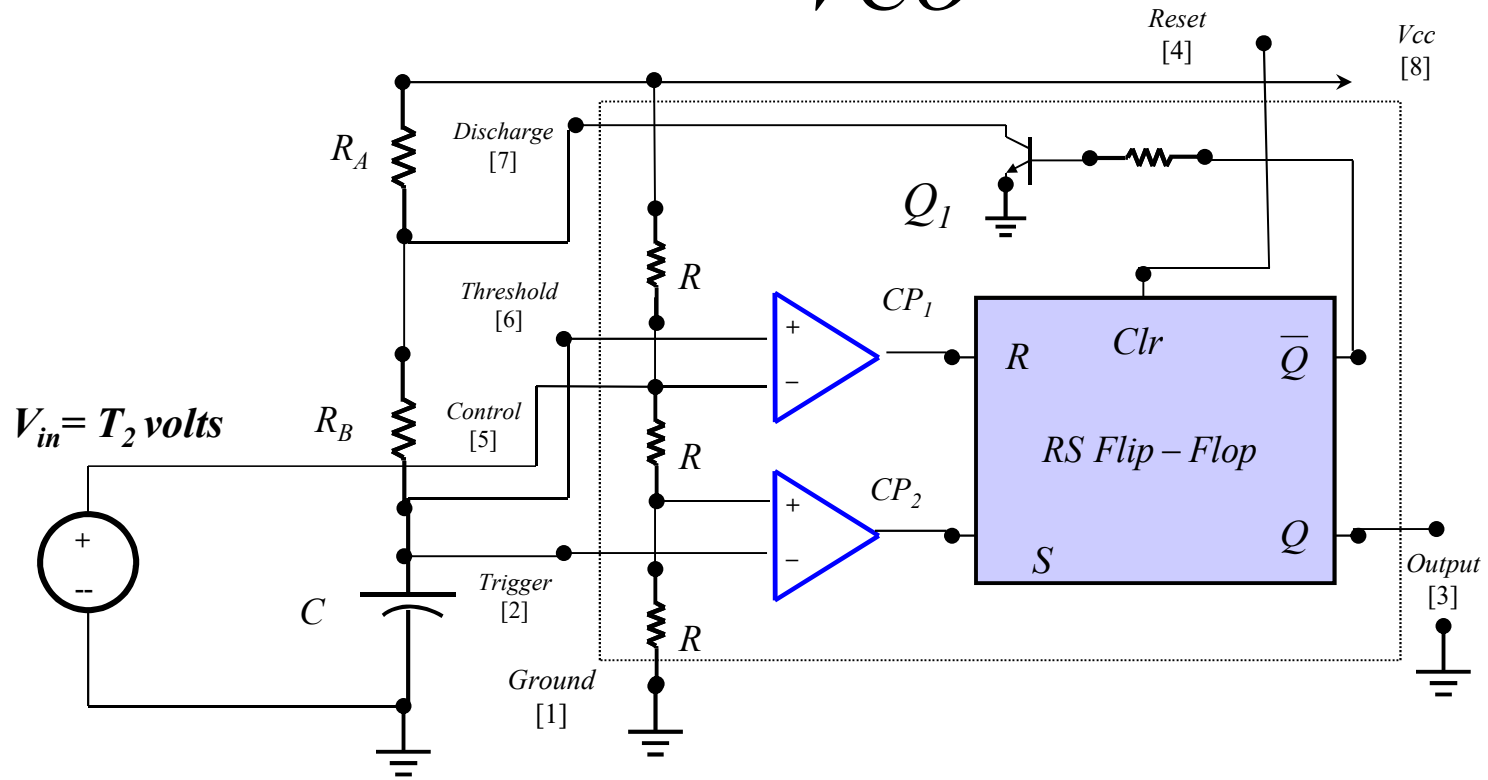
$$\frac{R_B}{R_A + R_B} = 1 - \frac{1}{DC\%} = Y$$

$$\frac{R_B}{R_A} = \frac{Y}{1 - Y}$$

DC%	Y	RB/RA
0.1	9.0	-1.13
0.2	4.0	-1.33
0.3	2.3	-1.75
0.4	1.5	-3.00
0.5	1.0	#DIV/0!
0.6	0.7	2.00
0.7	0.4	0.75
0.8	0.3	0.33
0.9	0.1	0.13
1	0.0	0.00

Note that for Duty Cycle  $\leq 0.5$  there is no solution. Also note that for Duty Cycle = 0.51,  $R_B/R_A = 24.5$ .

