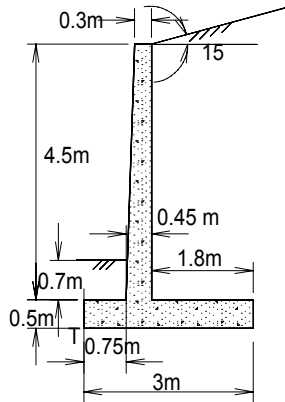


Example 1

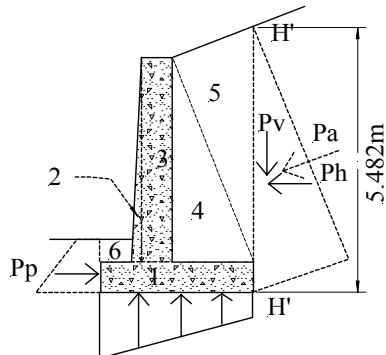
Check the retaining wall safety for overturning, sliding, and bearing capacity. Stem: top = 0.30 m, bottom = 0.45 m, length = 4.5 m. Base: thickness = 0.5 m, length = 3 m, front projection = 0.75 m, footing's bottom 1.2 m below ground, $\gamma_{\text{conc}} = 23.58 \text{ kN/m}^3$. For underlying soil and soil in front of the wall use $\phi = 22^\circ$, $c = 50 \text{ kPa}$, and $\gamma = 19.3 \text{ kN/m}^3$. Backfill $\phi = 30^\circ$, $c = 0$, $\delta = 0.67\phi$, slope = 15° , and $\gamma = 18.5 \text{ kN/m}^3$.

Solution



Use 1m length of wall. Consider vertical plane HH'.

$$HH' = 5 + 1.8 \tan 15 = 5.482 \text{ m}$$



Active forces

$$^1K_a = 0.373$$

$$P_a = 18.5 \times 5.482^2 \frac{0.373}{2} = 103.7 \text{ kN}$$

$$P_h = 103.7 \times \cos 15 = 100.2 \text{ kN}$$

$$P_v = 103.7 \times \sin 15 = 26.8 \text{ kN}$$

Passive resistance

$$K_p = 2.2, \quad \sqrt{K_p} = 1.48$$

$$P_p = 19.3 \times 1.2^2 \times 2.2 \div 2 + 2 \times 50 \times 1.2 \times 1.48 = 208.5 \text{ kN}$$

Overturning

¹ See tables in the book

Resisting moments

no	force kN	arm m	M _R about C
1	$0.5 \times 3 \times 23.58 = 35.37$	1.5	53.06
2	$0.15 \times 4.5 \times 23.58 \times 0.5 = 7.96$	$0.75 + 0.15 \times 2/3$	6.76
3	$0.3 \times 4.5 \times 23.58 = 31.83$	$0.75 + 0.15 + 0.15$	33.42
4	$1.8 \times 4.5 \times 18.5 \times 0.5 = 74.93$	$1.2 + 0.6$	134.9
5	$1.8 \times 4.982 \times 18.5 \times 0.5 = 82.95$	$1.2 + 1.2$	199
6	$0.7 \times 0.75 \times 18.5 = 9.71$	$0.75/2$	3.64
P _v	26.83	3	80.49
ΣV	269.6	ΣM _R	511.3

Overturning moment

$$M_0 = 100.2 \times 5.482 \div 3 = 183 \text{ kN-m}$$

$$FS = 511.3/183 = 2.8$$

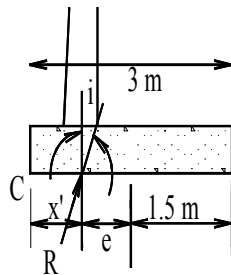
Sliding resistance

$$FS = \frac{\text{horizontal resisting forces}}{\text{horizontal driving forces}} = \frac{\Sigma F_R}{\Sigma F_d} \geq 1.5$$

$$\Sigma F_R = 269.6 \tan(22 \times 2/3) + 50 \times 3 + 208.5 = 429.0$$

$$FS = \frac{429.0}{100.2} = 4.28 \geq 1.5 \text{ This includes passive resistance}$$

Base reaction



$$i = \tan^{-1} \frac{100.2}{269.6} = 20.38^\circ$$

$$R = \sqrt{269.6^2 + 100.2^2} = 287.6 \text{ kN}$$

Take moment about ²toe

$$269.6 \times x' = \text{}^3\Sigma M_R - \Sigma M_0 = 511.3 - 183 = 328.3 \text{ kN-m}$$

$$x' = 1.22 \text{ m}$$

Bearing capacity

$$e = 3/2 - 1.22 = 0.28 \text{ m}$$

² Note horizontal component of R has no moment about toe.

