

Figures

Figure 1

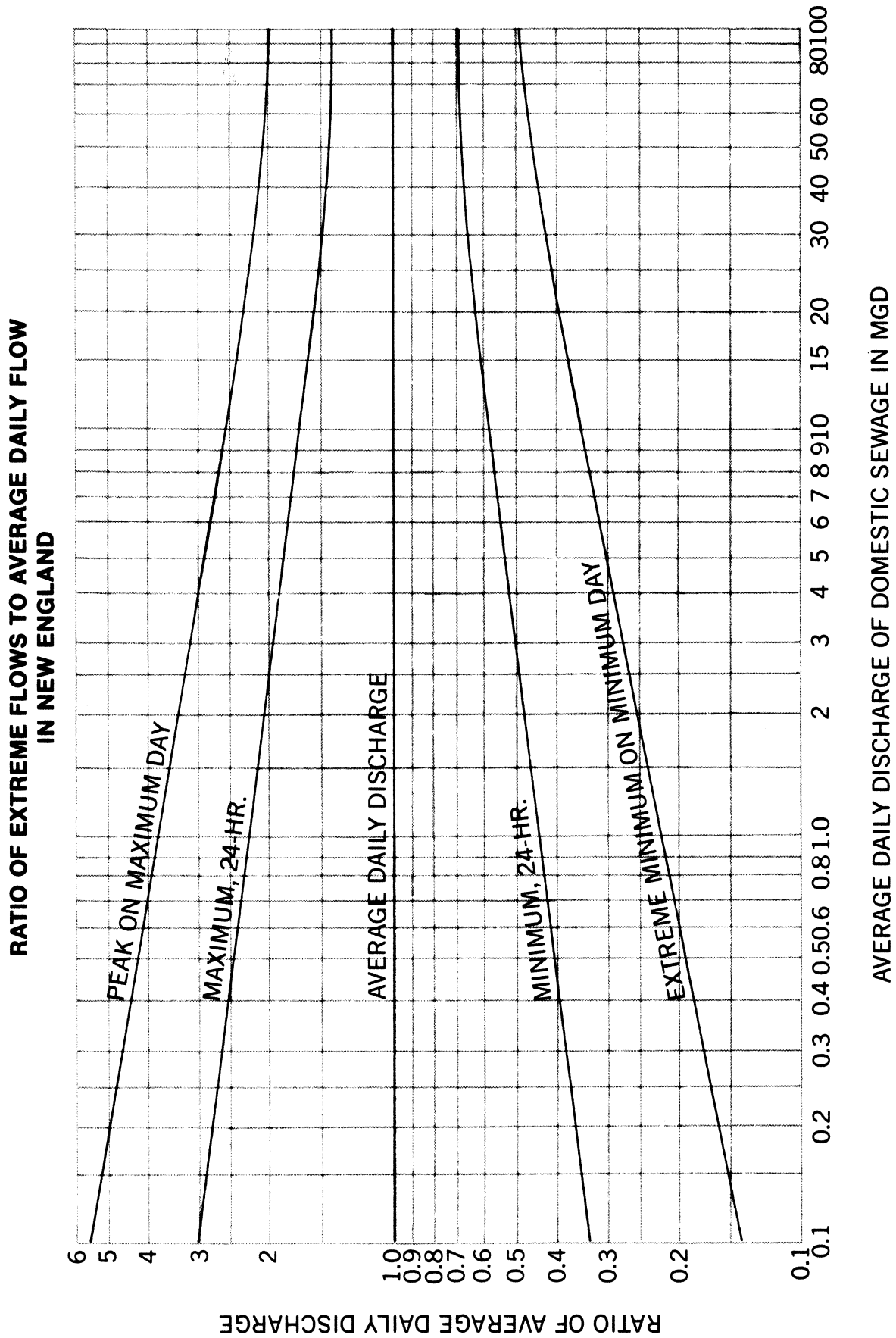


Figure 2

**FLOW FOR CIRCULAR PIPE FLOWING FULL
BASED ON MANNING'S EQUATION $n=0.010$**

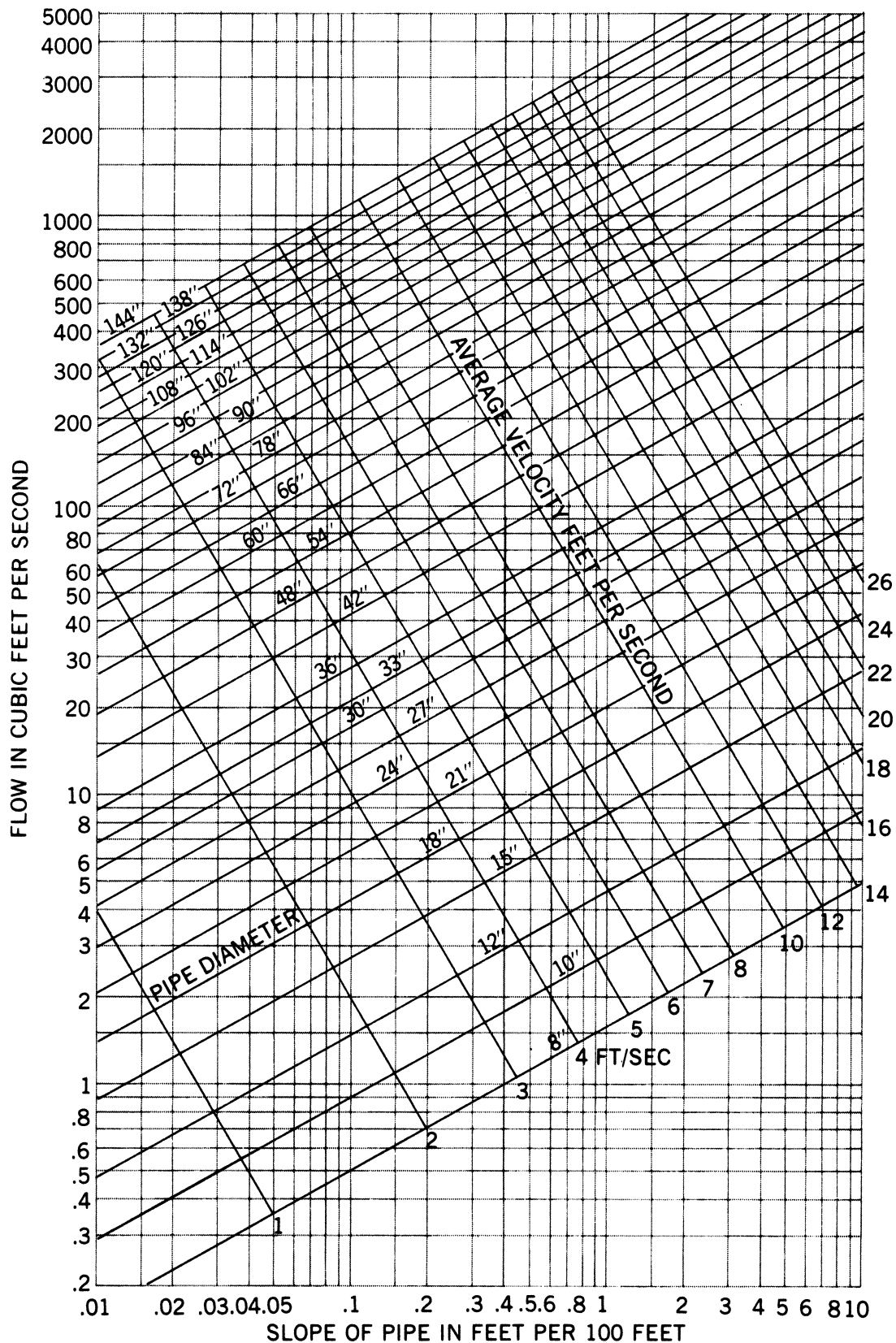


Figure 3

**FLOW FOR CIRCULAR PIPE FLOWING FULL
BASED ON MANNING'S EQUATION $n=0.011$**

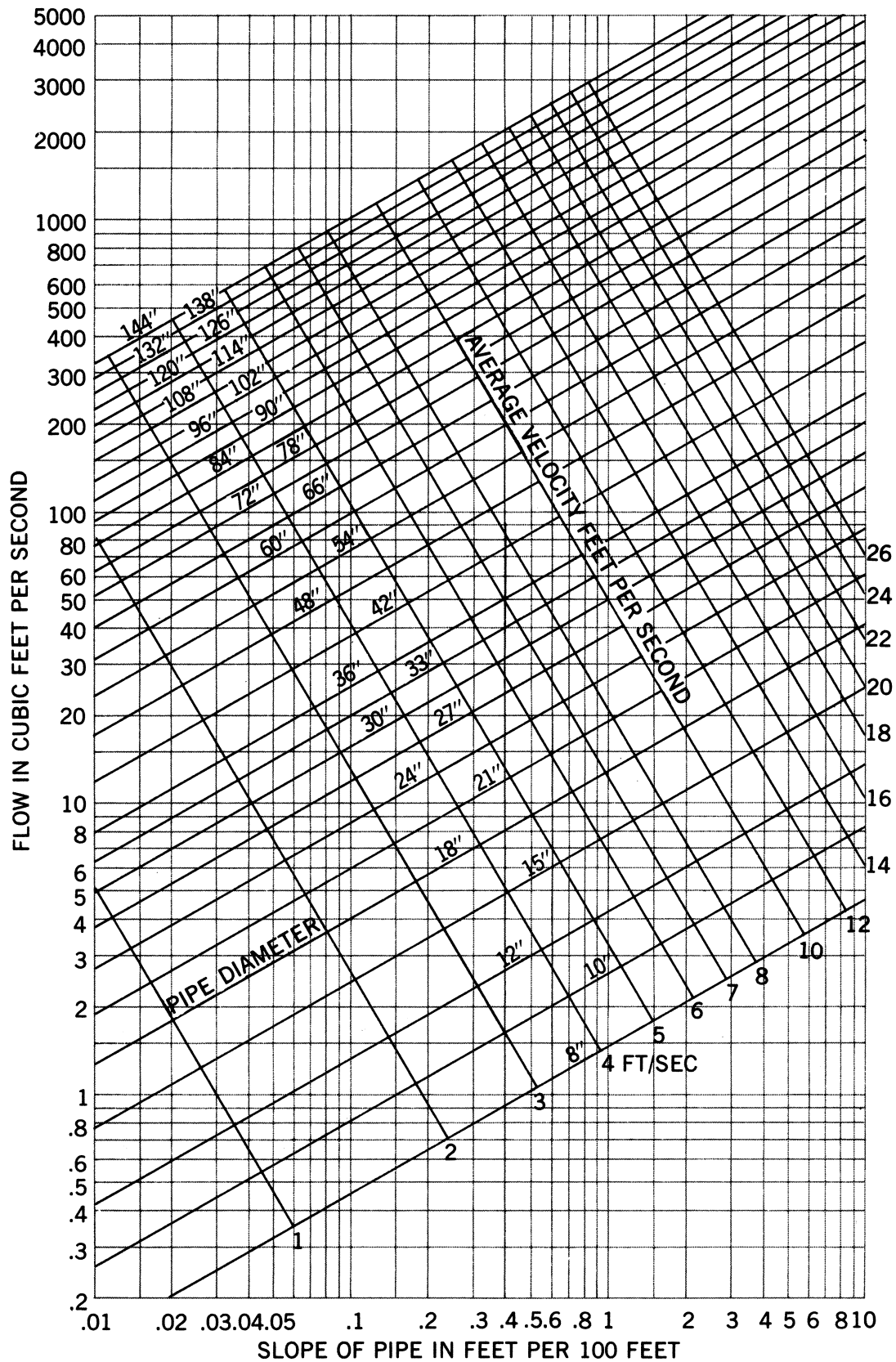


Figure 4

**FLOW FOR CIRCULAR PIPE FLOWING FULL
BASED ON MANNING'S EQUATION $n=0.012$**

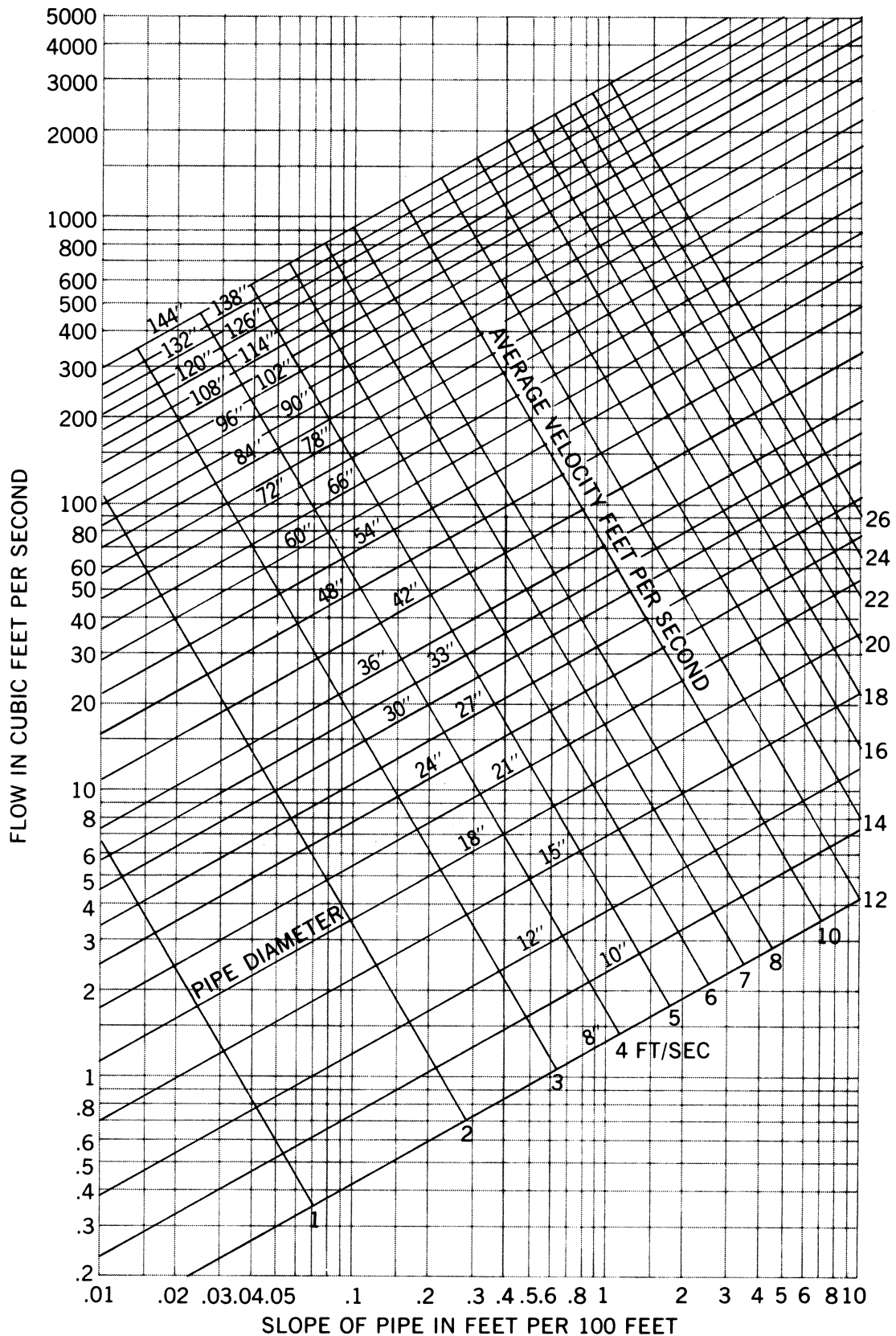


Figure 5

**FLOW FOR CIRCULAR PIPE FLOWING FULL
BASED ON MANNING'S EQUATION $n=0.013$**

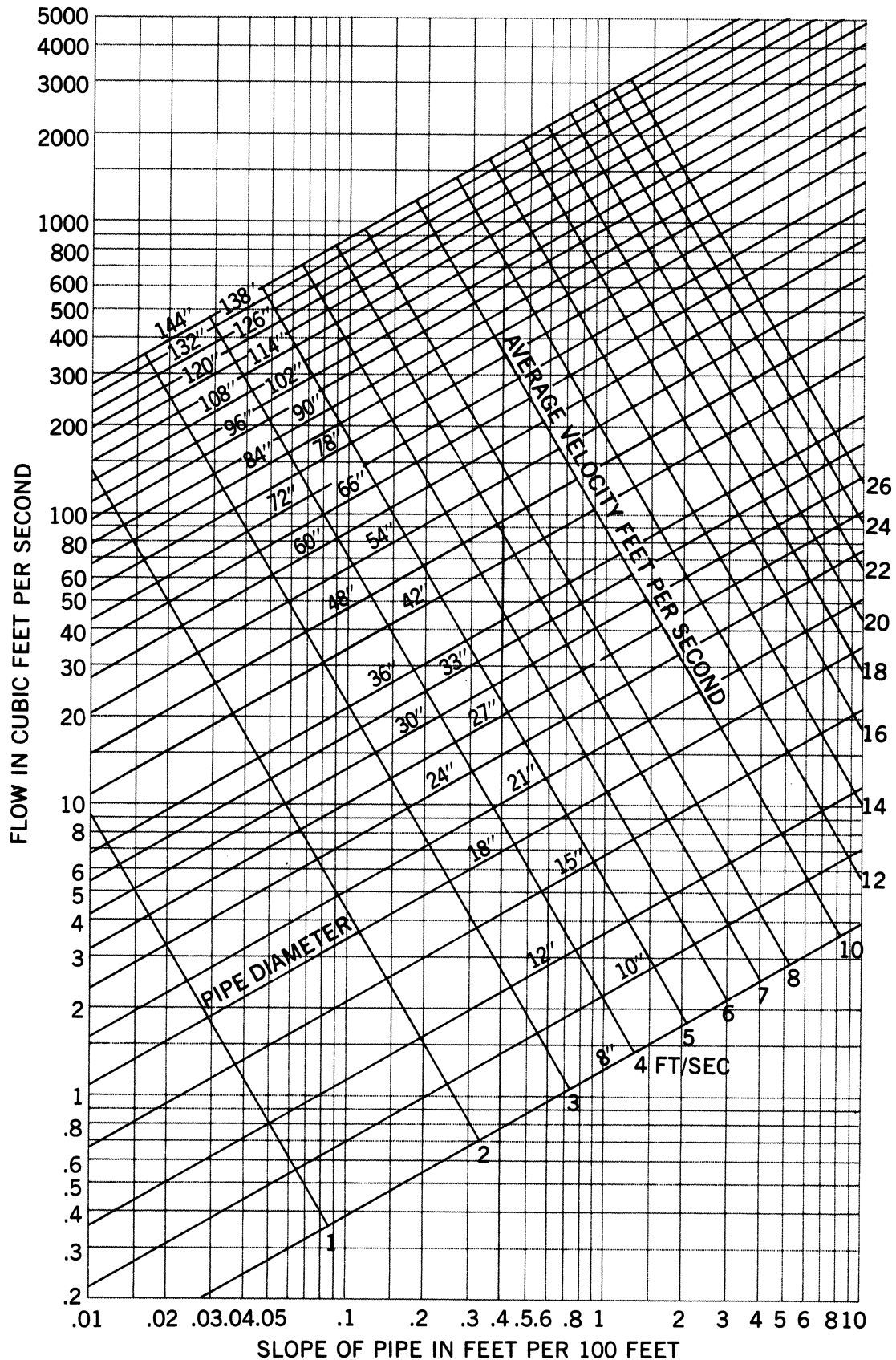


Figure 6

**FLOW FOR HORIZONTAL ELLIPTICAL PIPE FLOWING FULL
BASED ON MANNING'S EQUATION $n=0.010$**

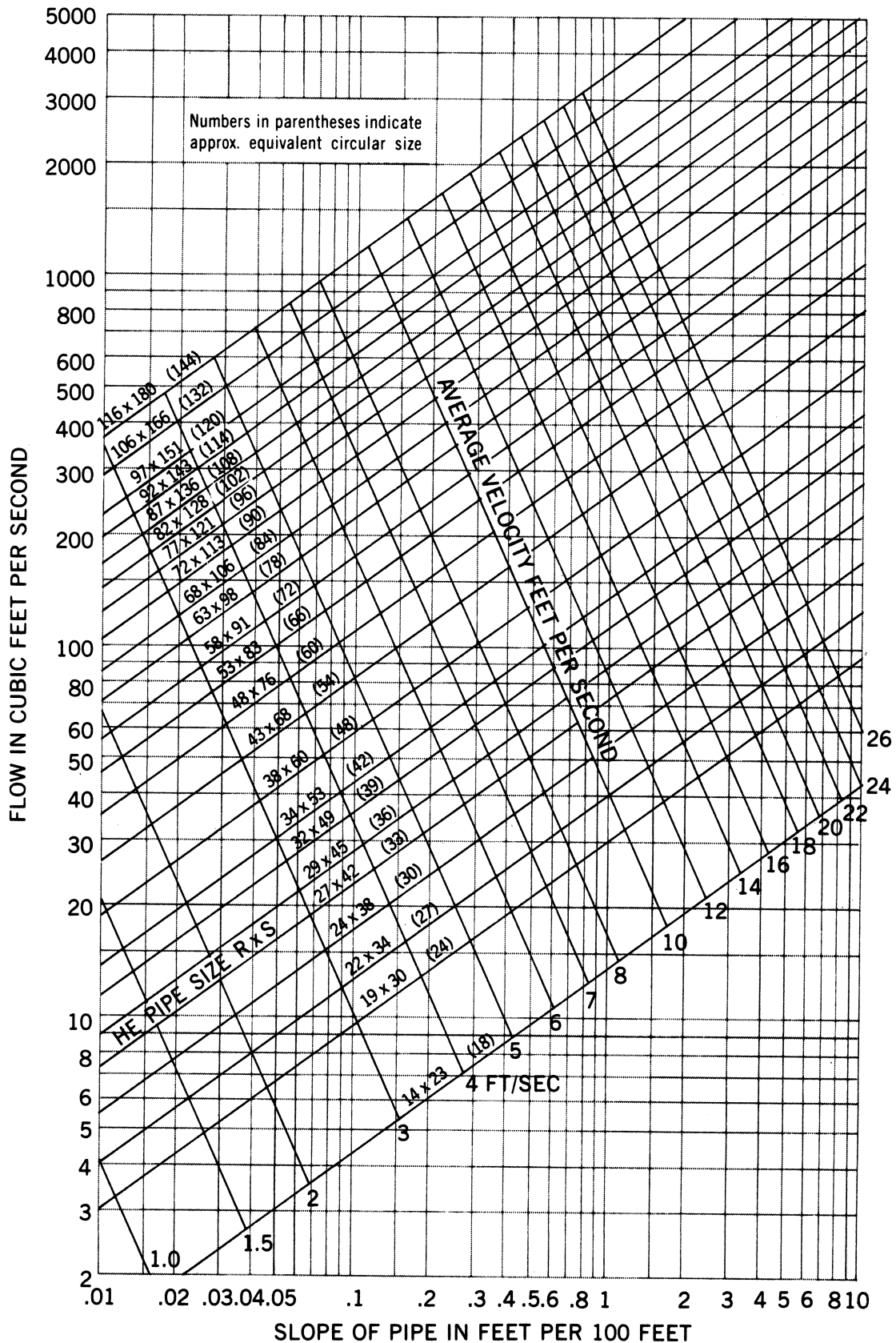


Figure 7

**FLOW FOR HORIZONTAL ELLIPTICAL PIPE FLOWING FULL
BASED ON MANNING'S EQUATION $n=0.011$**

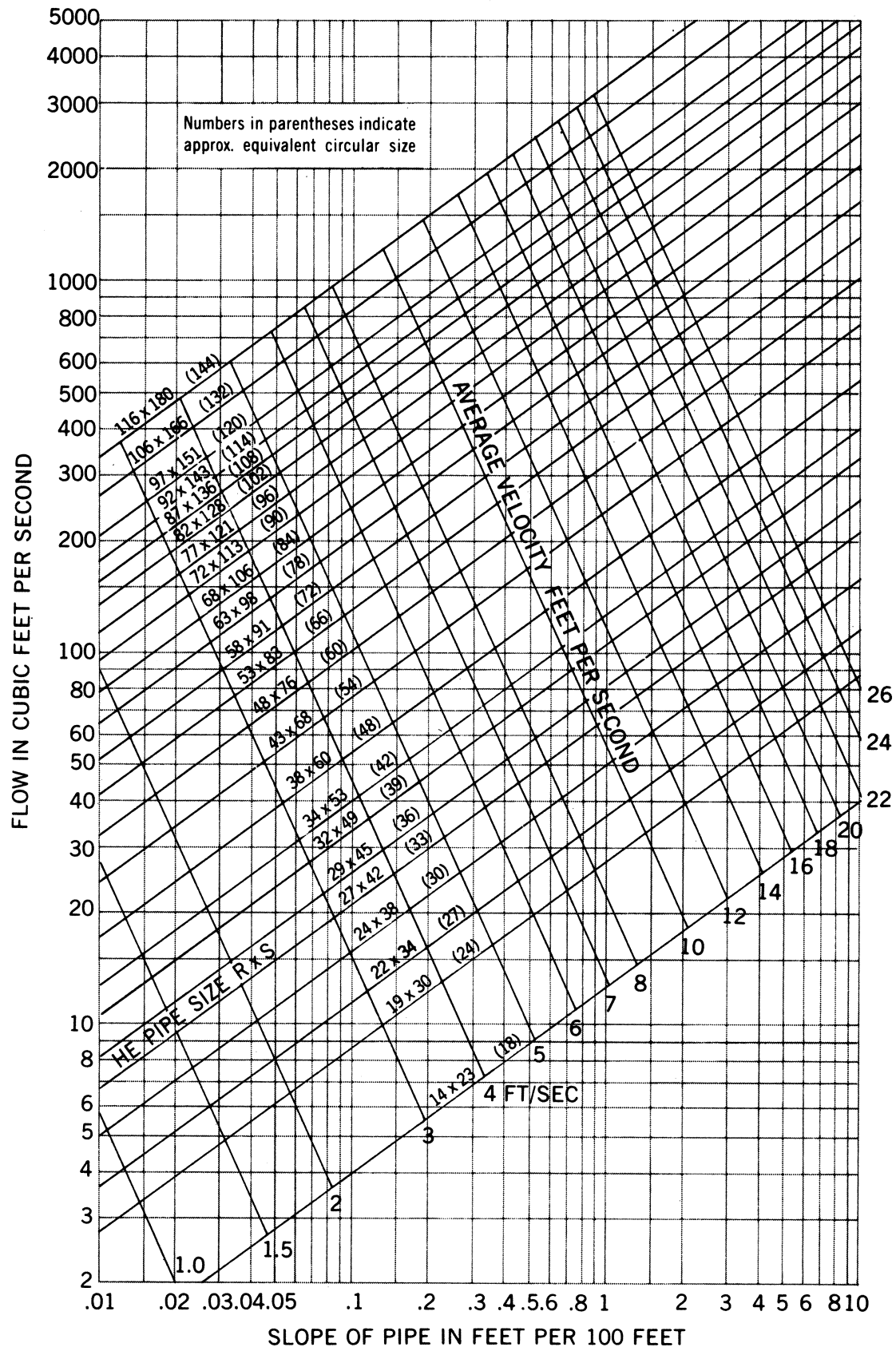


Figure 8

**FLOW FOR HORIZONTAL ELLIPTICAL PIPE FLOWING FULL
BASED ON MANNING'S EQUATION $n=0.012$**

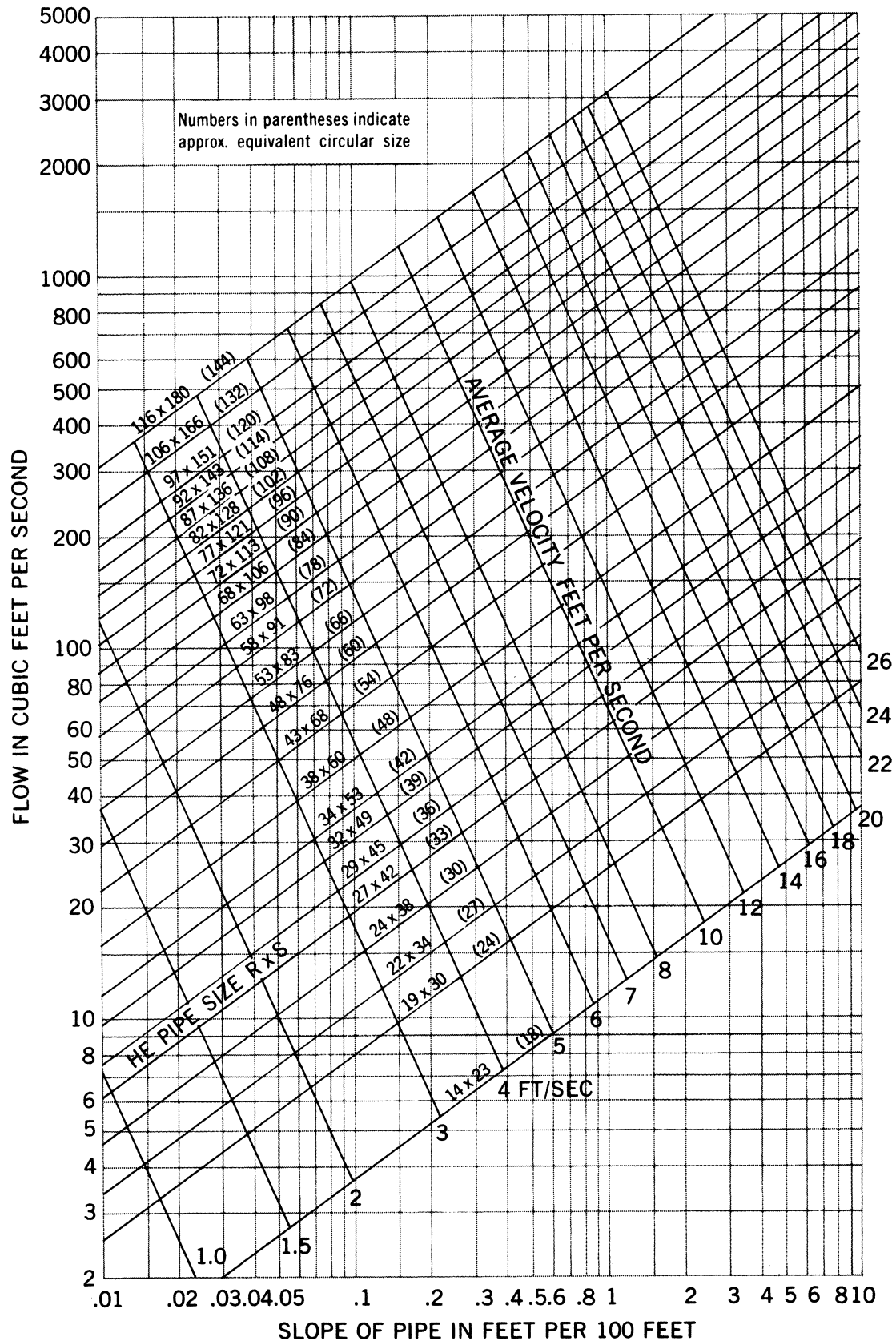


Figure 9

**FLOW FOR HORIZONTAL ELLIPTICAL PIPE FLOWING FULL
BASED ON MANNING'S EQUATION $n=0.013$**

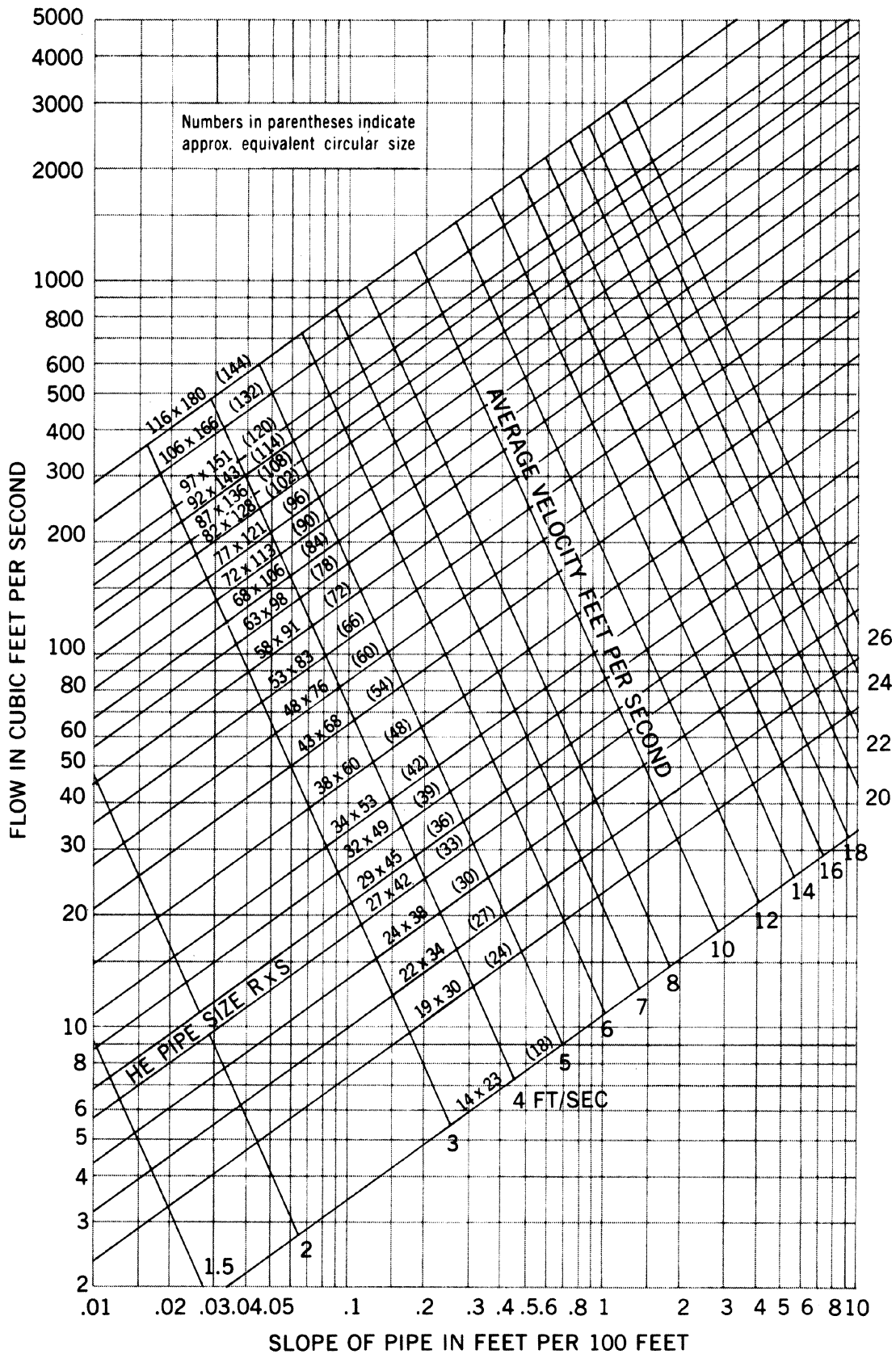


Figure 10

**FLOW FOR VERTICAL ELLIPTICAL PIPE FLOWING FULL
BASED ON MANNING'S EQUATION $n=0.010$**

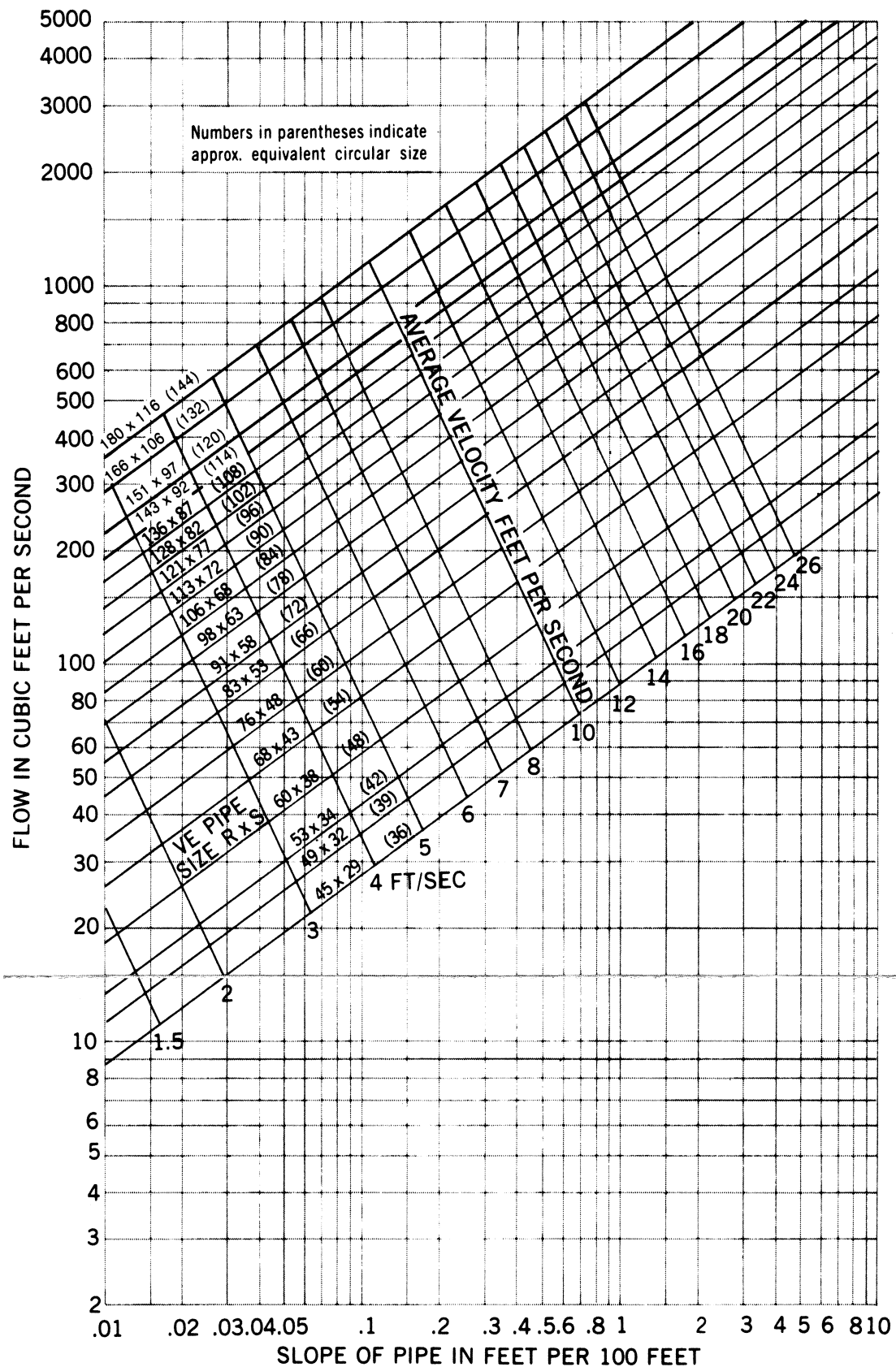


Figure 11

**FLOW FOR VERTICAL ELLIPTICAL PIPE FLOWING FULL
BASED ON MANNING'S EQUATION $n=0.011$**

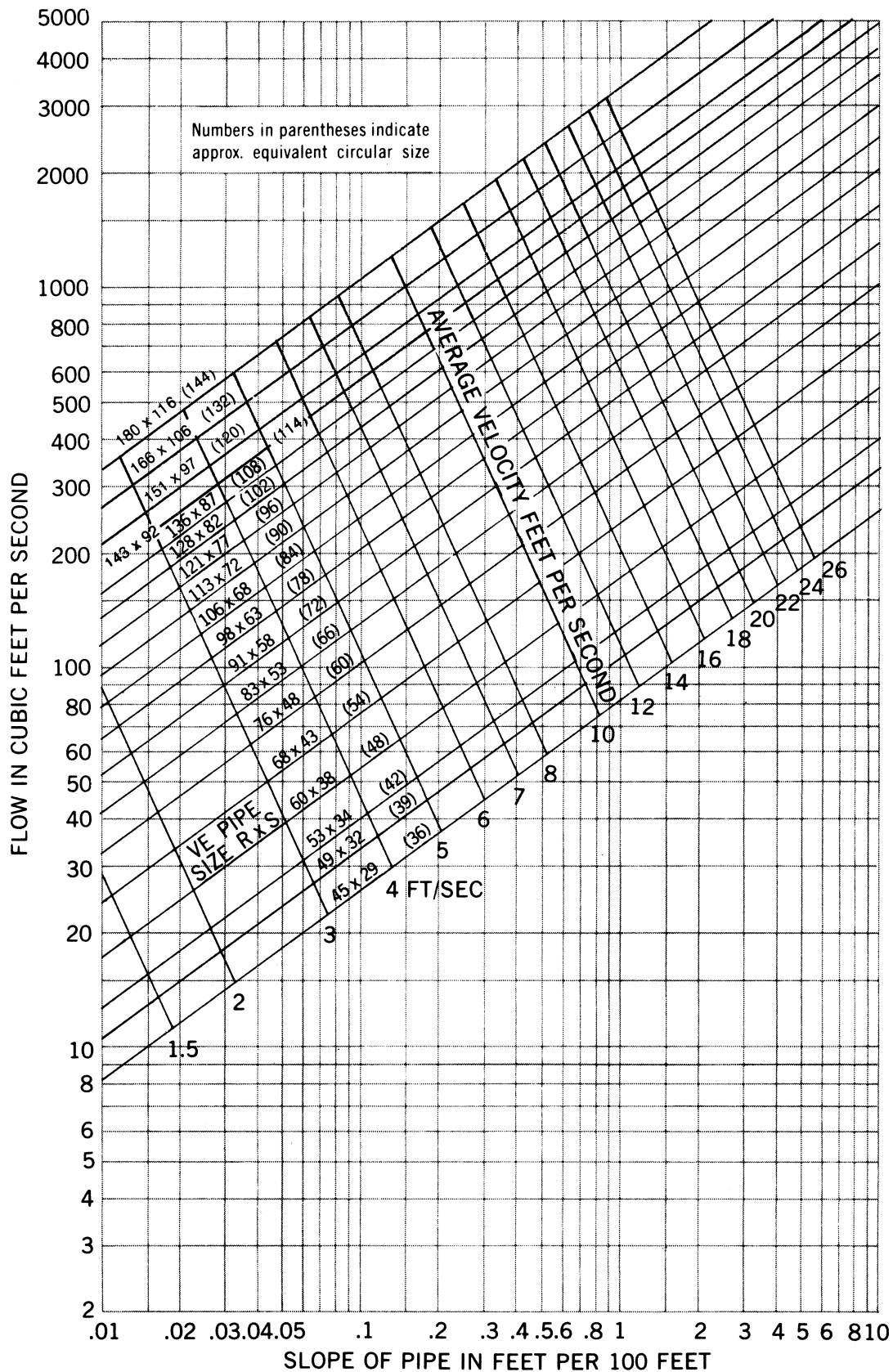


Figure 12

FLOW FOR VERTICAL ELLIPTICAL PIPE FLOWING FULL
BASED ON MANNING'S EQUATION $n=0.012$

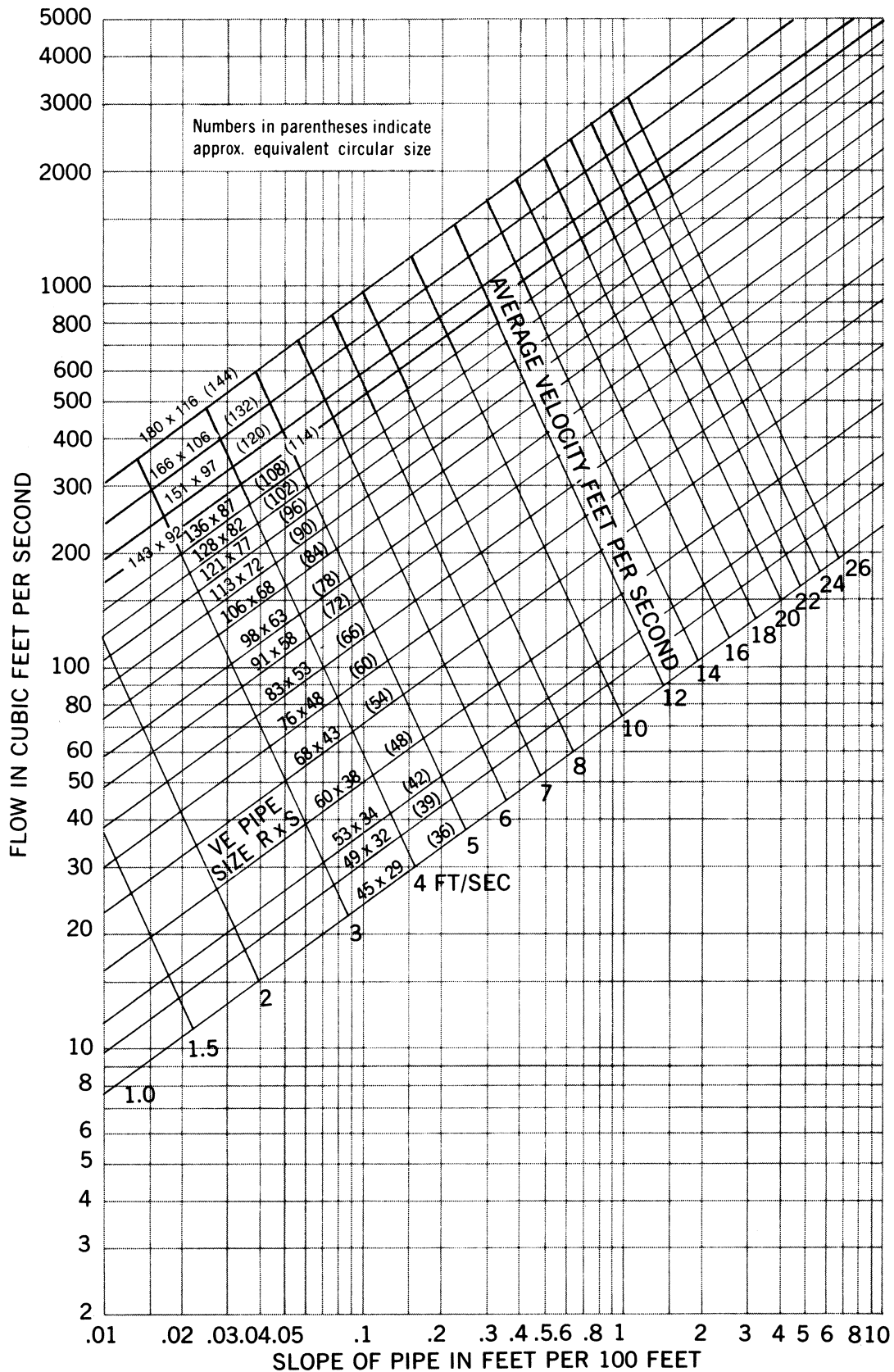


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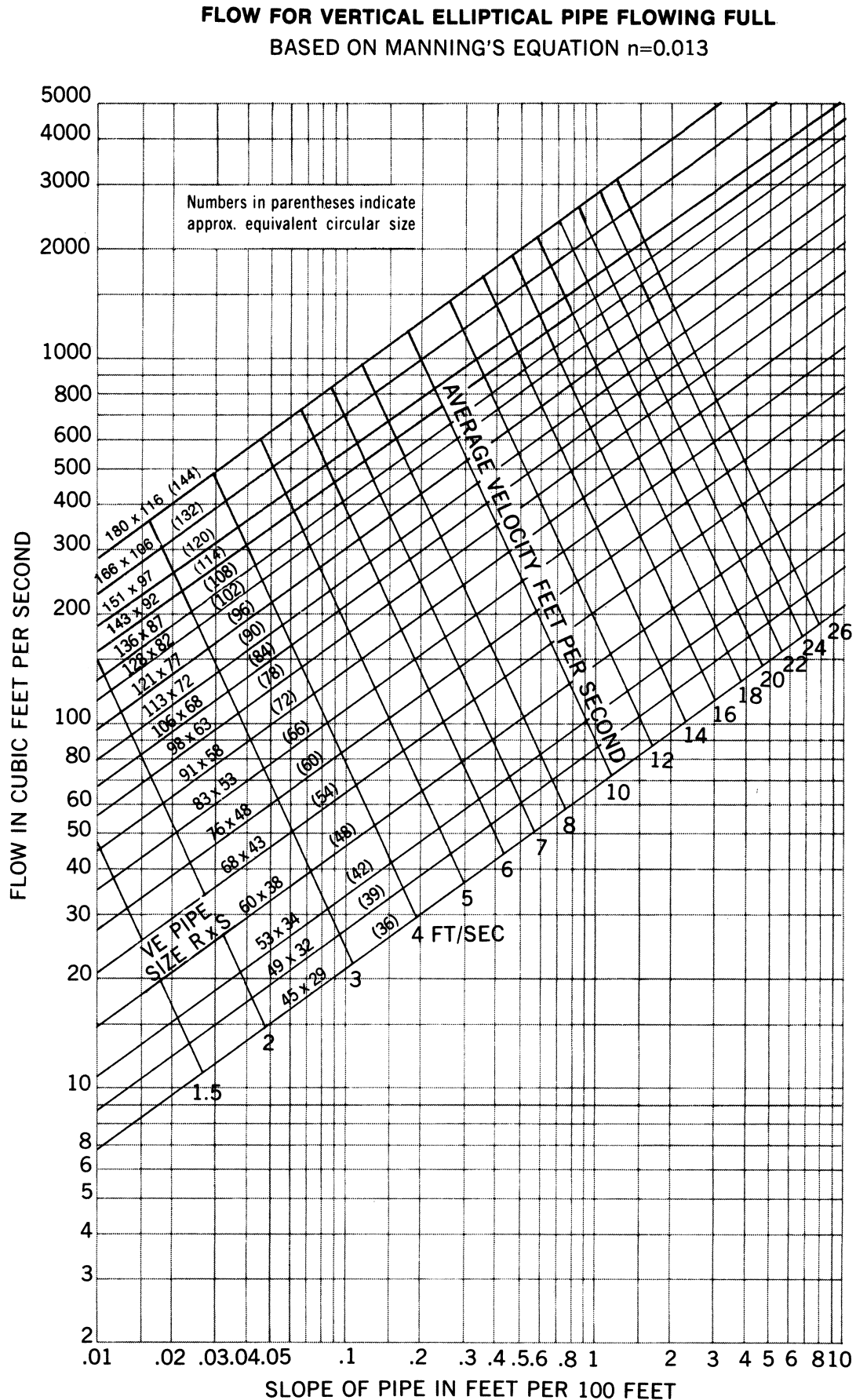