# VCO



# VCO

$$v_c(t) = K_1 + K_2 e^{-\frac{t}{(R_A + R_B)C}}$$

Low To High

$$v_c(0) = K_1 + K_2 = T_1$$

$$v_c(\infty) = K_1 = V_{CC}; K_2 = T_1 - V_{CC}$$

$$v_c(T_H) = V_{CC} + (T_1 - V_{CC})e^{-\frac{T_H}{(R_A + R_B)C}} = T_2$$

$$(T_1 - V_{CC})e^{-\frac{T_H}{(R_A + R_B)C}} = T_2 - V_{CC};$$

$$e^{-\frac{T_H}{(R_A + R_B)C}} = \frac{T_2 - V_{CC}}{T_1 - V_{CC}}$$

$$-\frac{T_H}{(R_A + R_B)C} = \ln\left(\frac{T_2 - V_{CC}}{T_1 - V_{CC}}\right)$$

$$T_H = (R_A + R_B)C \ln\left(\frac{V_{CC} - T_1}{V_{CC} - T_2}\right)$$

$$T_2 = xV_{CC}; T_2 = 2T_1$$

$$T_H = (R_A + R_B)C \ln\left(\frac{1 - 0.5x}{1 - x}\right)$$

$$v_c(t) = K_1 + K_2 e^{-\frac{t}{R_B C}}$$

High To Low

$$v_c(0) = K_1 + K_2 = T_2$$

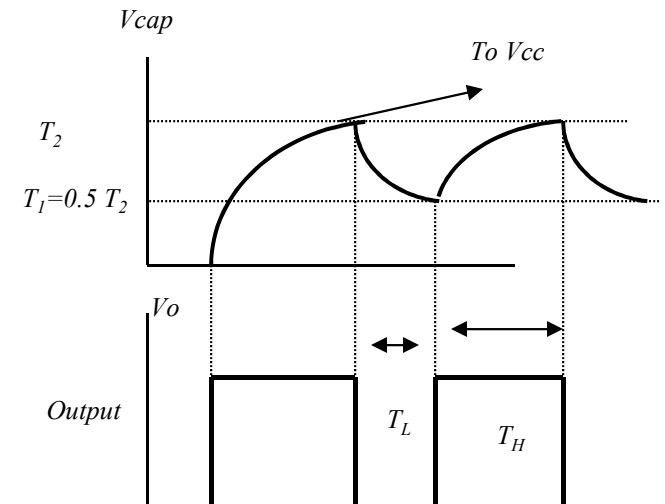
$$v_c(\infty) = K_1 = 0; K_2 = T_2$$

$$v_c(T_L) = T_2 e^{-\frac{T_L}{R_B C}} = T_1$$

$$T_2 e^{-\frac{T_L}{R_B C}} = T_1;$$

$$e^{-\frac{T_L}{R_B C}} = \frac{T_1}{T_2} = \frac{1}{2}$$

$$T_L = R_B C \ln(2)$$



# VCO

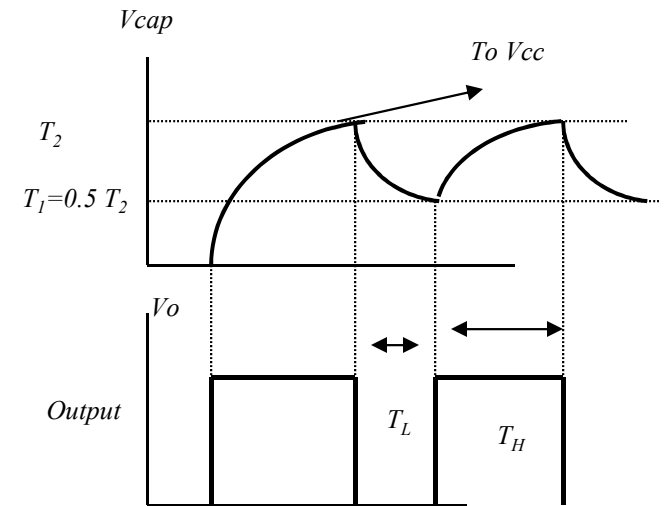
$$T = T_L + T_H$$

$$T_H = (R_A + R_B)C \ln\left(\frac{1 - 0.5x}{1 - x}\right)$$

$$T_L = R_B C \ln(2)$$