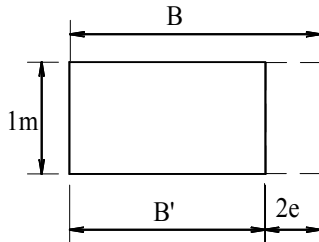
³ Net moment about toe

$$^4q = \frac{\sum V}{A} \left(1 \pm \frac{6e}{B} \right)$$

$$q_{\max} = \frac{269.59}{1 \times 3} \left(1 + \frac{6 \times 0.28}{3} \right) = 140.2 \text{ kPa}$$

$$q_{\min} = 35.5 \text{ kPa}$$

$$B' = 3 - 2 \times 0.28 = 2.44 \text{ m}$$



$$q_{ult} = cN_c F_{cs} F_{cd} F_{ci} + qN_q F_{qs} F_{qd} F_{qi} + 0.5\gamma B N_\gamma F_{\gamma s} F_{\gamma d} F_{\gamma i}$$

For continuous footings shape factors = 1

$$F_{cd} = 1 + 0.4 \frac{1.2}{3} = 1.16$$

$$F_{qd} = 1 + 2 \tan 22^\circ (1 - \sin 22^\circ)^2 \frac{1.2}{3} = 1.13$$

$$F_{\gamma d} = 1$$

$$F_{qi} = F_{ci} = \left(1 - \frac{20.37}{90} \right)^2 = 0.6$$

$$F_{\gamma i} = \left(1 - \frac{20.37}{22} \right)^2 = 0.01$$

$$N_c = 16.88, \quad N_q = 7.82, \quad N_\gamma = 7.13$$

$$q_{ult} = 50 \times 16.88 \times 1.16 \times 0.6 + 1.2 \times 18.5 \times 7.82 \times 1.13 \times 0.6 + 0.5 \times 19.3 \times 2.44 \times 7.13 \times 0.01 = 706.7 \text{ kPa}$$

$$q_0 \text{ (on reduced area)} = 269.59 / 1 \times 2.44 = 110.5 \text{ kPa}$$

$$FS = 706.7 / 110.5 = 6.4$$

$$FS \text{ against } q_{\max} = 706.7 / 140.2 = 5$$

⁴ $e \leq B/6$, else there will be tension on the base, which is not recommended

Semi-empirical Method

For wall heights 20' or less.

1. Determine H' as shown in Figures.
2. Select the appropriate backfill soil type. If not known use type 5.
3. Pressure on wall is assumed to vary linearly with depth
4. $P_h = 0.5 K_h H'^2$ $P_v = 0.5 K_v H'^2$
5. For soil type 5 reduce H' by 4' to compute horizontal and vertical pressures. Resultant is assumed to act still at H'/3 above the base.
6. If wall is designed before backfill material is selected use the most unsuitable material or give alternate design.

Walls on soft compressible layers

Wall settlement will reverse the direction of friction, and Pa will increase. For soils 1, 2, 3 and 5 multiply, Pa, by 1.5.

Example 2

Use empirical method to determine active and passive forces for Example 1. Assume backfill Type 1

Solution

$$\begin{aligned} K_h &= 5.5 \text{ kPa} & K_v &= 1.5 \text{ kPa} \\ P_h &= 0.5 \times 5.2 \times 5.482^2 = 78.14 \text{ kPa} & (101.15 \text{ kPa}) \\ P_v &= 0.5 \times 1.5 \times 5.482^2 = 25.60 \text{ kPa} & (26.83 \text{ kPa}) \end{aligned}$$