Figure 14

**FLOW FOR ARCH PIPE FLOWING FULL
BASED ON MANNING'S EQUATION $n=0.010$**

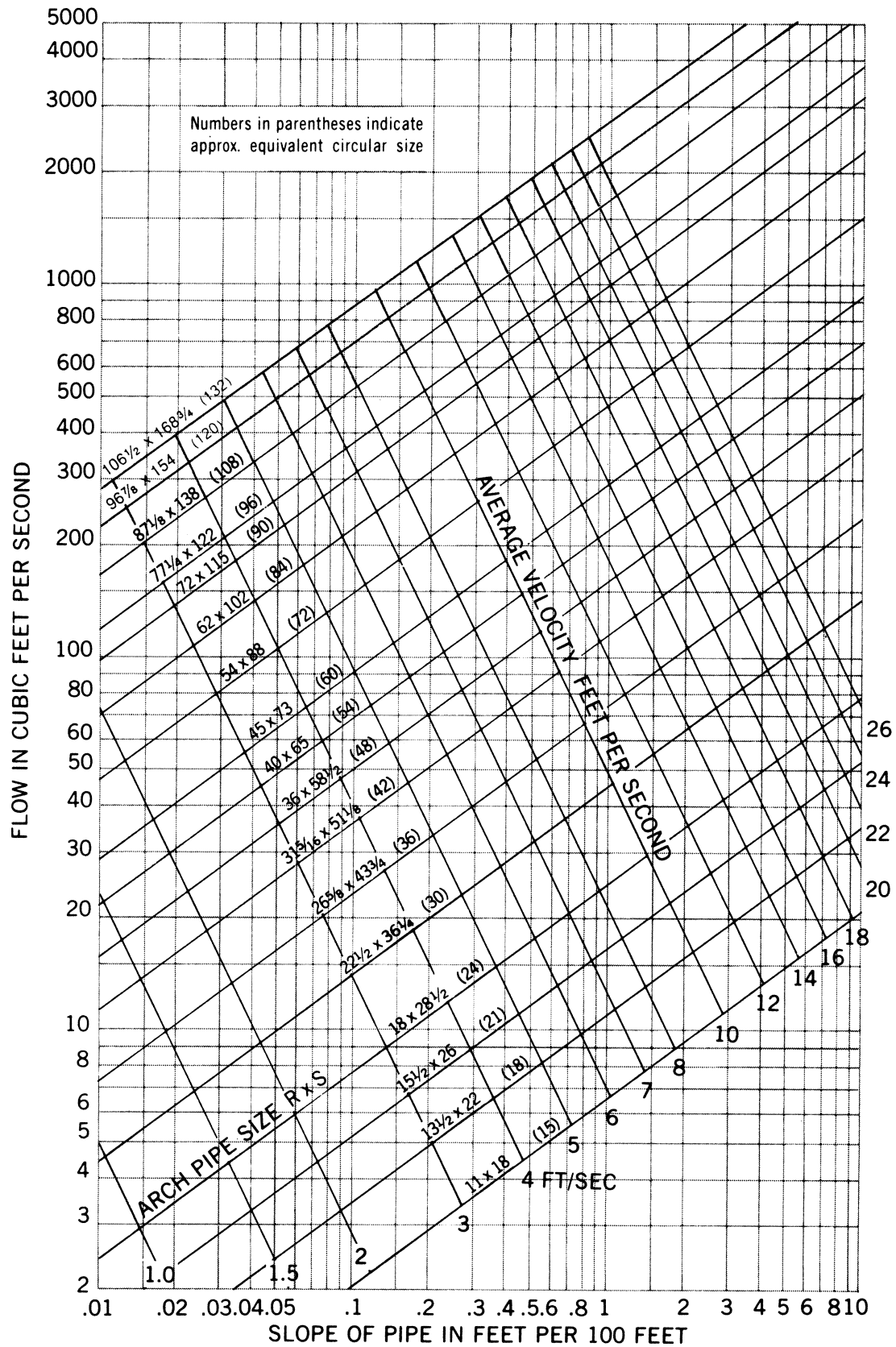


Figure 15

**FLOW FOR ARCH PIPE FLOWING FULL
BASED ON MANNING'S EQUATION $n=0.011$**

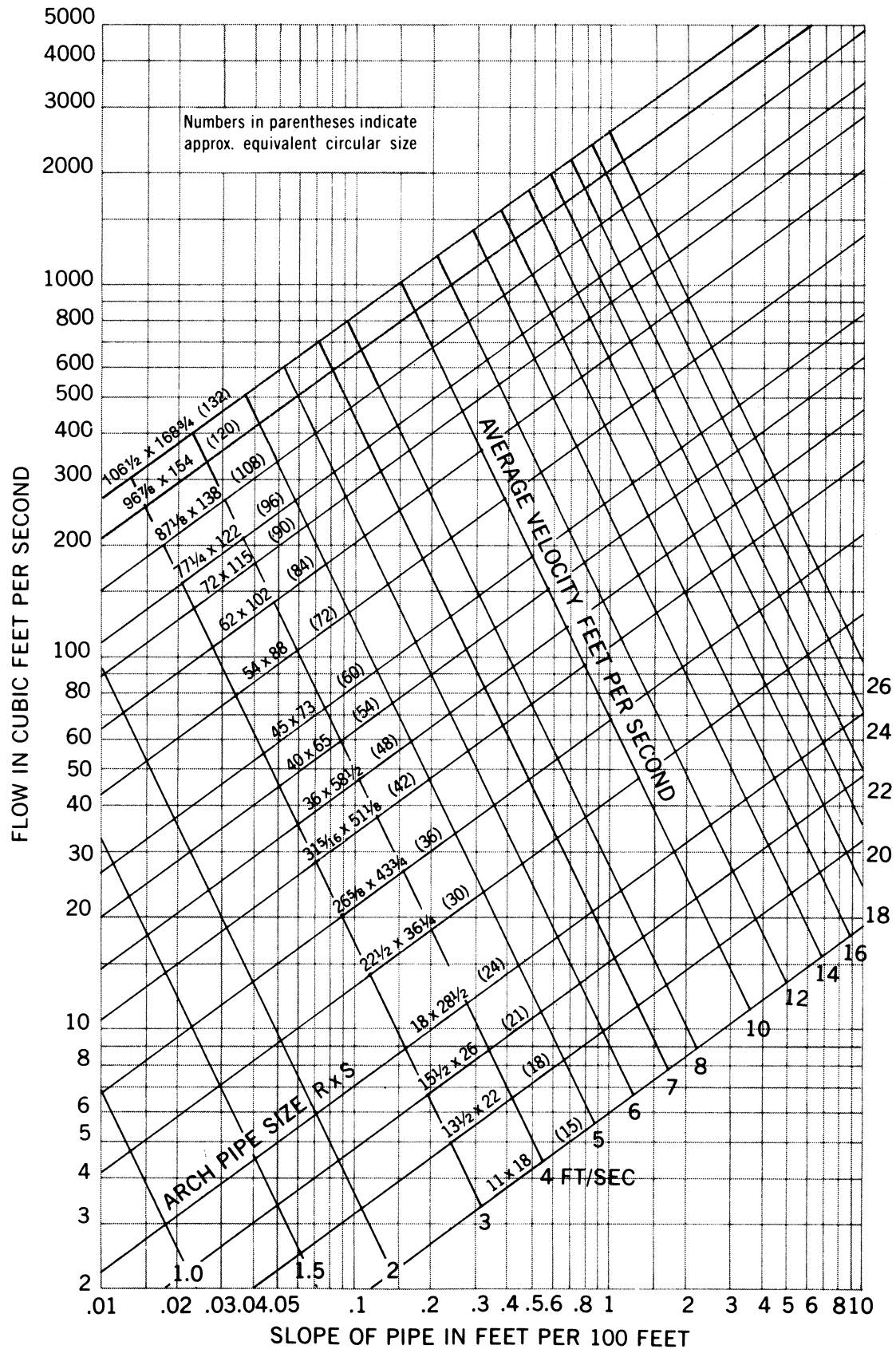


Figure 16

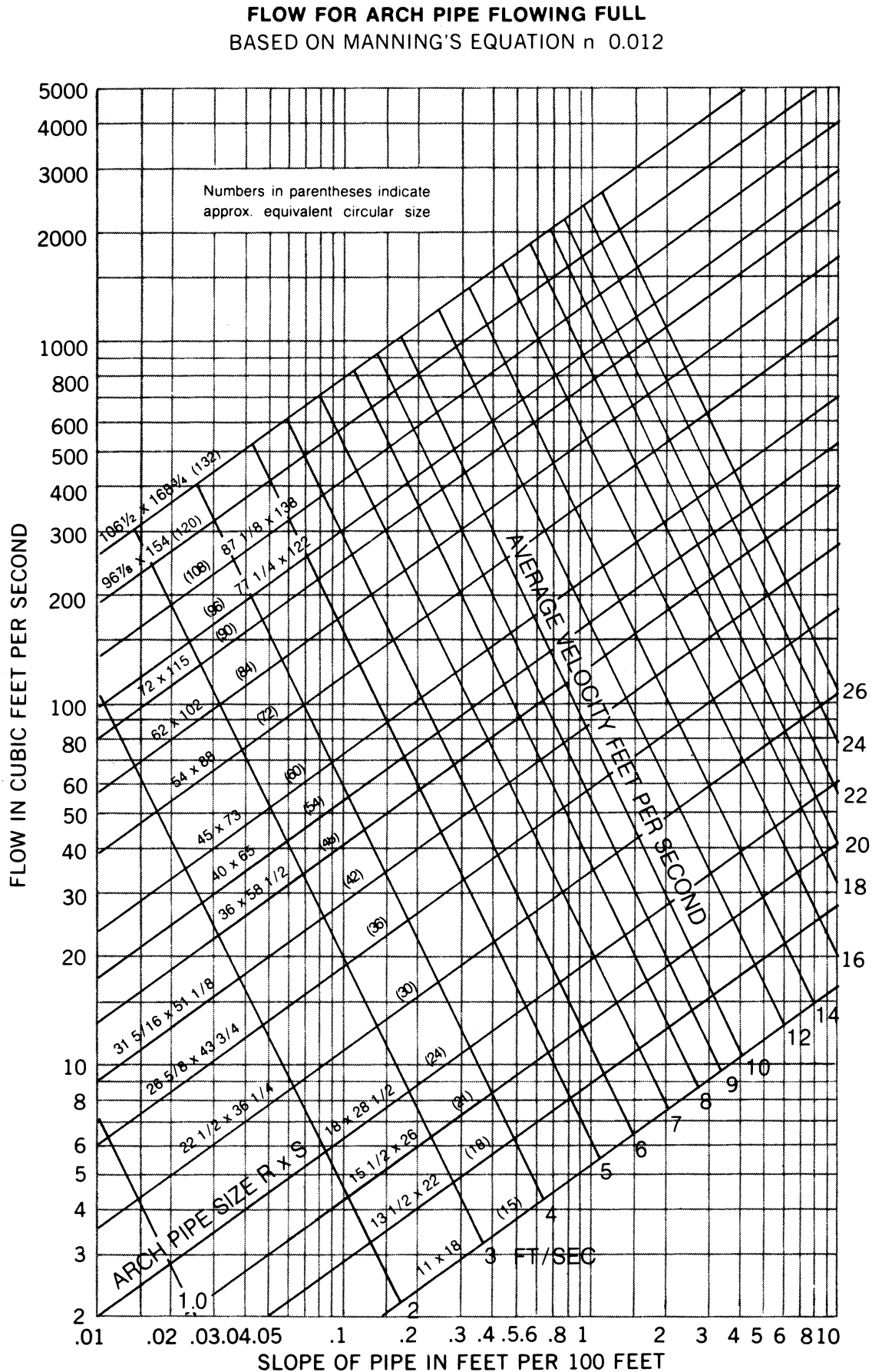


Figure 17

FLOW FOR ARCH PIPE FLOWING FULL
BASED ON MANNING'S EQUATION $n=0.013$

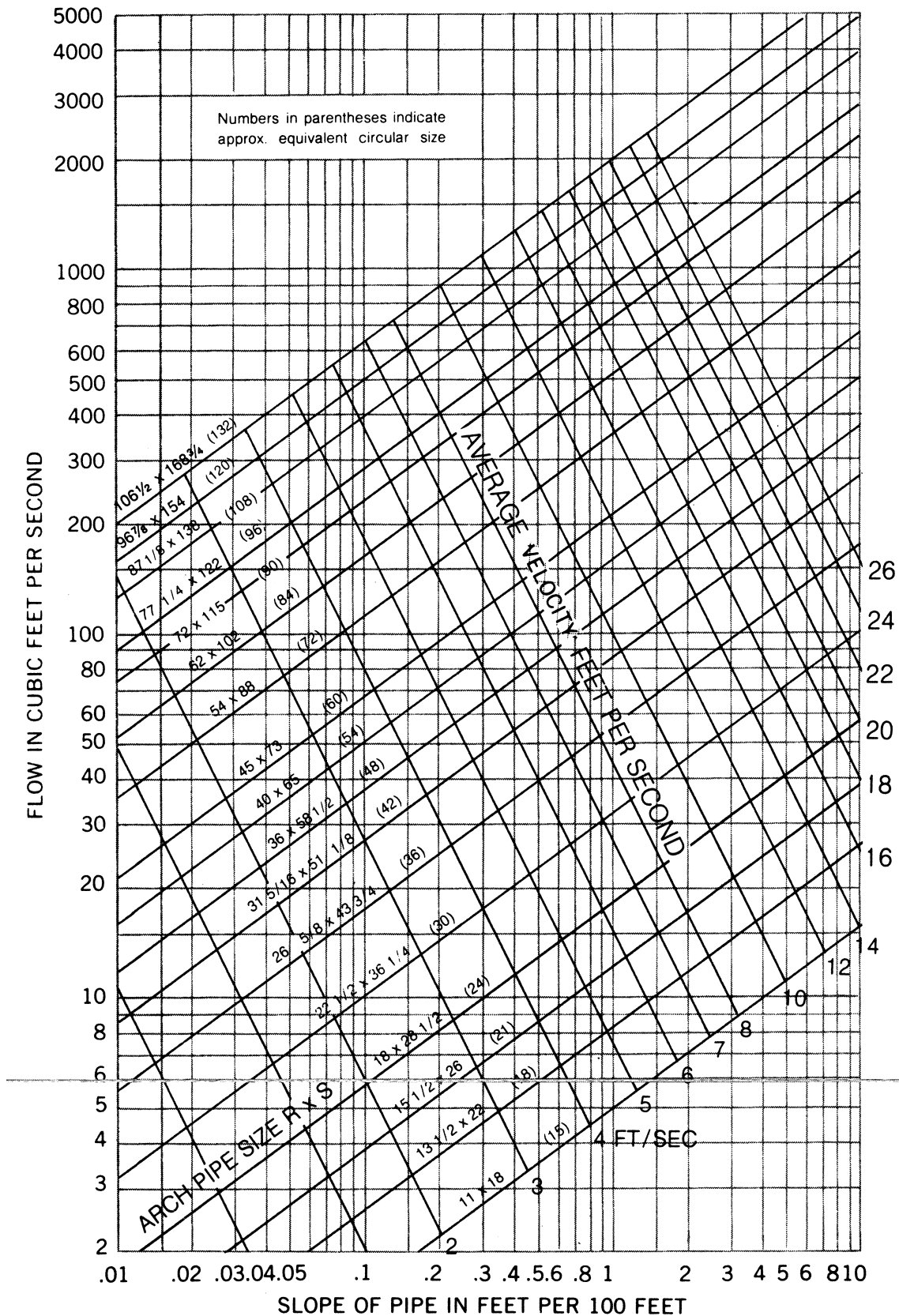


Figure 18.1

FLOW FOR BOX SECTIONS FLOWING FULL
BASED ON MANNINGS EQUATION $n = 0.012$

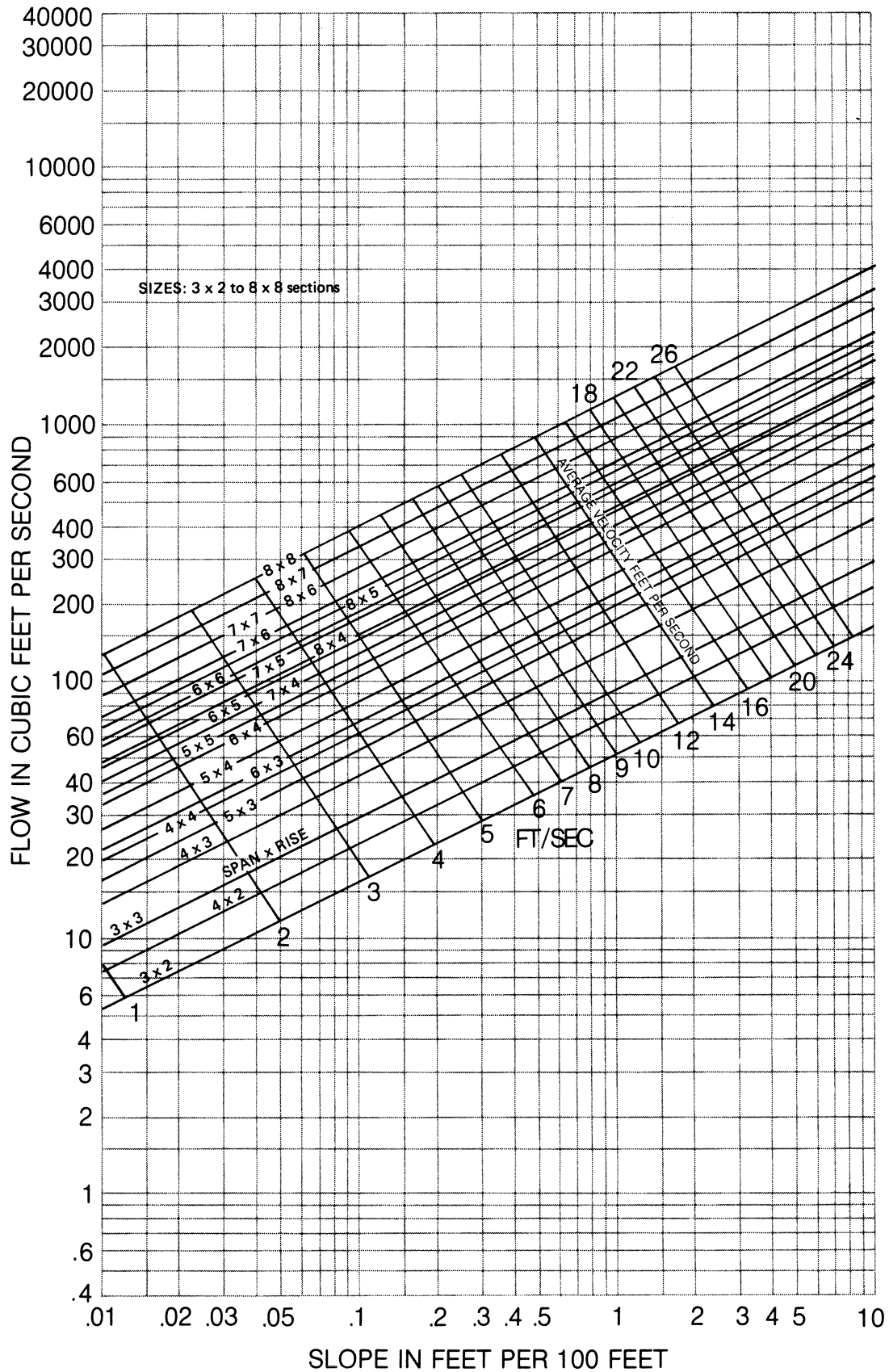


Figure 18.2

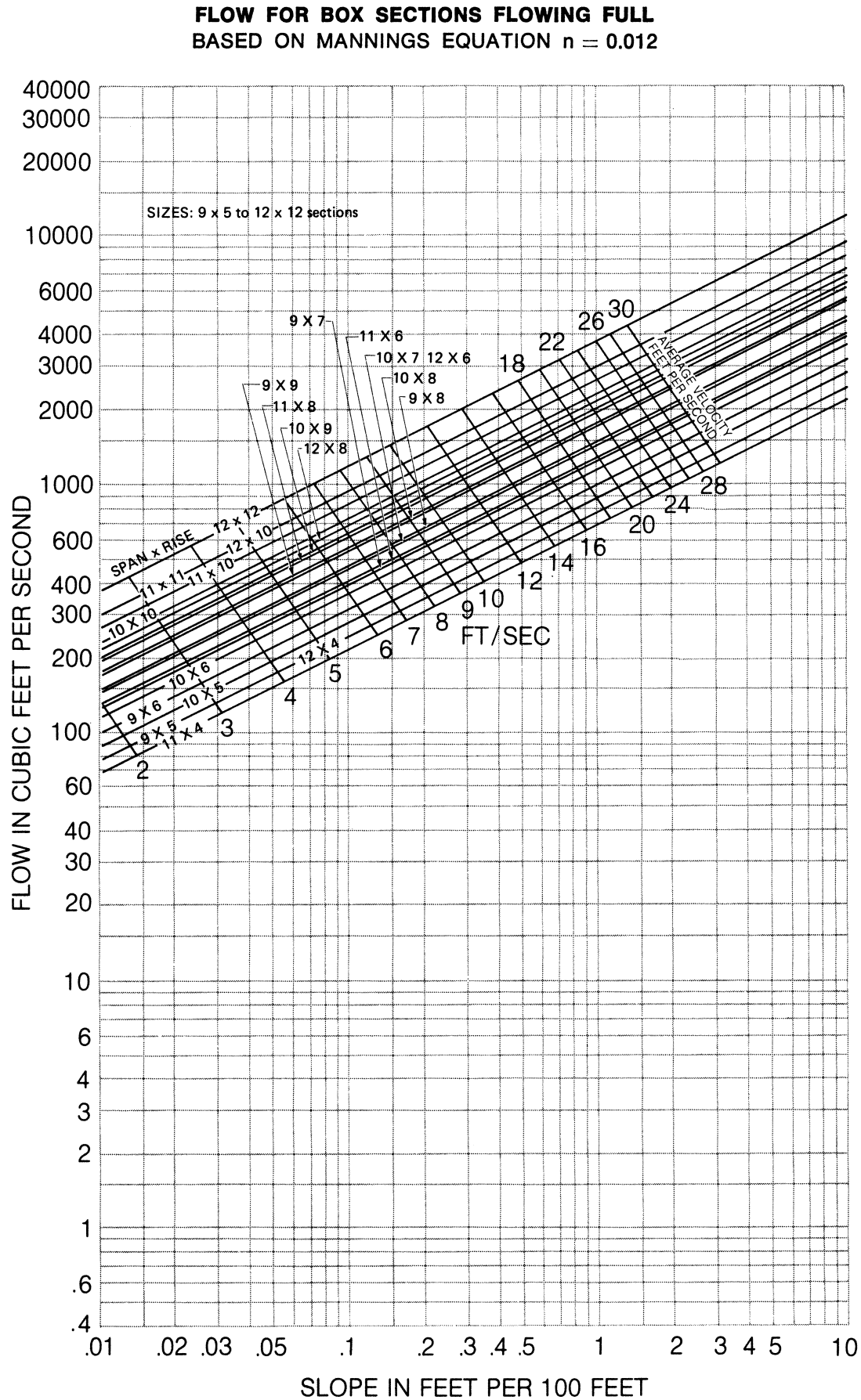


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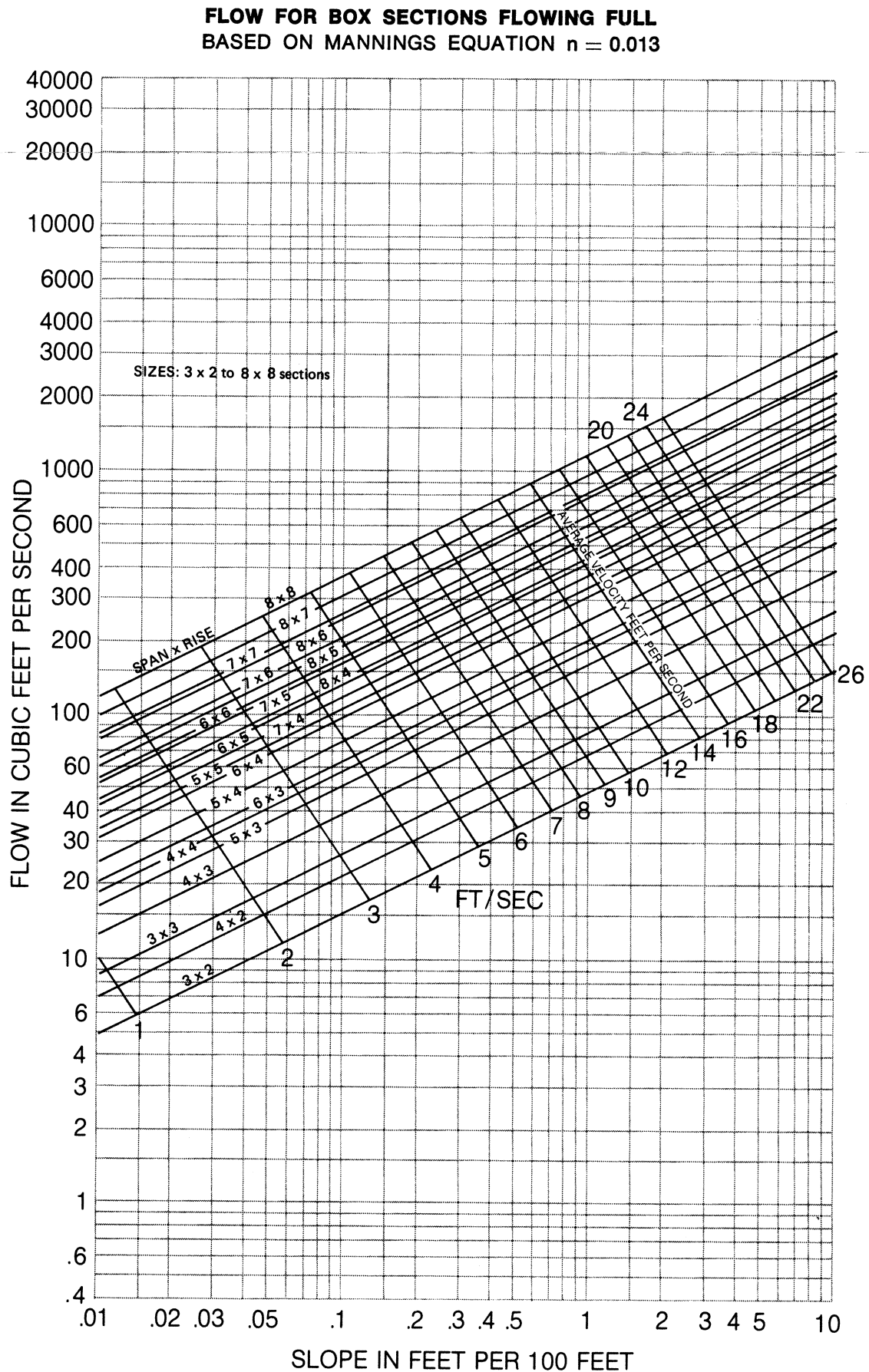


Figure 19.2

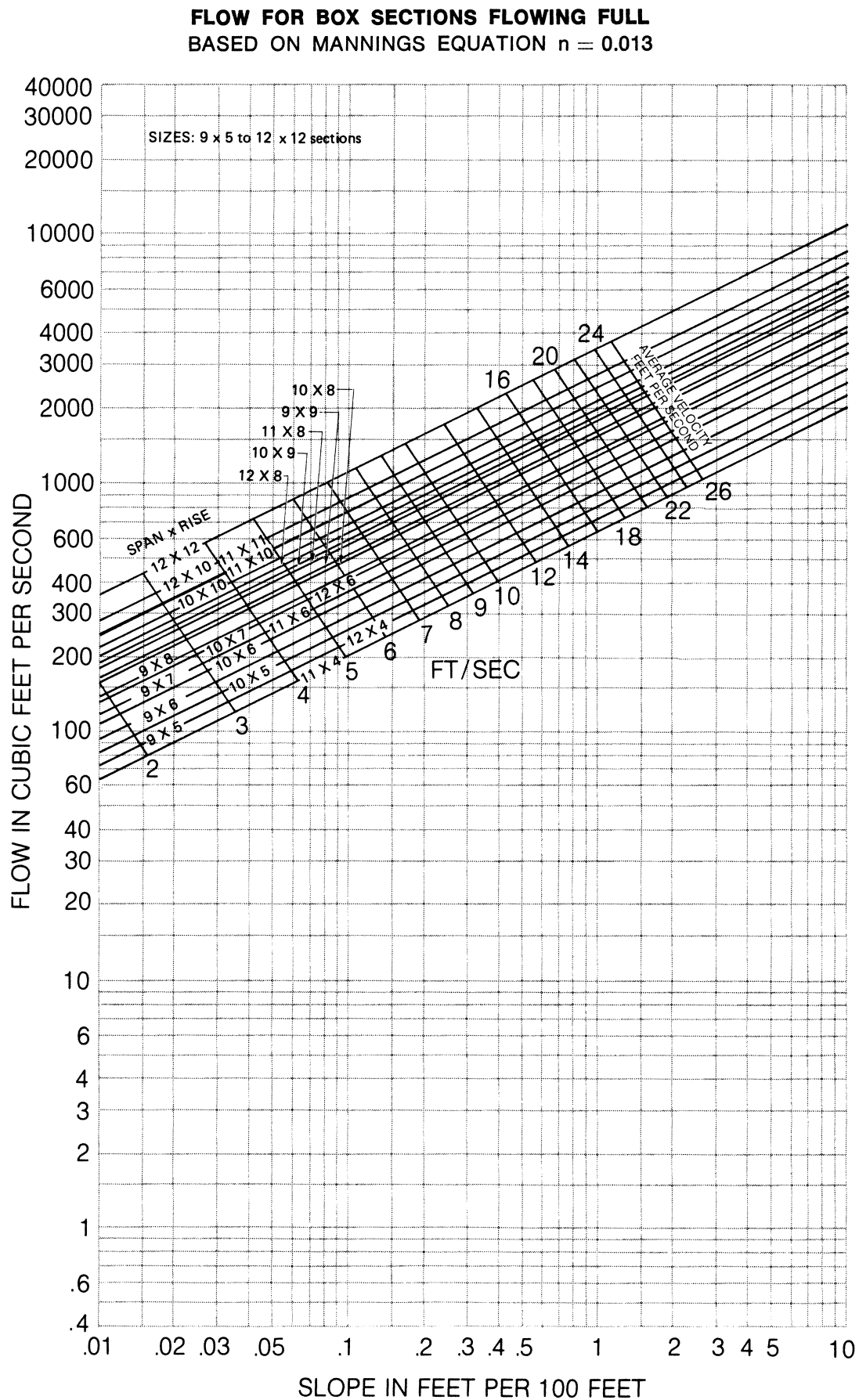


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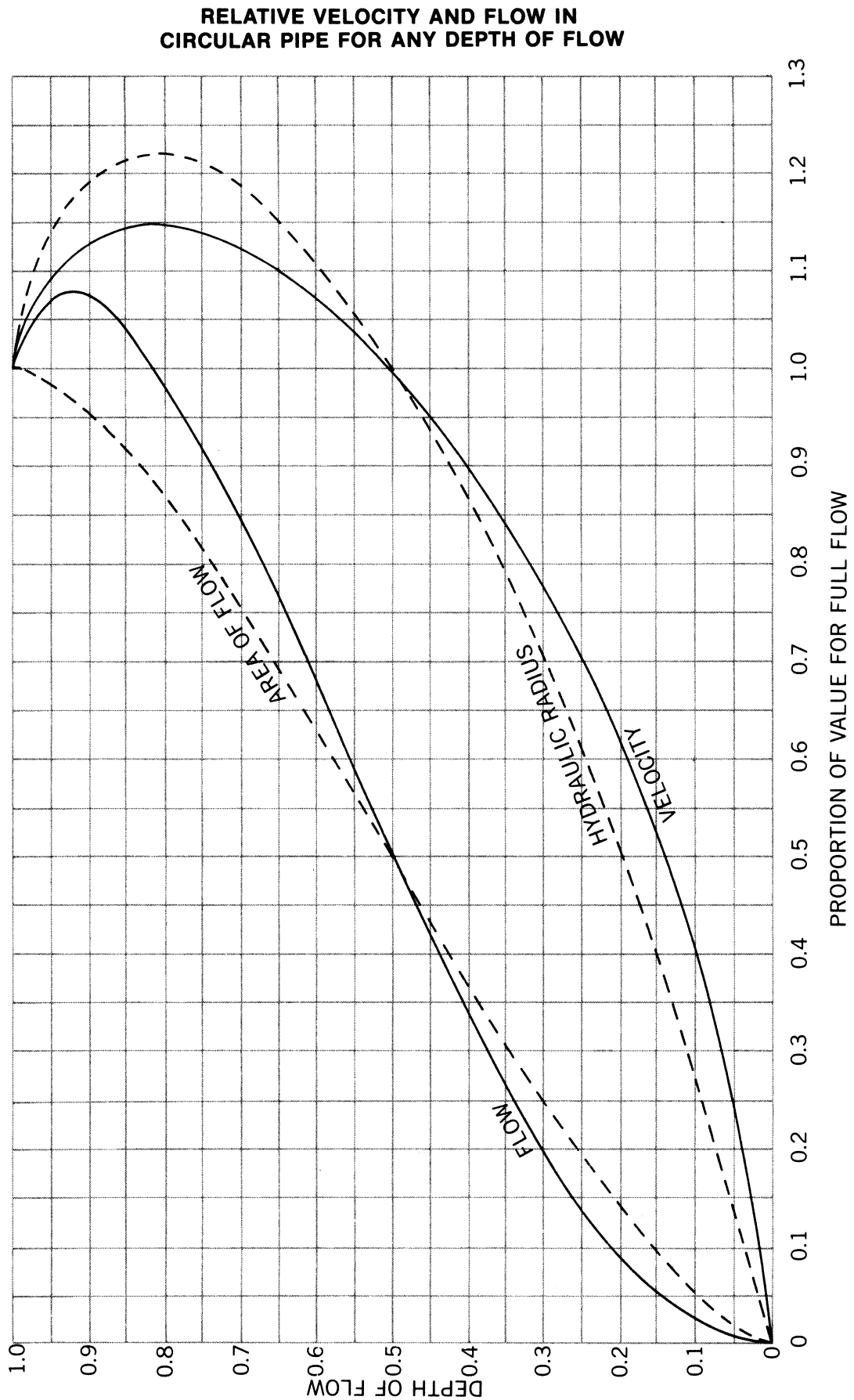


Figure 21

**RELATIVE VELOCITY AND FLOW IN
HORIZONTAL ELLIPTICAL PIPE FOR ANY DEPTH OF FLOW**

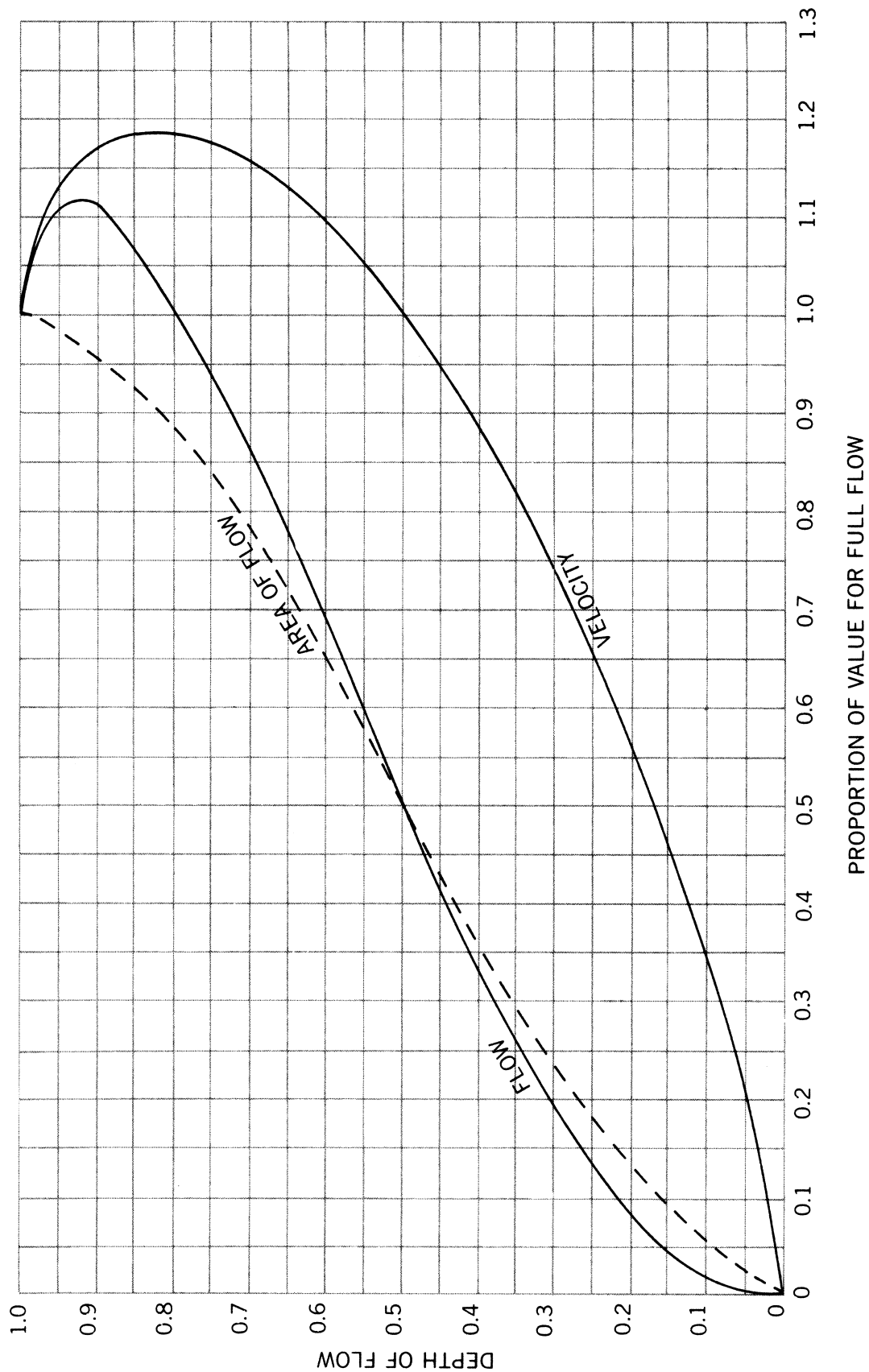


Figure 22

**RELATIVE VELOCITY AND FLOW IN
VERTICAL ELLIPTICAL PIPE FOR ANY DEPTH OF FLOW**

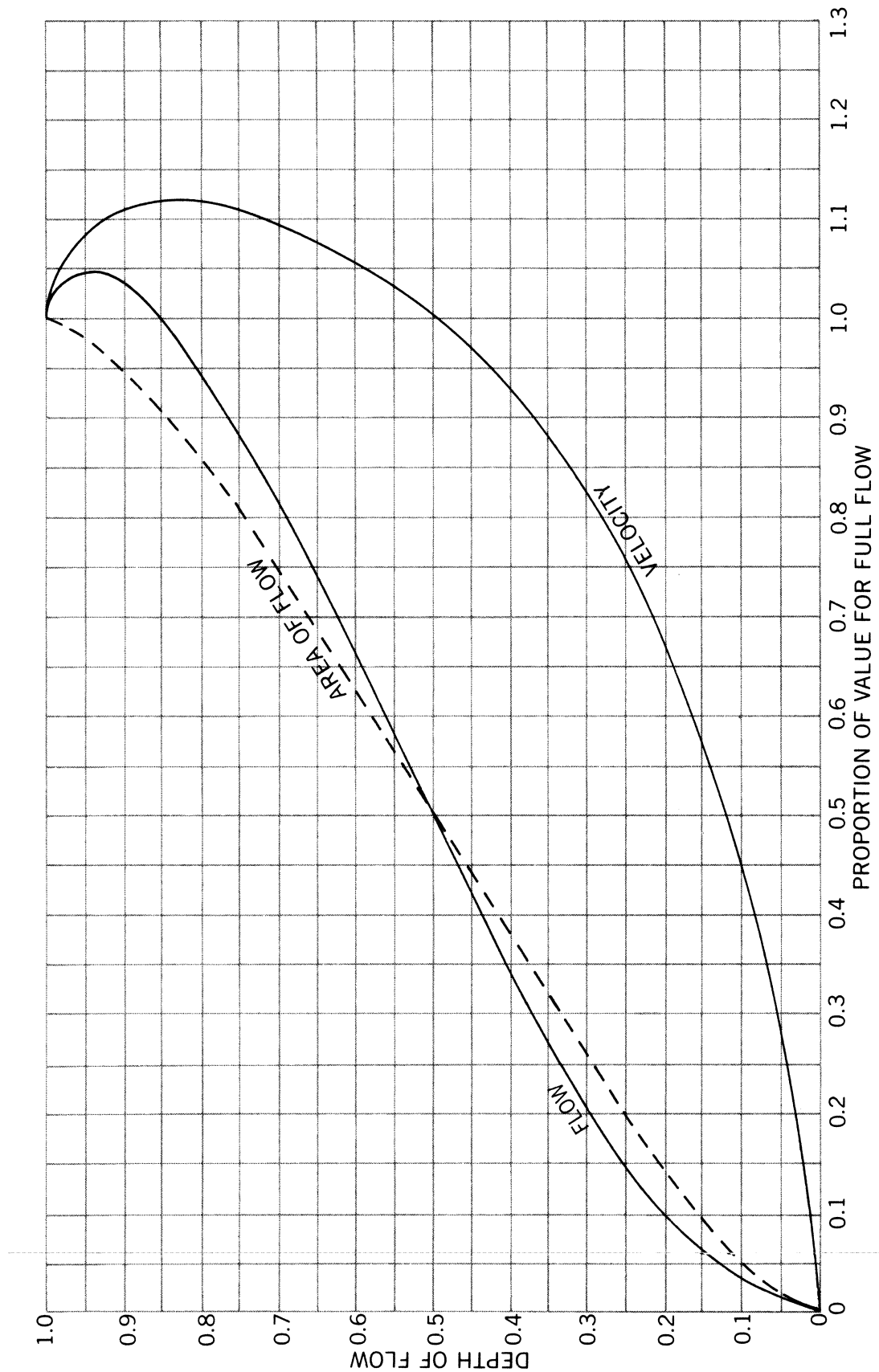


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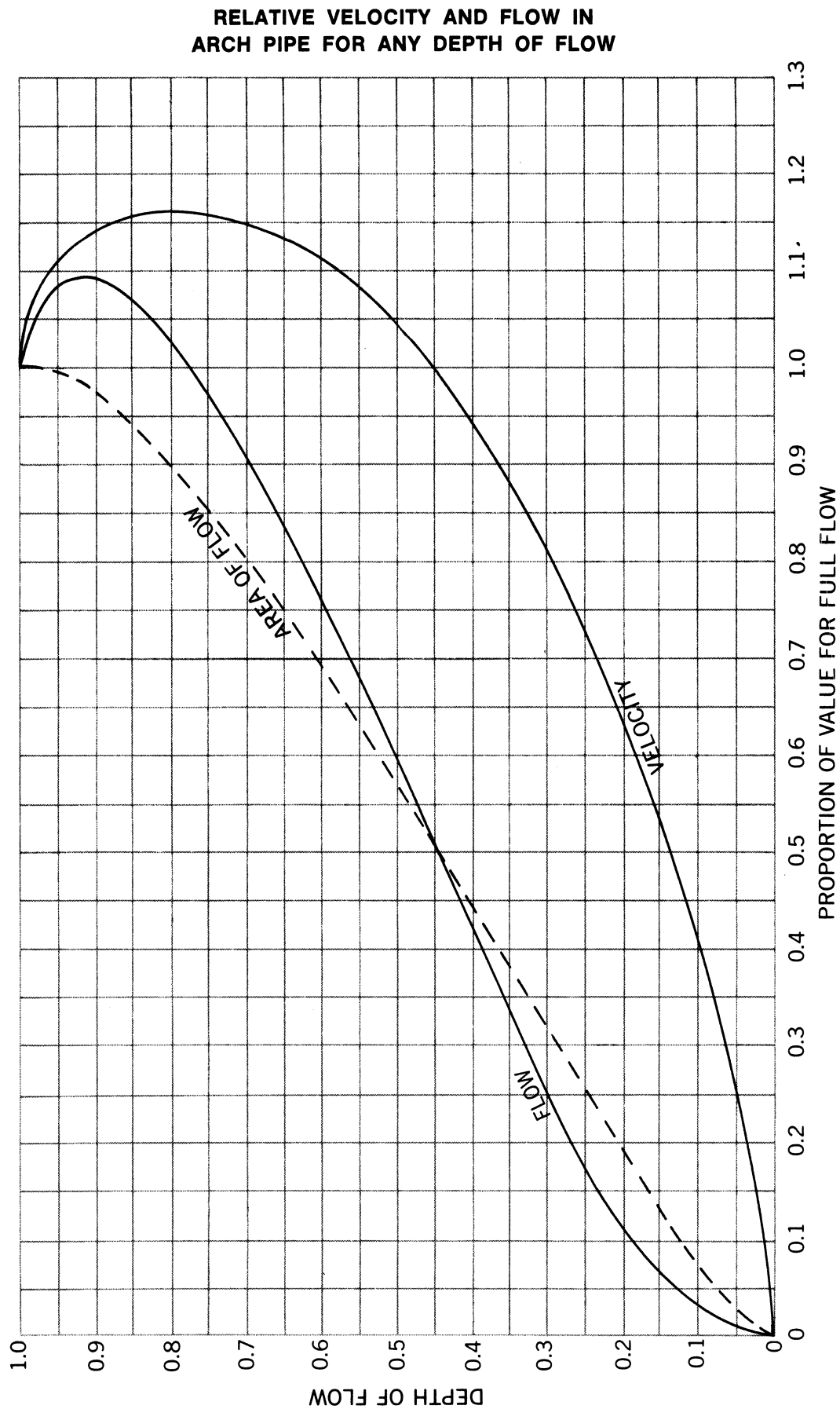