$$\begin{aligned} T &= R_B C \ln(2) + (R_A + R_B)C \ln\left(\frac{1 - 0.5x}{1 - x}\right) \\ &= R_B C \ln(2) + (R_A + R_B)C \frac{\ln\left(\frac{1 - 0.5x}{1 - x}\right)}{\ln(2)} \ln(2) \\ &= [R_B + (R_A + R_B)\lambda(x)]C \ln(2) \end{aligned}$$

$$\lambda(x) = \frac{\ln\left(\frac{1 - 0.5x}{1 - x}\right)}{\ln(2)}$$



# VCO

Standard Astable

$$T_{\text{stand}} = R_B C \ln(2) + (R_A + R_B) C \ln(2); f_{\text{stand}} = \frac{1}{[2R_B + R_A] C \ln(2)}$$

VCO

$$T_{VCO} = R_B C \ln(2) + (R_A + R_B) C \ln\left(\frac{1-0.5x}{1-x}\right); f_{VCO} = \frac{1}{[R_B + (R_A + R_B)\lambda(x)] C \ln(2)}$$

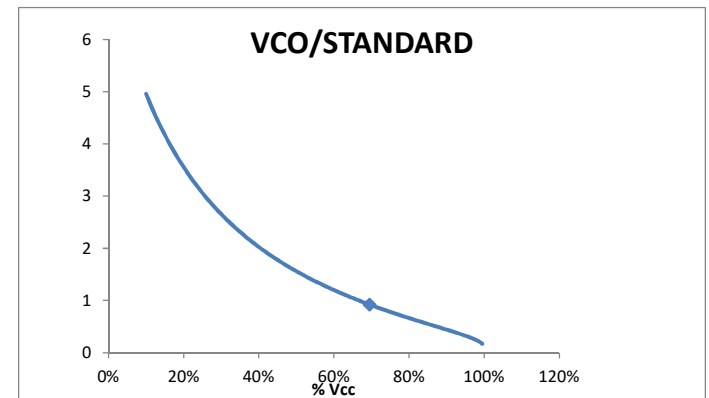
$$\frac{f_{VCO}}{f_{\text{stand}}} = \frac{\frac{1}{[R_B + (R_A + R_B)\lambda(x)] C \ln(2)}}{\frac{1}{[2R_B + R_A] C \ln(2)}}$$

$$= \frac{[2R_B + R_A] C \ln(2)}{[R_B + (R_A + R_B)\lambda(x)] C \ln(2)} = \frac{[2R_B + R_A] C \ln(2)}{[R_B + (R_A + R_B)\lambda(x)] C \ln(2)}$$

$$\lambda(x) = \frac{\ln\left(\frac{1-0.5x}{1-x}\right)}{\ln(2)}$$

When  $\lambda = 1$ , then  $f_{VCO} = f_{\text{stand}}$

$$\lambda(x) = 1 = \frac{\ln\left(\frac{1-0.5x}{1-x}\right)}{\ln(2)} \Rightarrow \frac{1-0.5x}{1-x} = 2 \Rightarrow x = \frac{2}{3}$$



# VCO

Standard Astable

$$T_{\text{stand}} = R_B C \ln(2) + (R_A + R_B) C \ln(2); f_{\text{stand}} = \frac{1}{[2R_B + R_A] C \ln(2)}$$

VCO

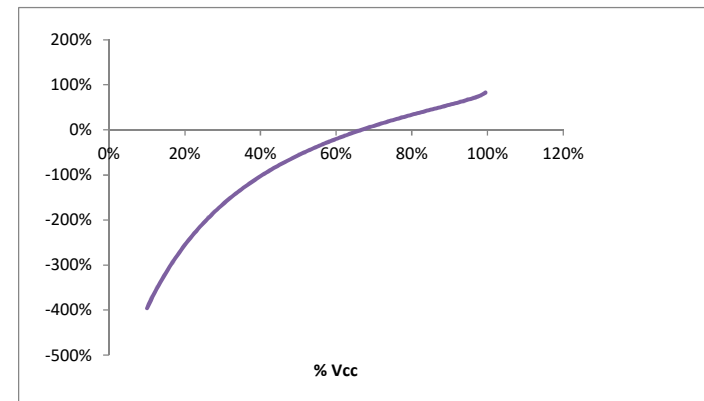
$$T_{VCO} = R_B C \ln(2) + (R_A + R_B) C \ln\left(\frac{1 - 0.5x}{1 - x}\right); f_{VCO} = \frac{1}{[R_B + (R_A + R_B)\lambda(x)] C \ln(2)}$$

$$\% \text{ Change} = \frac{f_{\text{stand}} - f_{VCO}}{f_{\text{stand}}} = \frac{\frac{1}{[2R_B + R_A] C \ln(2)} - \frac{1}{[R_B + (R_A + R_B)\lambda(x)] C \ln(2)}}{\frac{1}{[2R_B + R_A] C \ln(2)}}$$

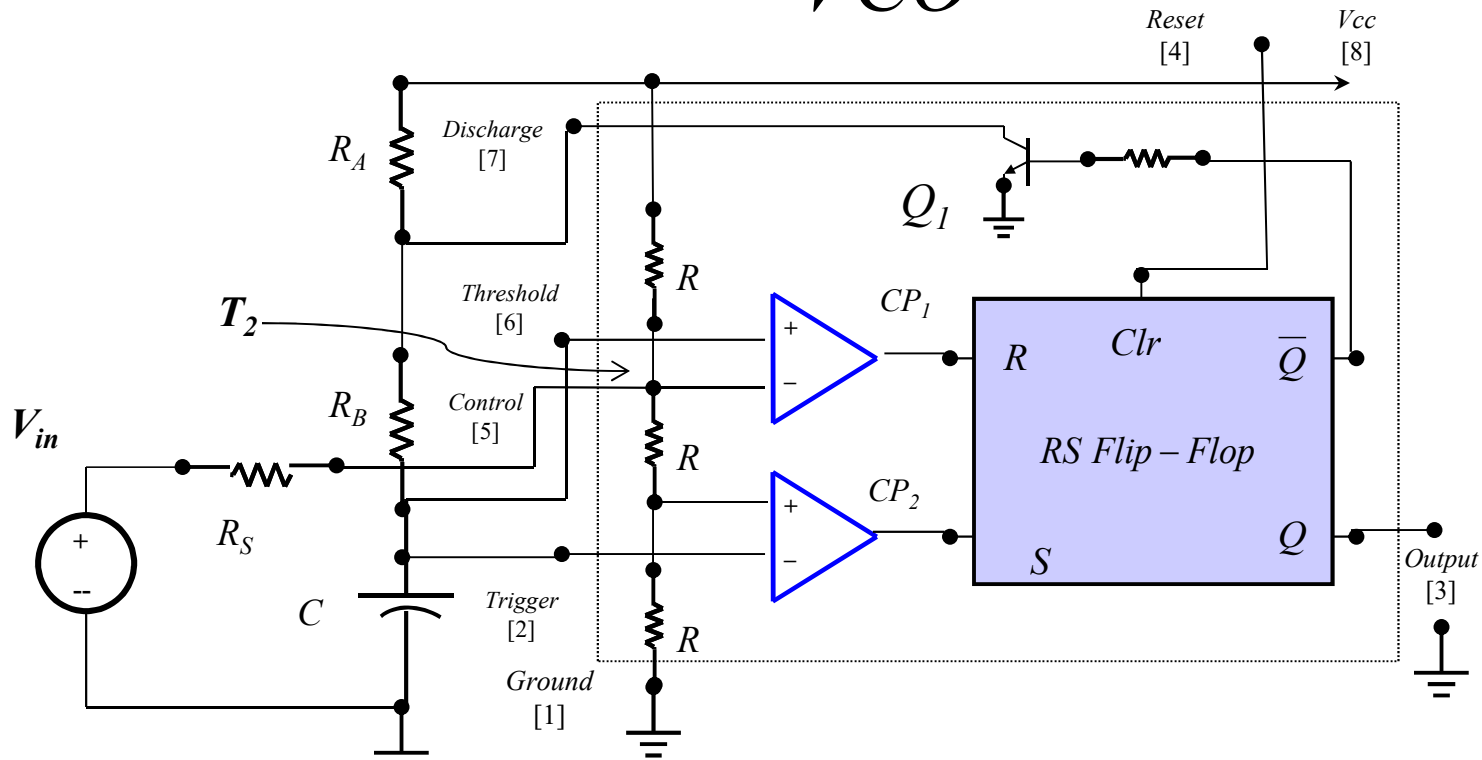
$$= \frac{\frac{1}{[2R_B + R_A]} - \frac{1}{[R_B + (R_A + R_B)\lambda(x)]}}{\frac{1}{[2R_B + R_A]}}$$