Figure 24.1

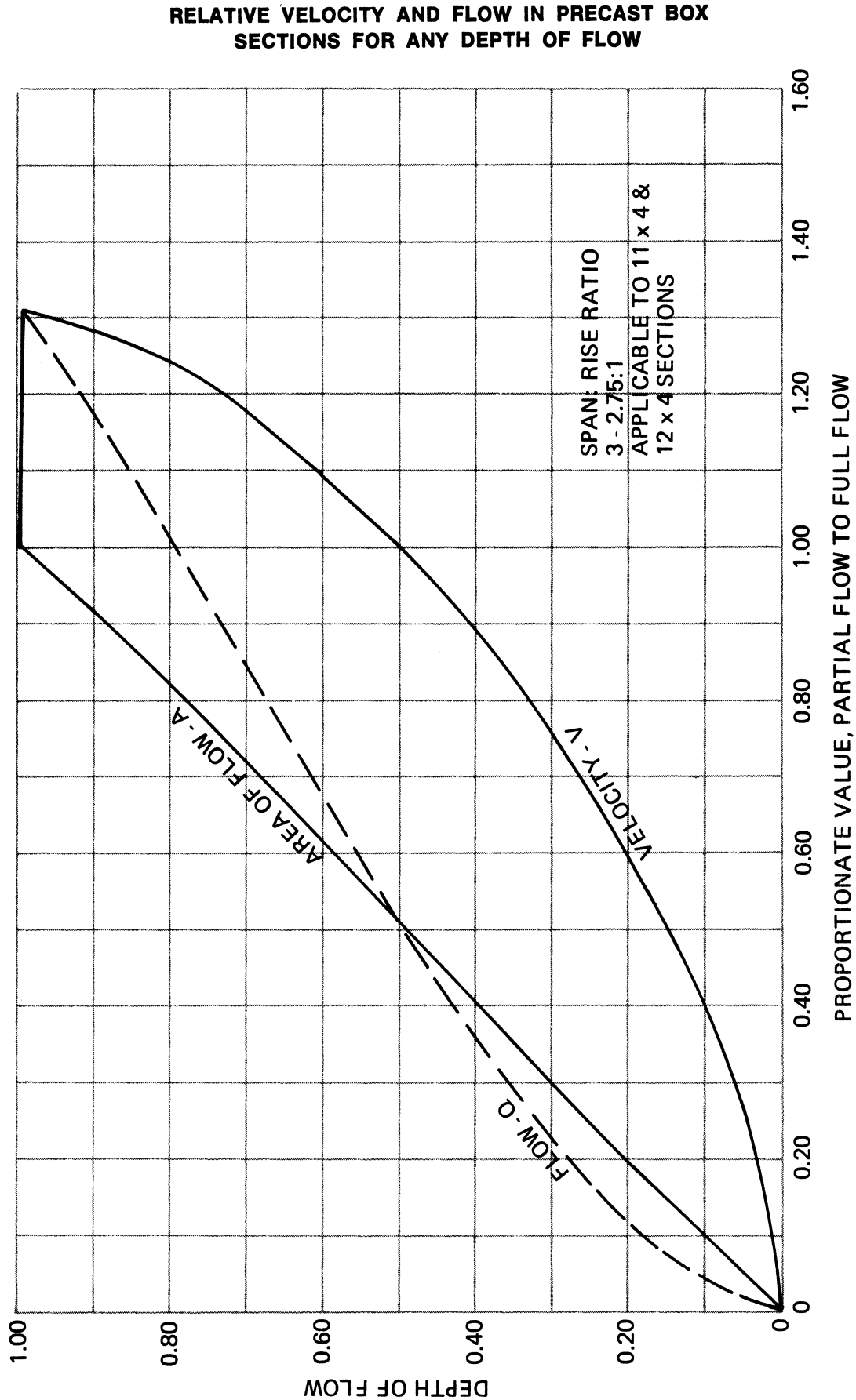


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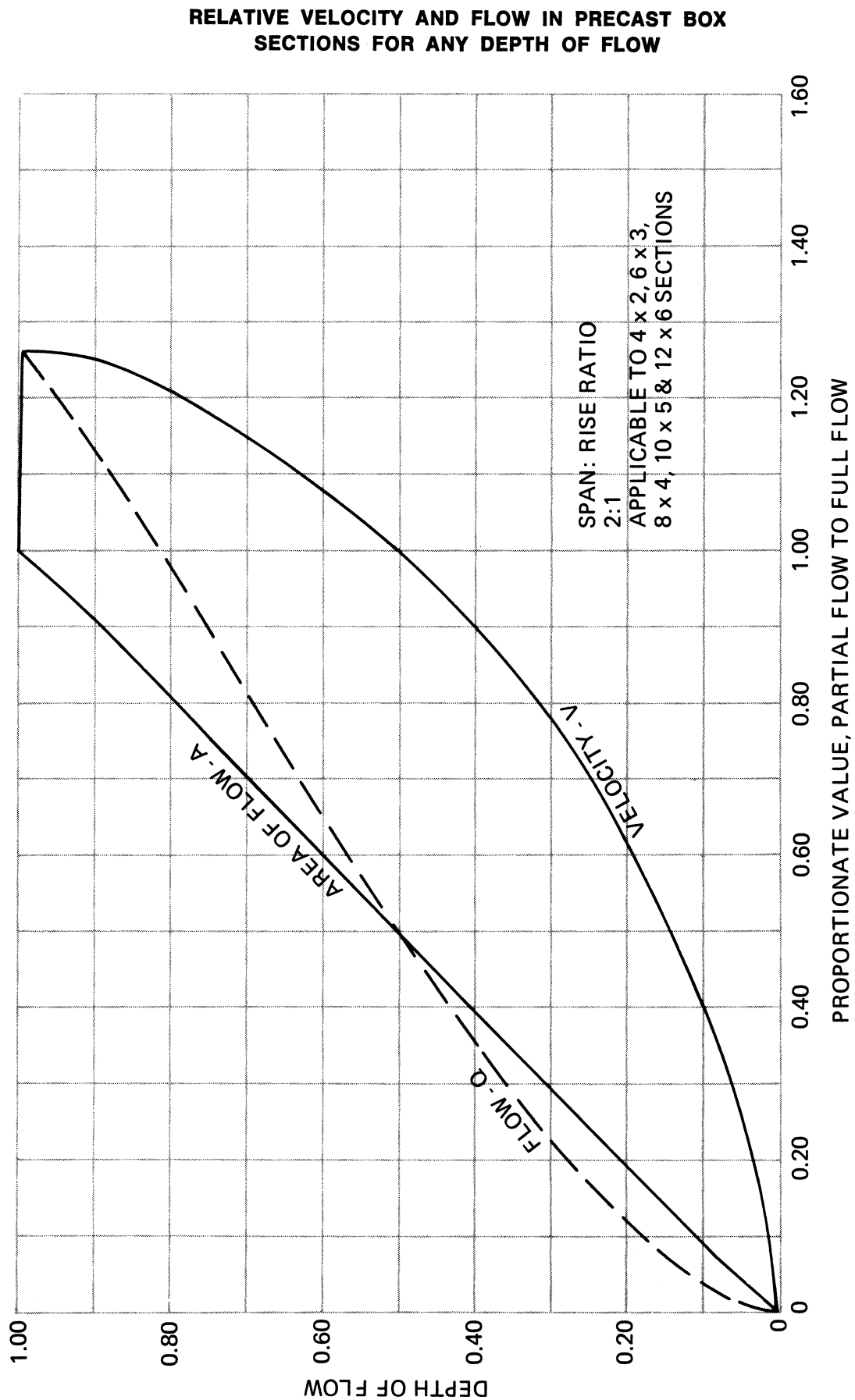


Figure 24.3

**RELATIVE VELOCITY AND FLOW IN PRECAST BOX
SECTIONS FOR ANY DEPTH OF FLOW**

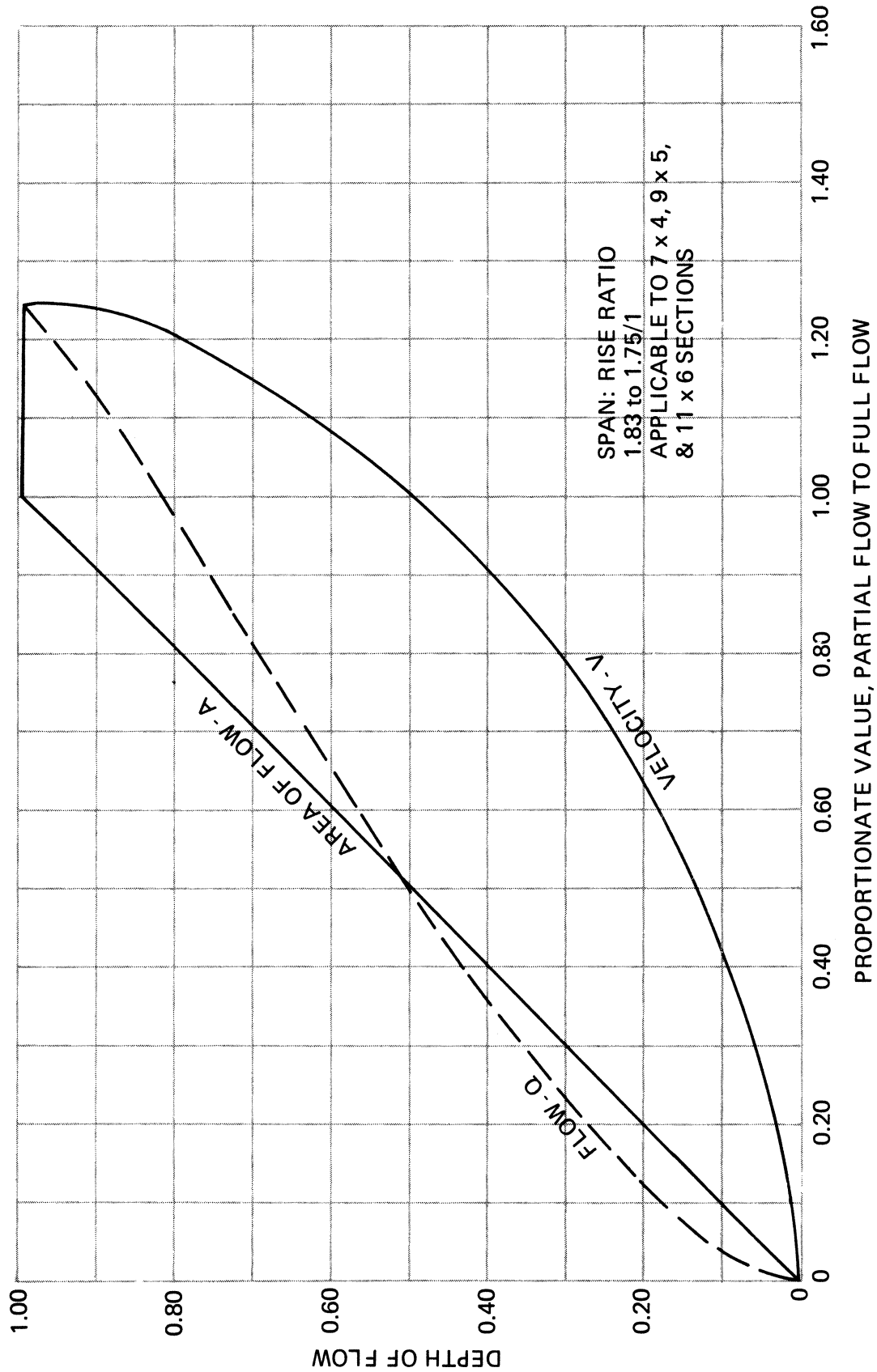


Figure 24.4

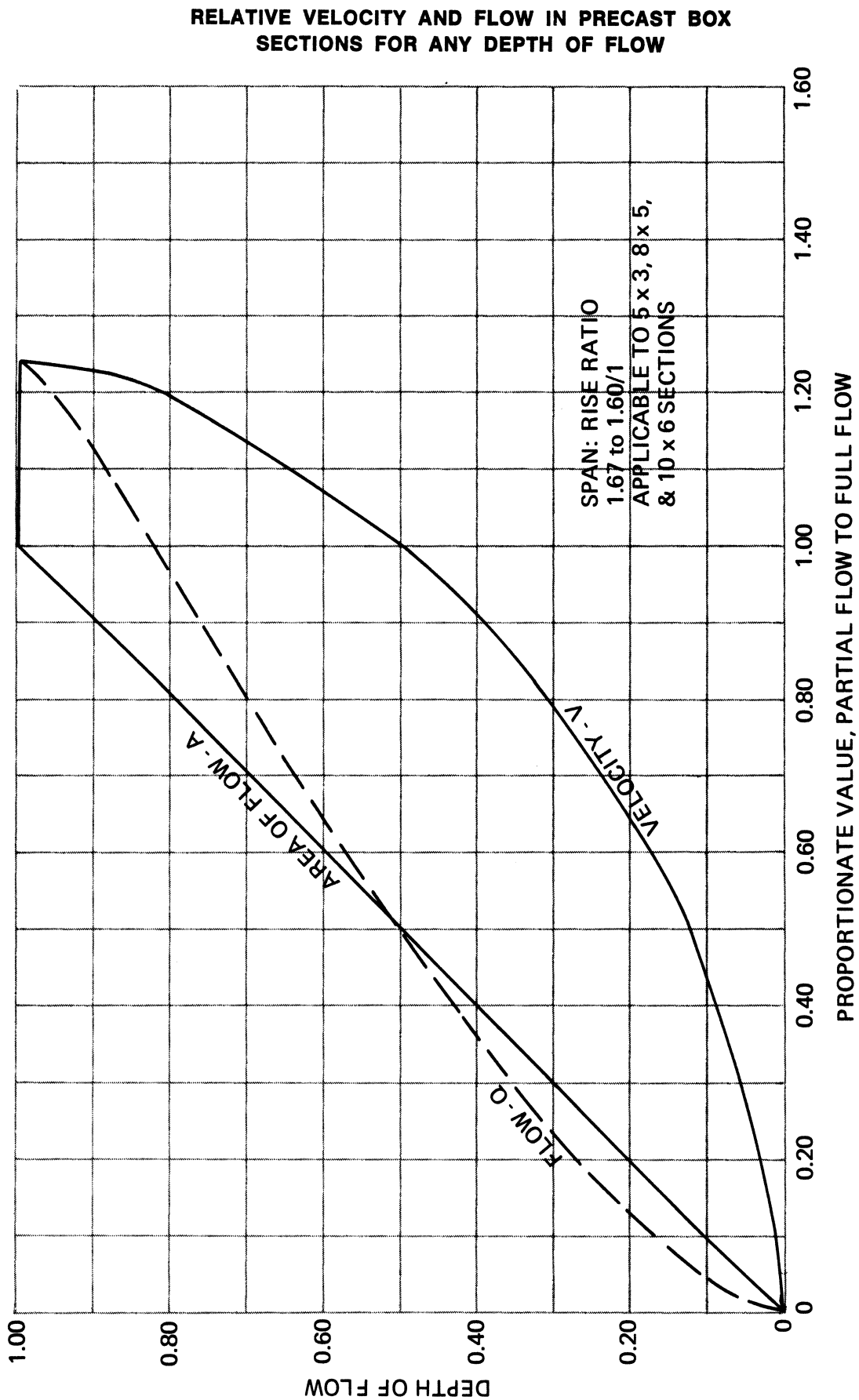


Figure 24.5

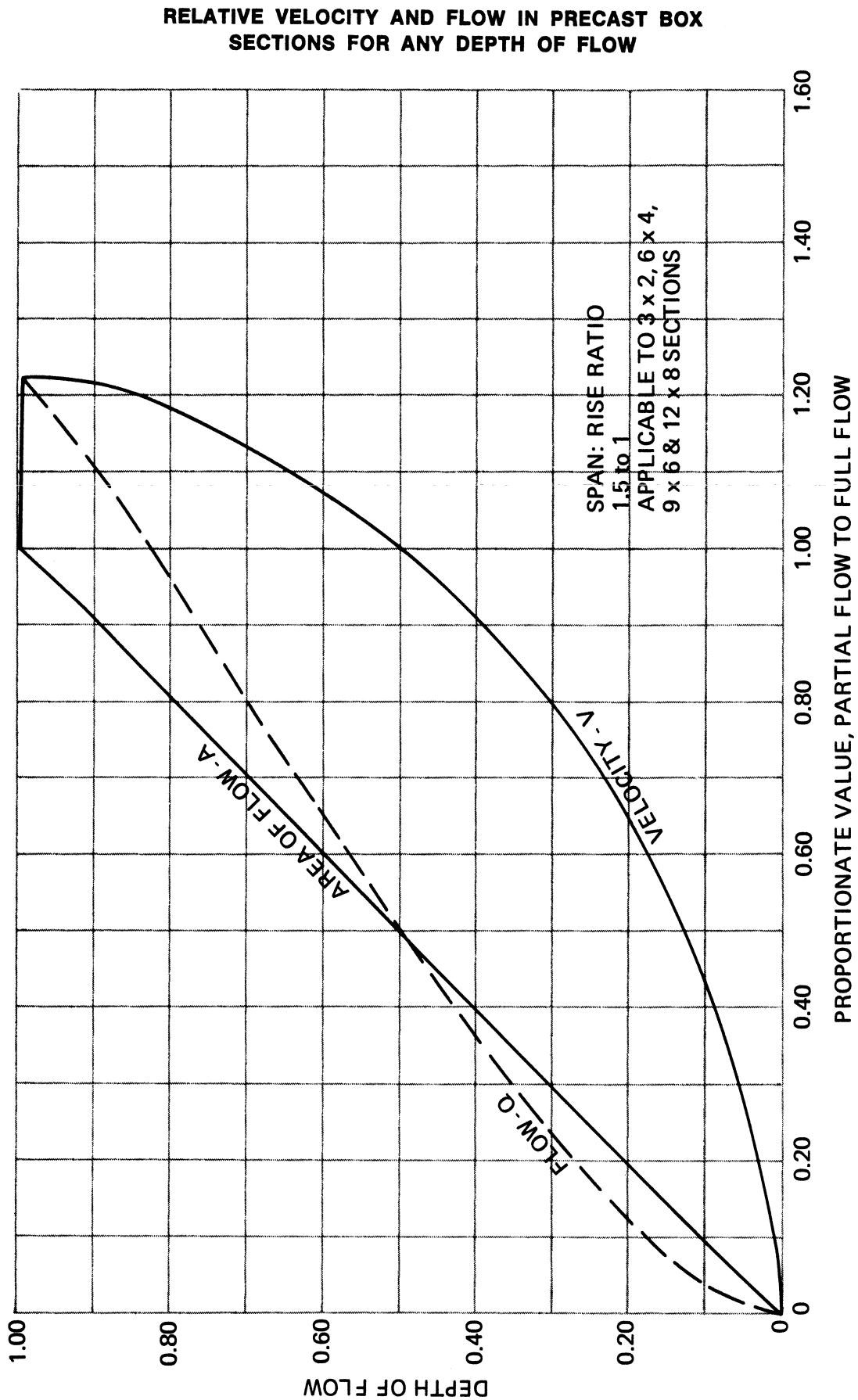


Figure 24.6

**RELATIVE VELOCITY AND FLOW IN PRECAST BOX
SECTIONS FOR ANY DEPTH OF FLOW**

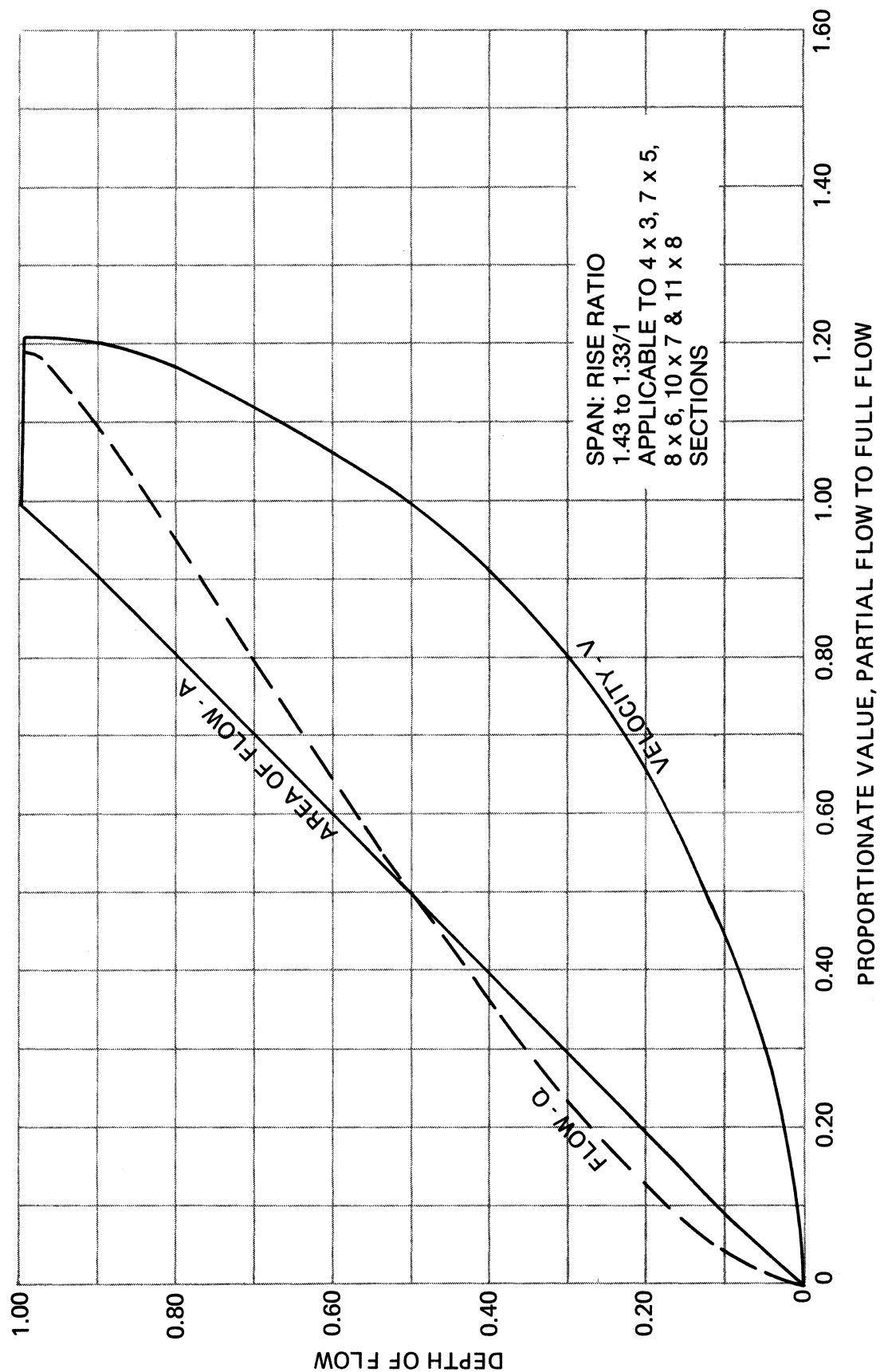


Figure 24.7

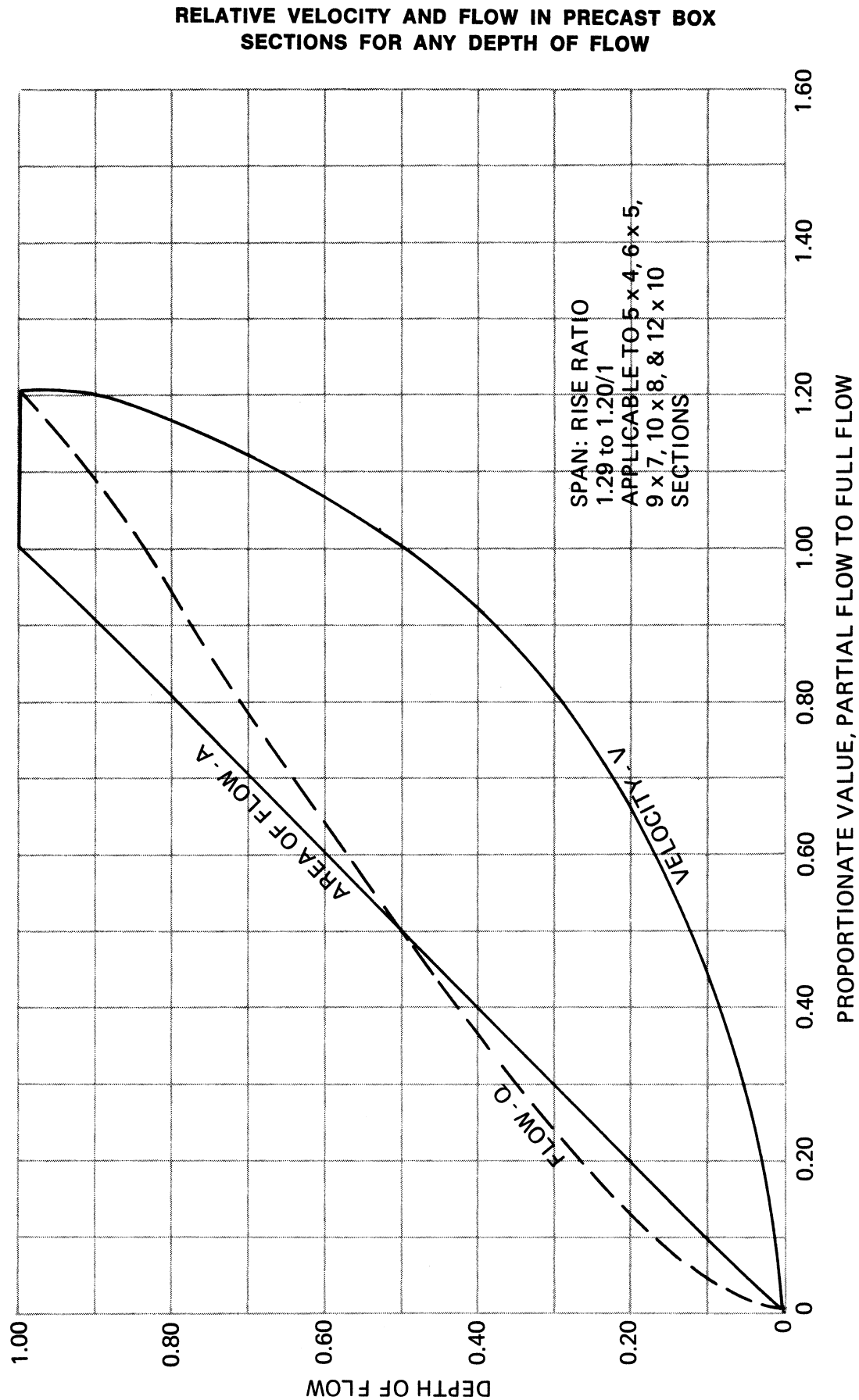


Figure 24.8

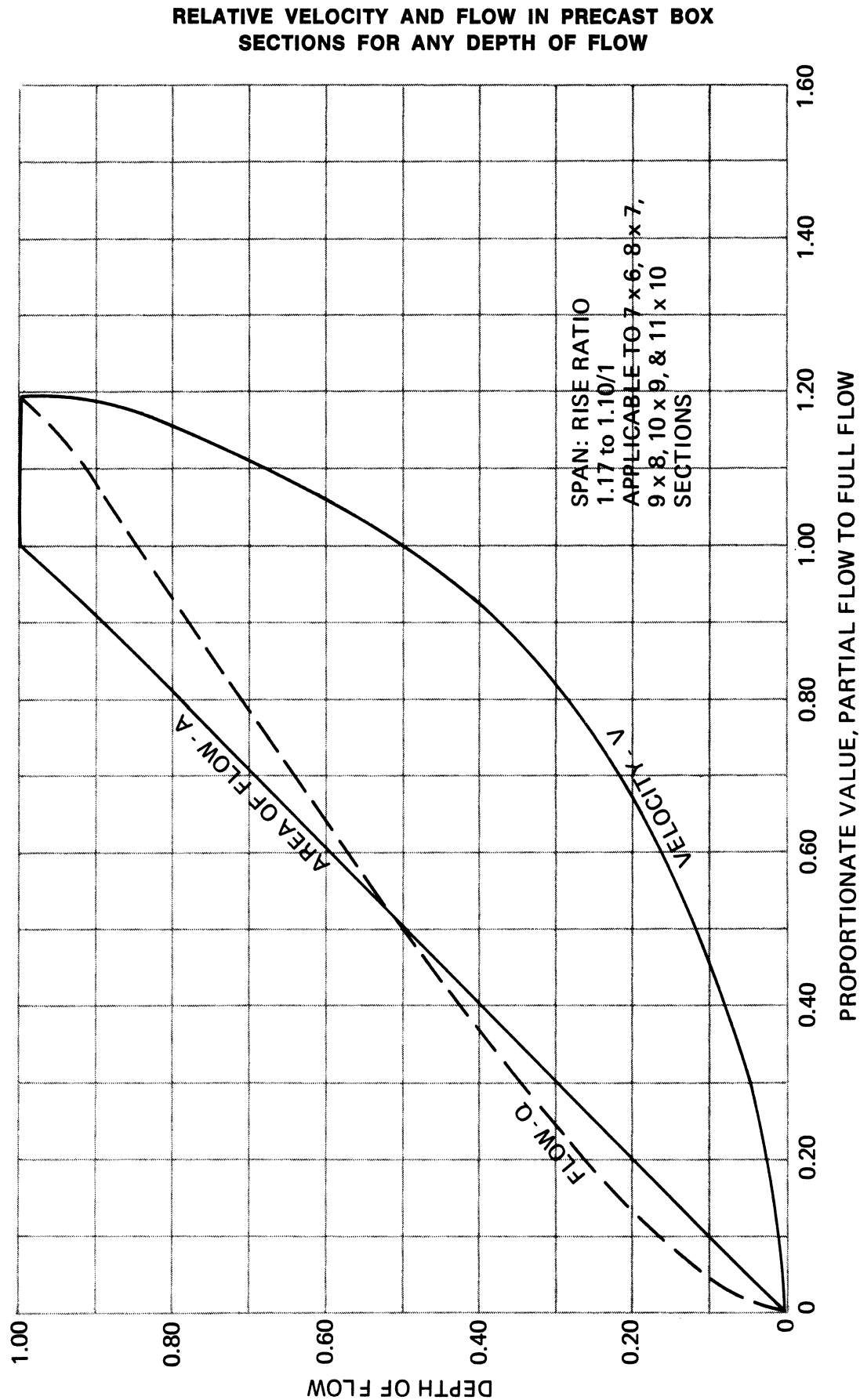


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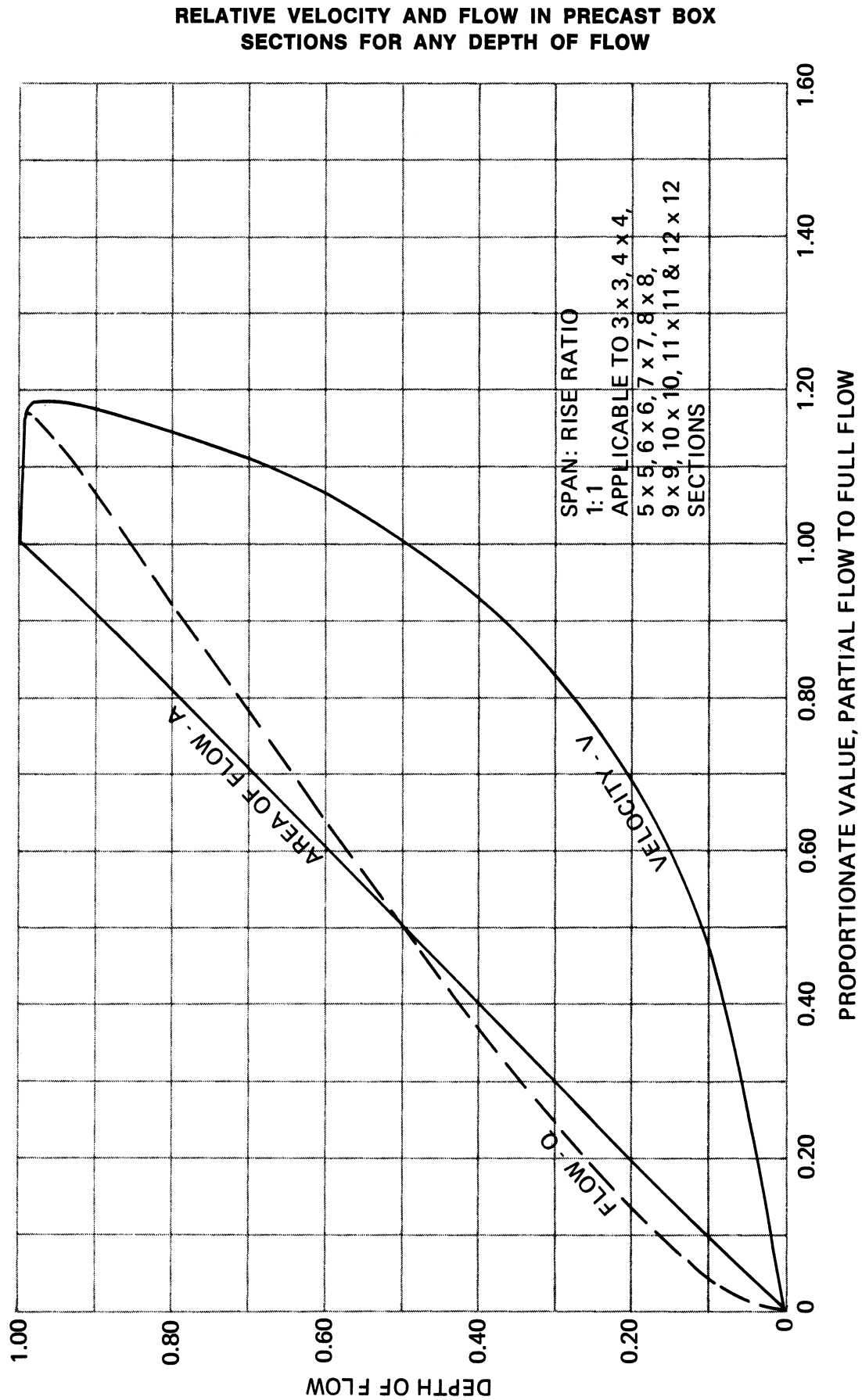
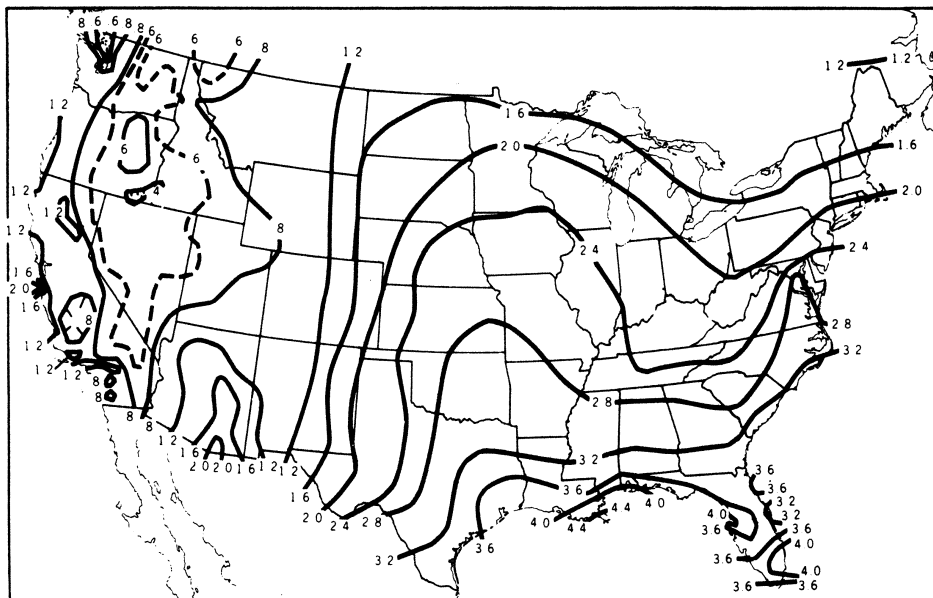


Figure 25

**MAP OF THE UNITED STATES
2-YEAR, 30-MINUTE RAINFALL INTENSITY**



ADAPTED FROM CHART 2, RAINFALL FREQUENCY ATLAS OF THE UNITED STATES,
U.S. DEPARTMENT OF COMMERCE, WEATHER BUREAU, TECHNICAL PAPER NO. 40
MAY 1961

Figure 26

INTENSITY-DURATION CURVE

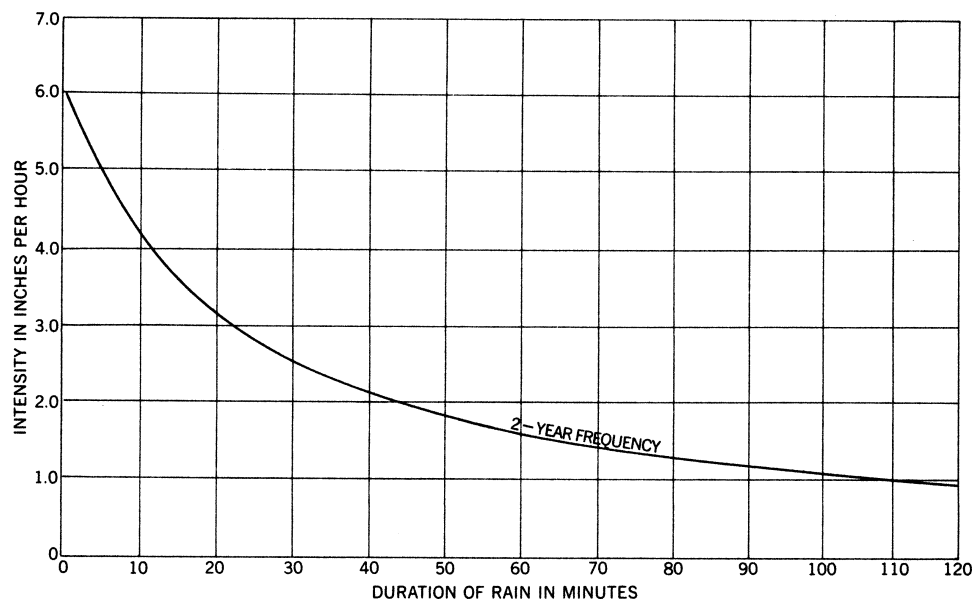


Figure 27

CALIFORNIA CHART "A" FOR CALCULATION OF "DESIGN DISCHARGES"

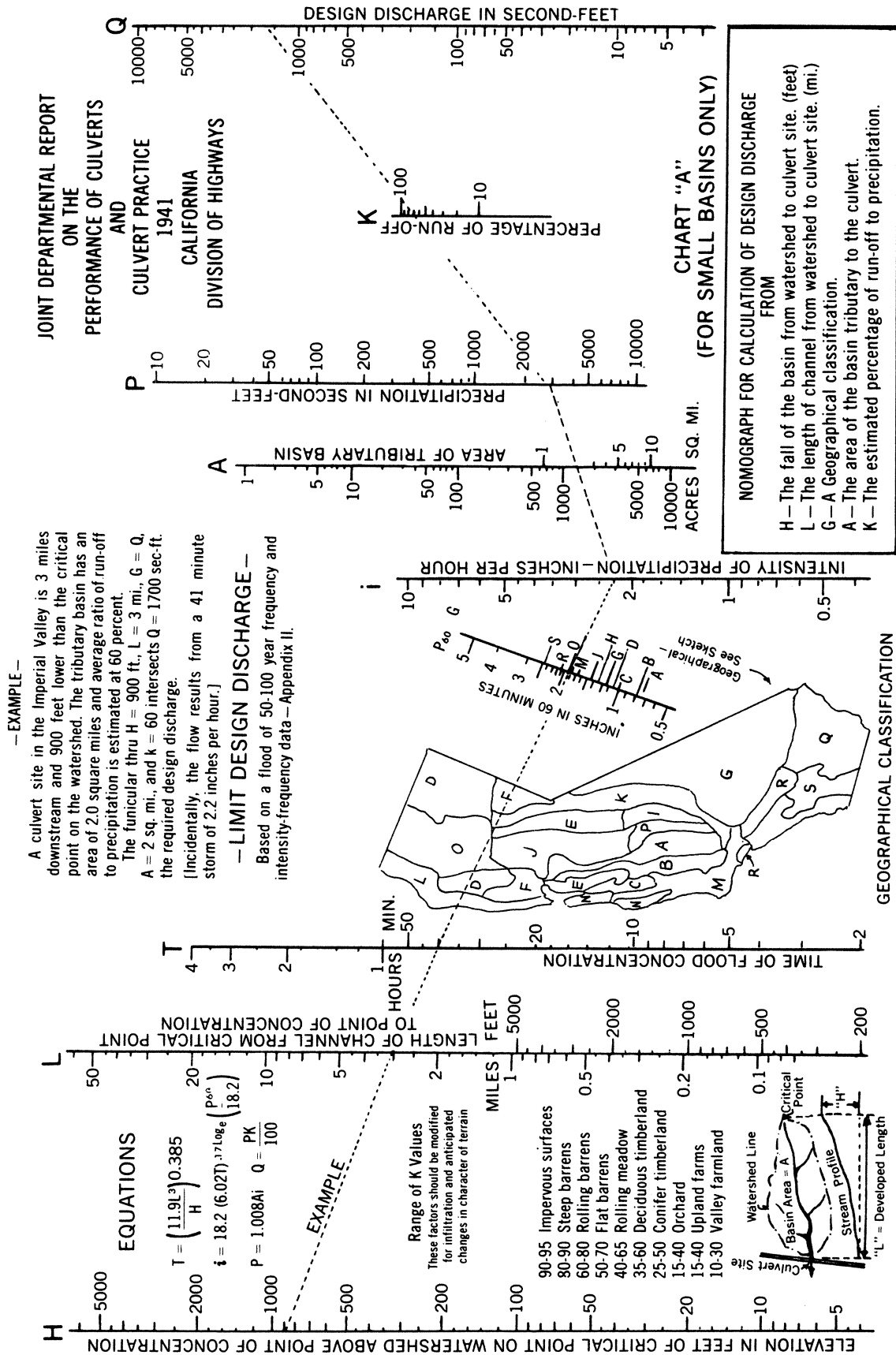
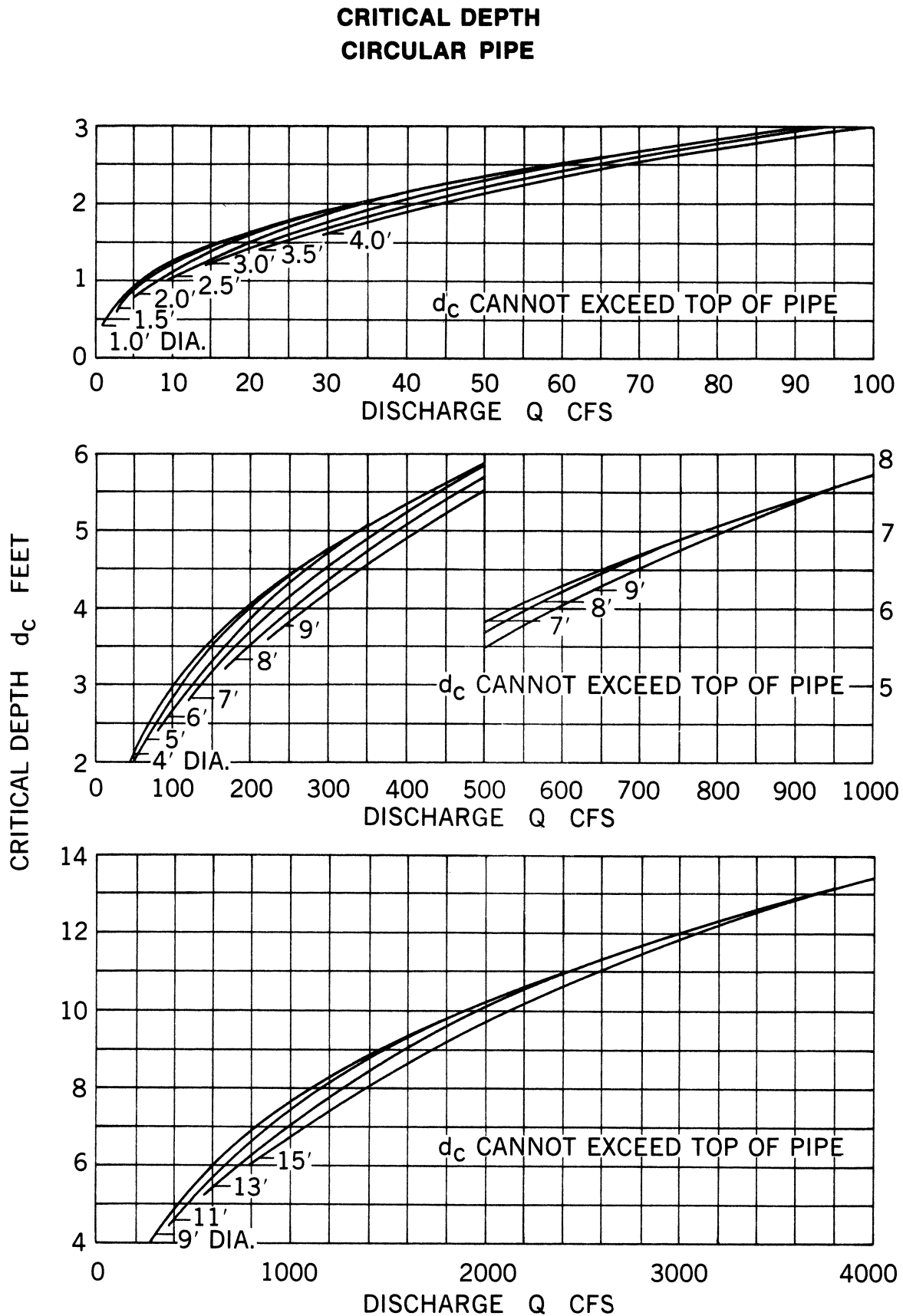
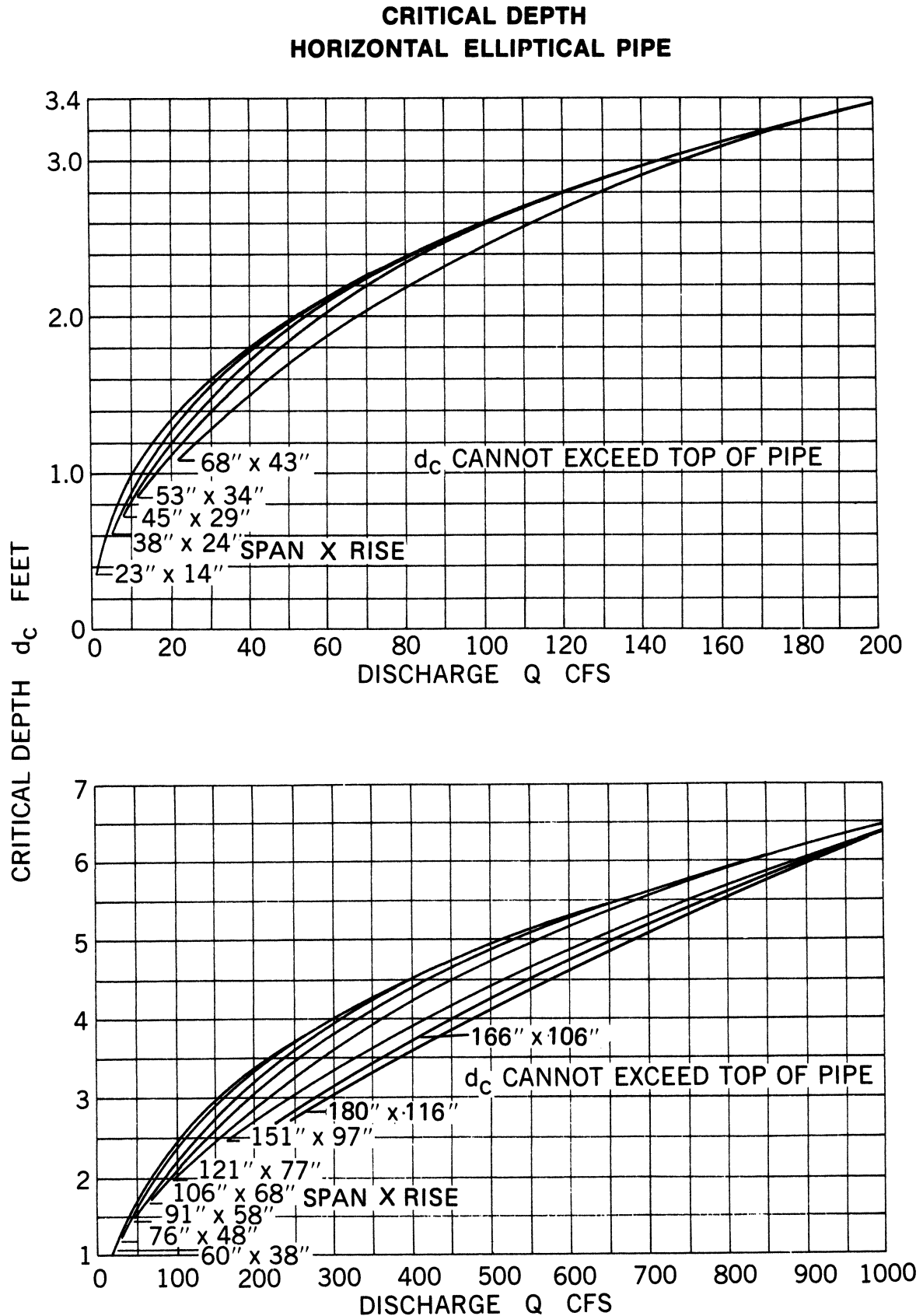