$$= 1 - \frac{[2R_B + R_A]}{[R_B + (R_A + R_B)\lambda(x)]}$$

$$\lambda(x) = \frac{\ln\left(\frac{1 - 0.5x}{1 - x}\right)}{\ln(2)}$$



# VCO



$$\frac{T_2 - V_{in}}{R_s} + \frac{T_2 - V_{cc}}{R} + \frac{T_2}{2R} = 0$$

$$T_2 \left( \frac{1}{R_s} + \frac{1}{R} + \frac{1}{2R} \right) = \frac{V_{in}}{R_s} + \frac{V_{cc}}{R}$$

$$T_2 = \frac{RV_{in} + R_s V_{cc}}{R + \frac{3}{2}R_s}; V_{in} = xV_{cc}$$

$$T_2 = \left( \frac{Rx + R_s}{R + \frac{3}{2}R_s} \right) V_{cc}$$



# VCO

$$v_c(t) = K_1 + K_2 e^{-\frac{t}{(R_A + R_B)C}}$$

Low To High

$$v_c(0) = K_1 + K_2 = T_1$$

$$v_c(\infty) = K_1 = V_{CC}; K_2 = T_1 - V_{CC}$$

$$v_c(T_H) = V_{CC} + (T_1 - V_{CC}) e^{-\frac{T_H}{(R_A + R_B)C}} = T_2$$

$$(T_1 - V_{CC}) e^{-\frac{T_H}{(R_A + R_B)C}} = T_2 - V_{CC};$$

$$e^{-\frac{T_H}{(R_A + R_B)C}} = \frac{T_2 - V_{CC}}{T_1 - V_{CC}}$$

$$-\frac{T_H}{(R_A + R_B)C} = \ln\left(\frac{T_2 - V_{CC}}{T_1 - V_{CC}}\right)$$

$$T_H = (R_A + R_B)C \ln\left(\frac{V_{CC} - T_1}{V_{CC} - T_2}\right)$$

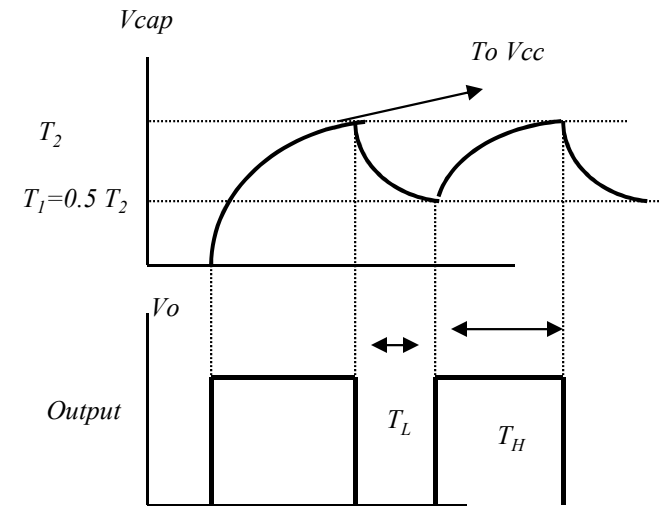
$$T_2 = \left(\frac{Rx + R_s}{R + \frac{3}{2}R_s}\right)V_{CC}; T_2 = 2T_1; T_1 = \left(\frac{Rx + R_s}{2R + 3R_s}\right)V_{CC}$$

$$T_H = (R_A + R_B)C \ln\left(\frac{1 - \left(\frac{Rx + R_s}{2R + 3R_s}\right)}{1 - \left(\frac{Rx + R_s}{R + \frac{3}{2}R_s}\right)}\right) = (R_A + R_B)C \ln\left(\frac{2R + 3R_s - (Rx + R_s)}{2\left[R + \frac{3}{2}R_s - (Rx + R_s)\right]}\right)$$

$$= (R_A + R_B)C \ln\left(\frac{(2-x)R + 2R_s}{2(1-x)R + R_s}\right)$$

where  $R_s = yR$

$$= (R_A + R_B)C \ln\left(\frac{2-x+2y}{2-2x+y}\right)$$



# VCO

$$v_c(t) = K_1 + K_2 e^{-\frac{t}{R_B C}}$$

High To Low

$$v_c(0) = K_1 + K_2 = T_2$$

$$v_c(\infty) = K_1 = 0; K_2 = T_1$$

$$v_c(T_L) = T_1 e^{-\frac{T_L}{R_B C}} = T_2$$

$$T_1 e^{-\frac{T_H}{R_B C}} = T_2;$$

$$e^{-\frac{T_H}{R_B C}} = \frac{T_2}{T_1} = 2$$

$$T_L = R_B C \ln(2)$$

$$T = T_L + T_H$$

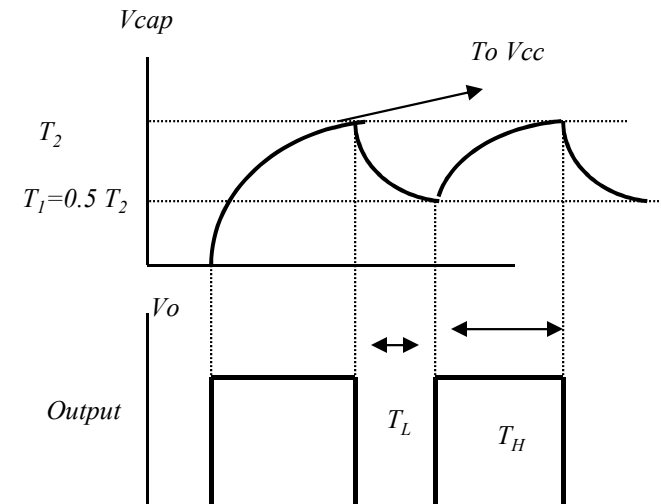
$$T_H = (R_A + R_B) C \ln\left(\frac{2 - x + 2y}{2 - 2x + y}\right)$$

$$T_L = R_B C \ln(2)$$

$$T = R_B C \ln(2) + (R_A + R_B) C \ln\left(\frac{2 - x + 2y}{2 - 2x + y}\right)$$