Figure 28



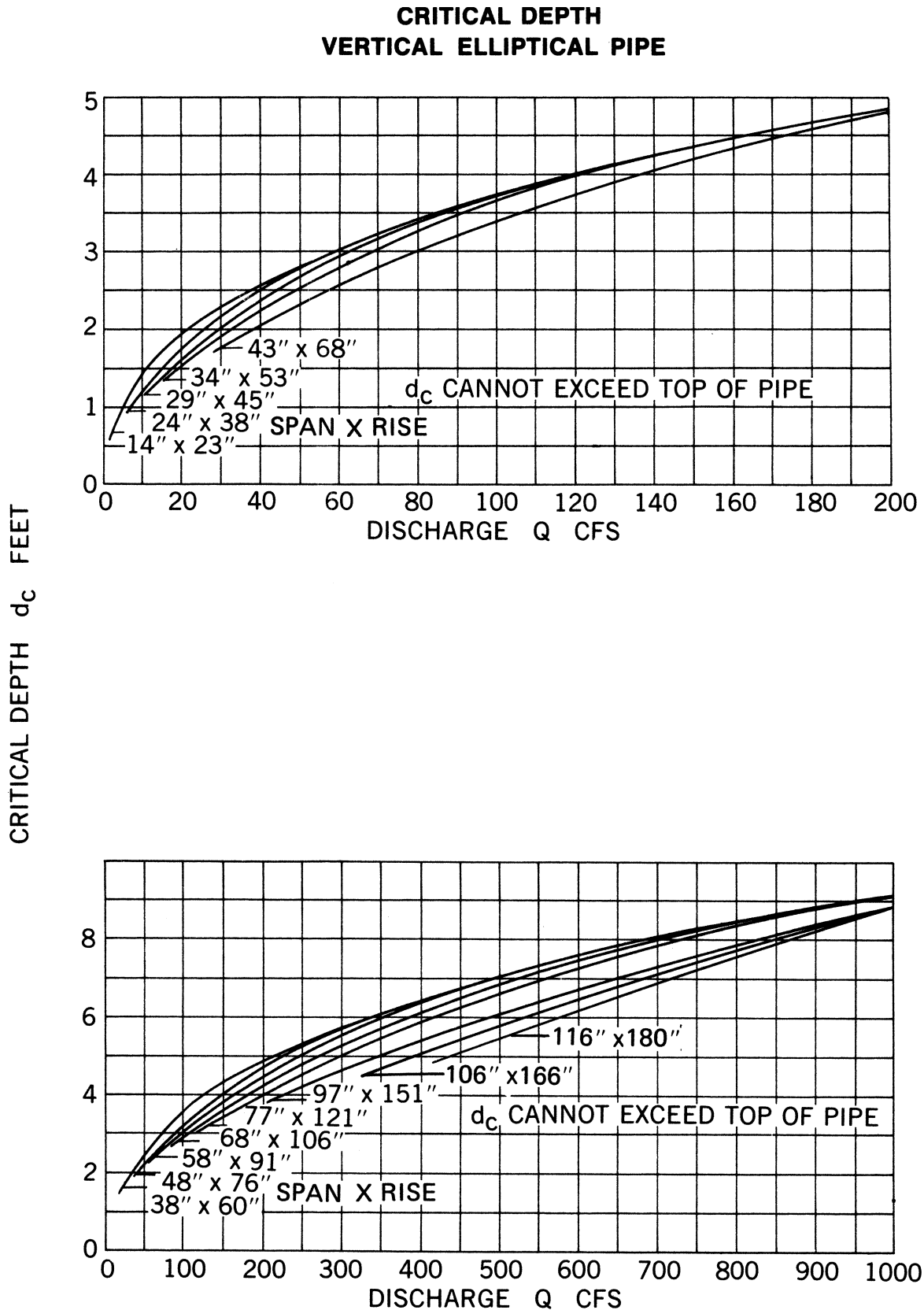
BUREAU OF PUBLIC ROADS JAN. 1964

Figure 29



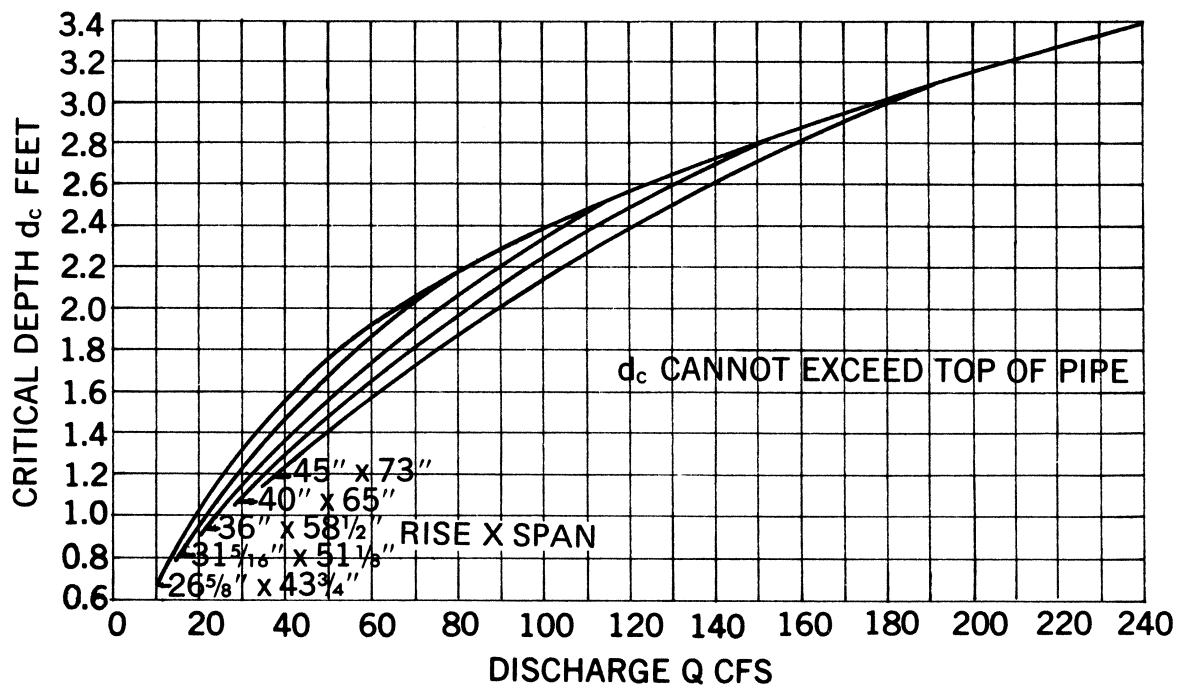
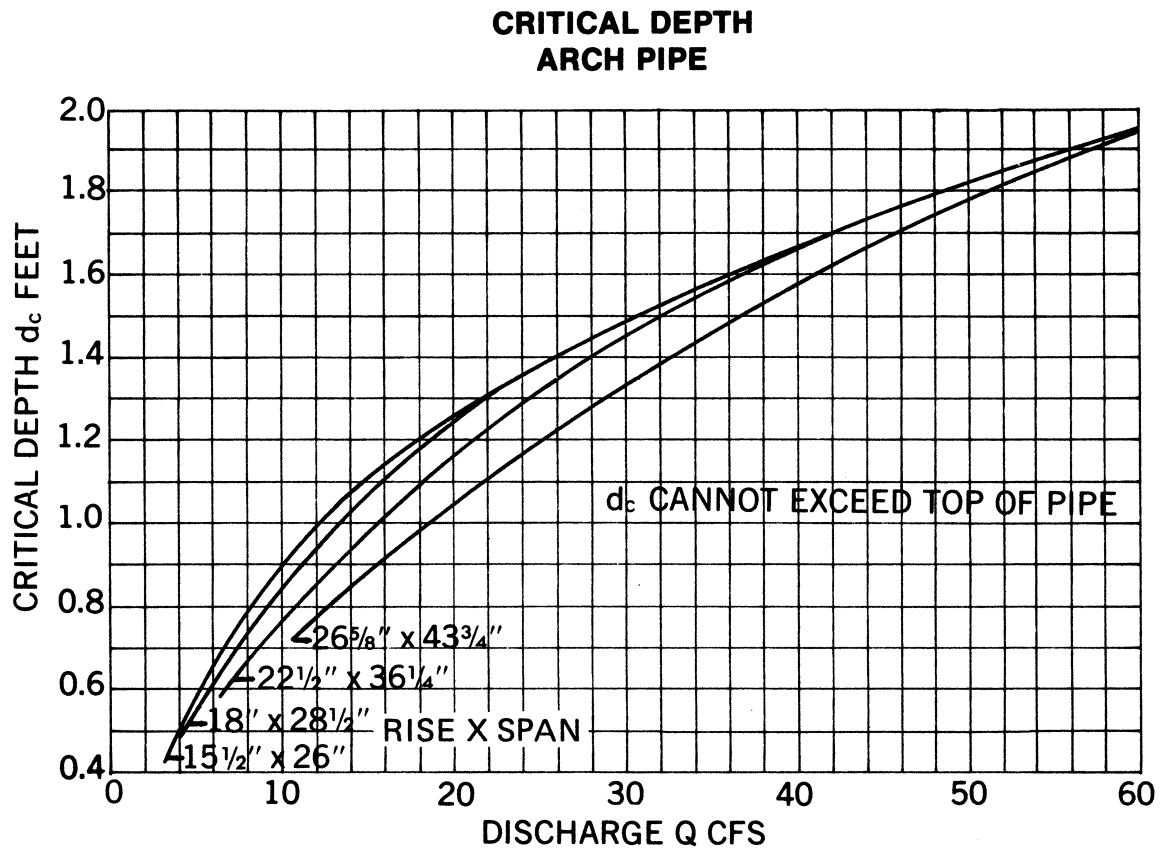
BUREAU OF PUBLIC ROADS JAN. 1964

Figure 30



BUREAU OF PUBLIC ROADS JAN. 1964

Figure 31.1



BUREAU OF PUBLIC ROADS, JAN. 1964

Figure 31.2

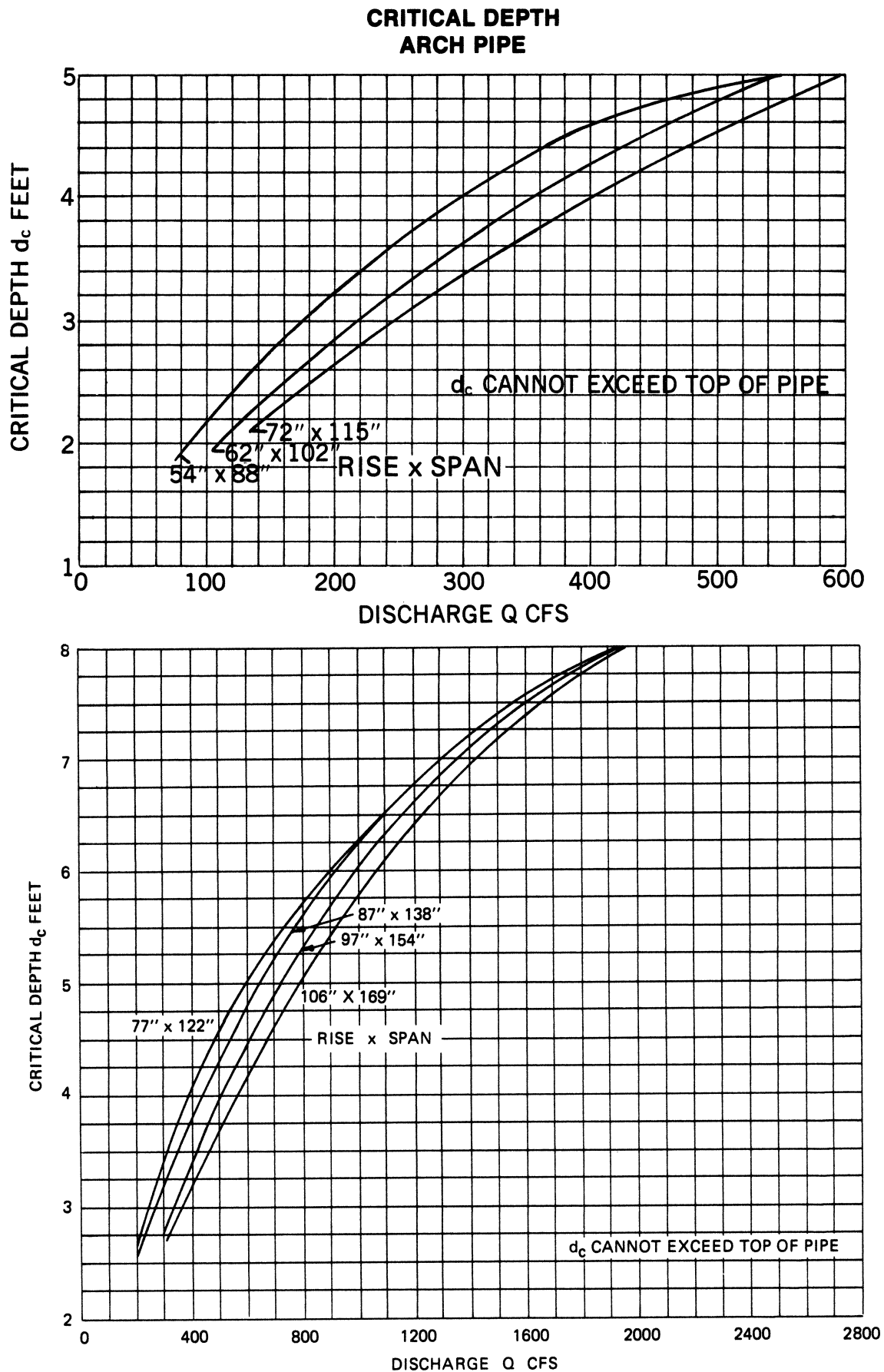


Figure 32

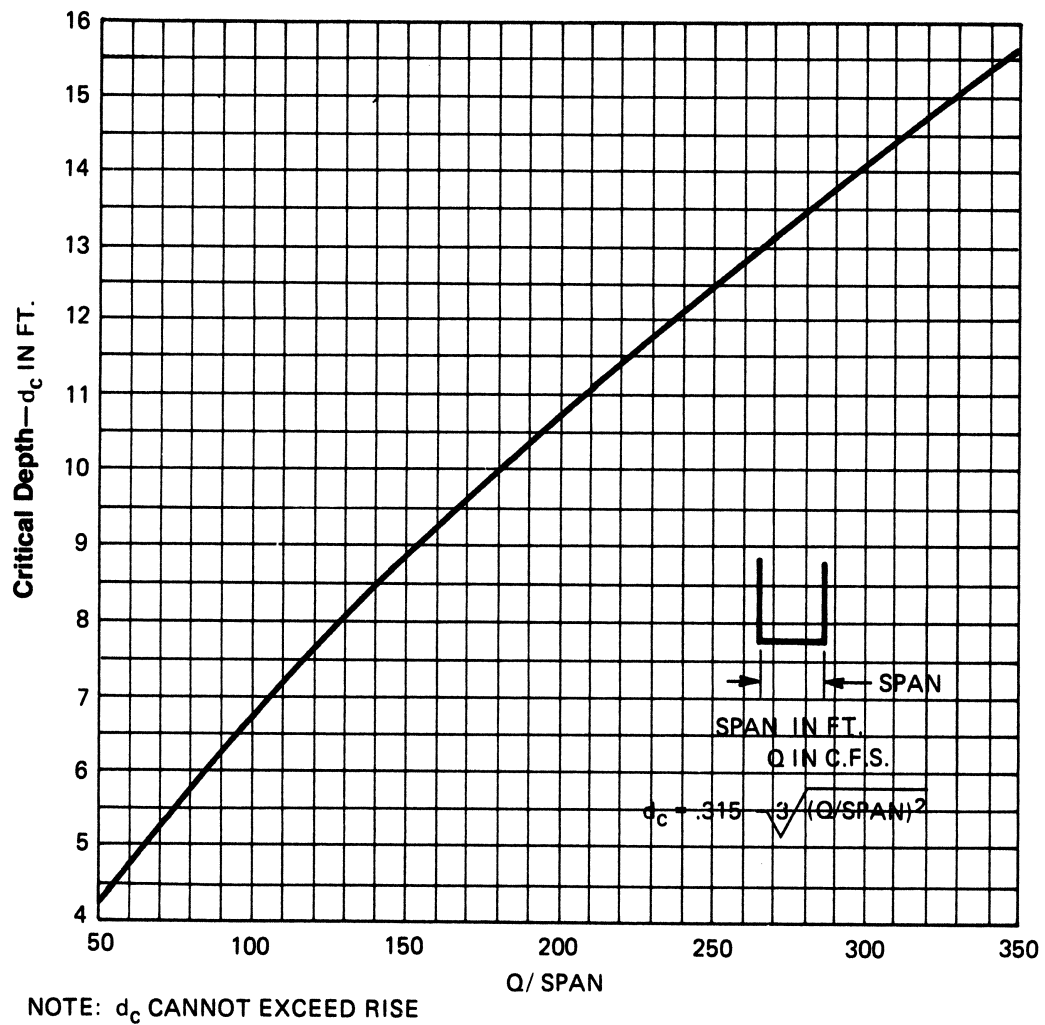
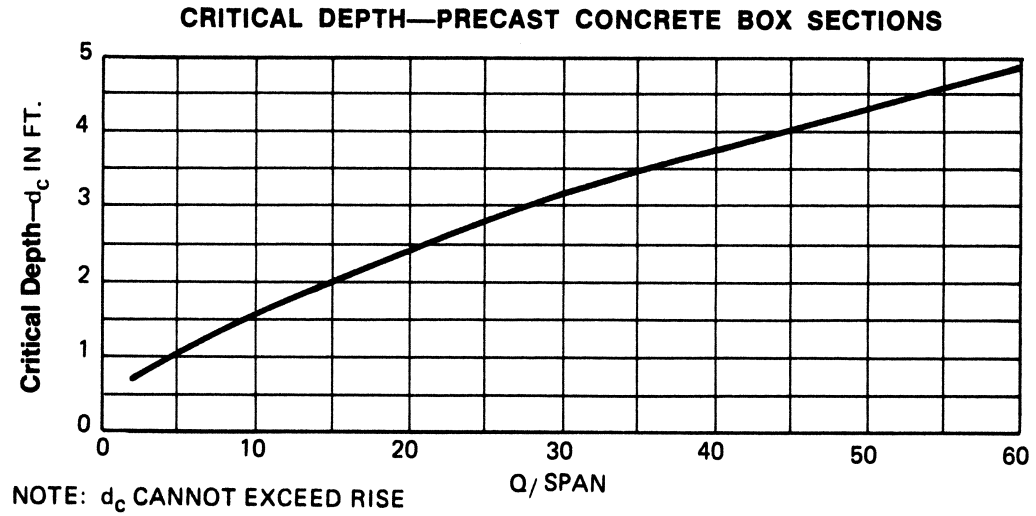


Figure 33

HEADWATER DEPTH FOR CIRCULAR CONCRETE PIPE CULVERTS WITH INLET CONTROL

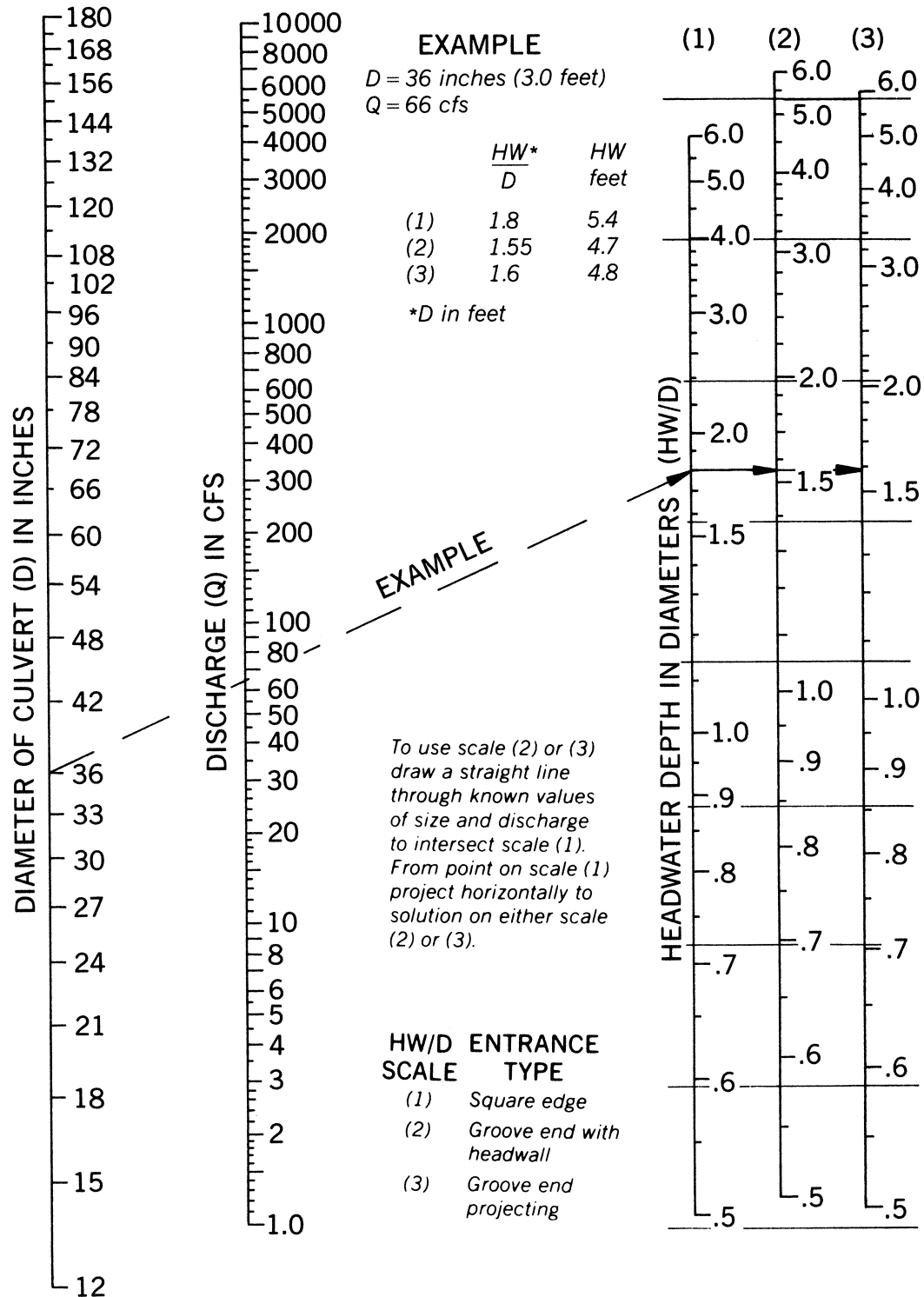
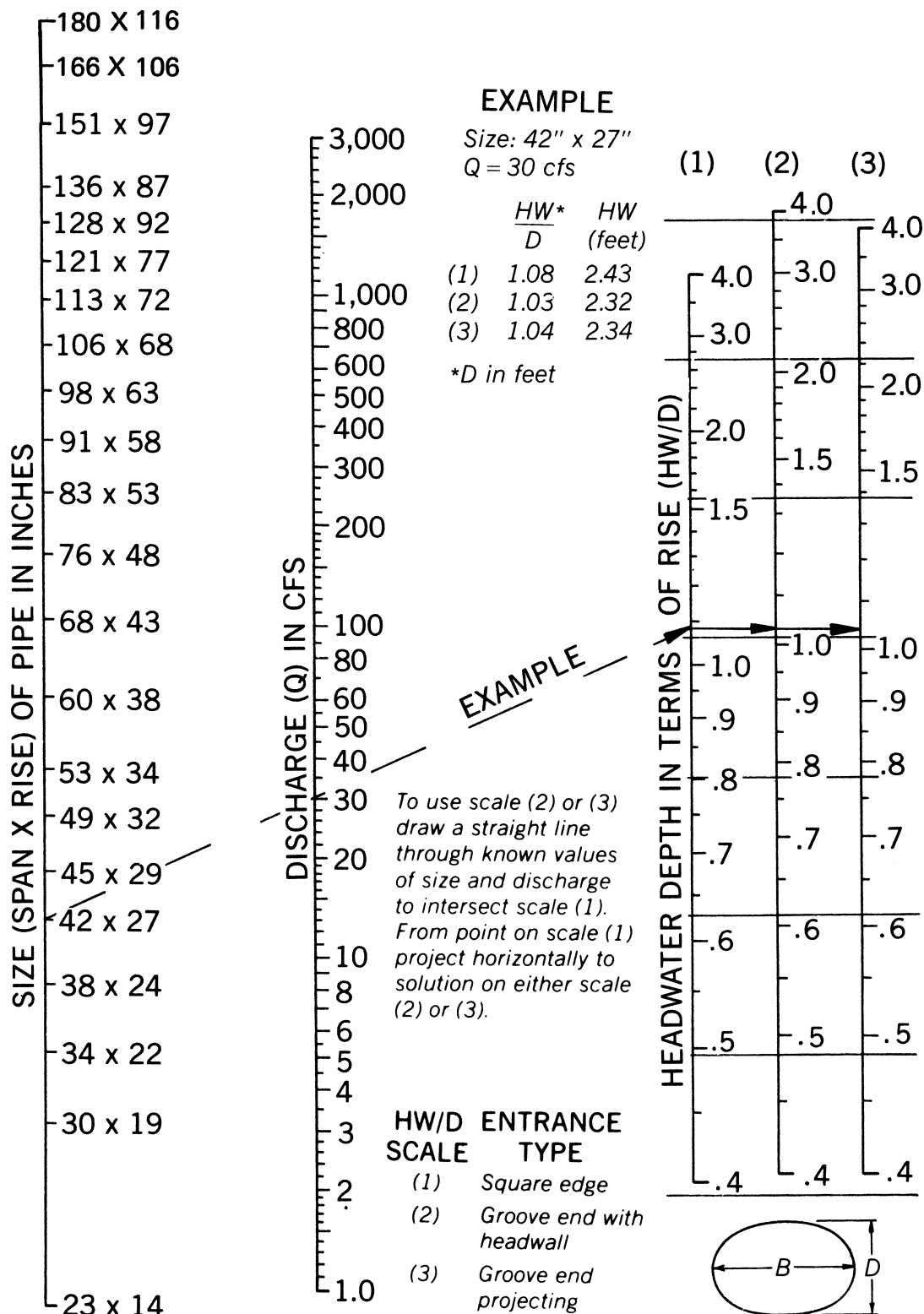


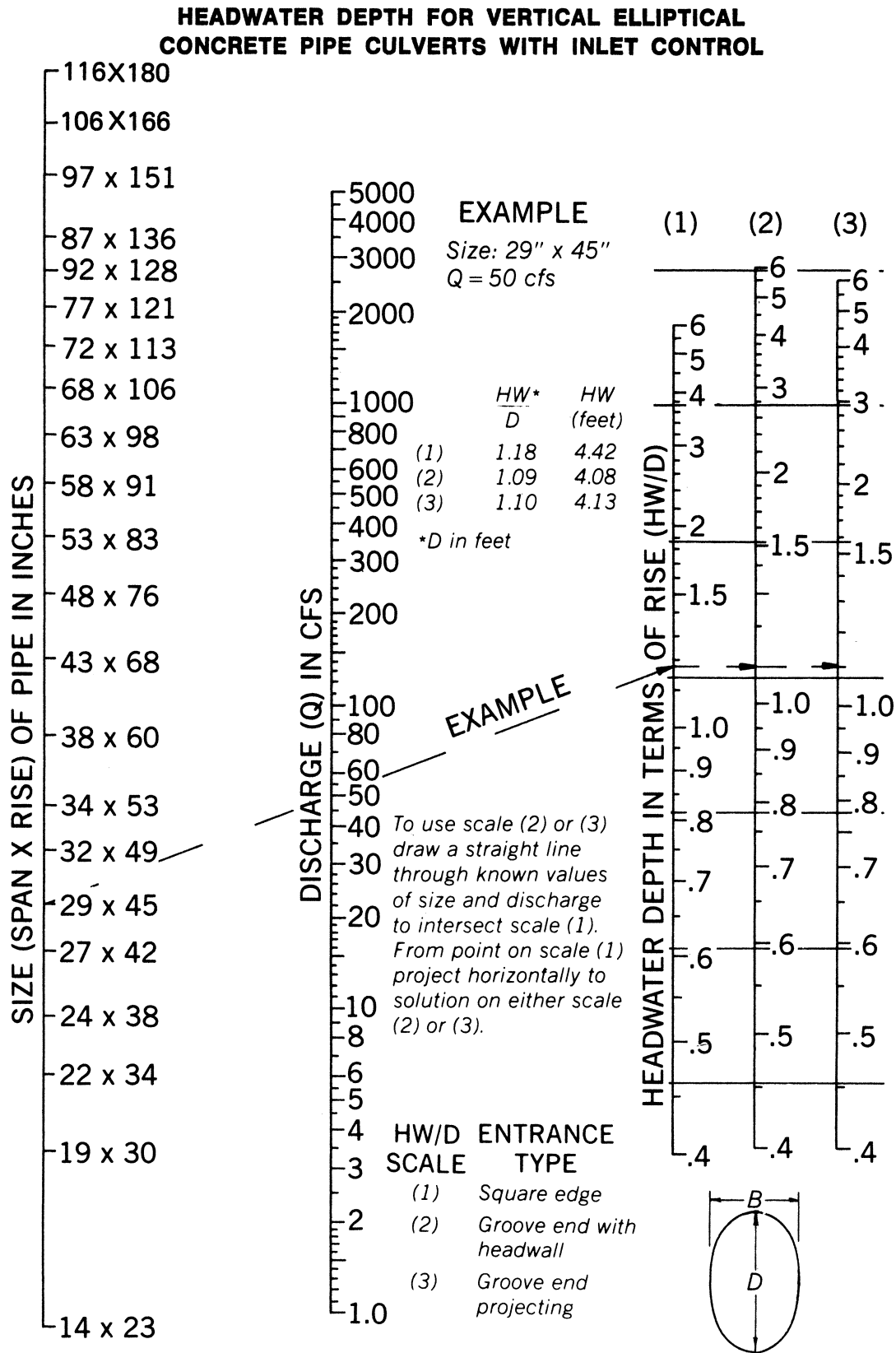
Figure 34

HEADWATER DEPTH FOR HORIZONTAL ELLIPTICAL CONCRETE PIPE CULVERTS WITH INLET CONTROL



BUREAU OF PUBLIC ROADS JAN. 1963

Figure 35



BUREAU OF PUBLIC ROADS JAN. 1963

Figure 36

HEADWATER DEPTH FOR CONCRETE ARCH CULVERTS WITH INLET CONTROL

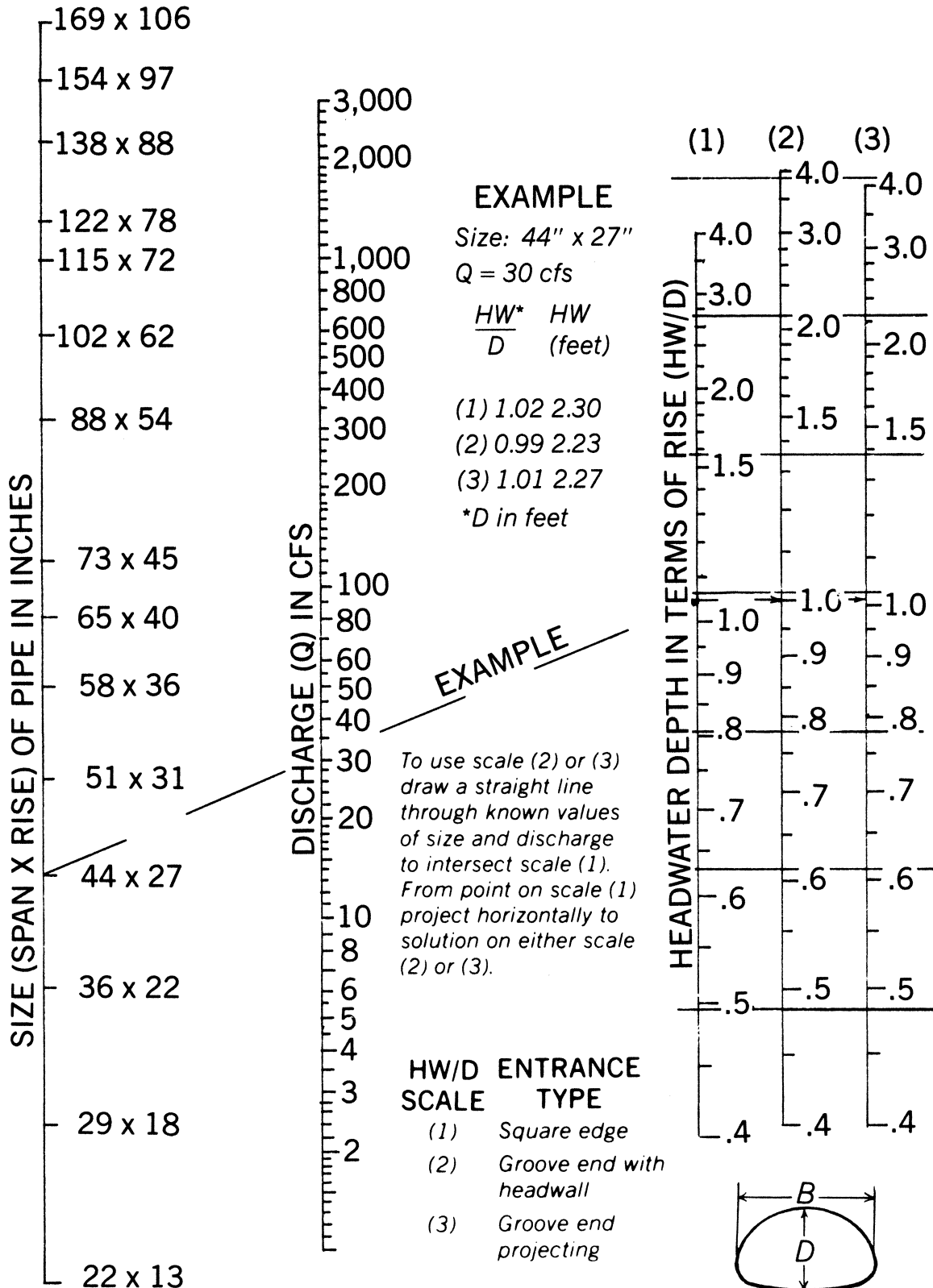
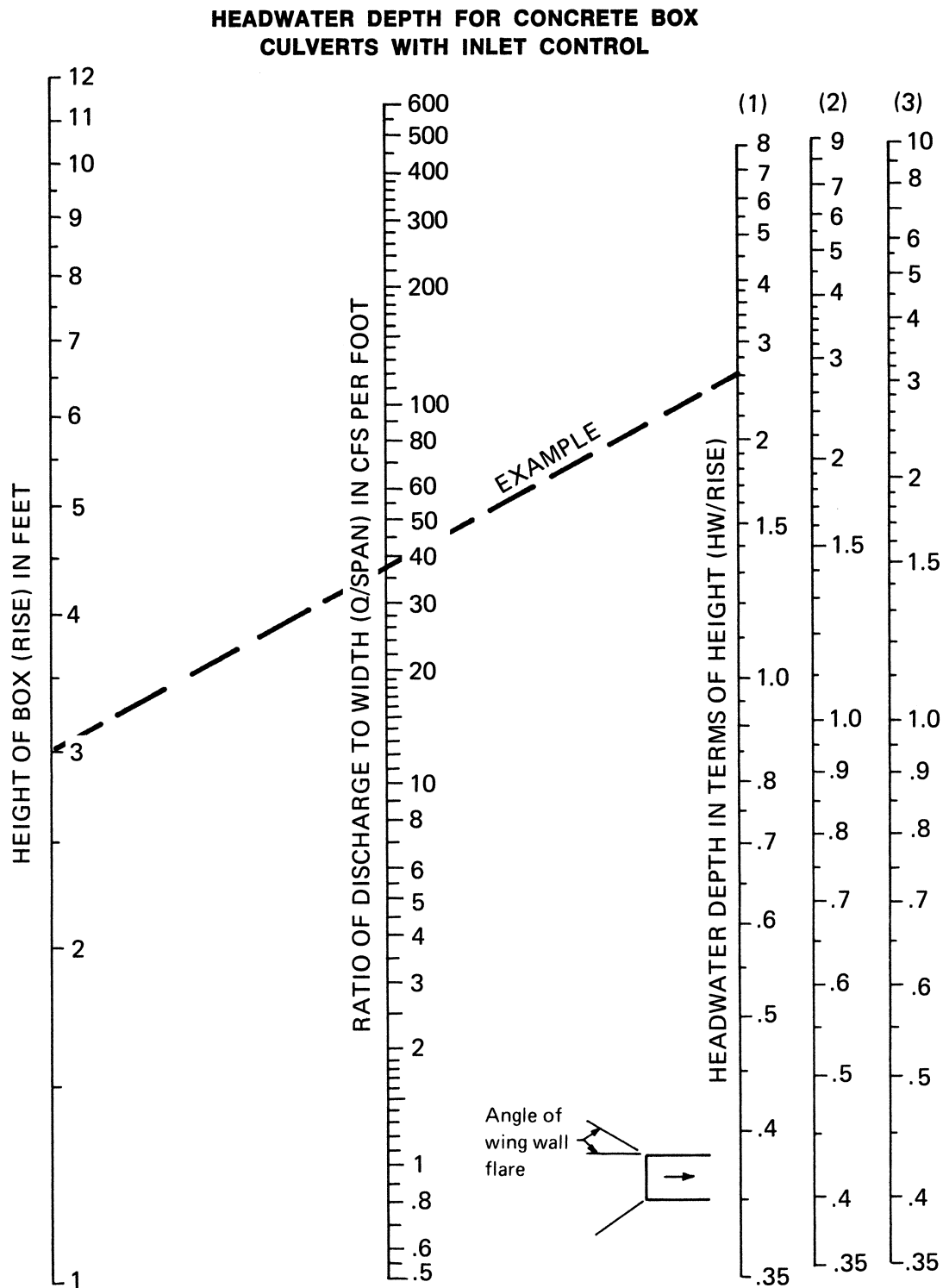


Figure 37



EXAMPLE		
6' x 3' Box Q = 225 cfs		
Q/Span = 37.5 cfs/ft		
Inlet	HW Rise	HW ft
(1)	2.6	7.8

HW Rise	SCALE	WING WALL FLARE
(1)		30° to 75°
(2)		90° and 15°
(3)		0° (extensions of sides)

To use scale (2) or (3) project horizontally to scale (1), then use straight inclined line through rise and Q scales, or reverse as illustrated.

BUREAU OF PUBLIC ROADS - JAN 1963

Figure 38

**HEAD FOR CIRCULAR CONCRETE PIPE
CULVERTS FLOWING FULL**
 $n = 0.012$

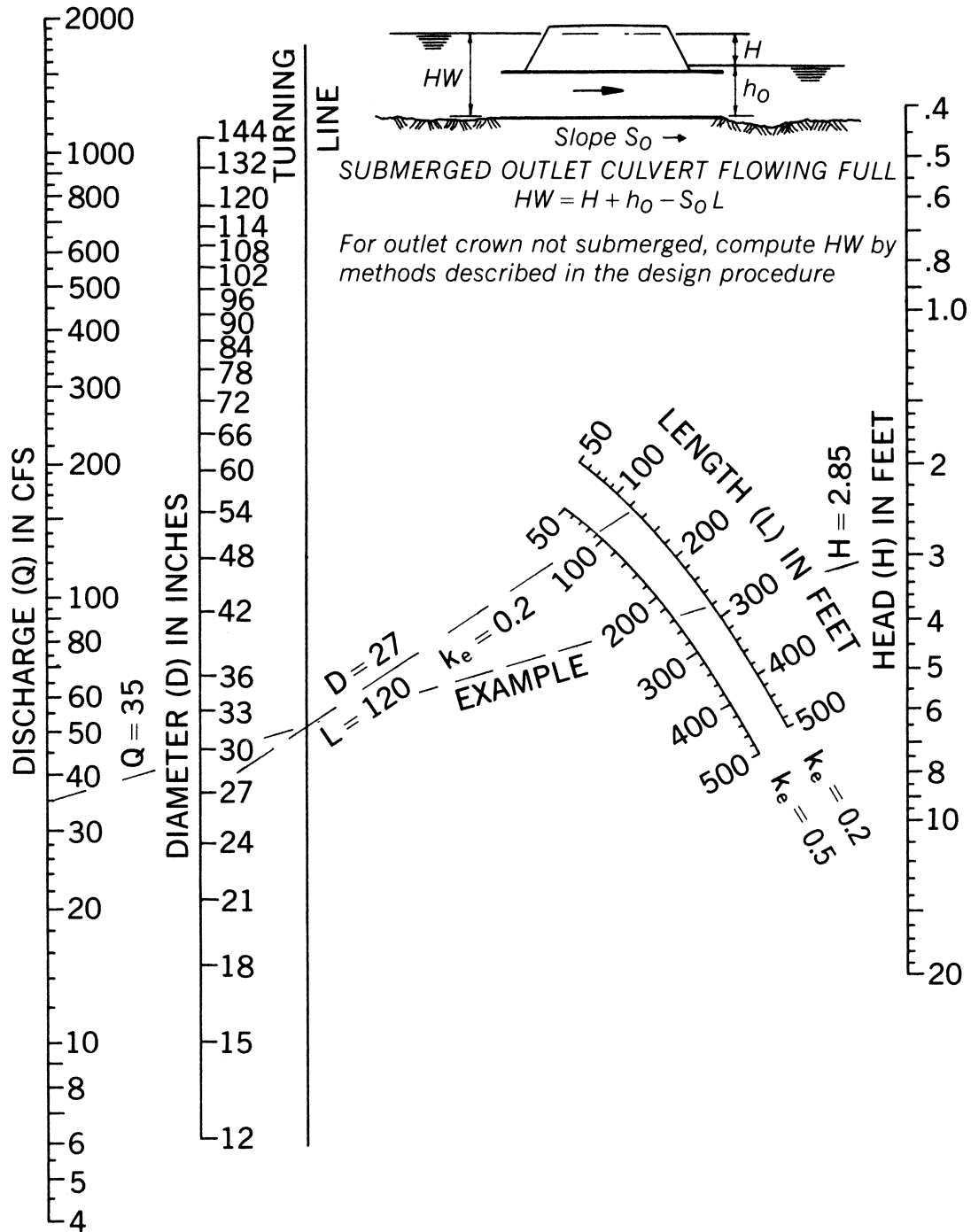


Figure 39

HEAD FOR ELLIPTICAL CONCRETE PIPE CULVERTS FLOWING FULL

$n = 0.012$

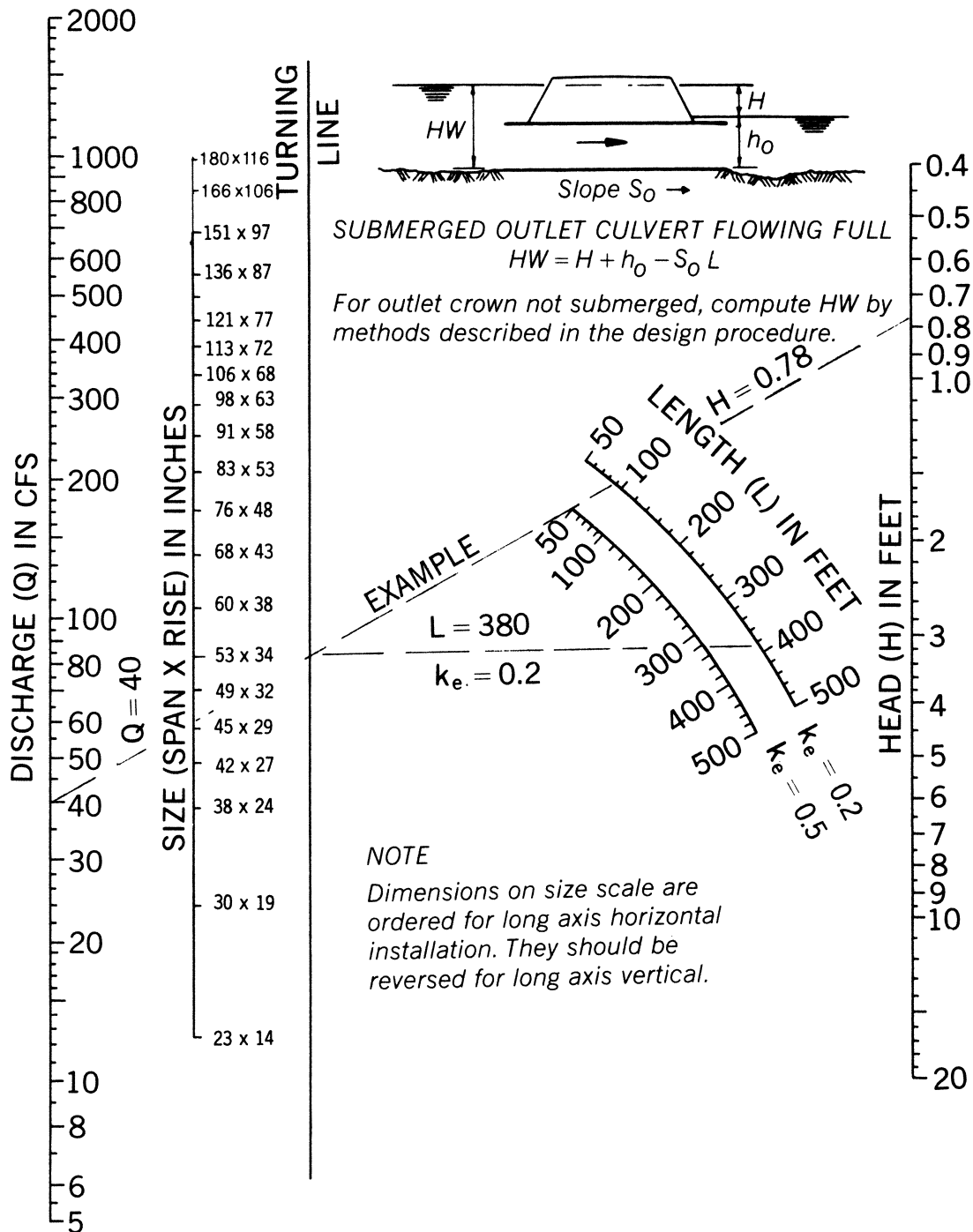


Figure 40

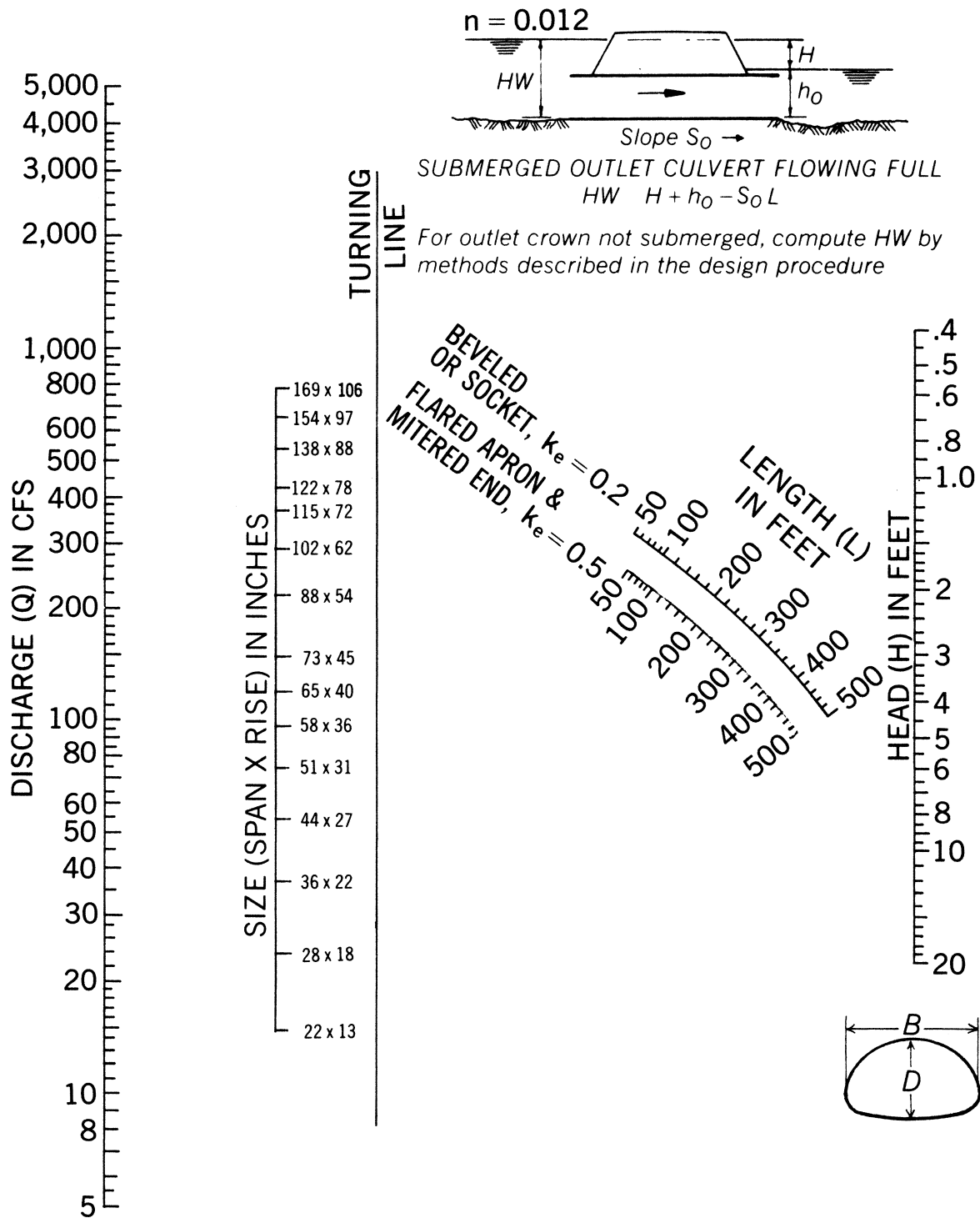
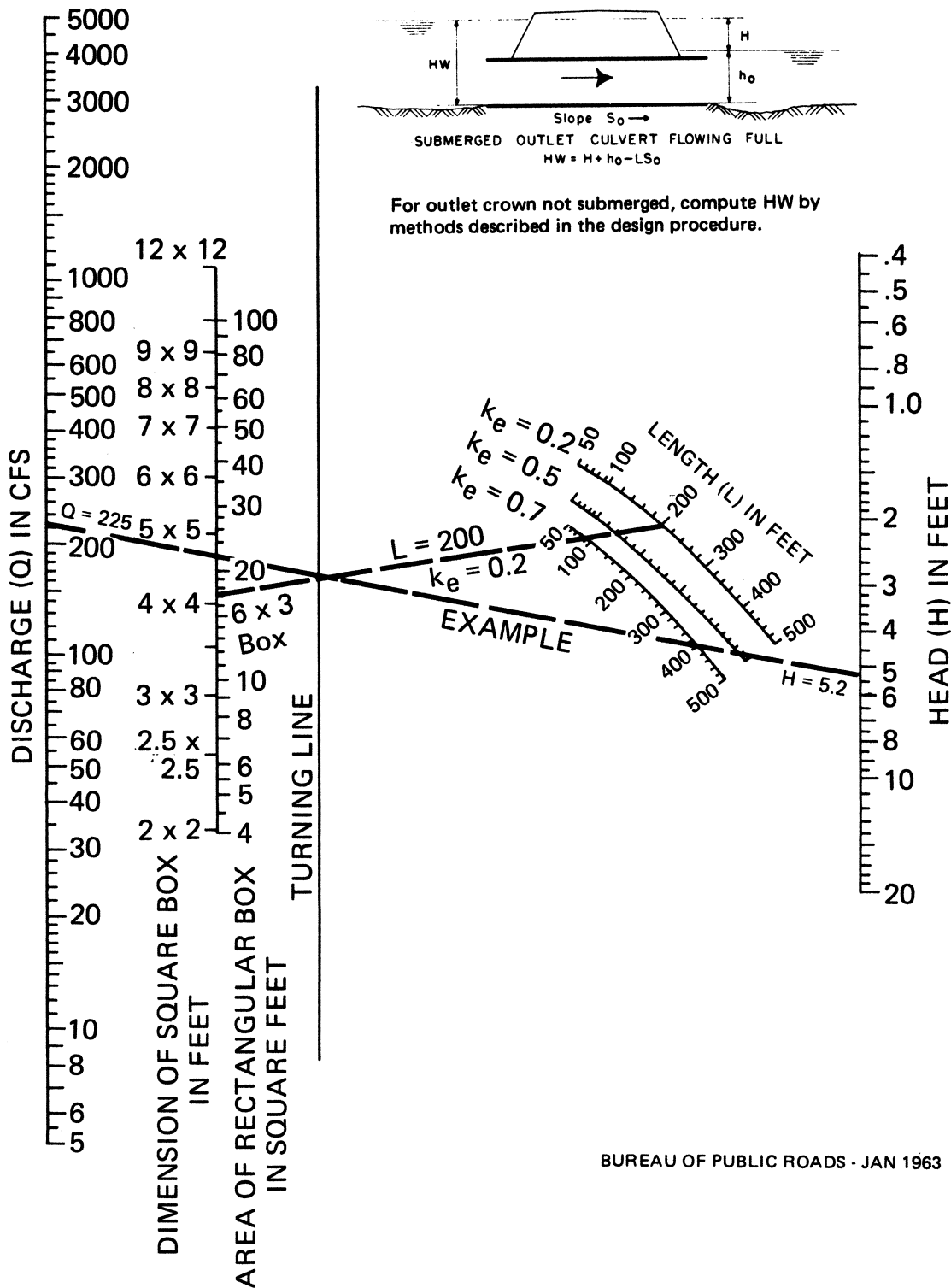
HEAD FOR CONCRETE ARCH CULVERTS FLOWING FULL

Figure 41

**HEAD FOR CONCRETE BOX
CULVERTS FLOWING FULL**
 $n = 0.012$



BUREAU OF PUBLIC ROADS - JAN 1963

Figure 42

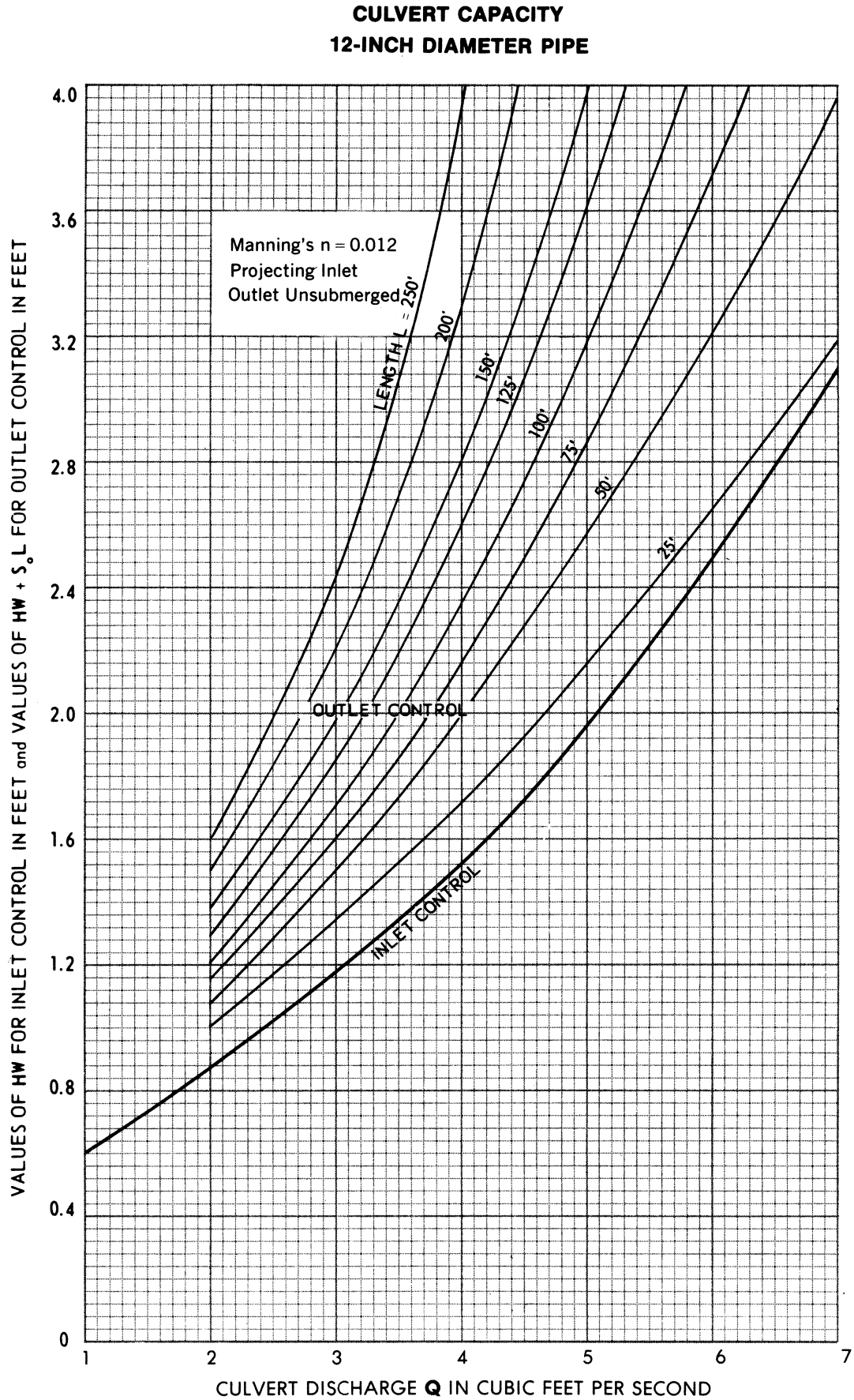


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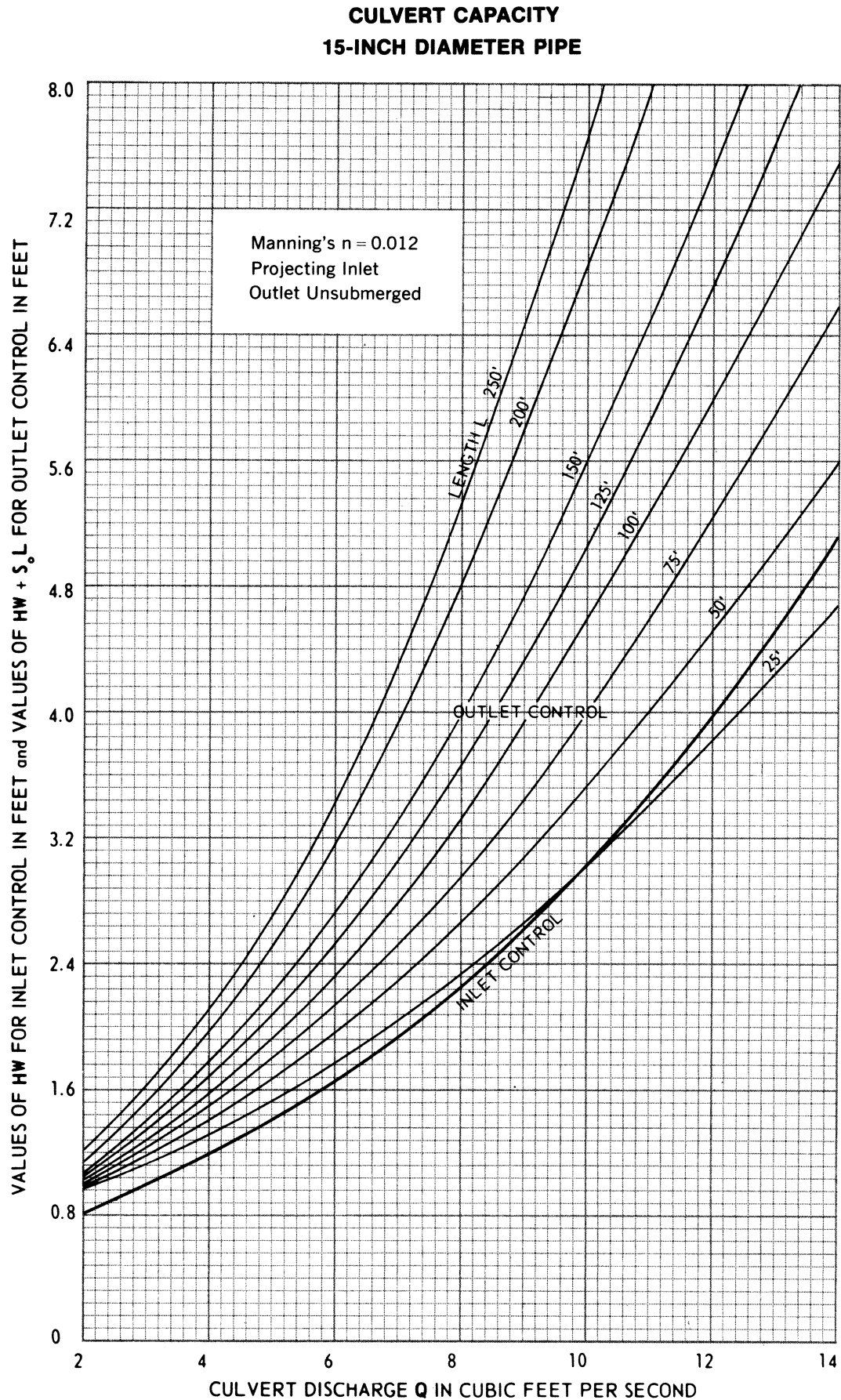


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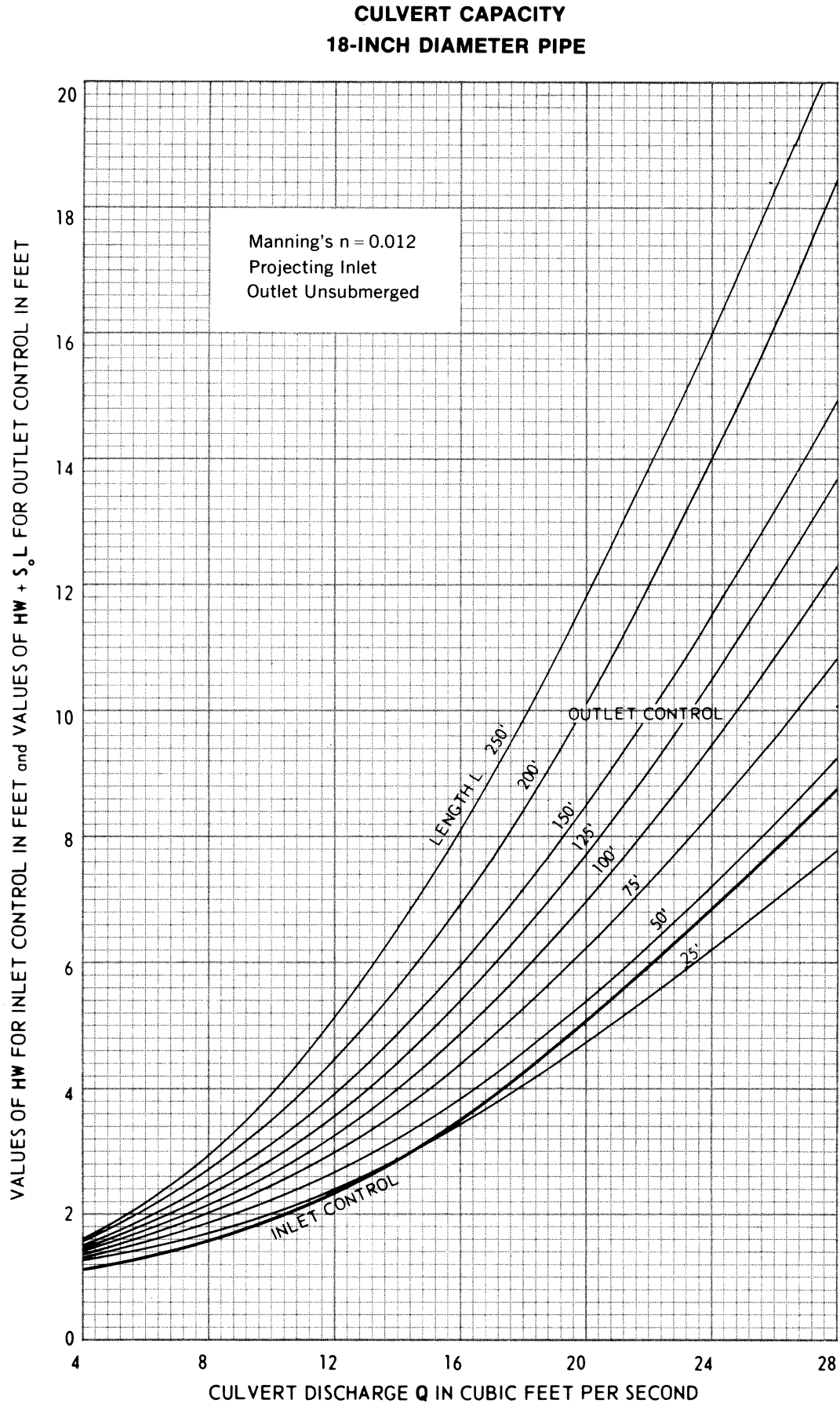


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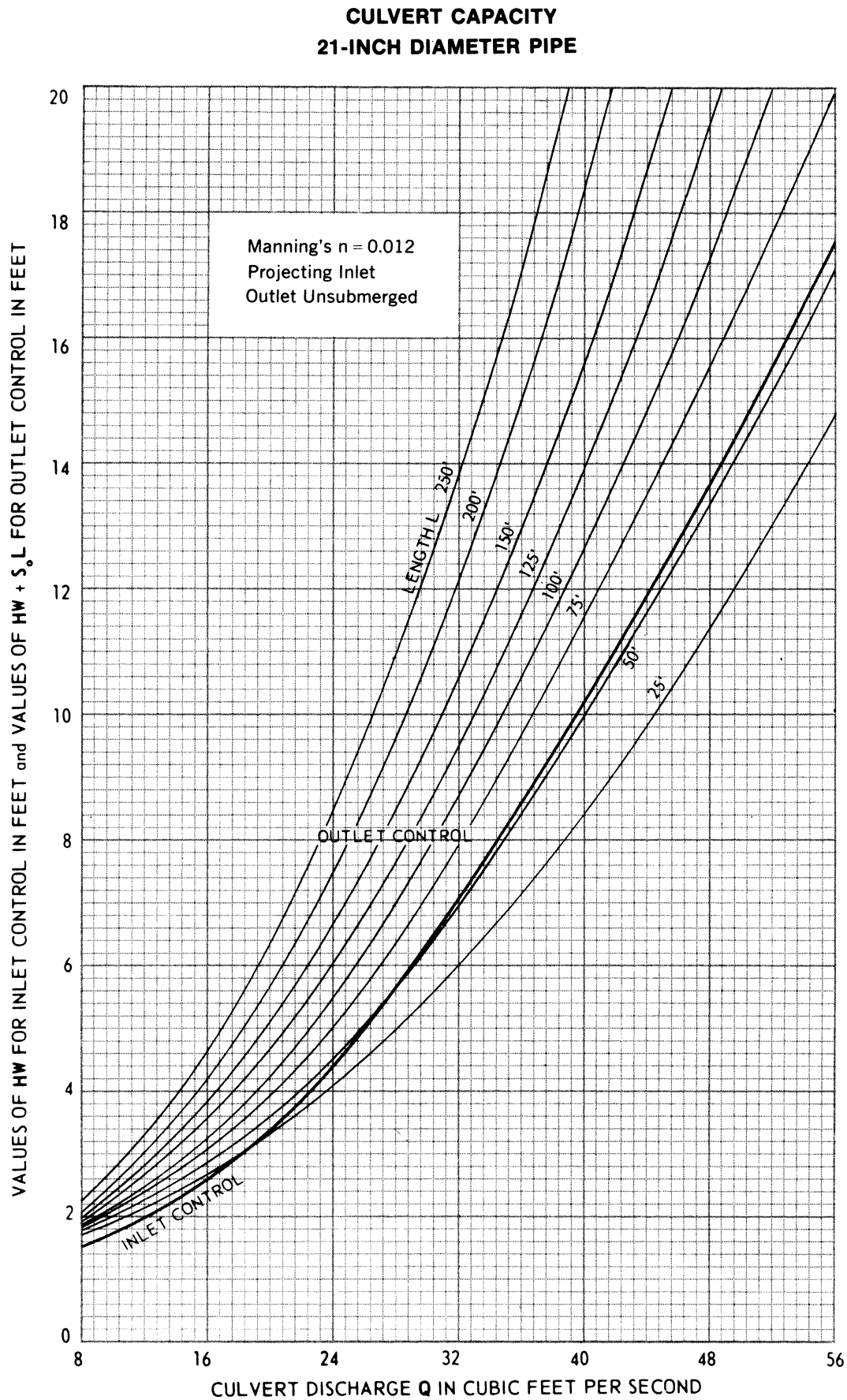


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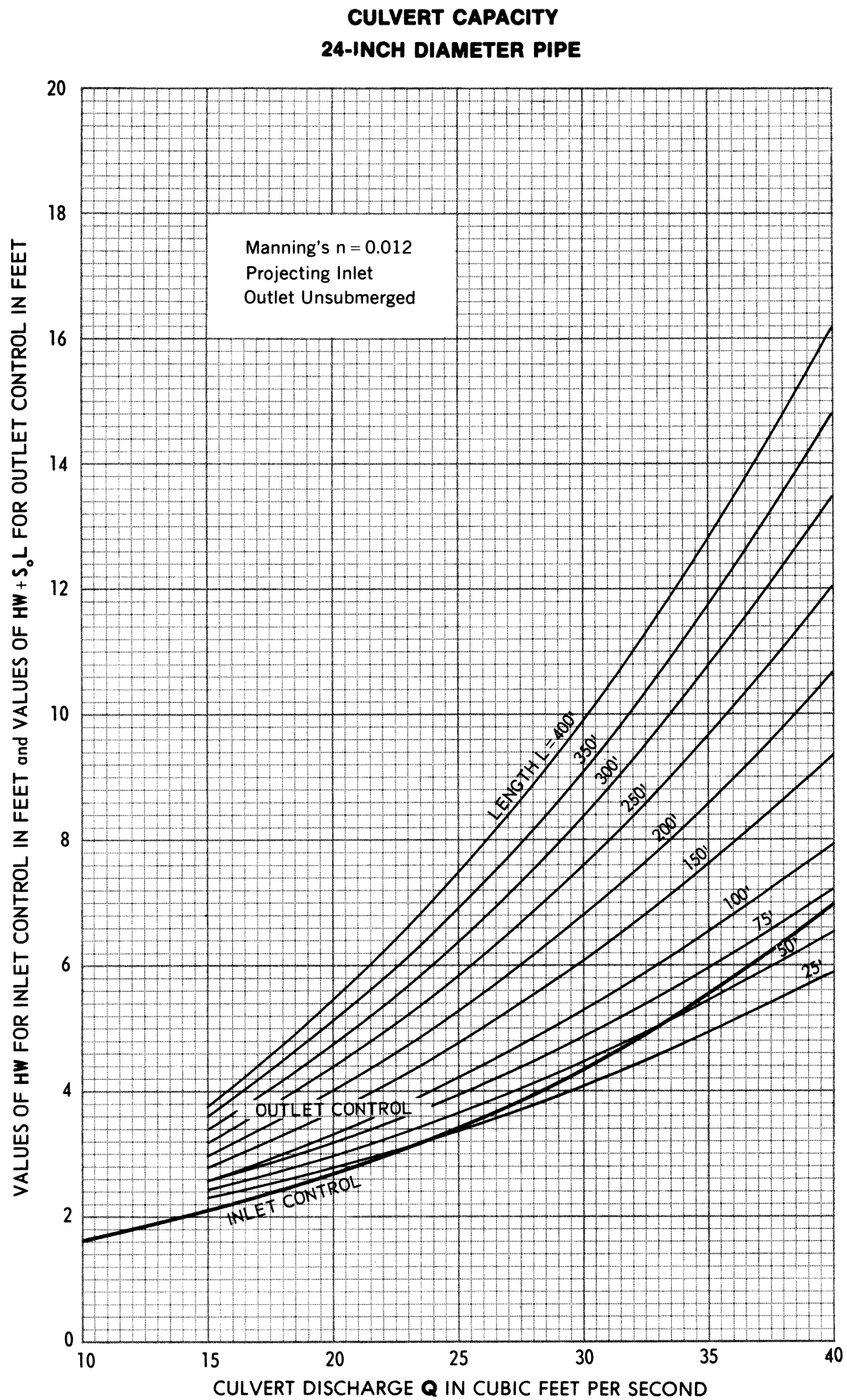


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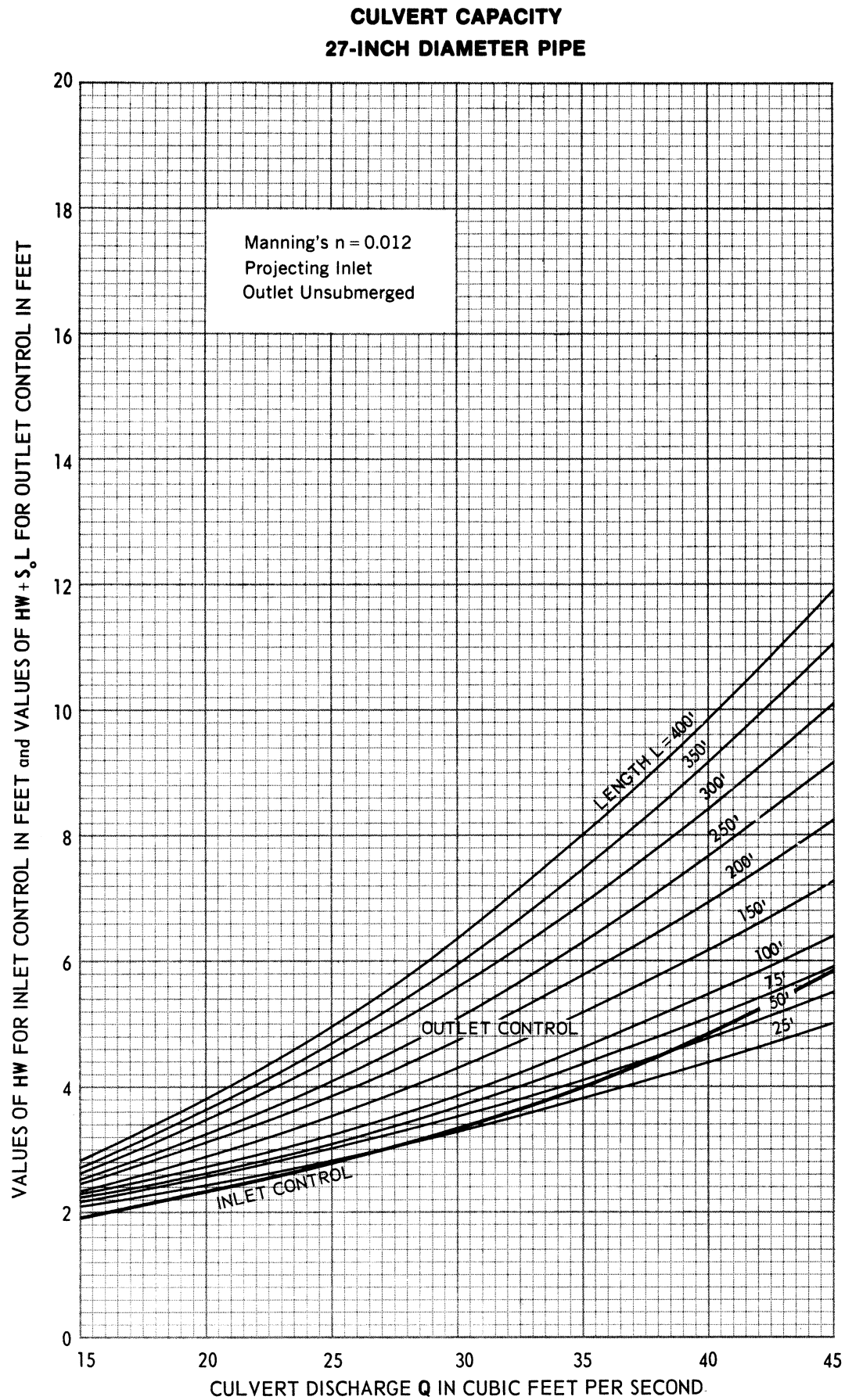


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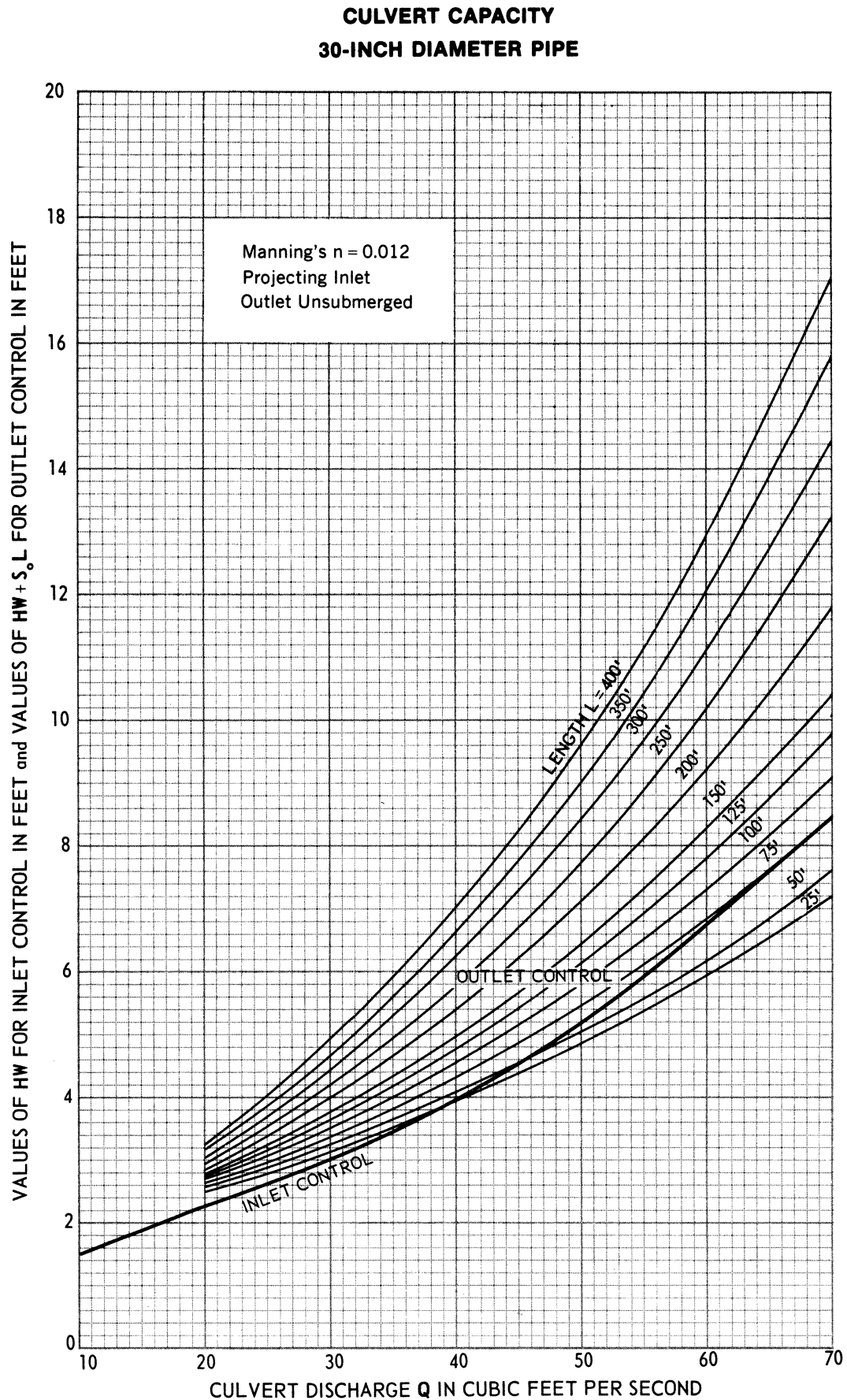


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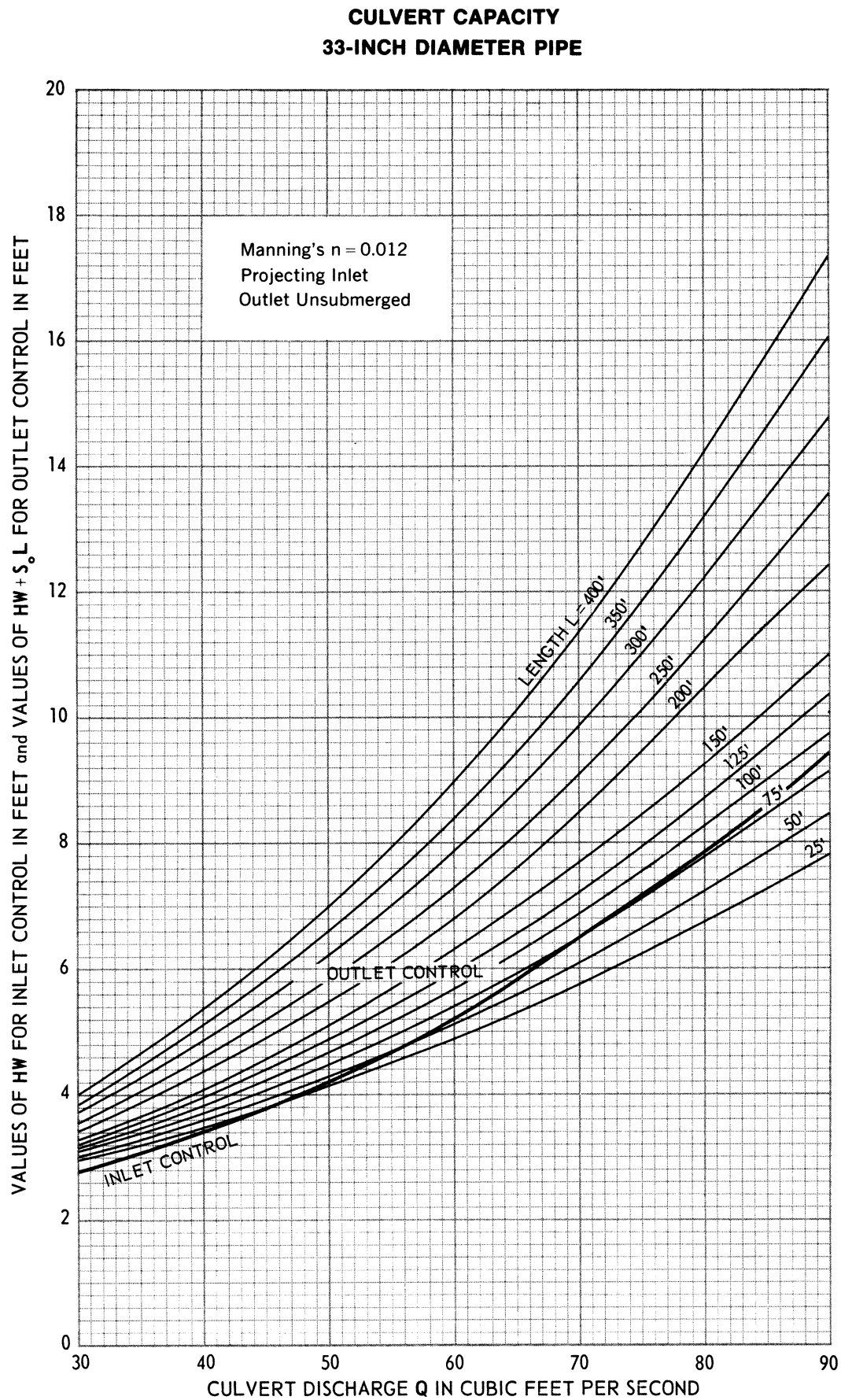


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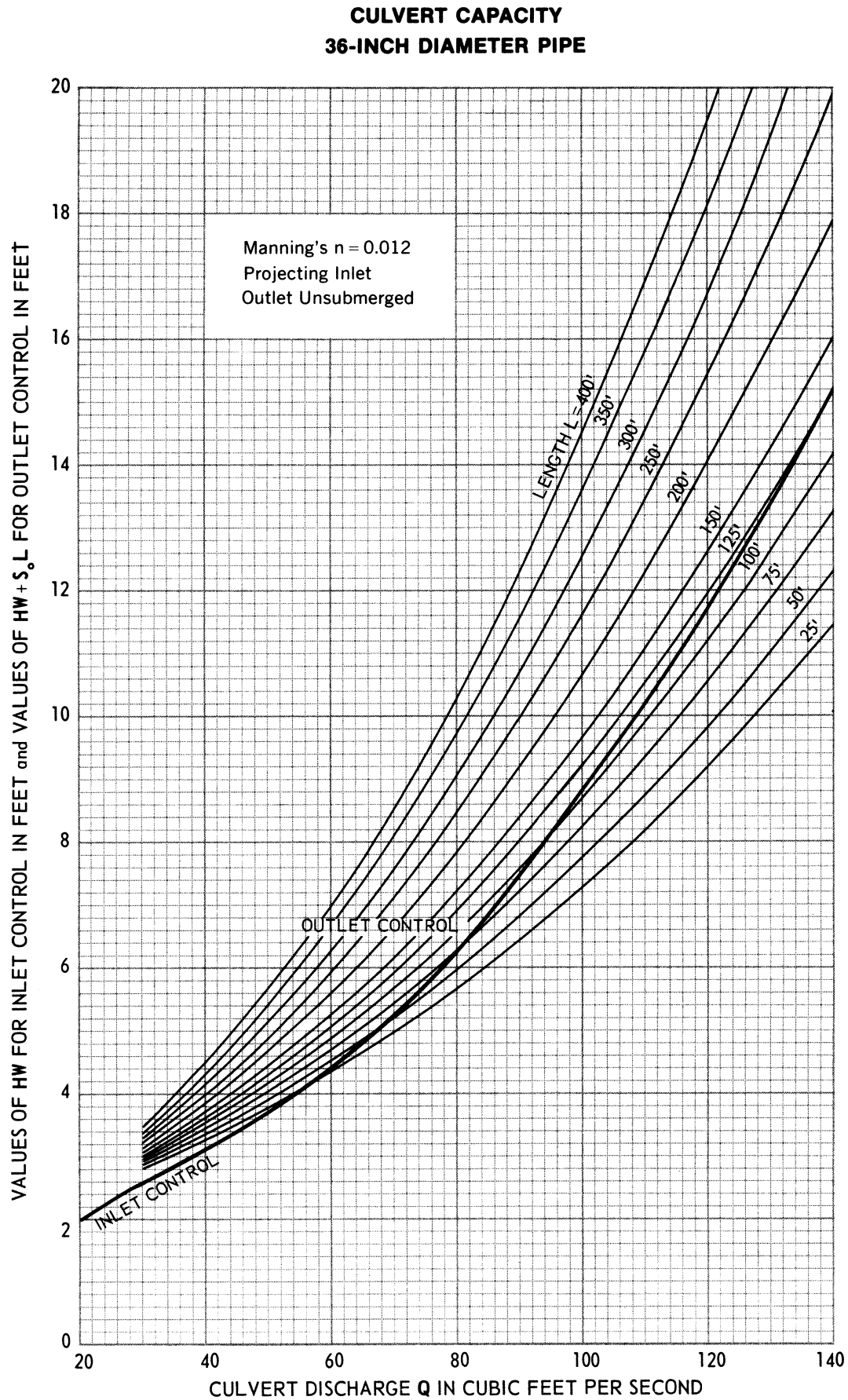


Figure 51

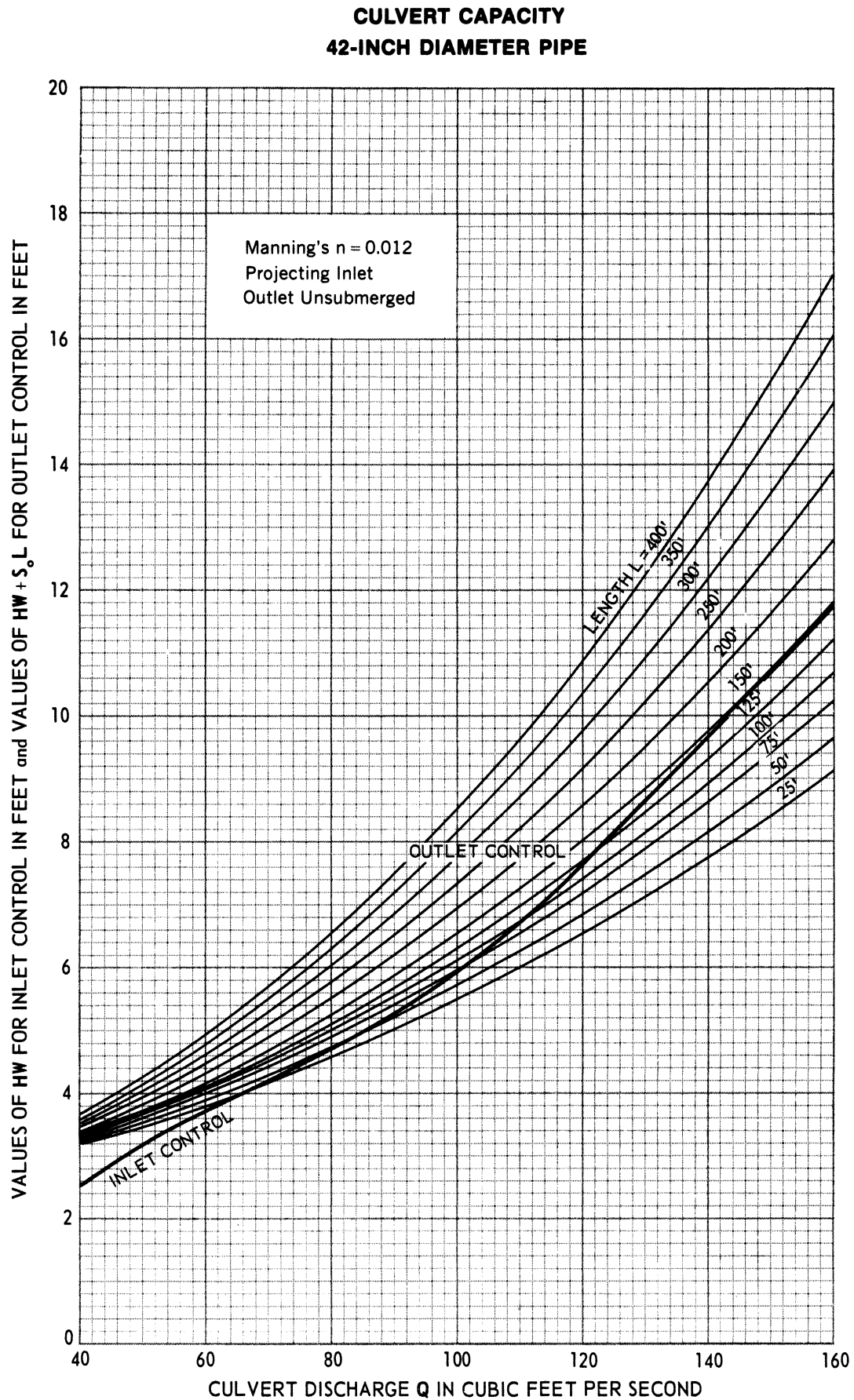


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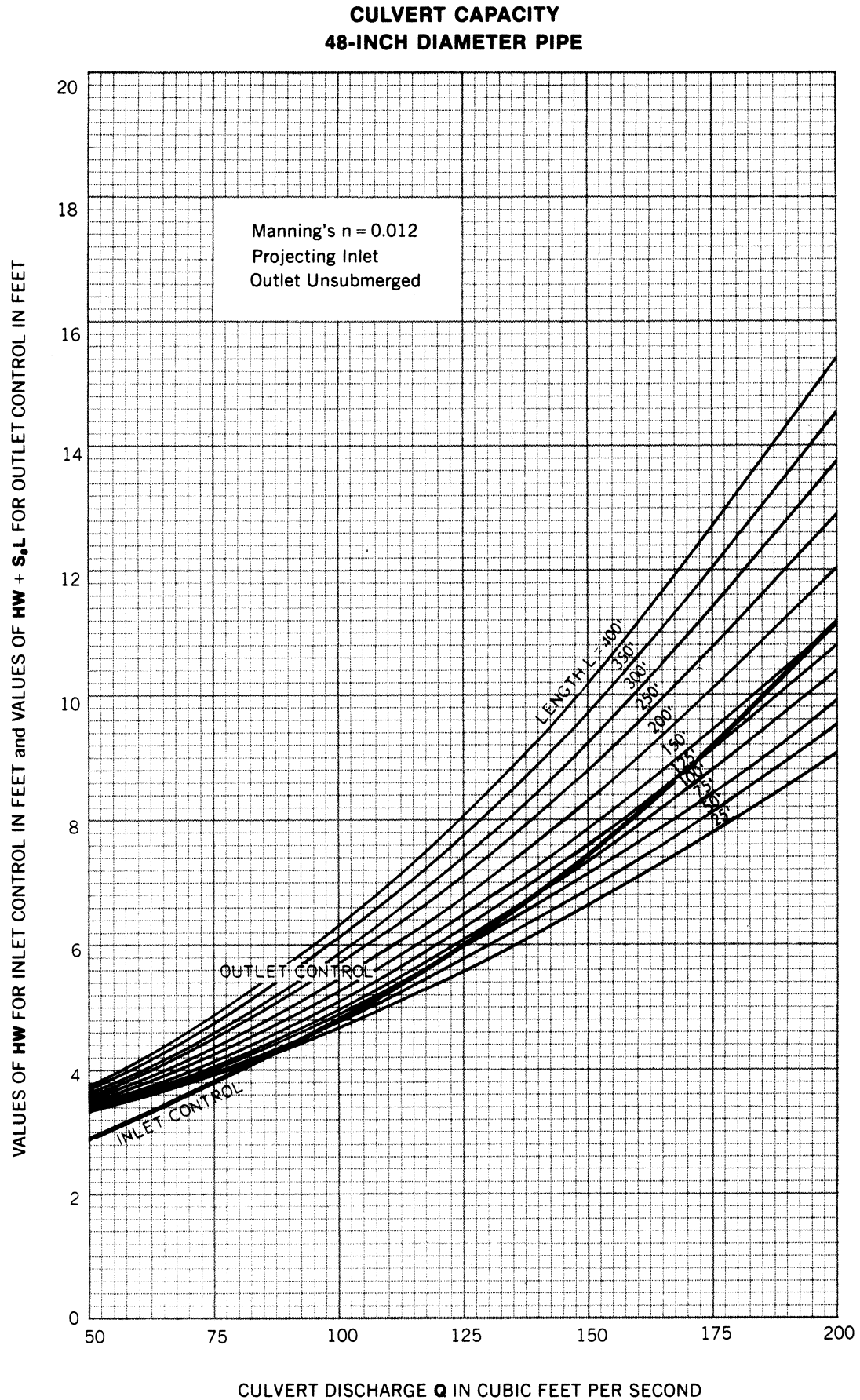


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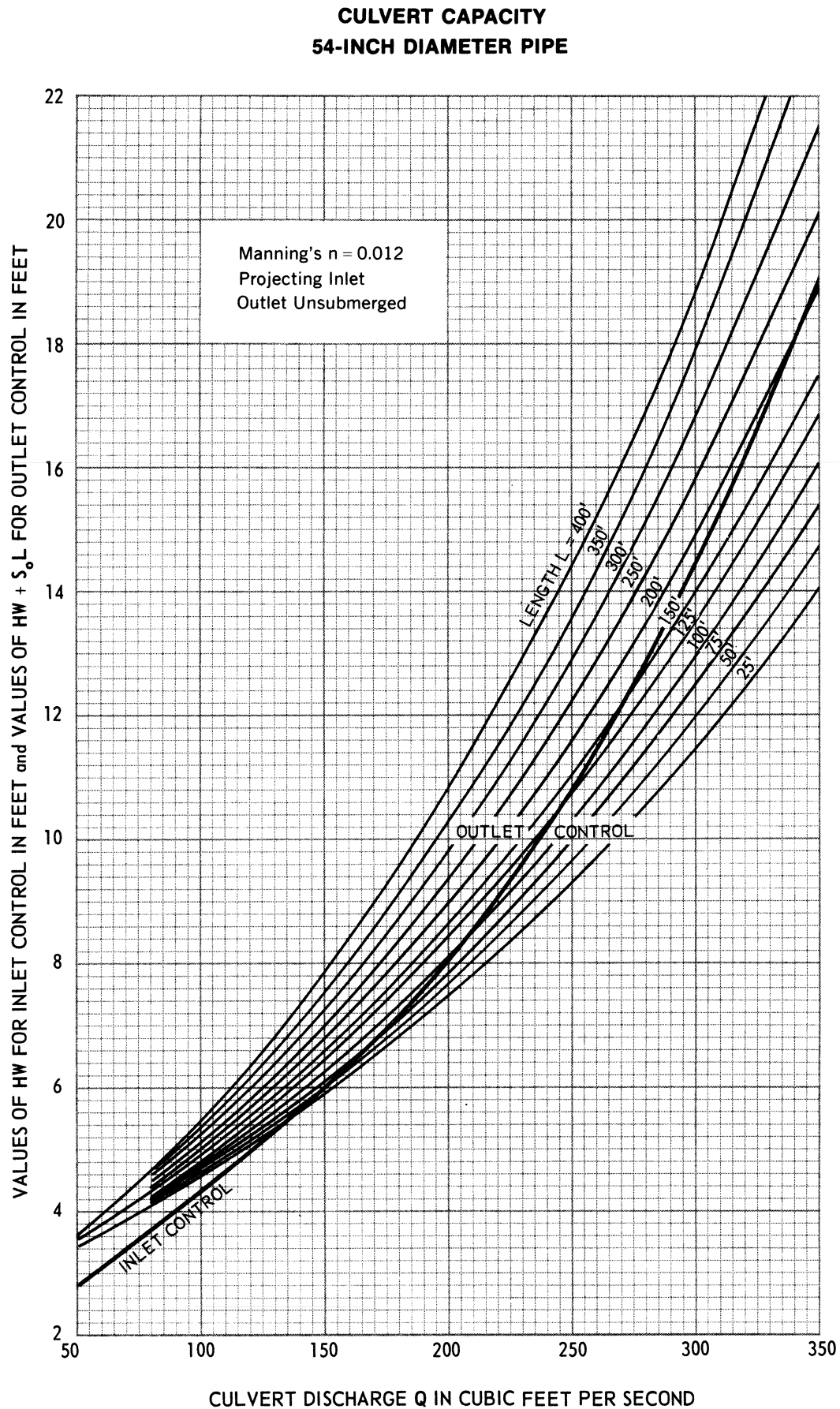