$$\lambda(x, y) = \frac{\ln\left(\frac{2 - x + 2y}{2 - 2x + y}\right)}{\ln(2)}$$

$$T = [R_B + (R_A + R_B)\lambda(x, y)] C \ln(2)$$



# VCO

Standard Astable

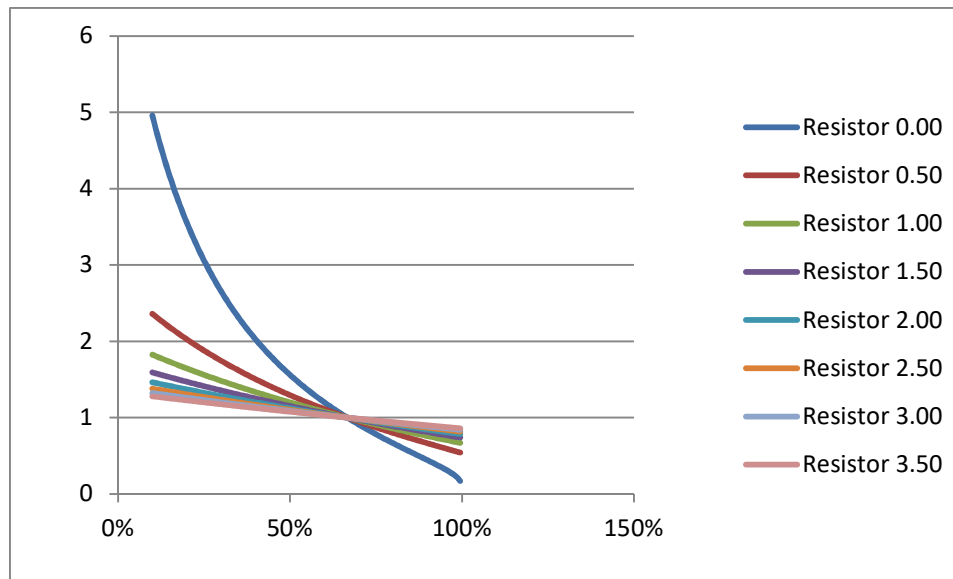
$$T_{\text{stand}} = R_B C \ln(2) + (R_A + R_B) C \ln(2); f_{\text{stand}} = \frac{1}{[2R_B + R_A] C \ln(2)}$$