Figure 54

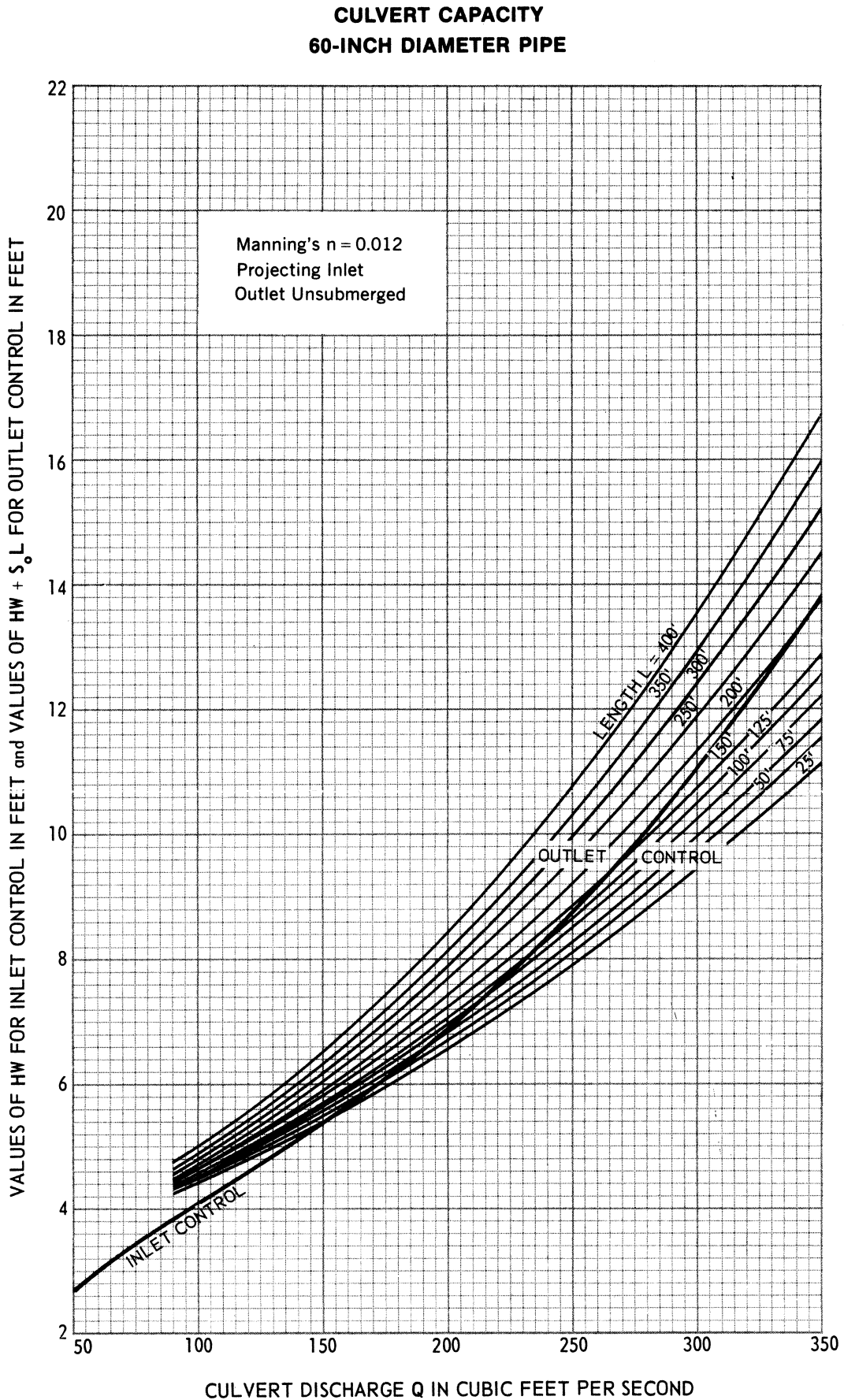


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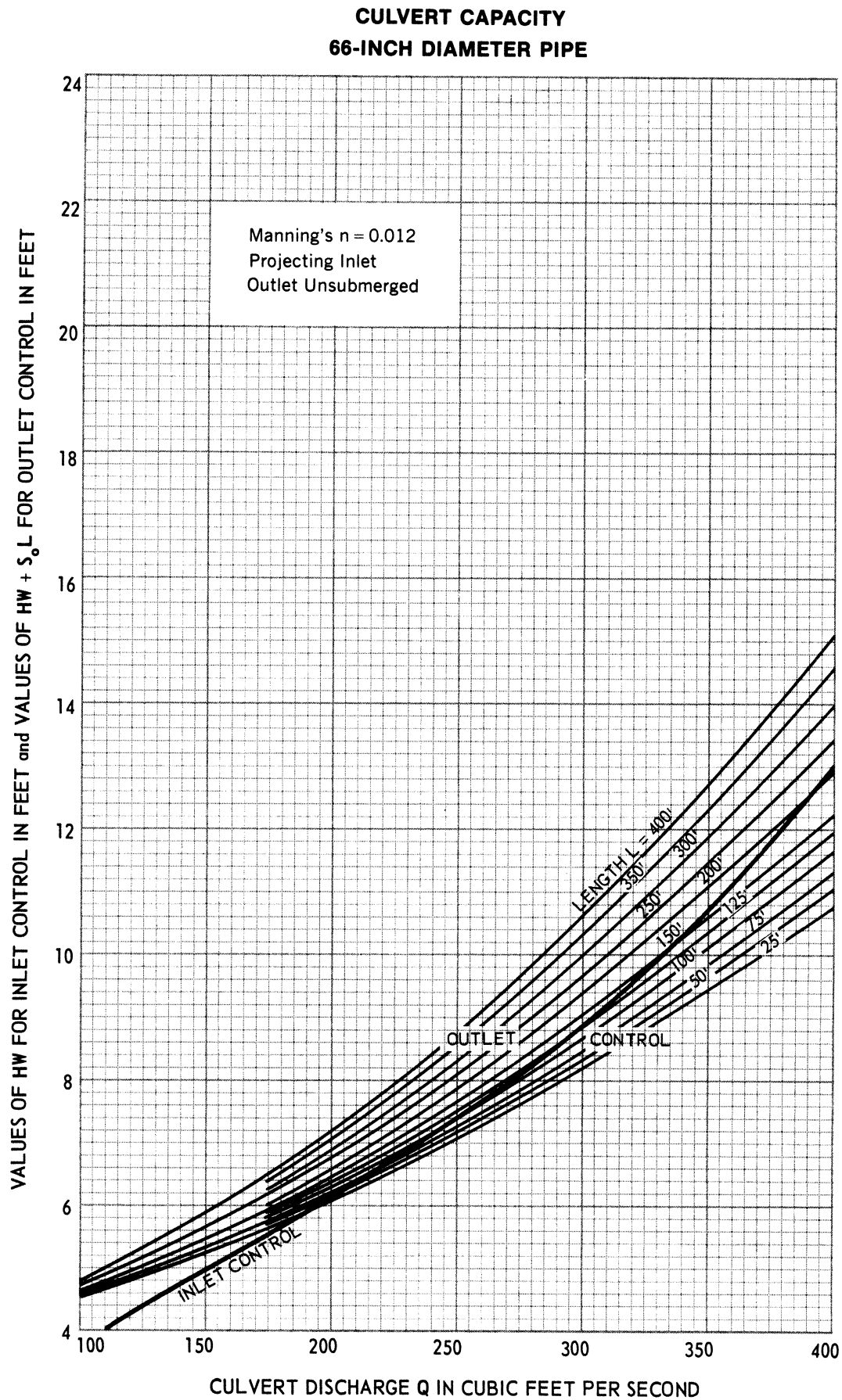


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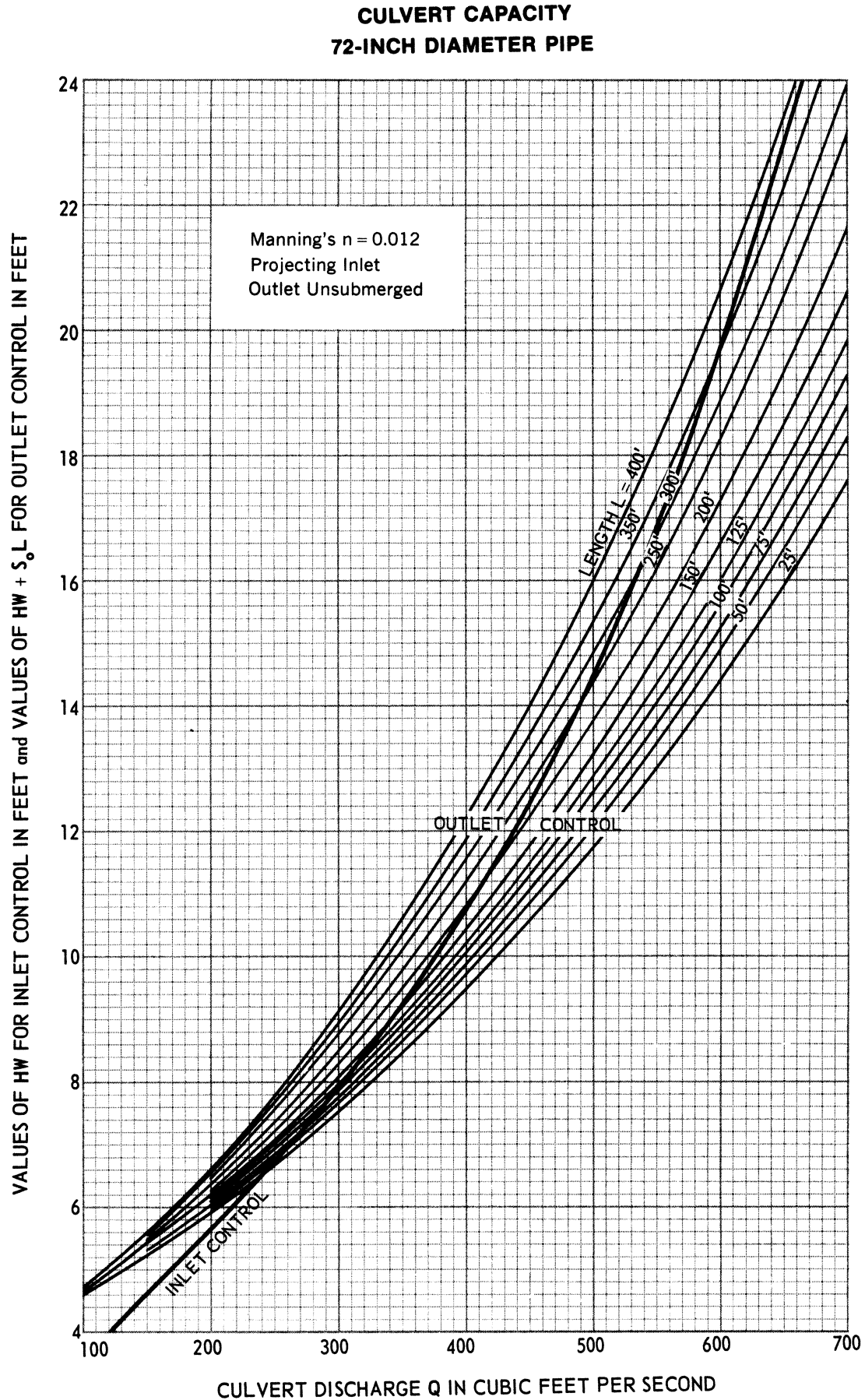


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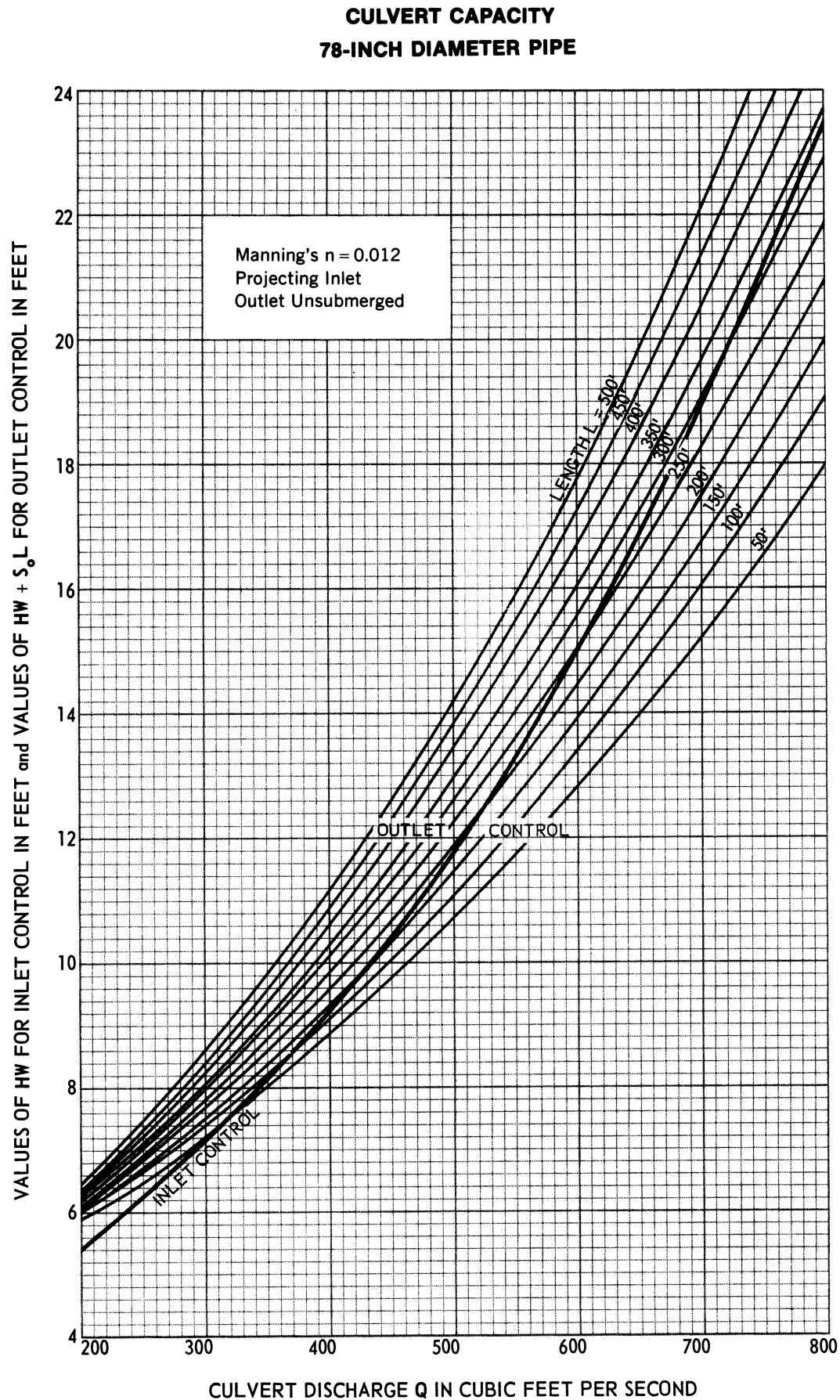


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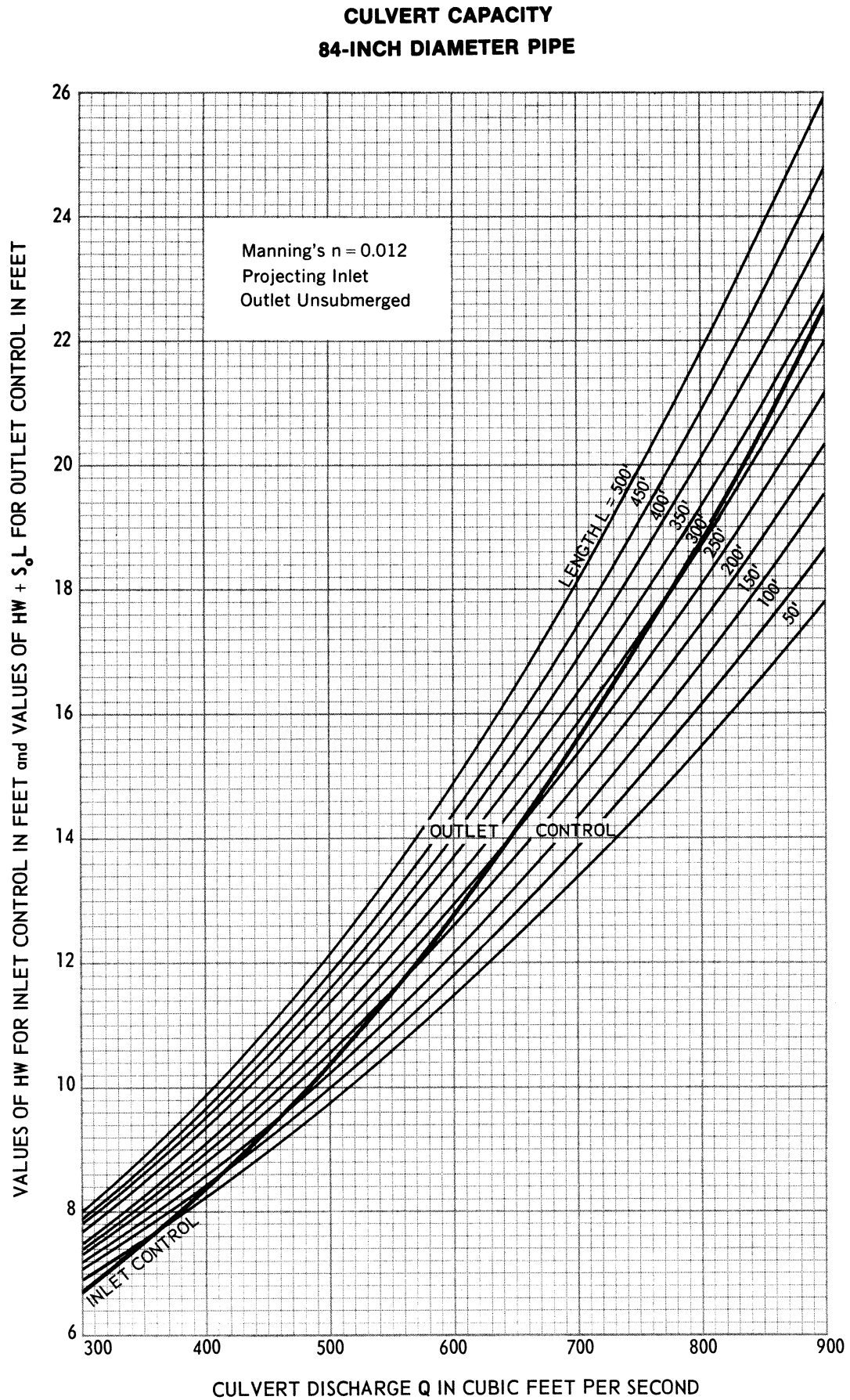


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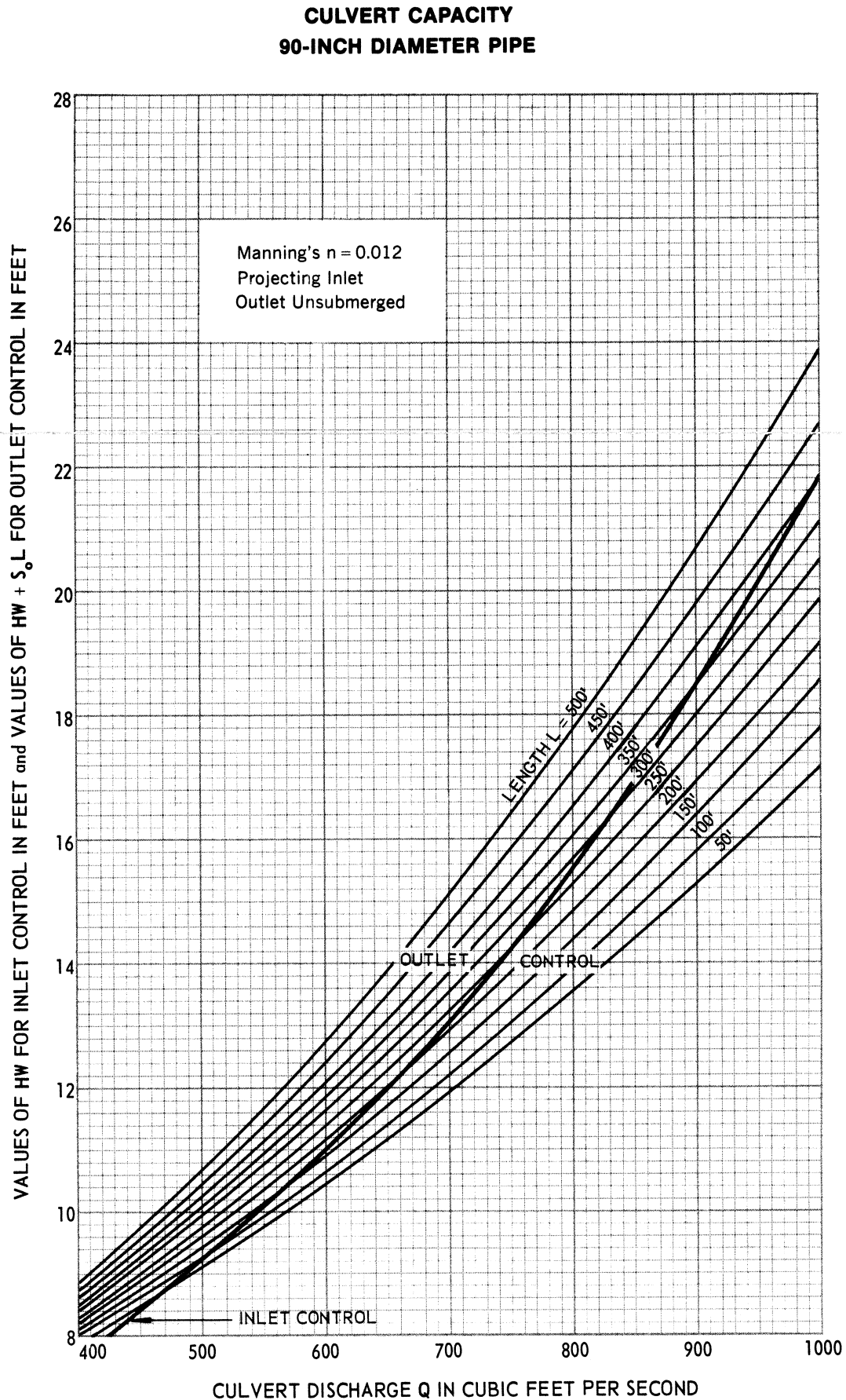


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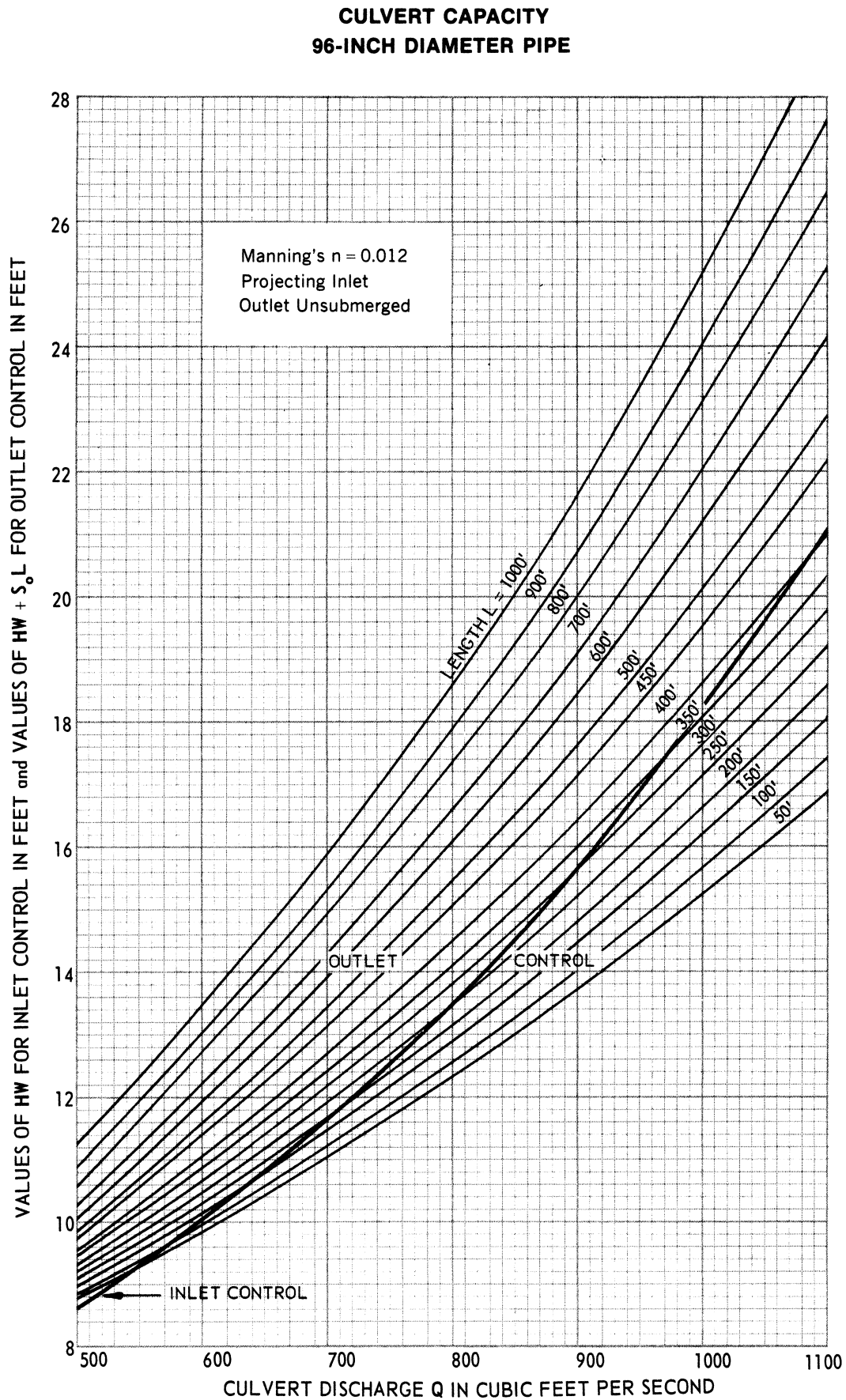


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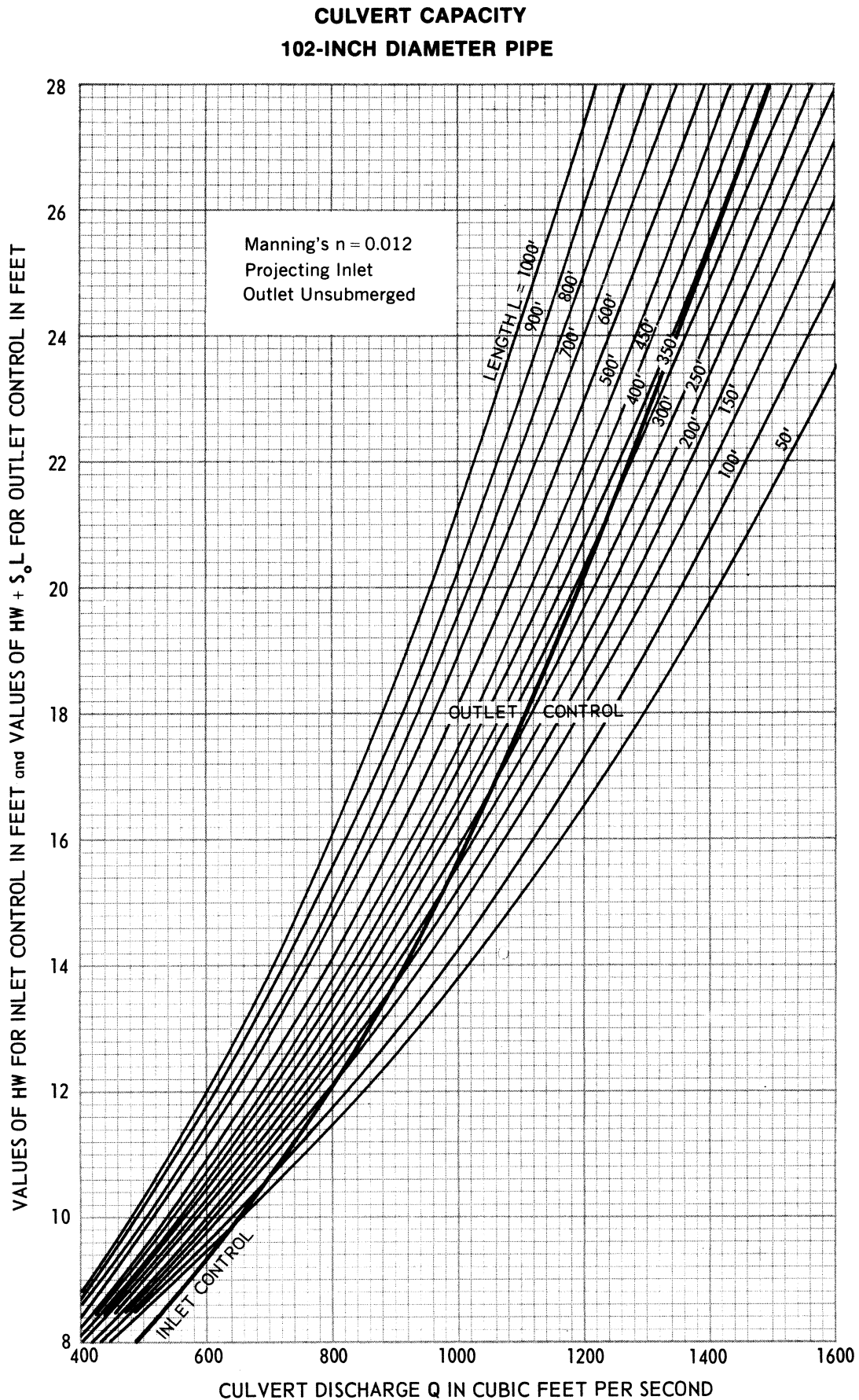


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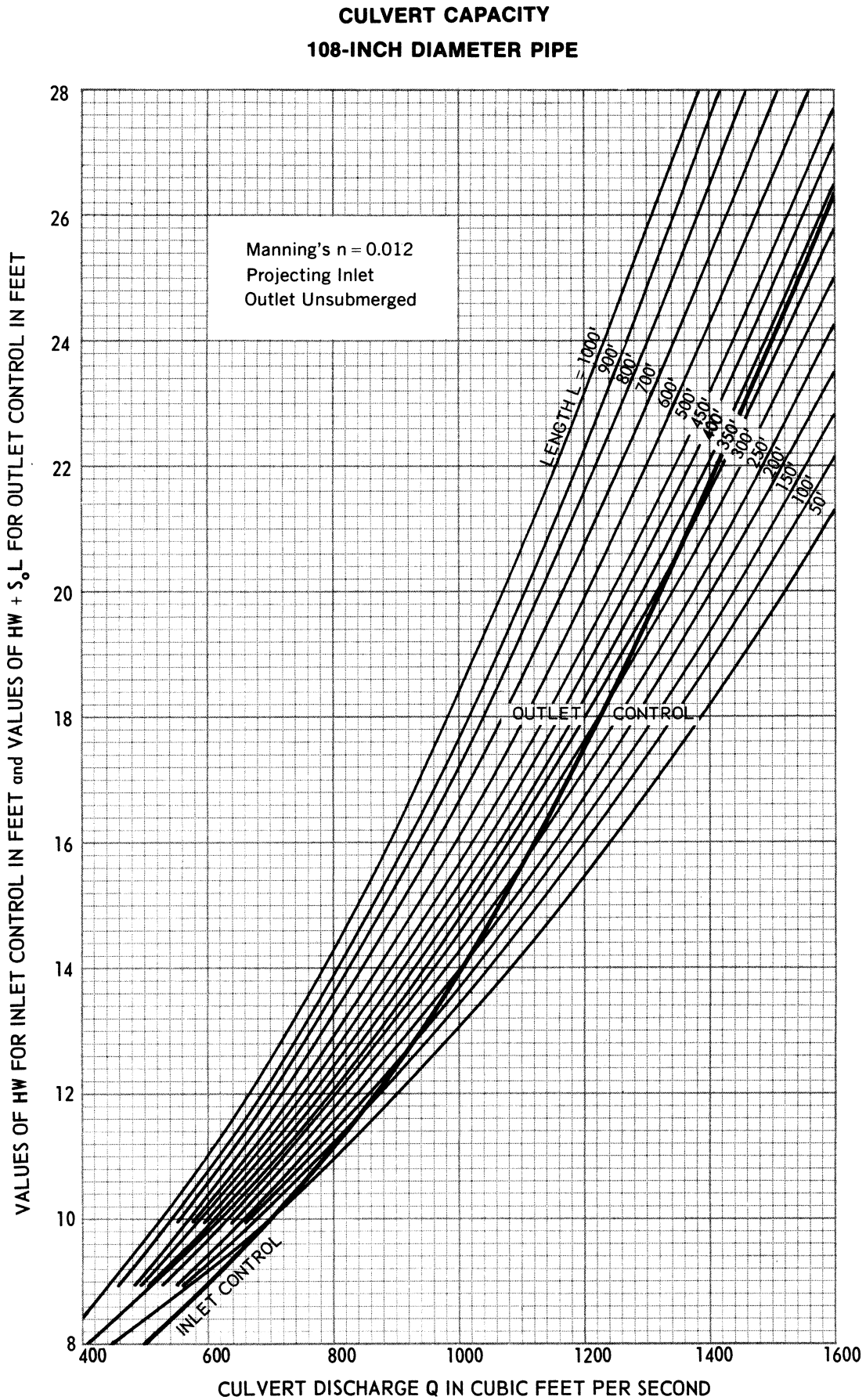


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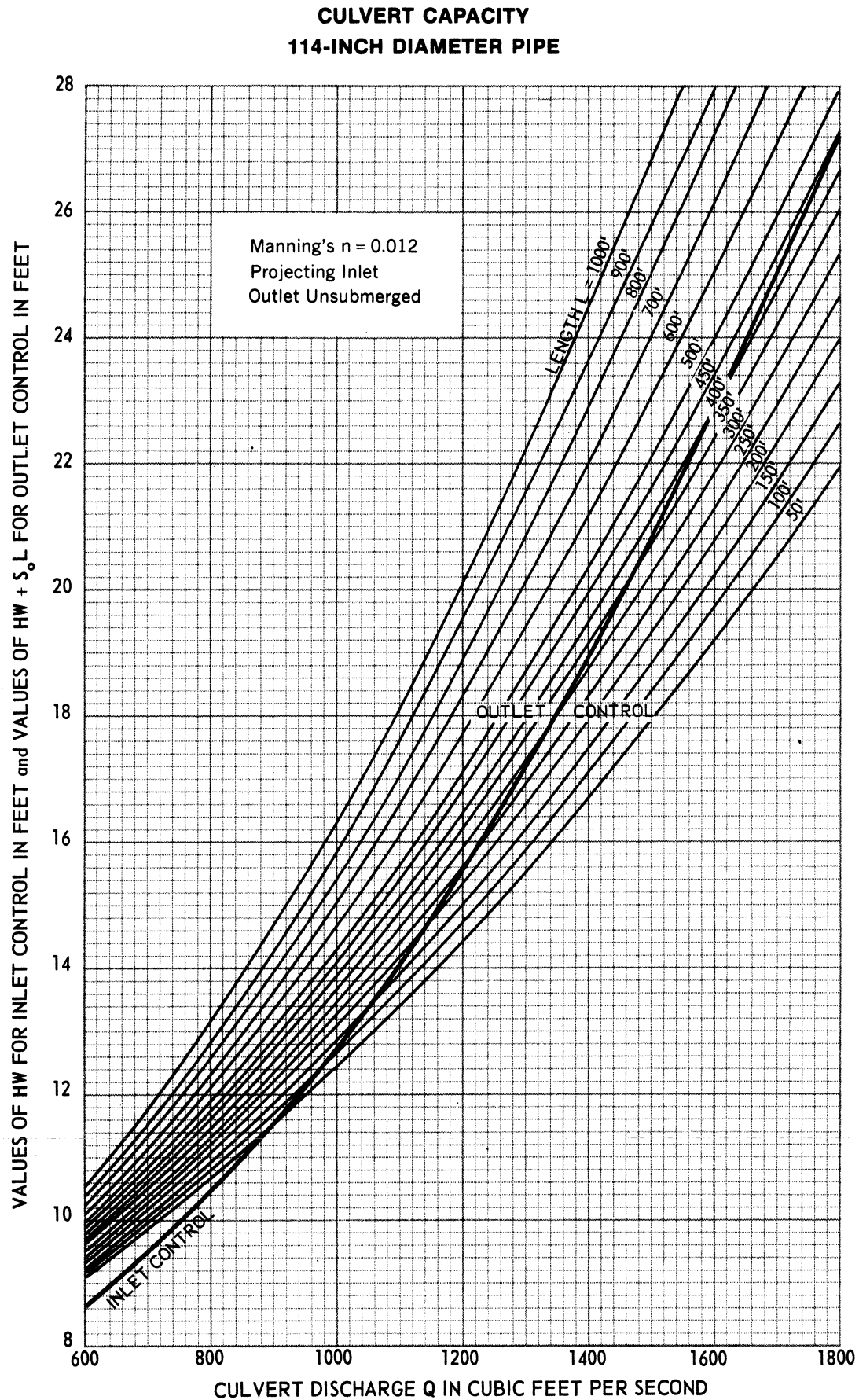


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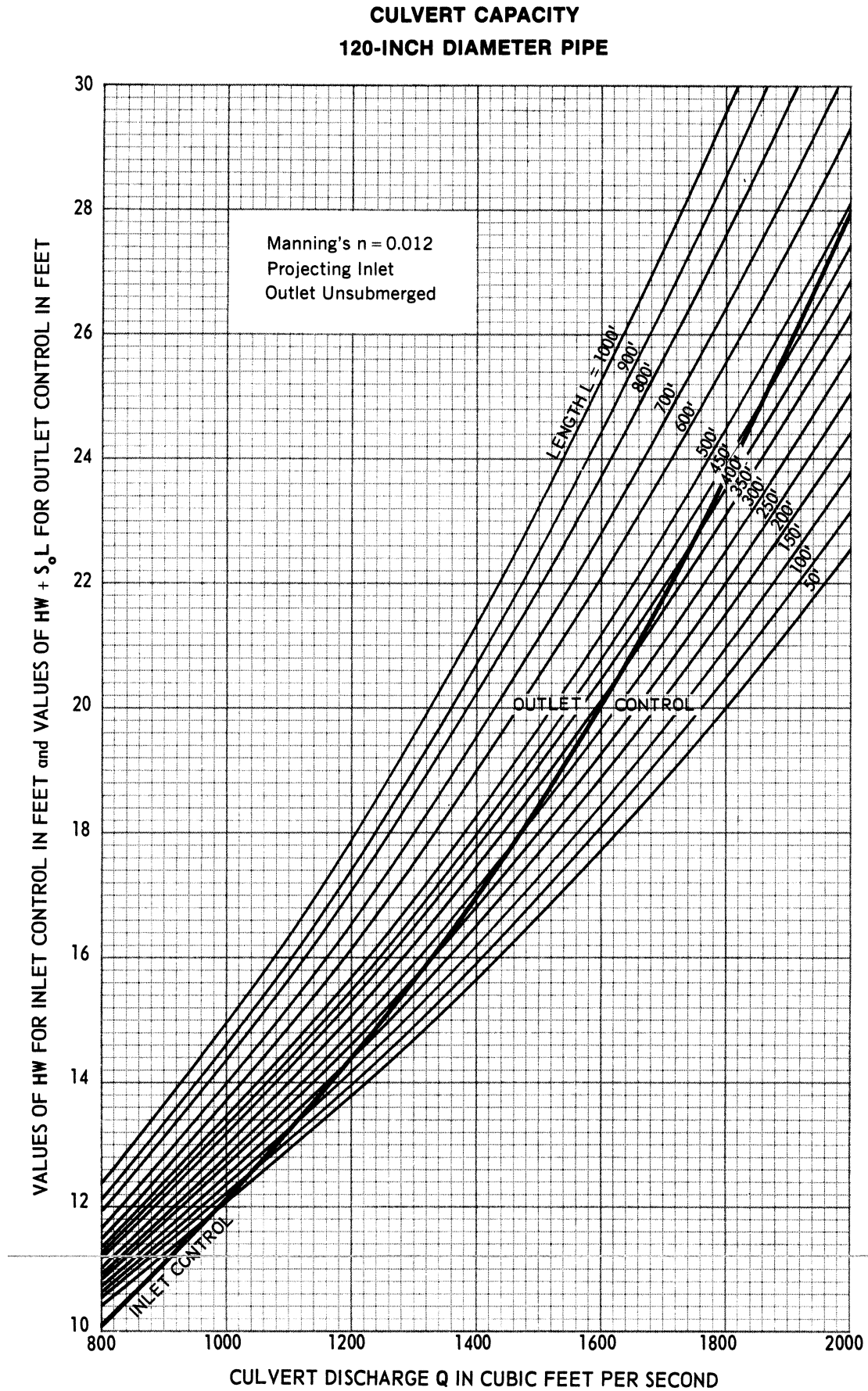


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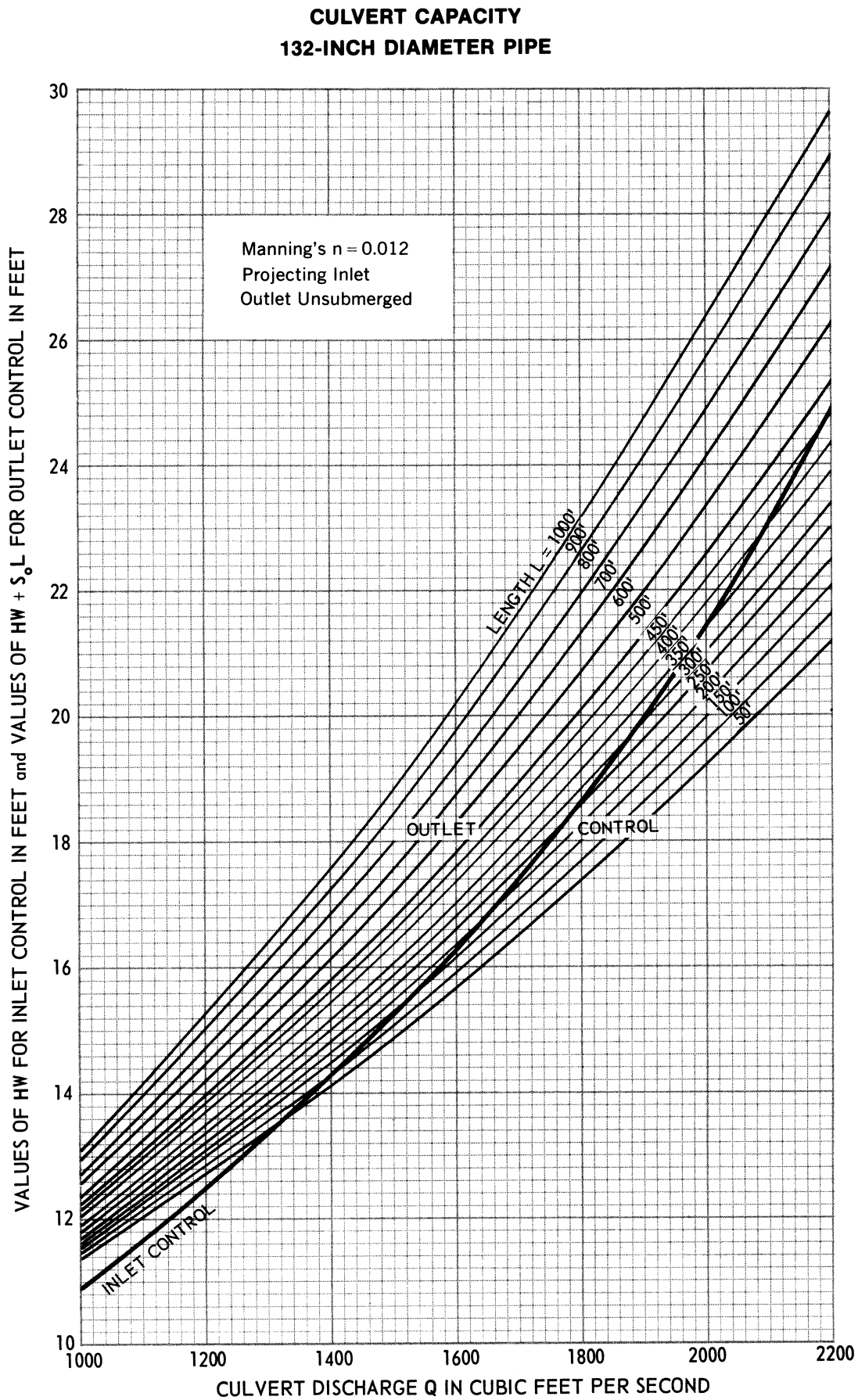


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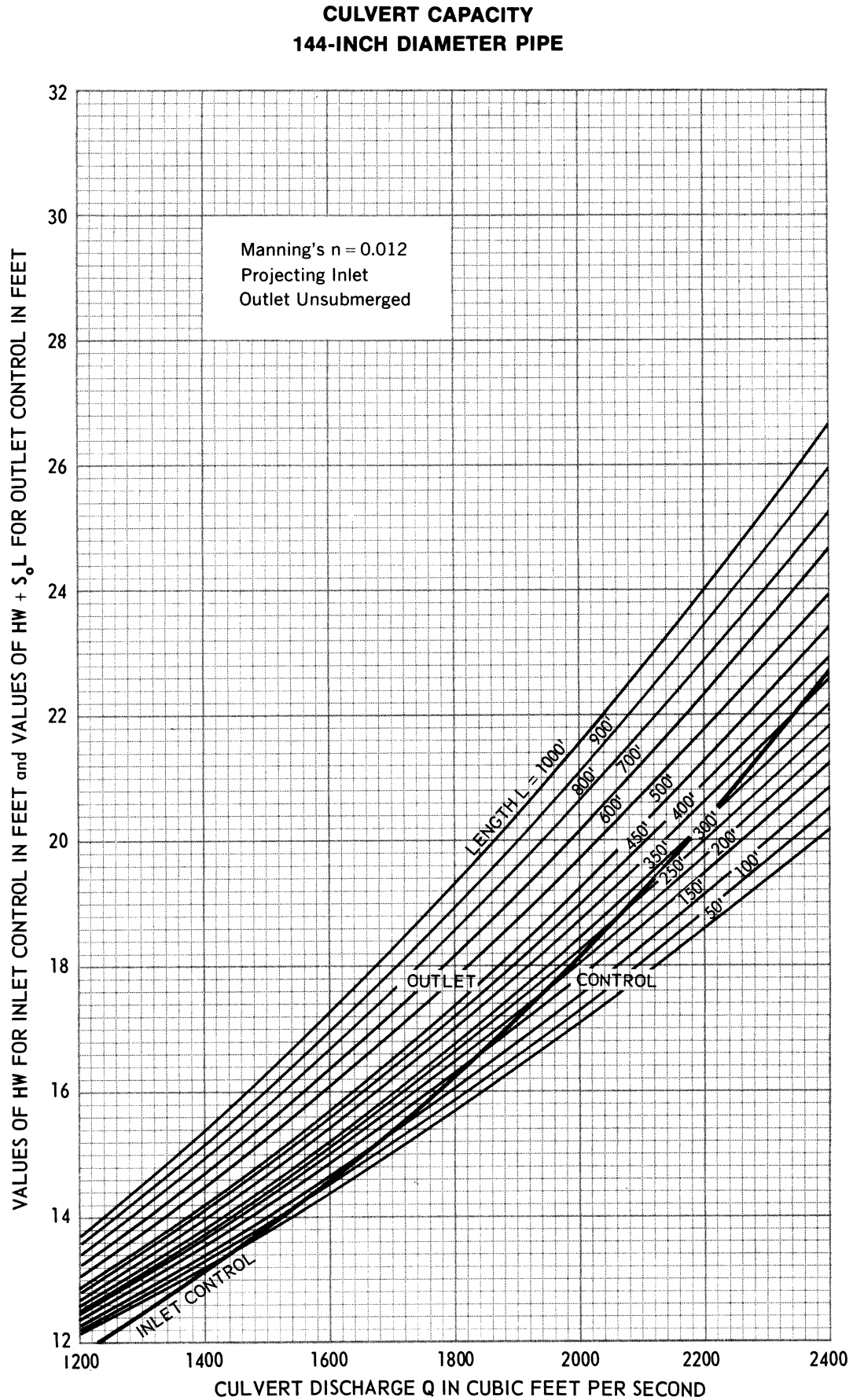


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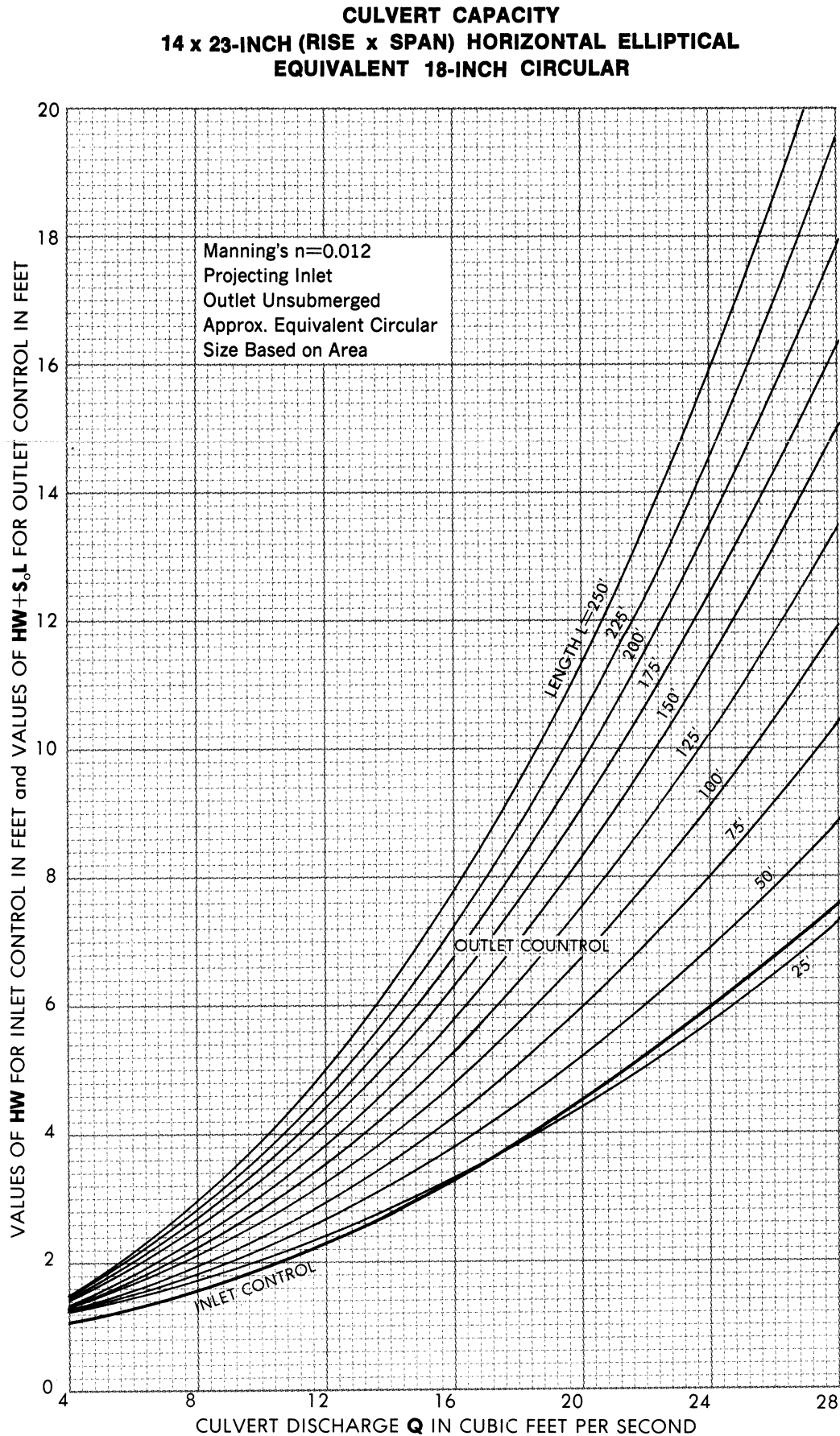


Figure 68

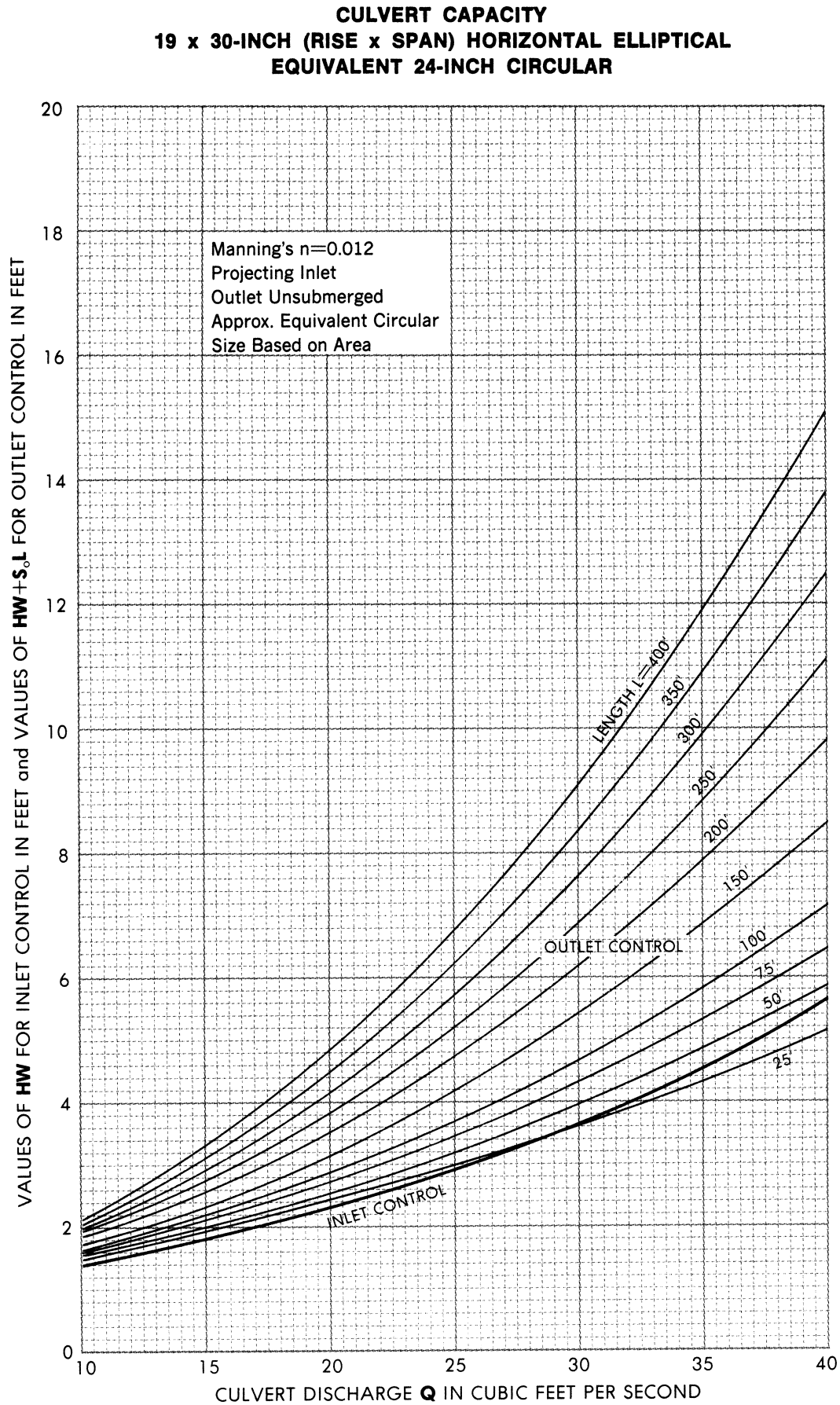


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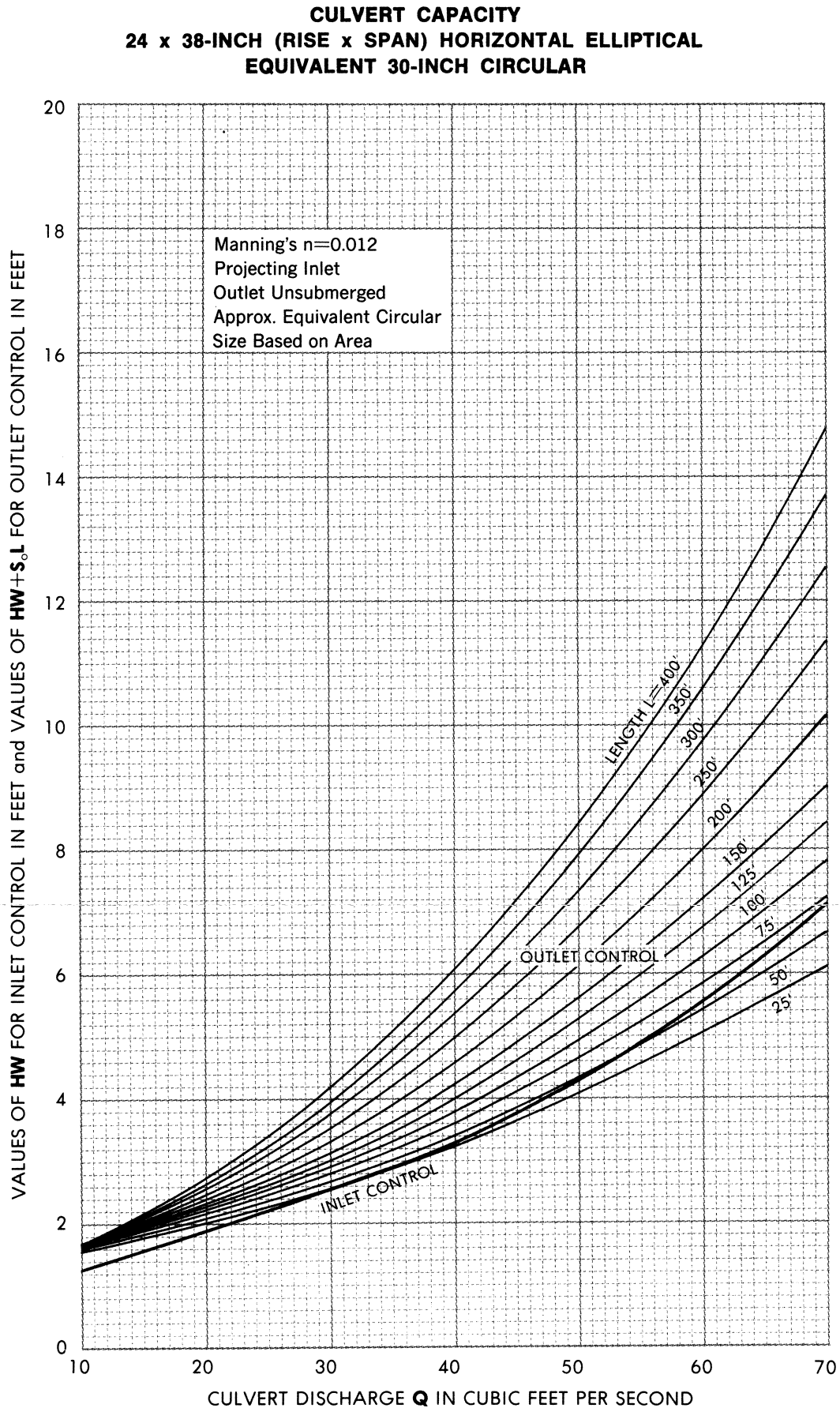


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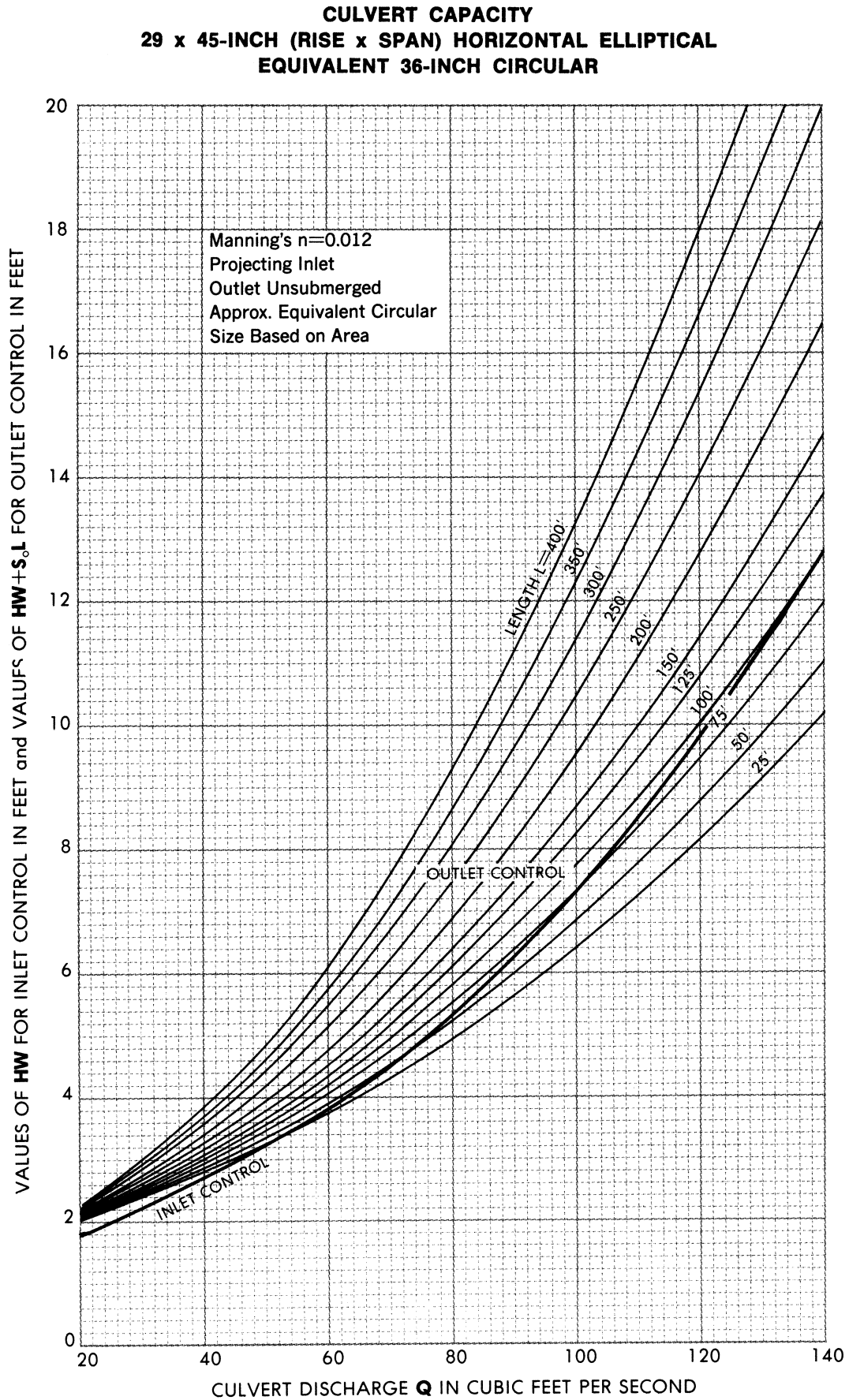


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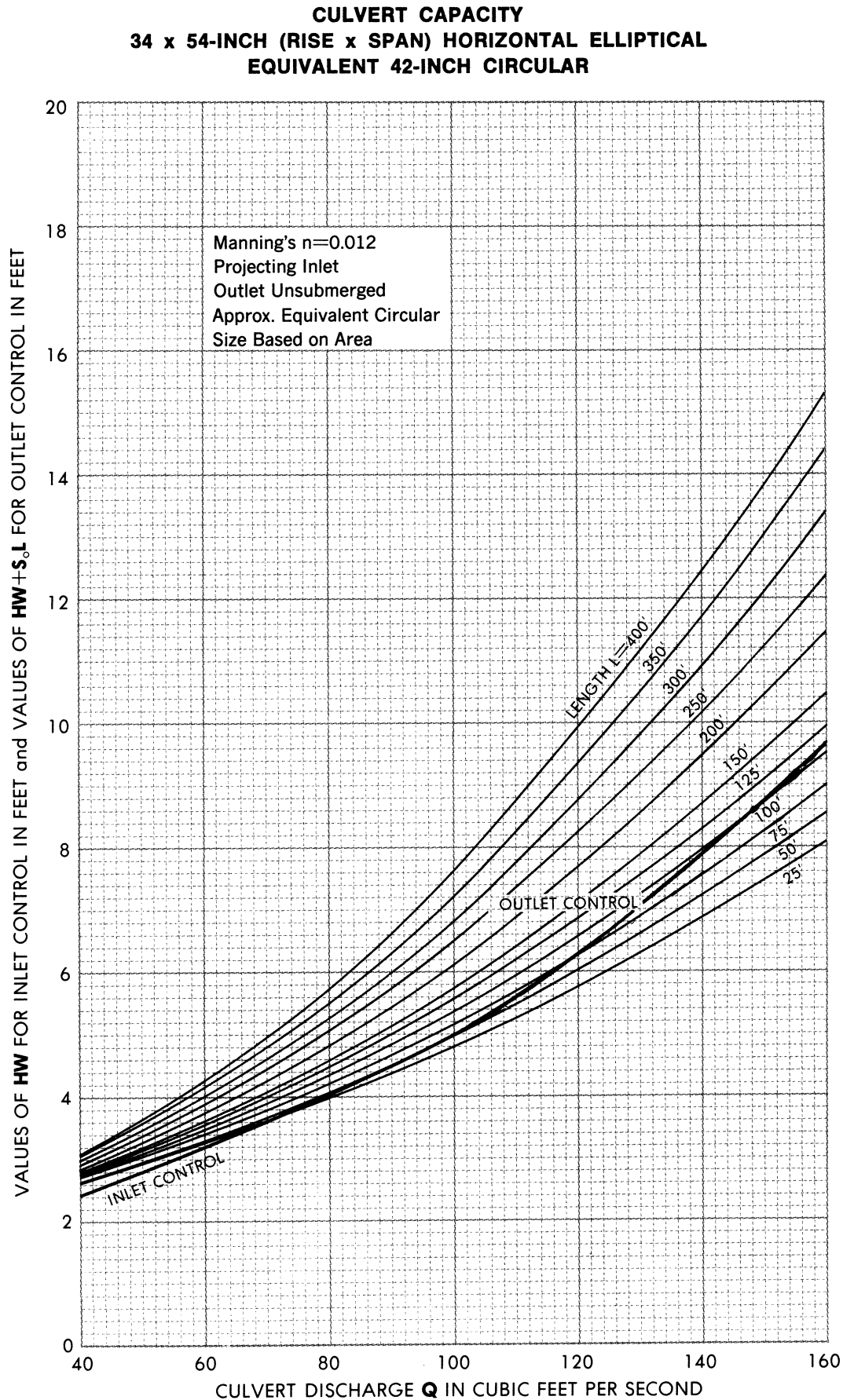


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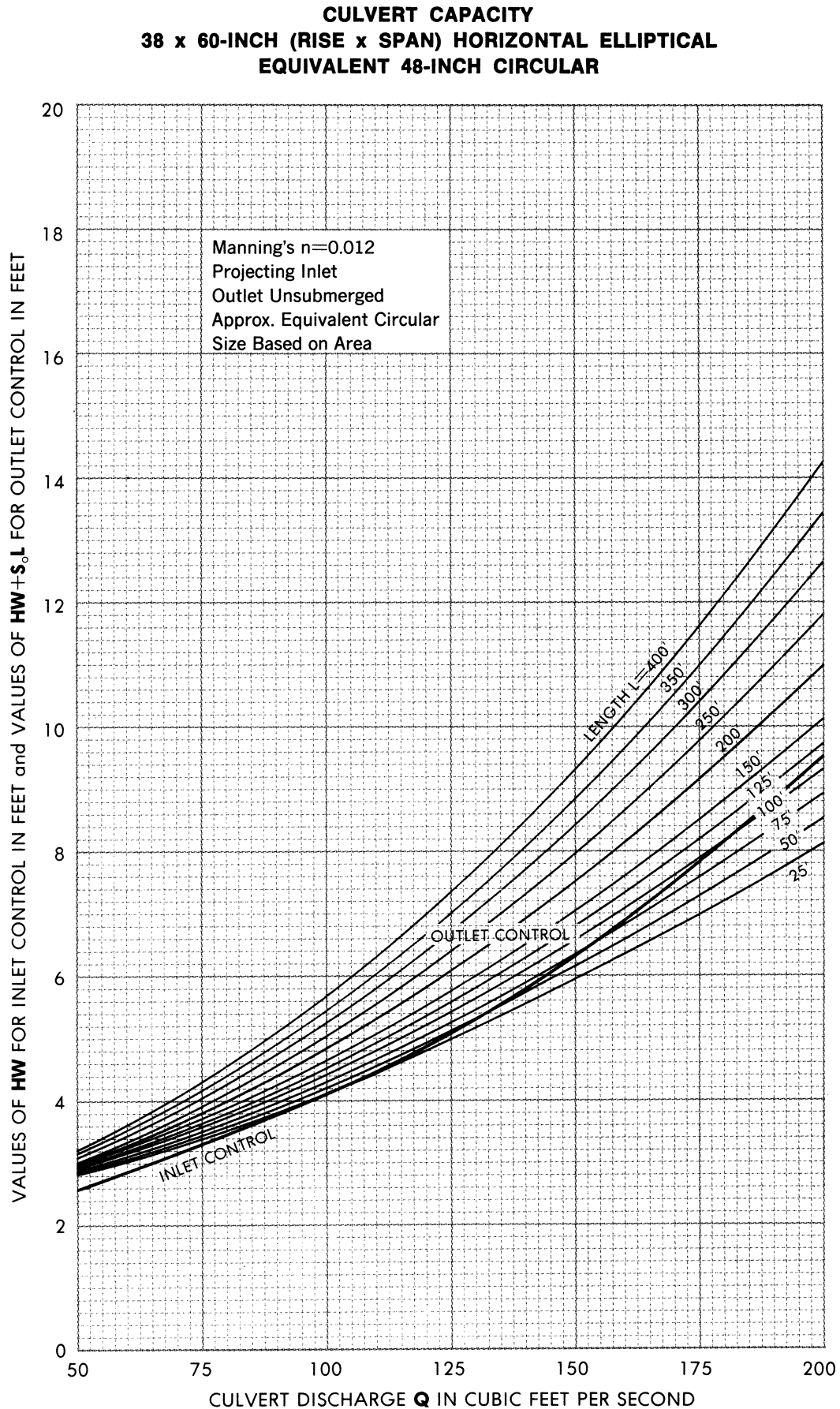


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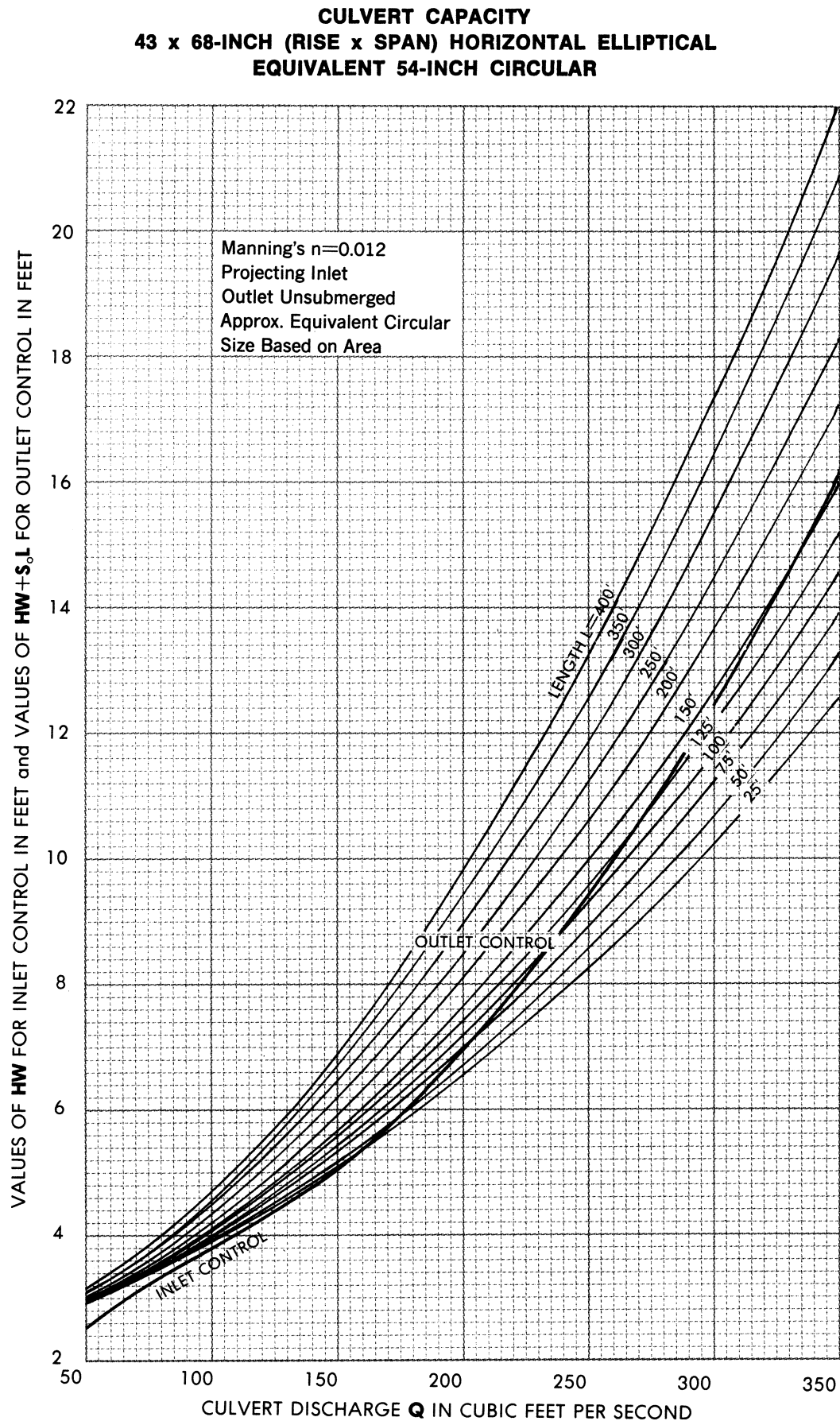


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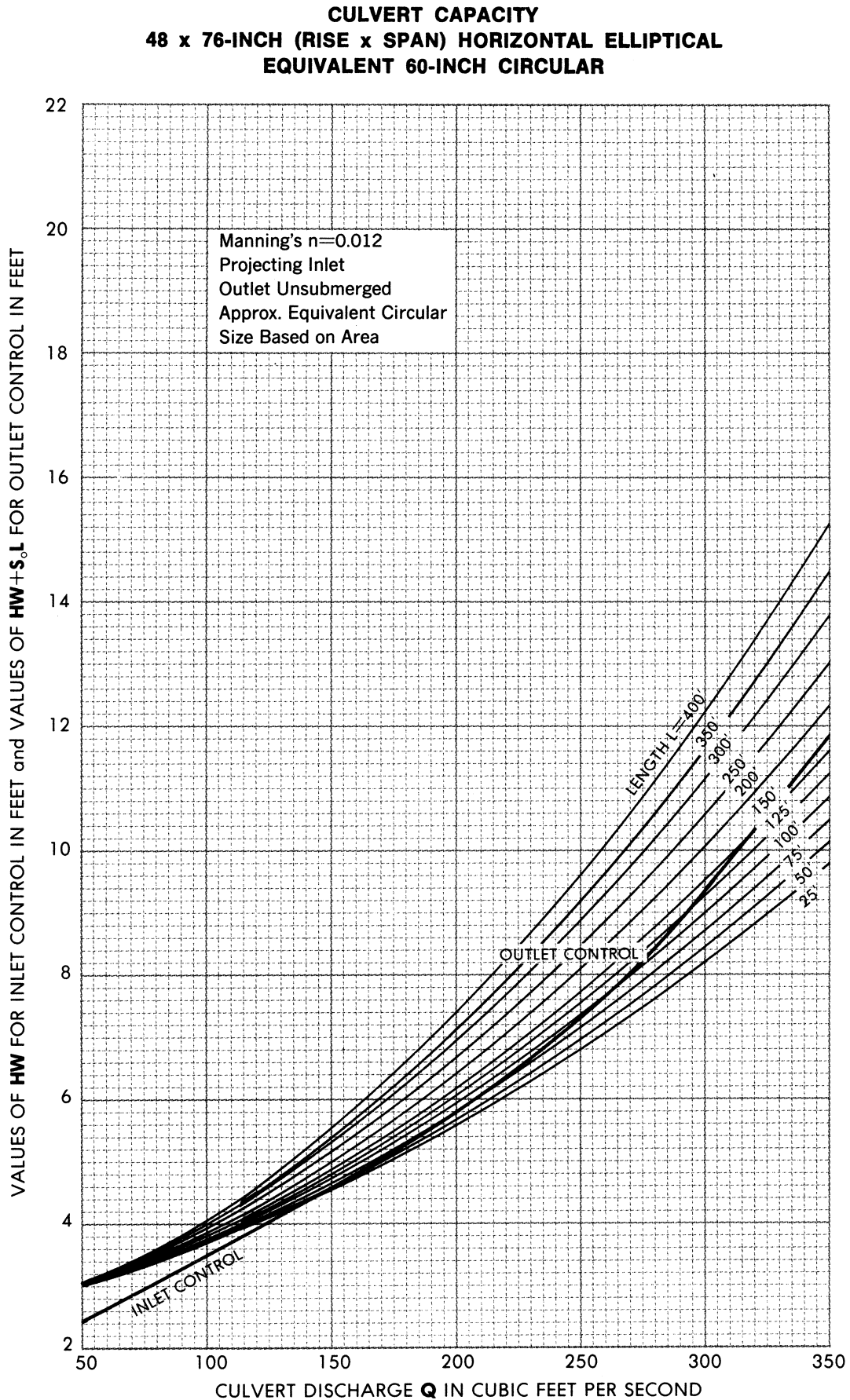


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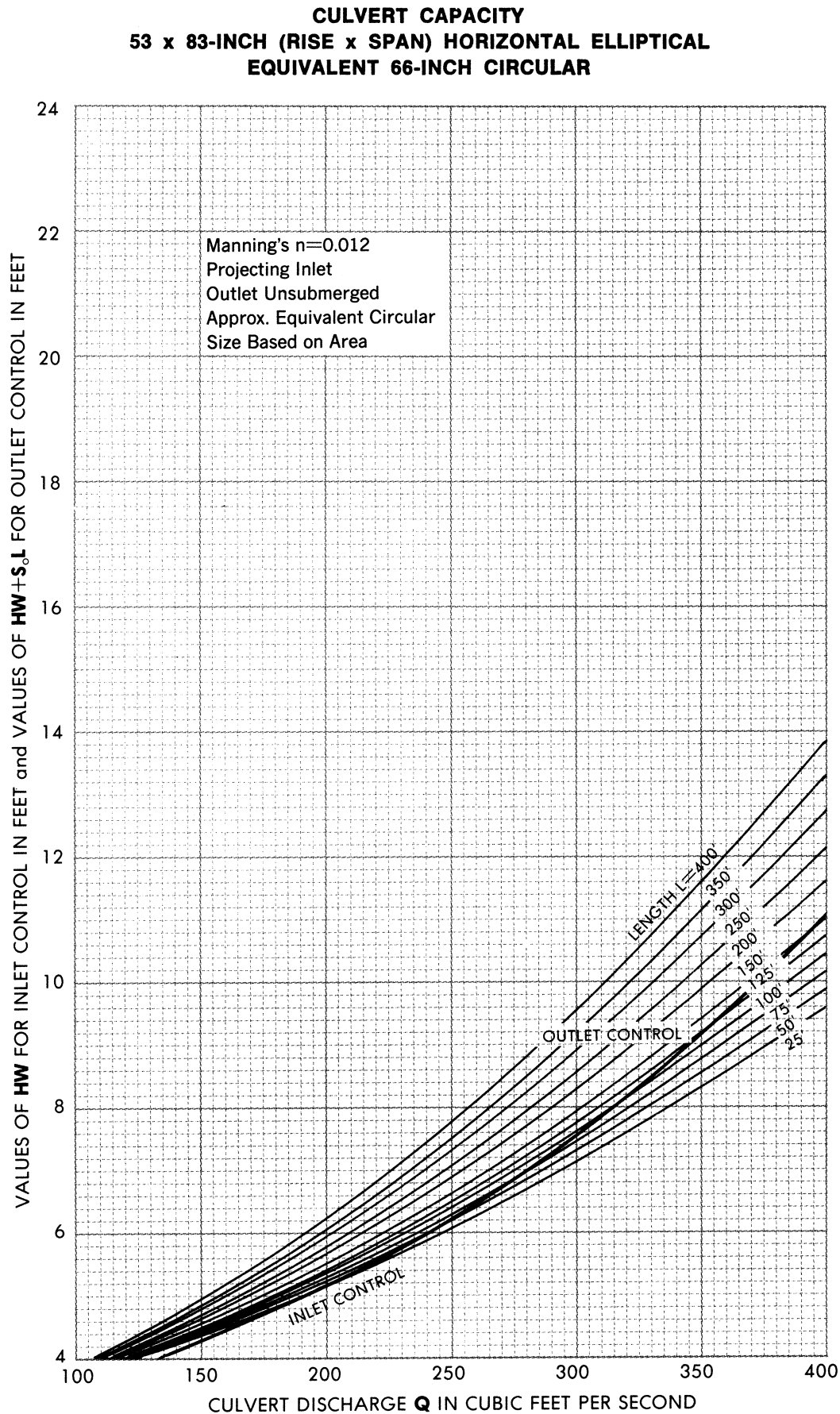


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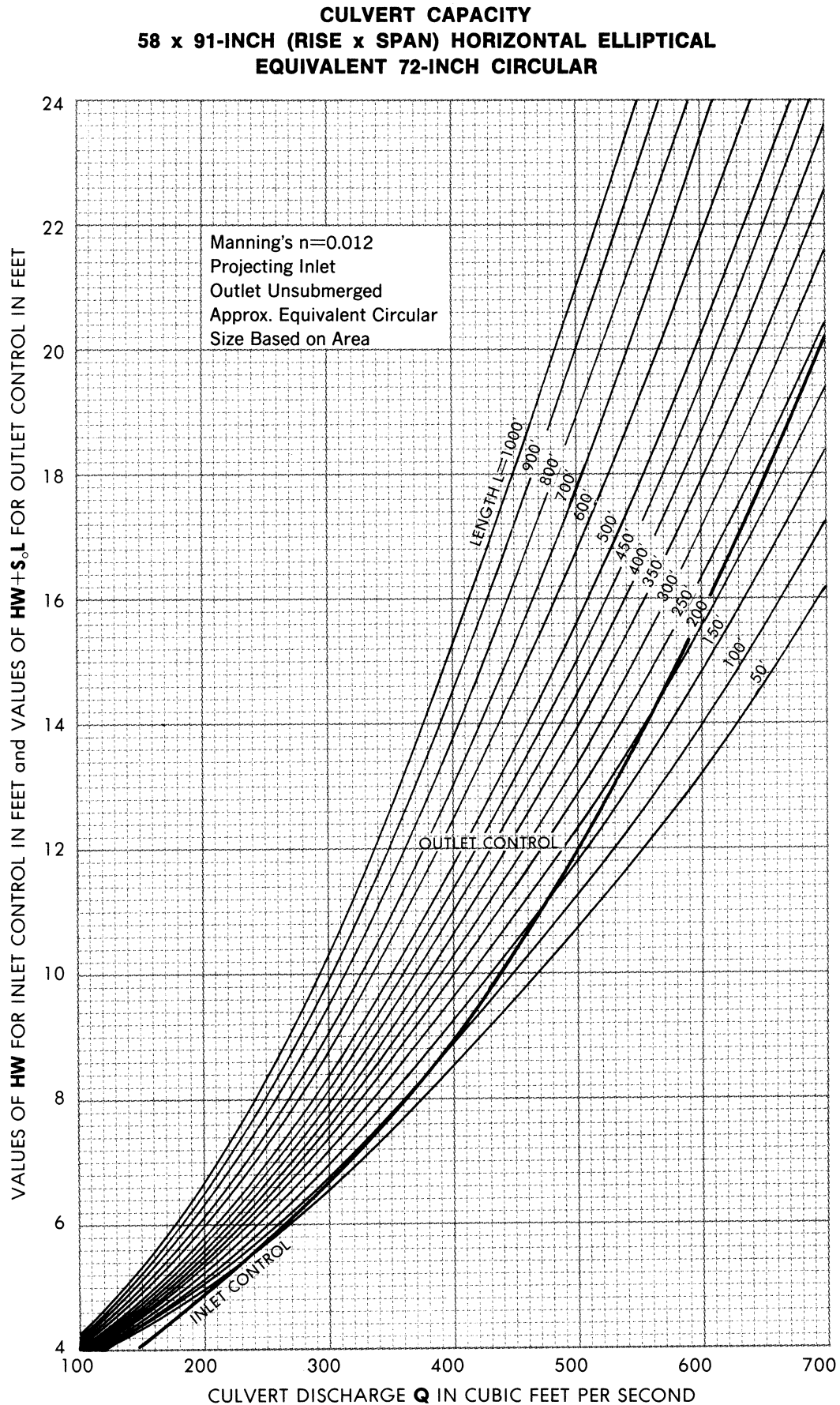


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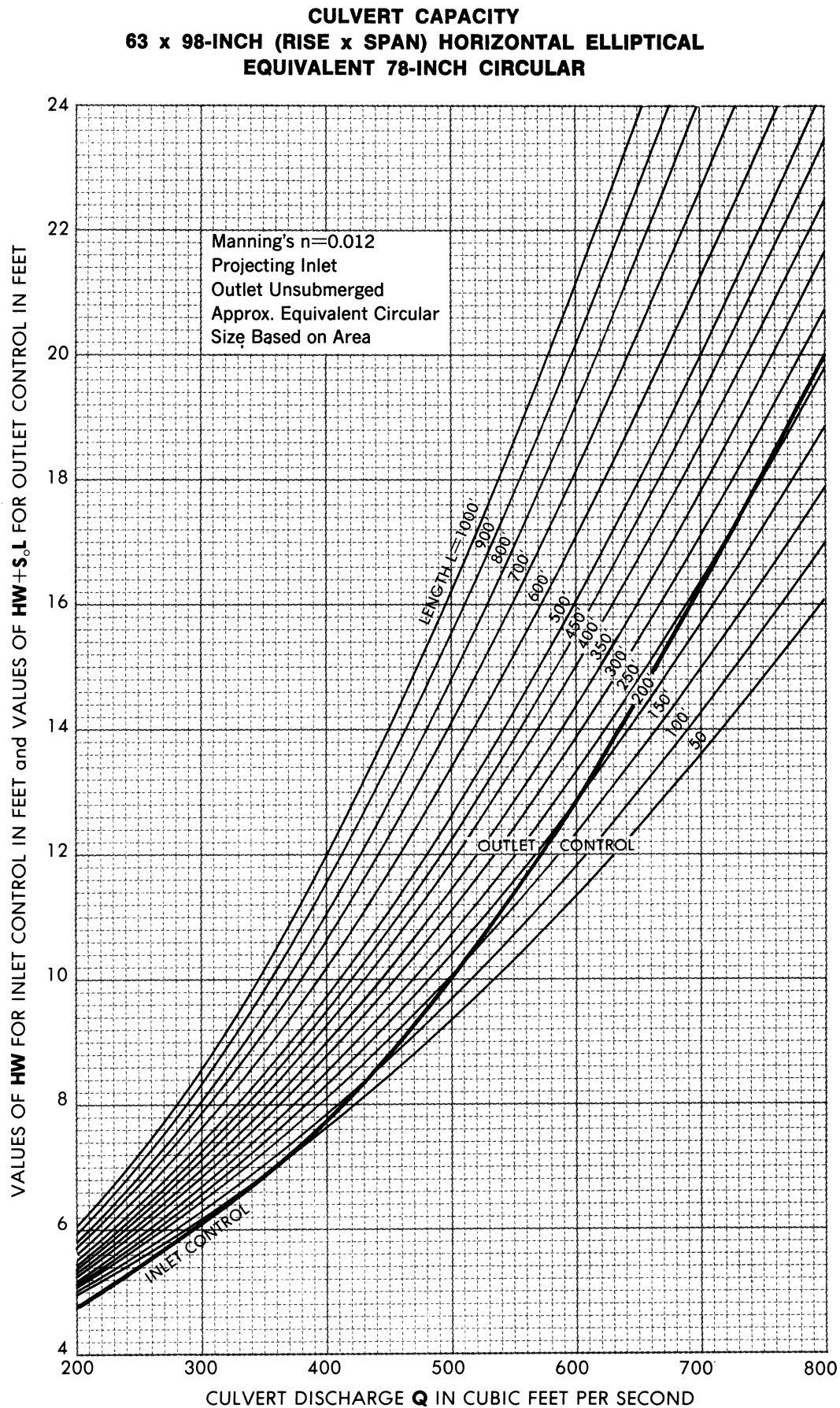


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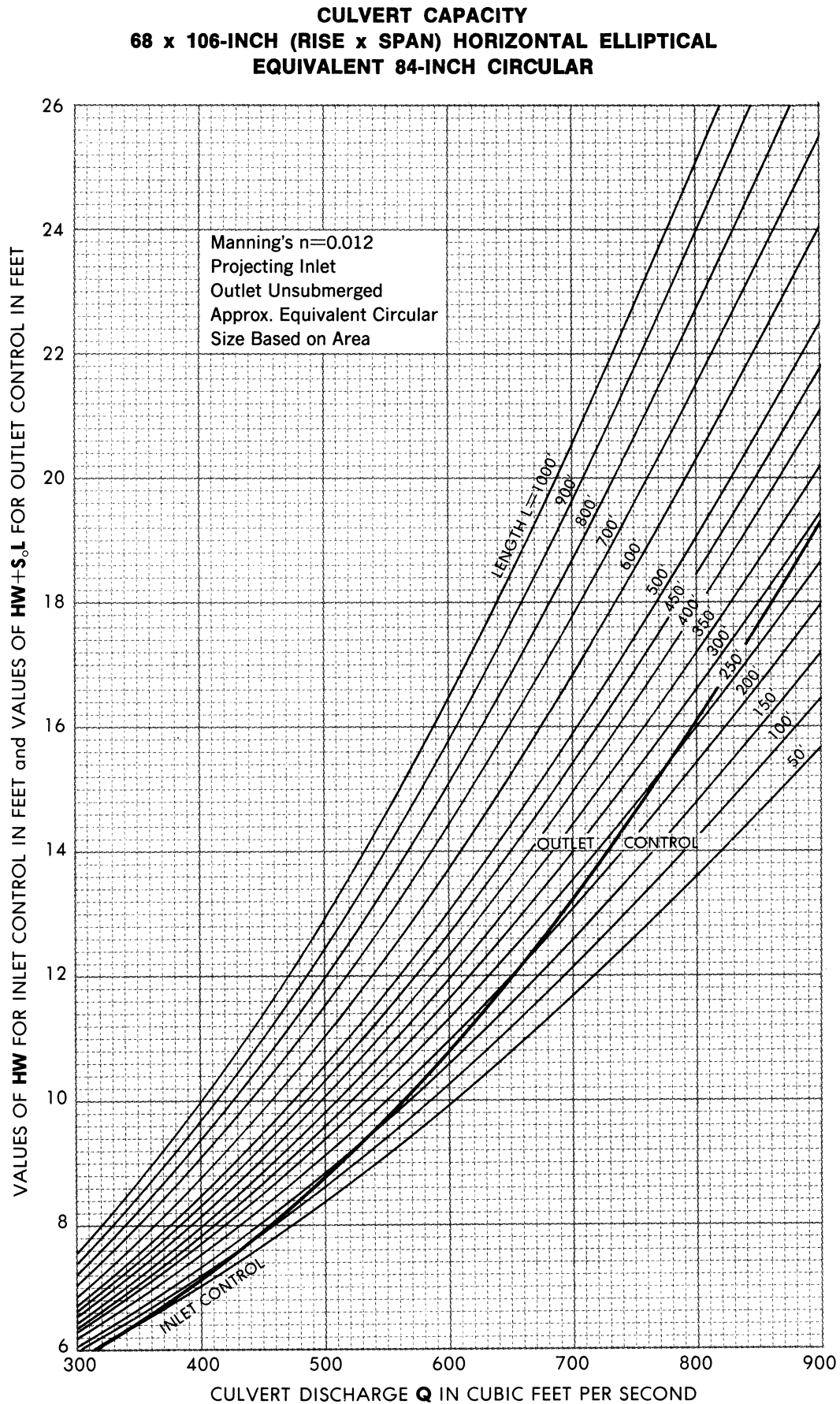


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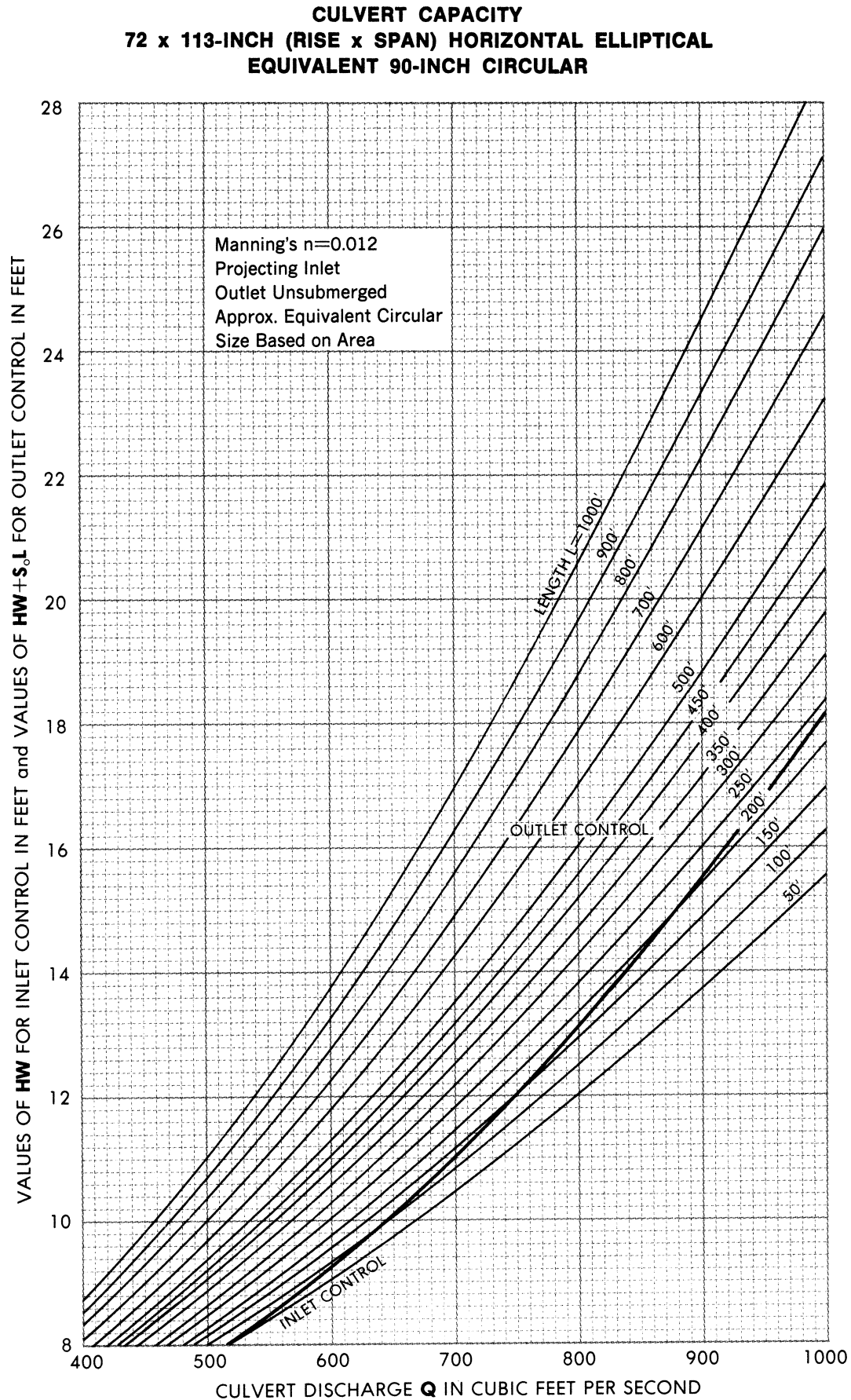


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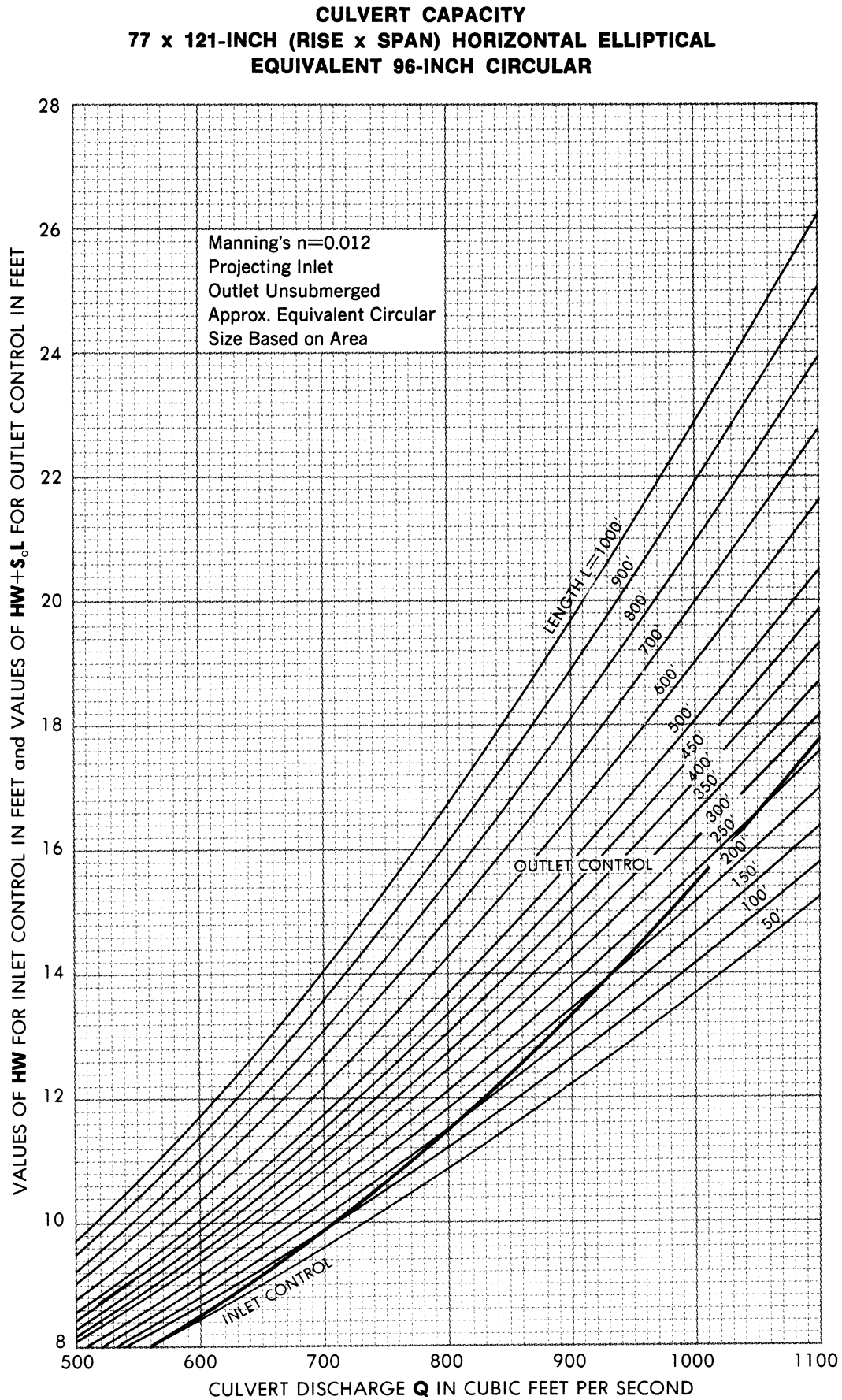


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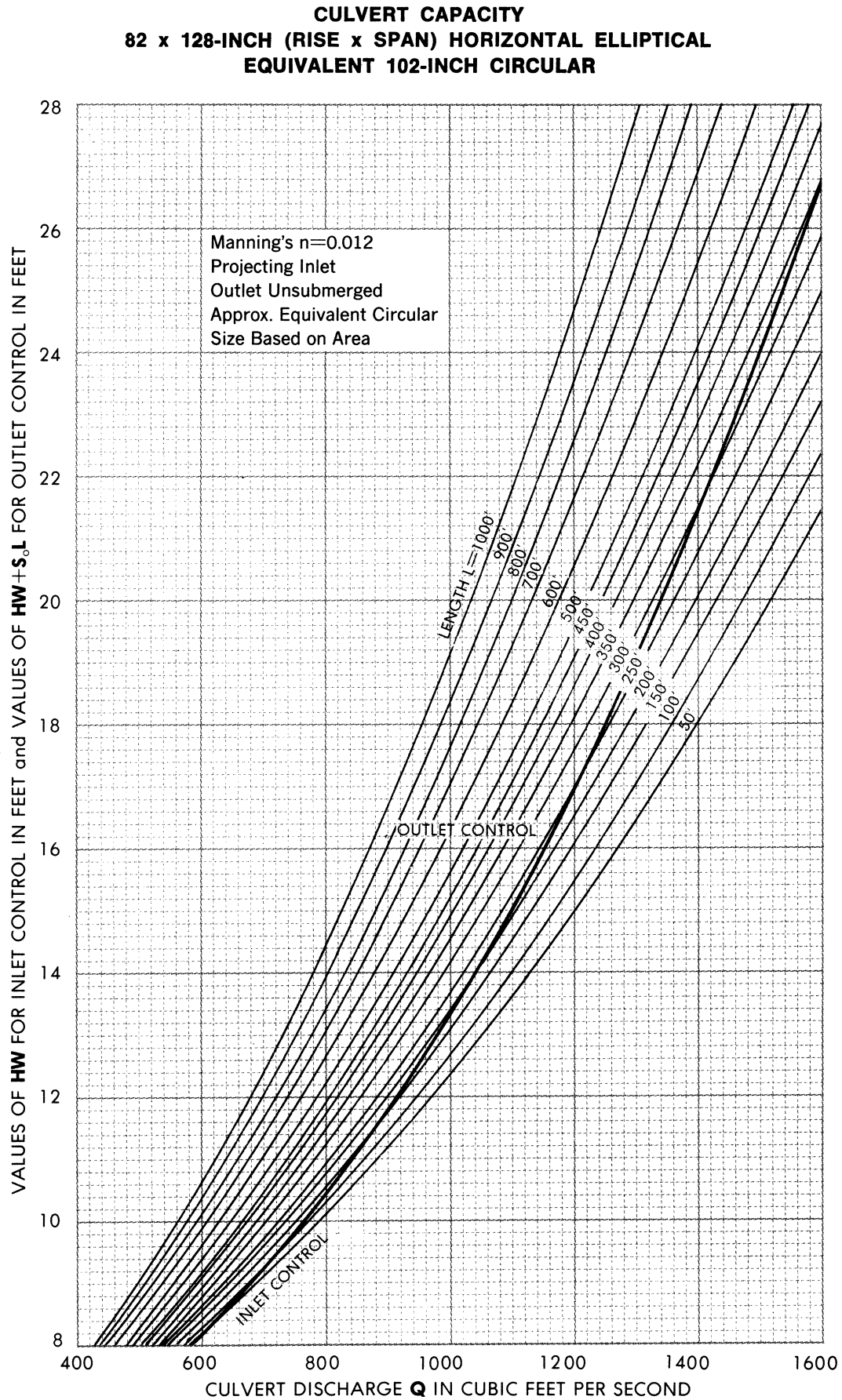