VCO

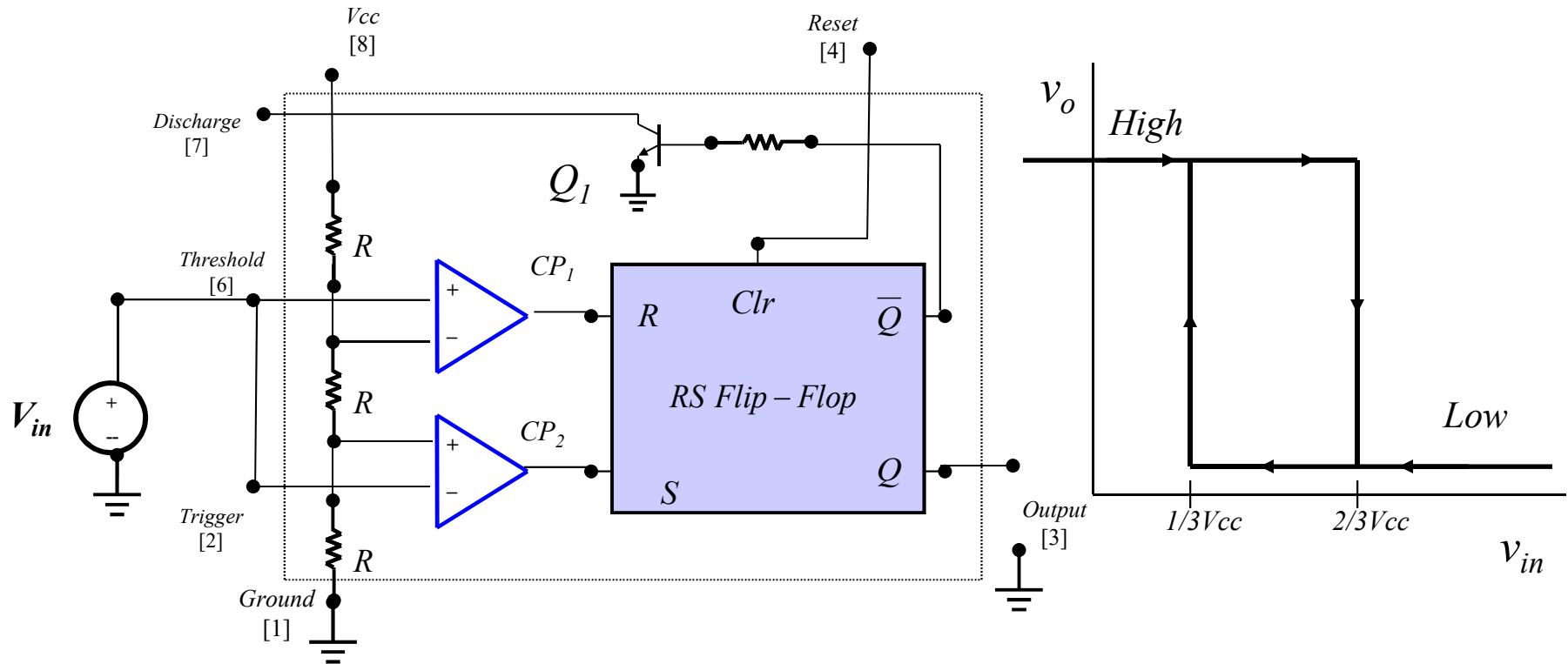
$$T_{VCO} = [R_B + (R_A + R_B)\lambda(x, y)] C \ln(2); f_{VCO} = \frac{1}{[R_B + (R_A + R_B)\lambda(x, y)] C \ln(2)}$$

$$\lambda(x, y) = \frac{\ln\left(\frac{2-x+2y}{2-2x+y}\right)}{\ln(2)}$$

$$\begin{aligned} \% \text{ Change} &= \frac{f_{\text{stand}} - f_{VCO}}{f_{\text{stand}}} = \frac{\frac{1}{[2R_B + R_A] C \ln(2)} - \frac{1}{[R_B + (R_A + R_B)\lambda(x, y)] C \ln(2)}}{\frac{1}{[2R_B + R_A] C \ln(2)}} \\ &= \frac{\frac{1}{[2R_B + R_A]} - \frac{1}{[R_B + (R_A + R_B)\lambda(x, y)]}}{\frac{1}{[2R_B + R_A]}} \\ &= 1 - \frac{[2R_B + R_A]}{[R_B + (R_A + R_B)\lambda(x, y)]} \end{aligned}$$



# 555 Schmitt Trigger



Schmitt Trigger				
State	$V_{in}$ going from 0 to $V_{cc}$			
$V_{in}$	$<1/3V_{cc}$	$=1/3V_{cc}+$	$=2/3V_{cc}+$	$>2/3V_{cc}$
CP2	High	Low	Low	Low
Set	1	0	0	0
CP1	Low	Low	High	High
Reset	0	0	1	1
Q	High	NC	Low	Low
Qnot	Low	NC	High	High

Schmitt Trigger				
State	$V_{in}$ going from $V_{cc}$ to 0			
$V_{in}$	$>2/3V_{cc}$	$<2/3V_{cc}$	$=1/3V_{cc}-$	$<1/3V_{cc}$
CP2	Low	Low	High	High
Set	0	0	1	1
CP1	High	Low	Low	Low
Reset	1	0	0	0
Q	Low	NC	High	High
Qnot	High	NC	Low	Low

# *Homework*

- 555 Timer
  - Problems: 12.18-20