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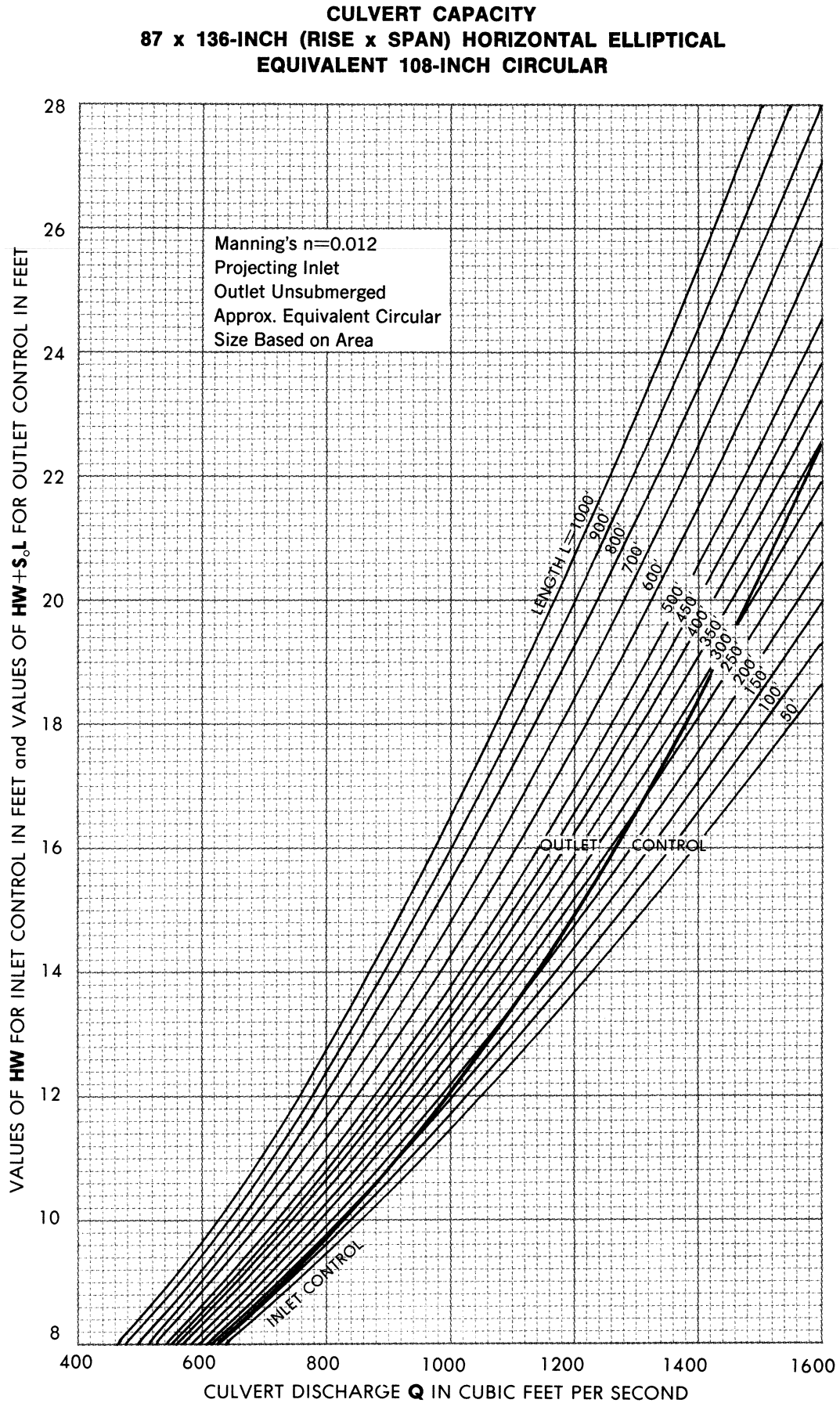


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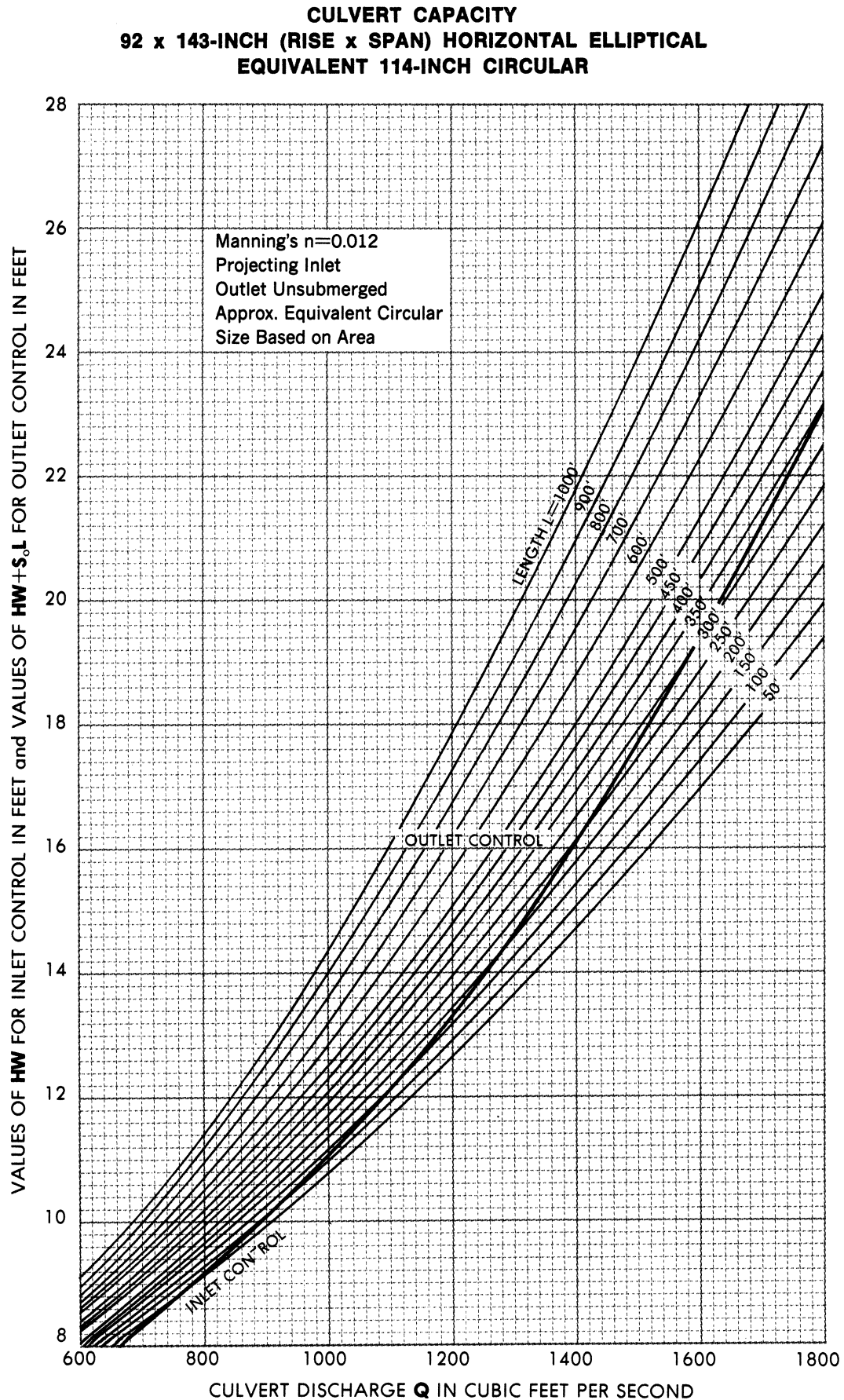


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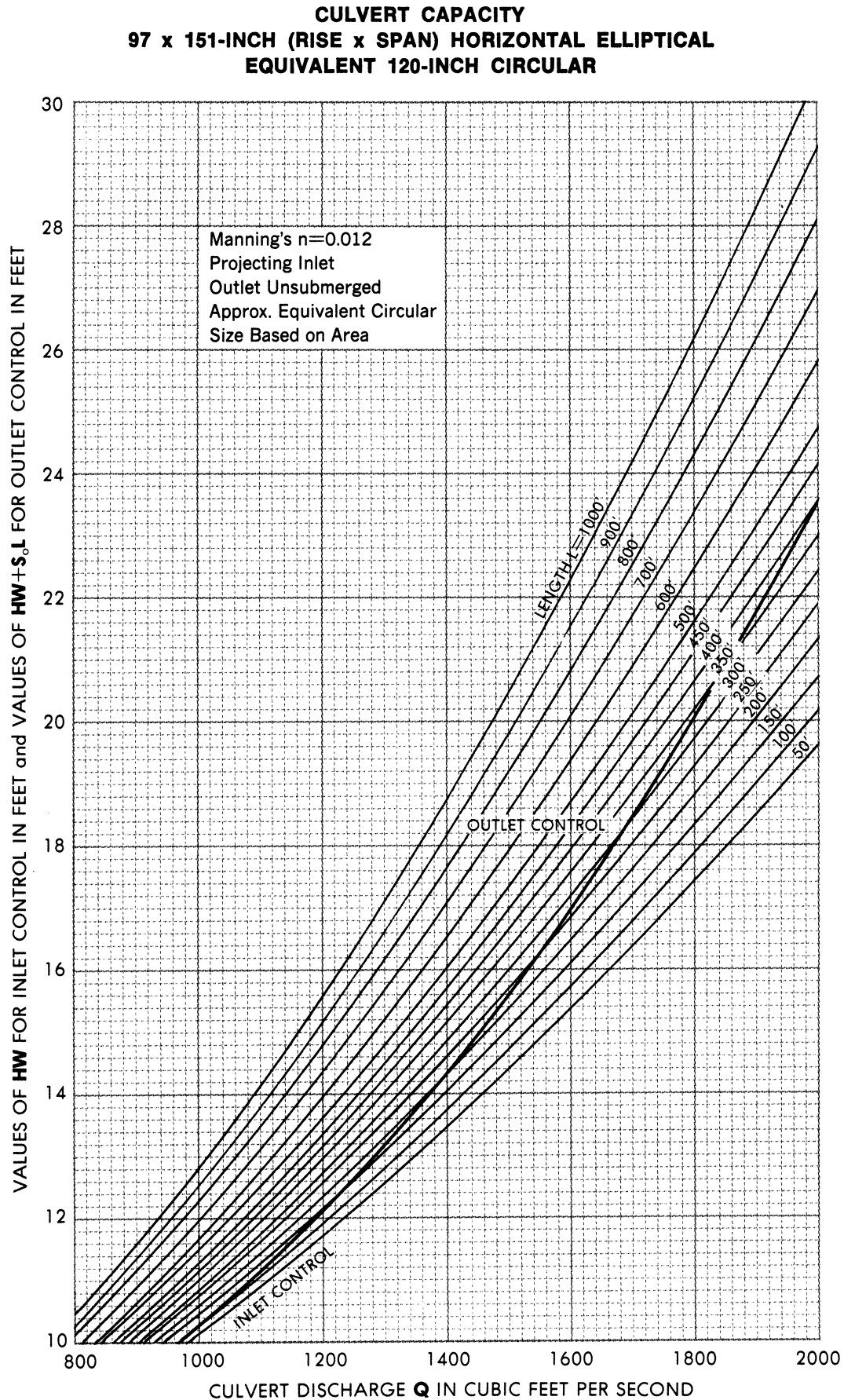


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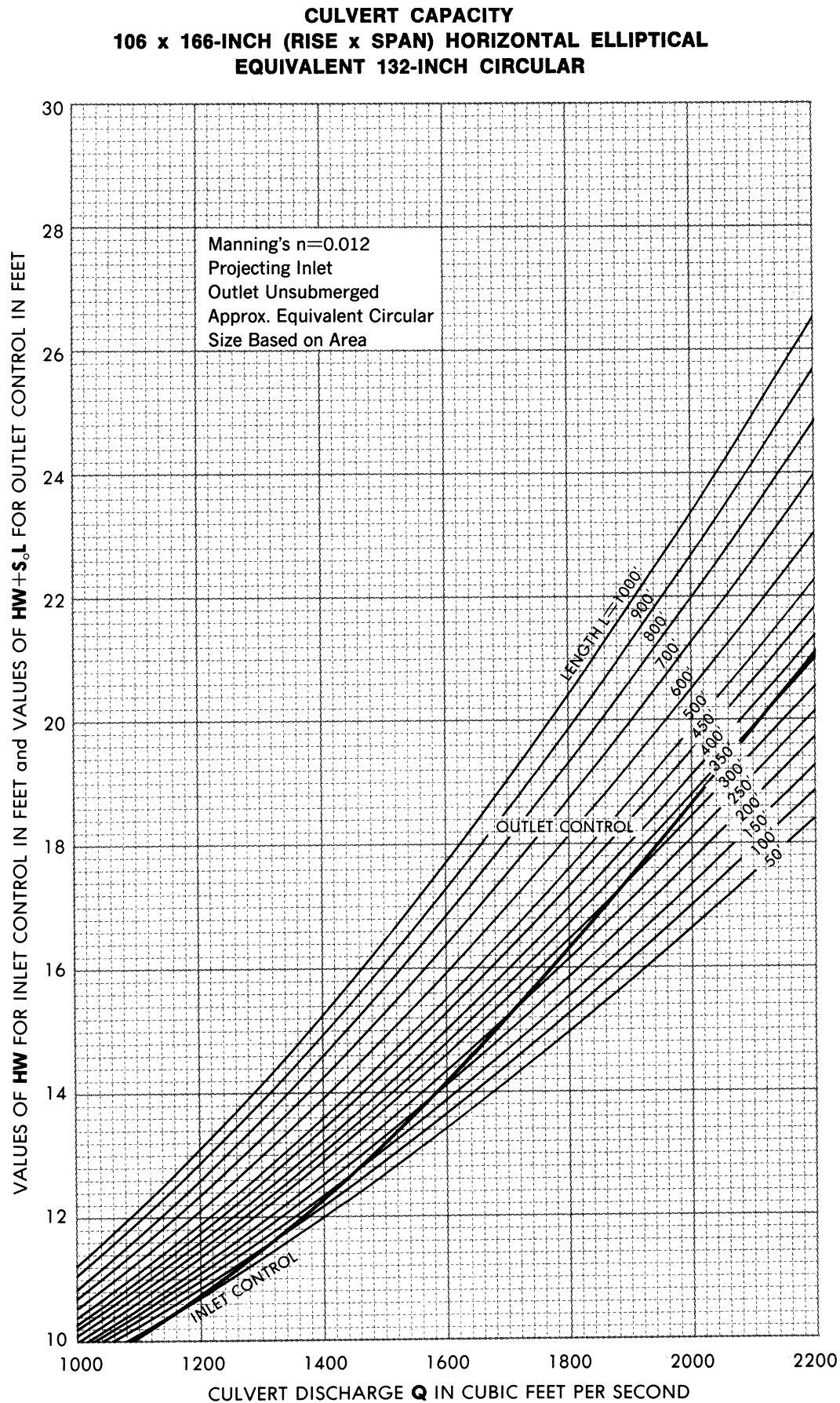


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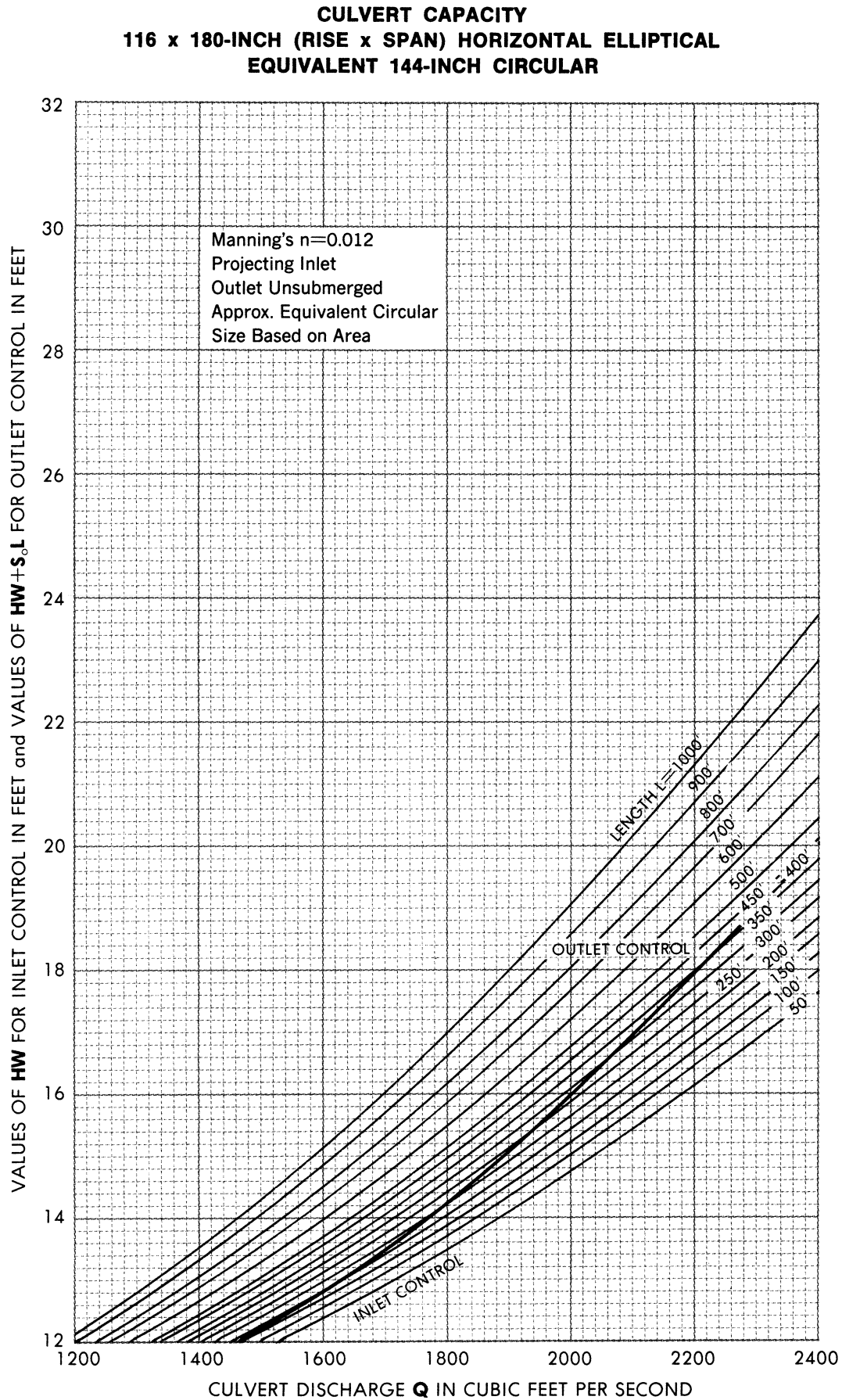


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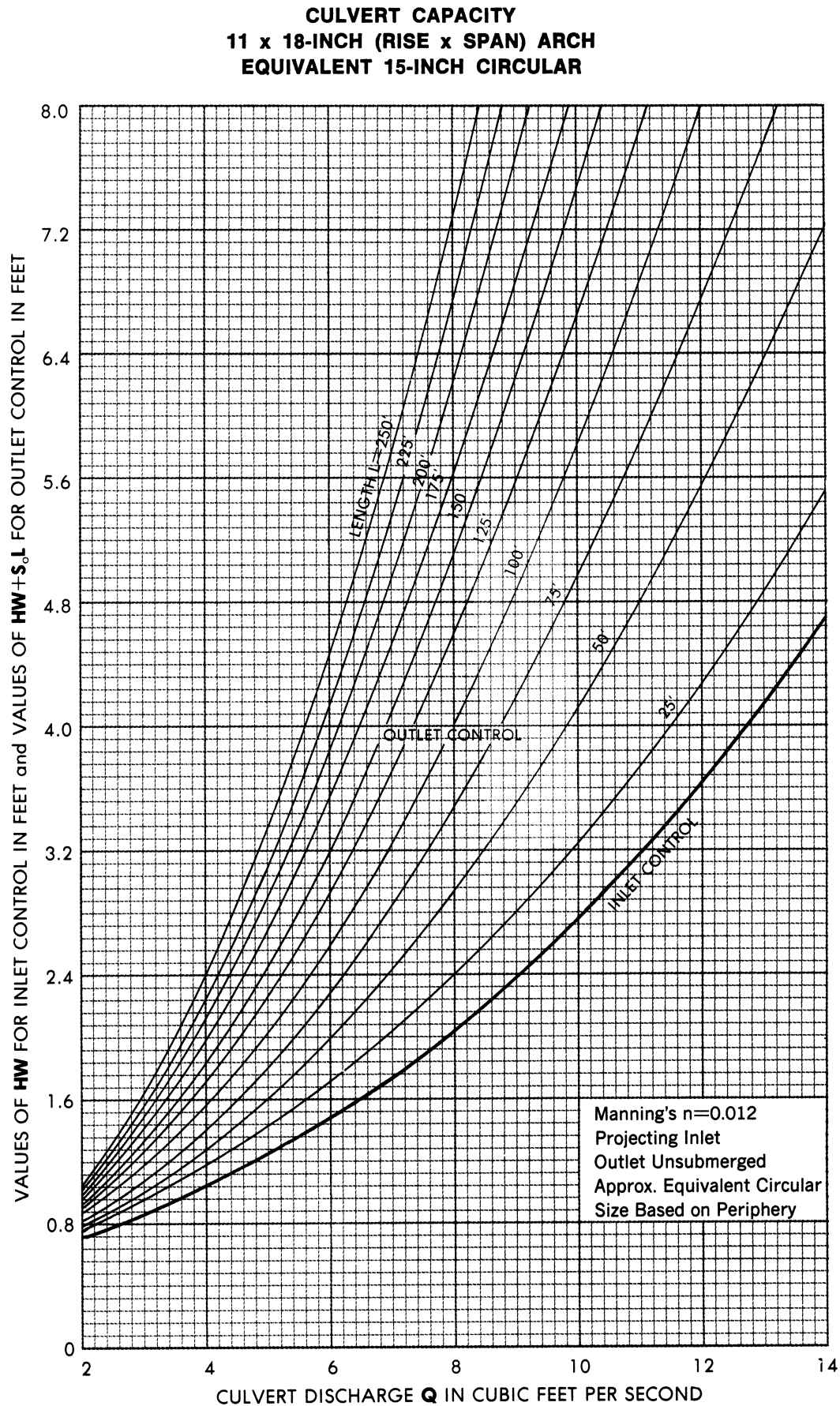


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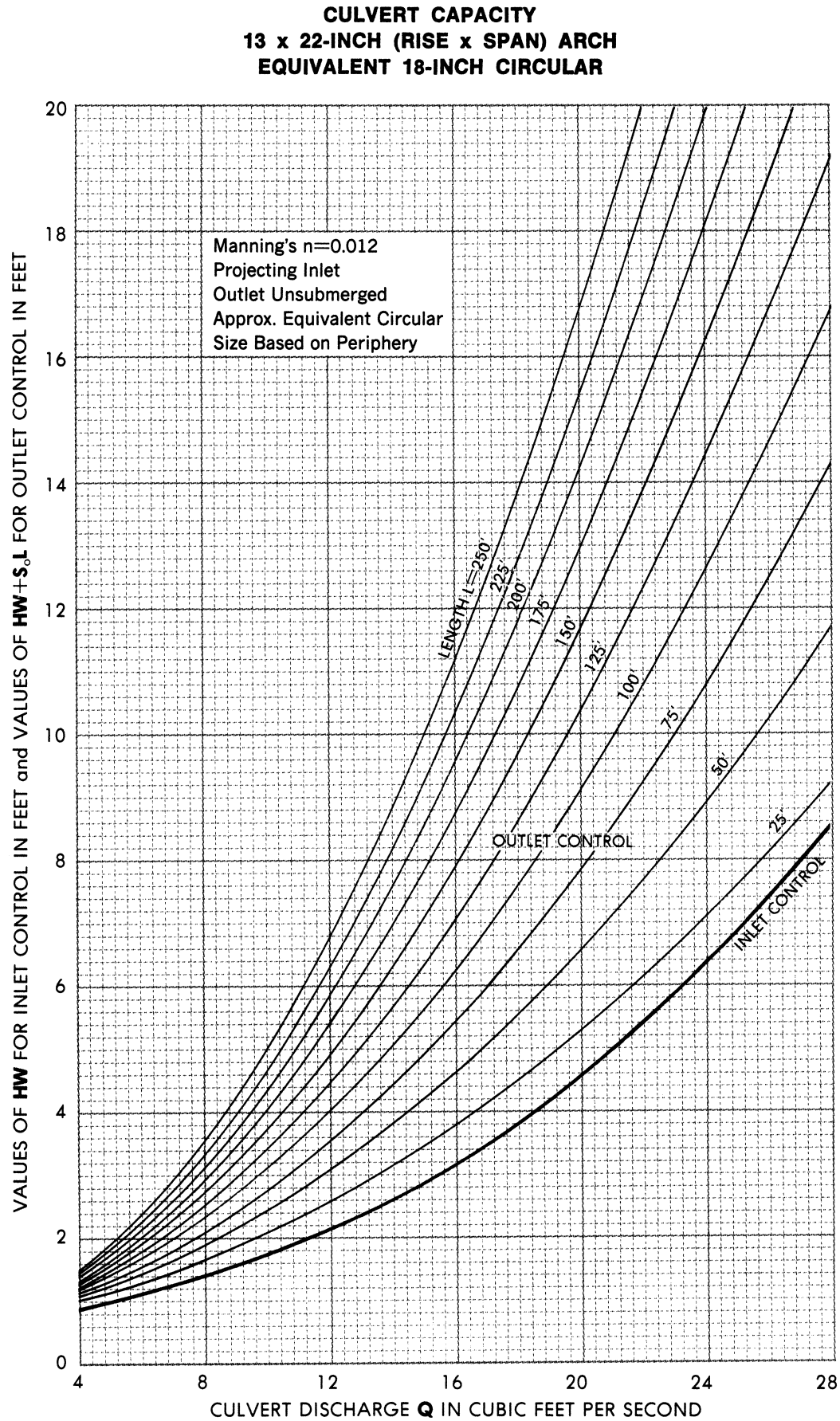


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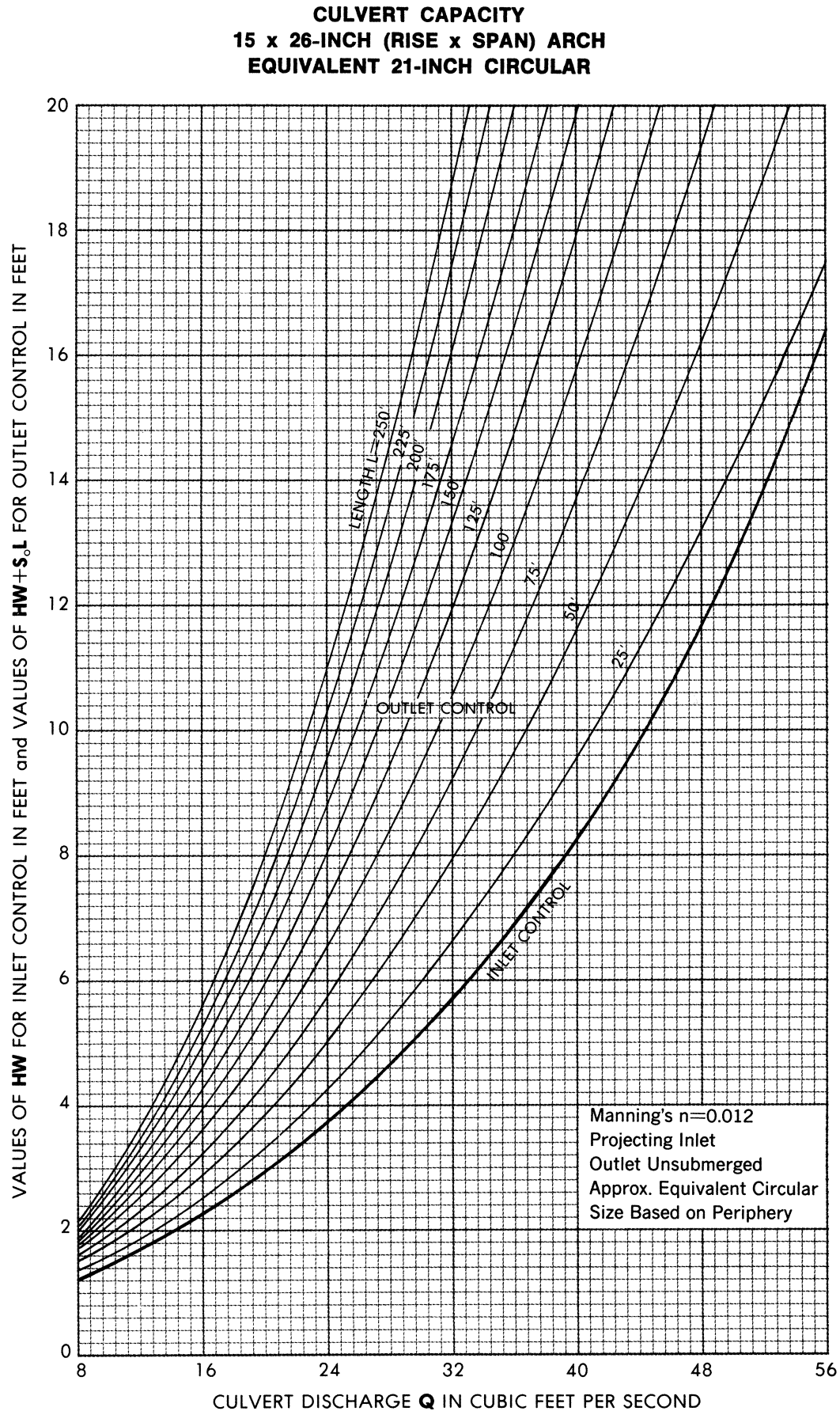


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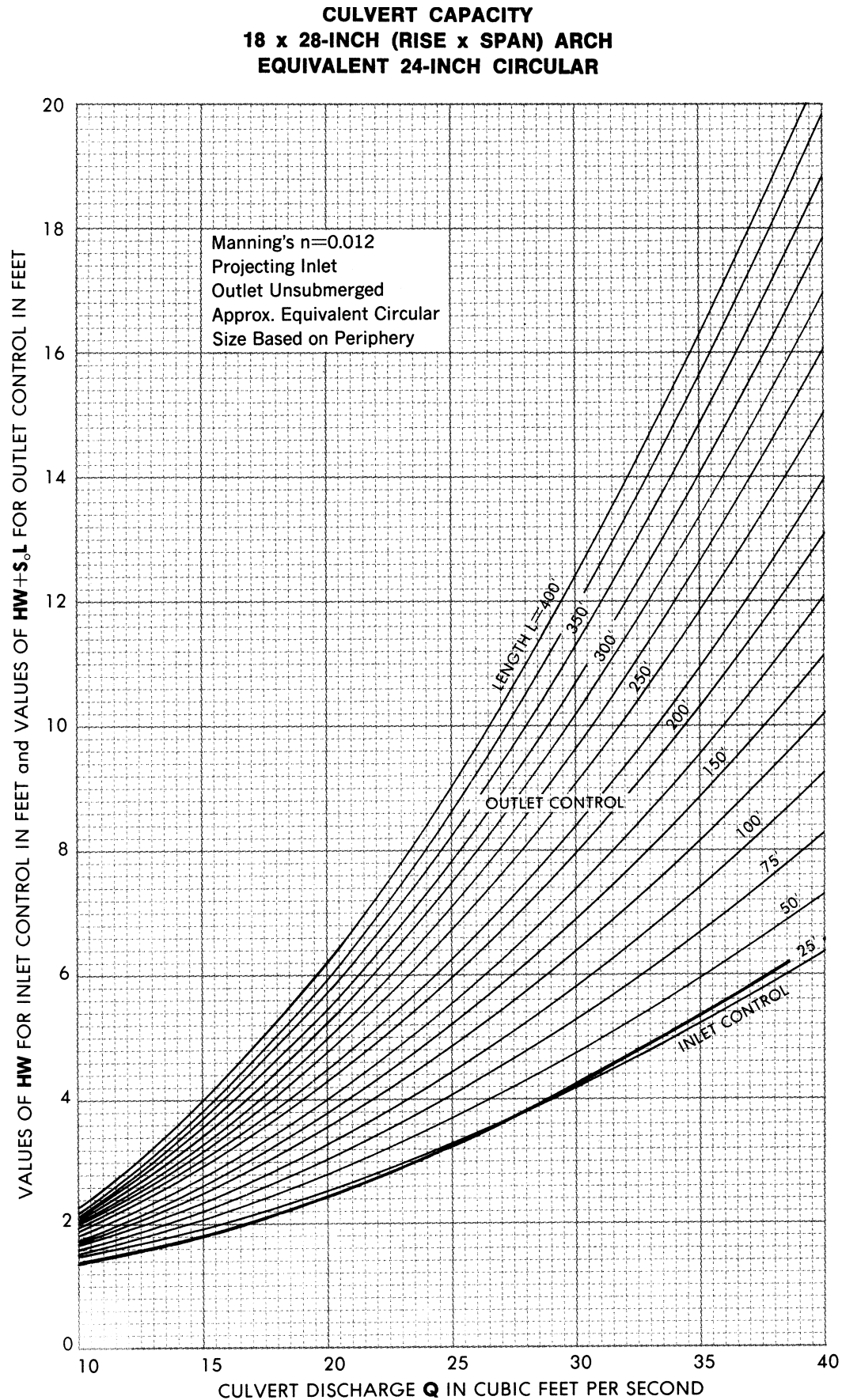


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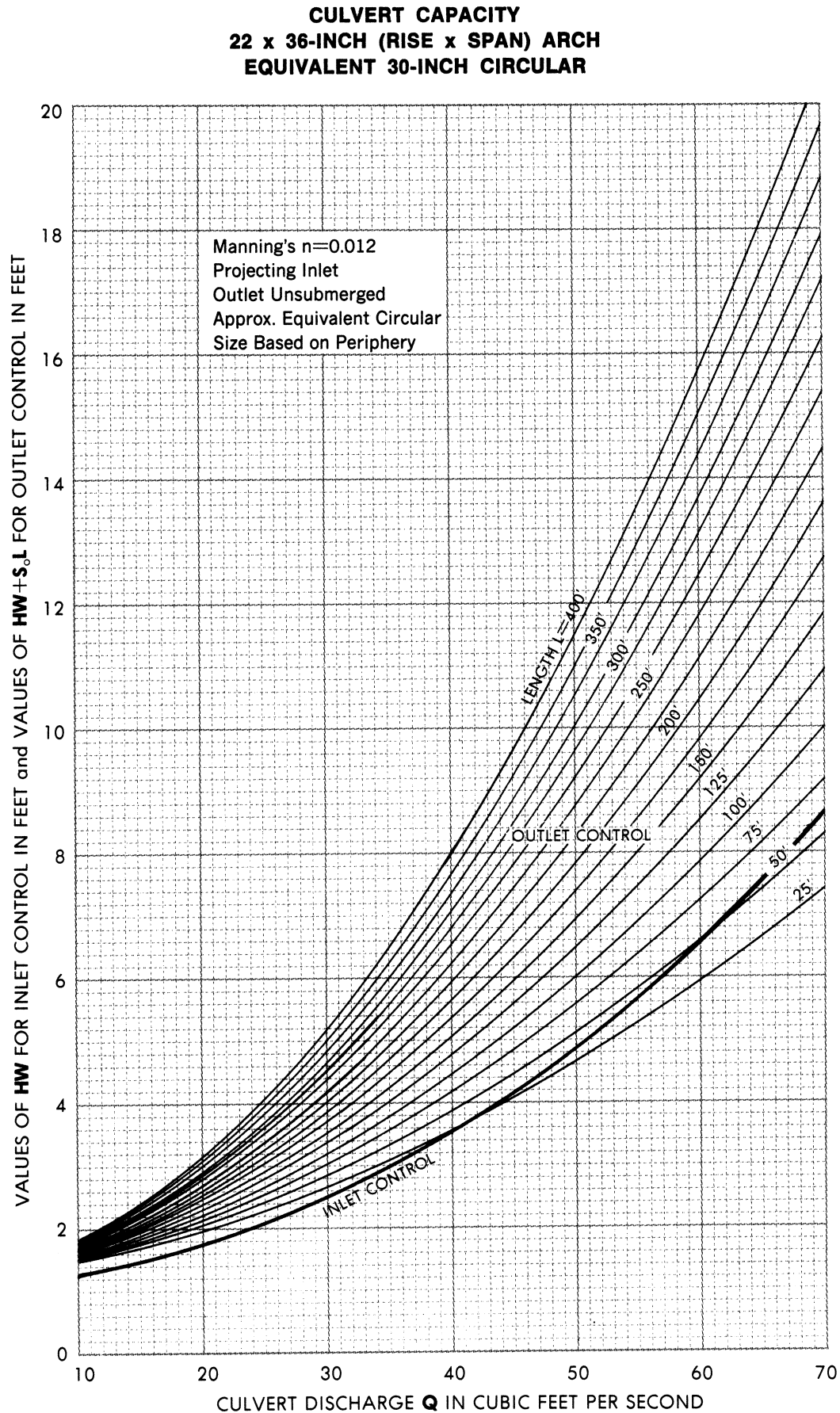


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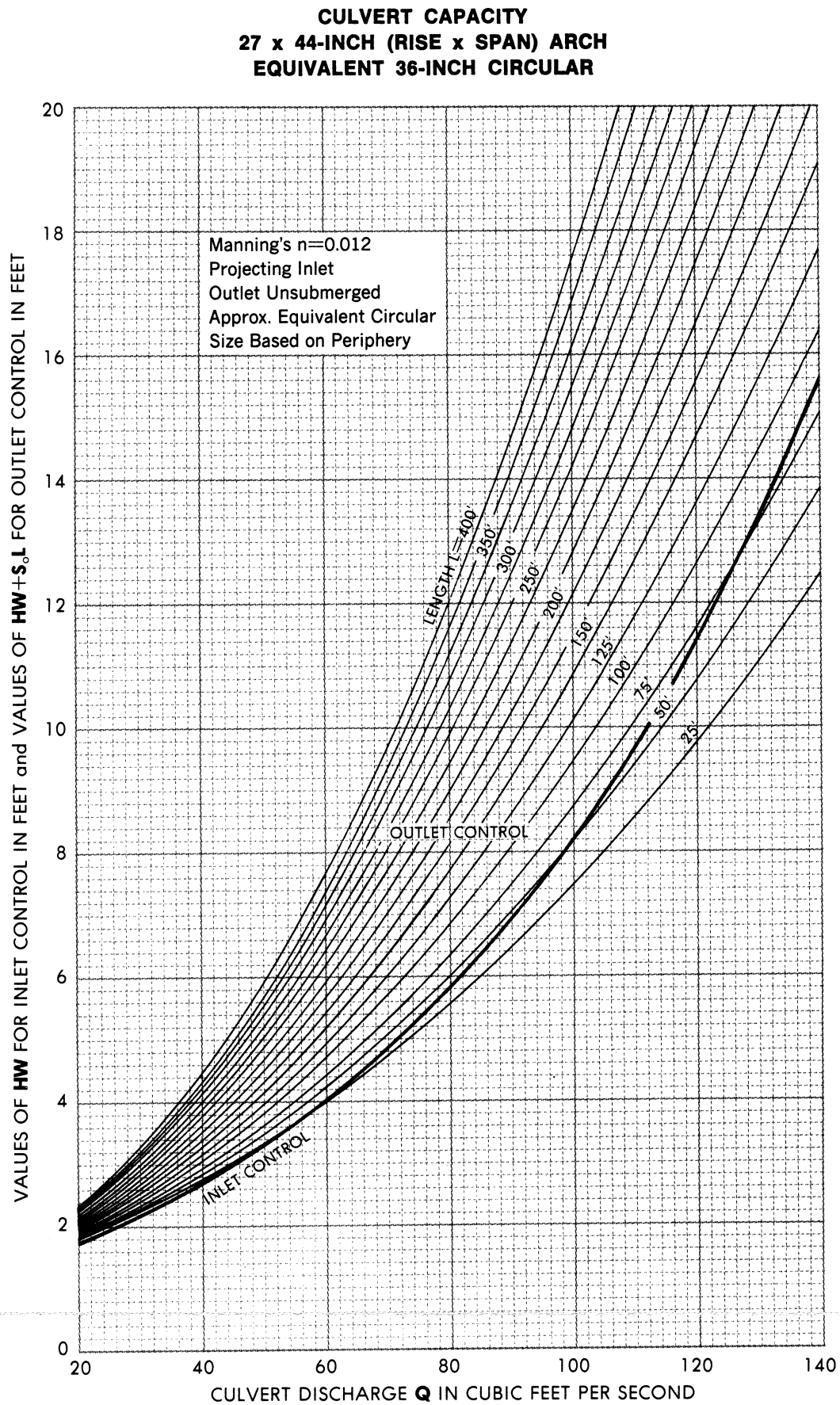


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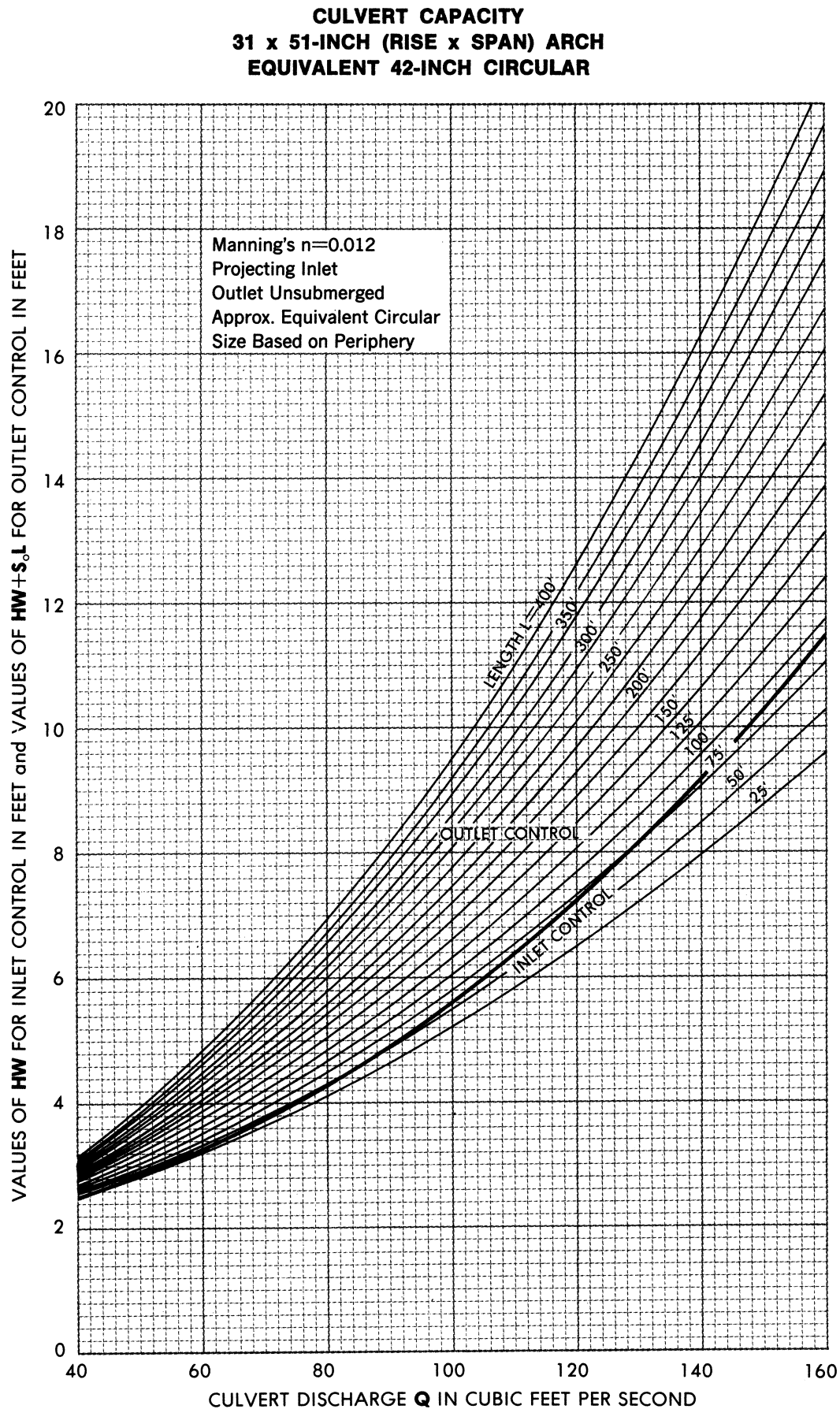


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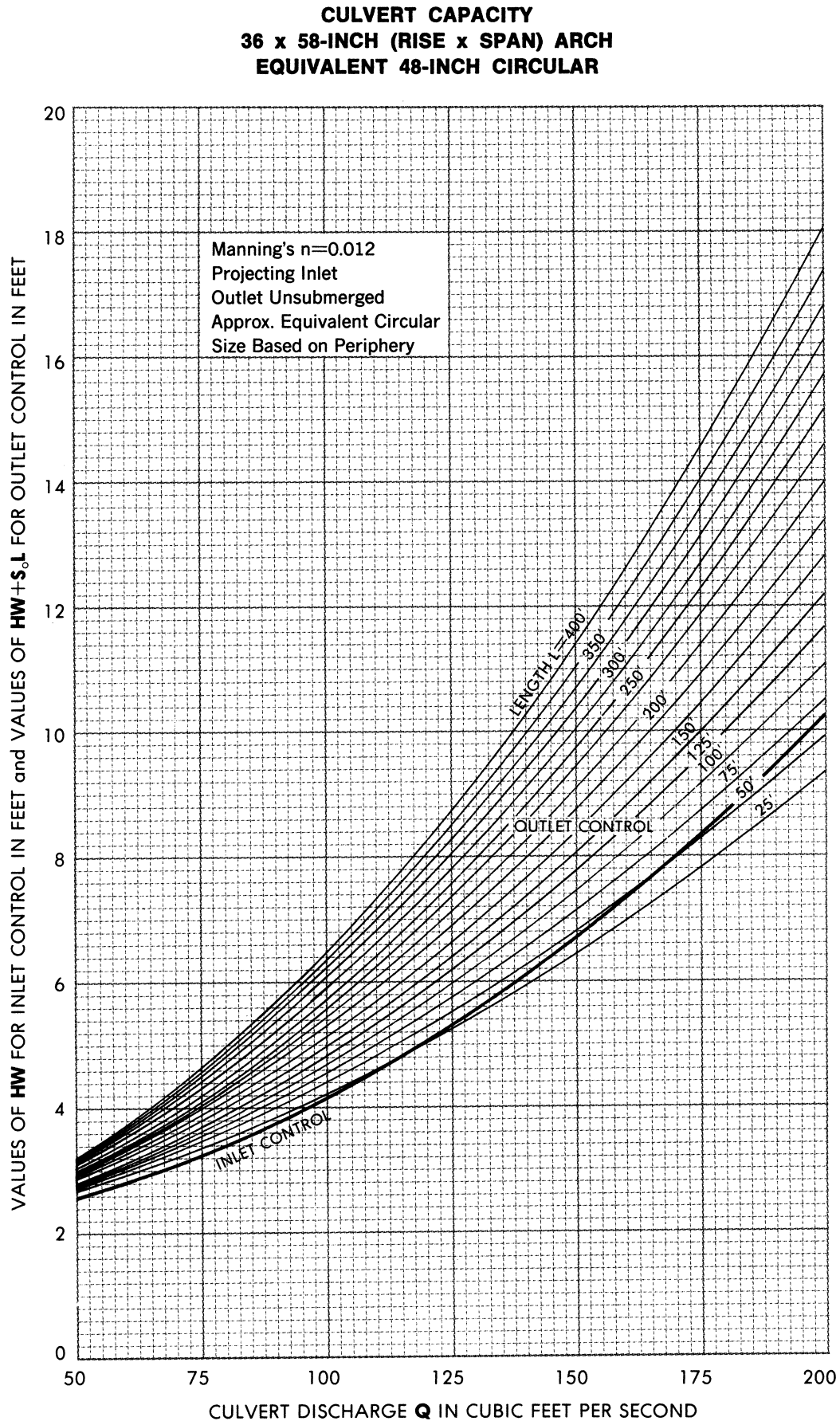


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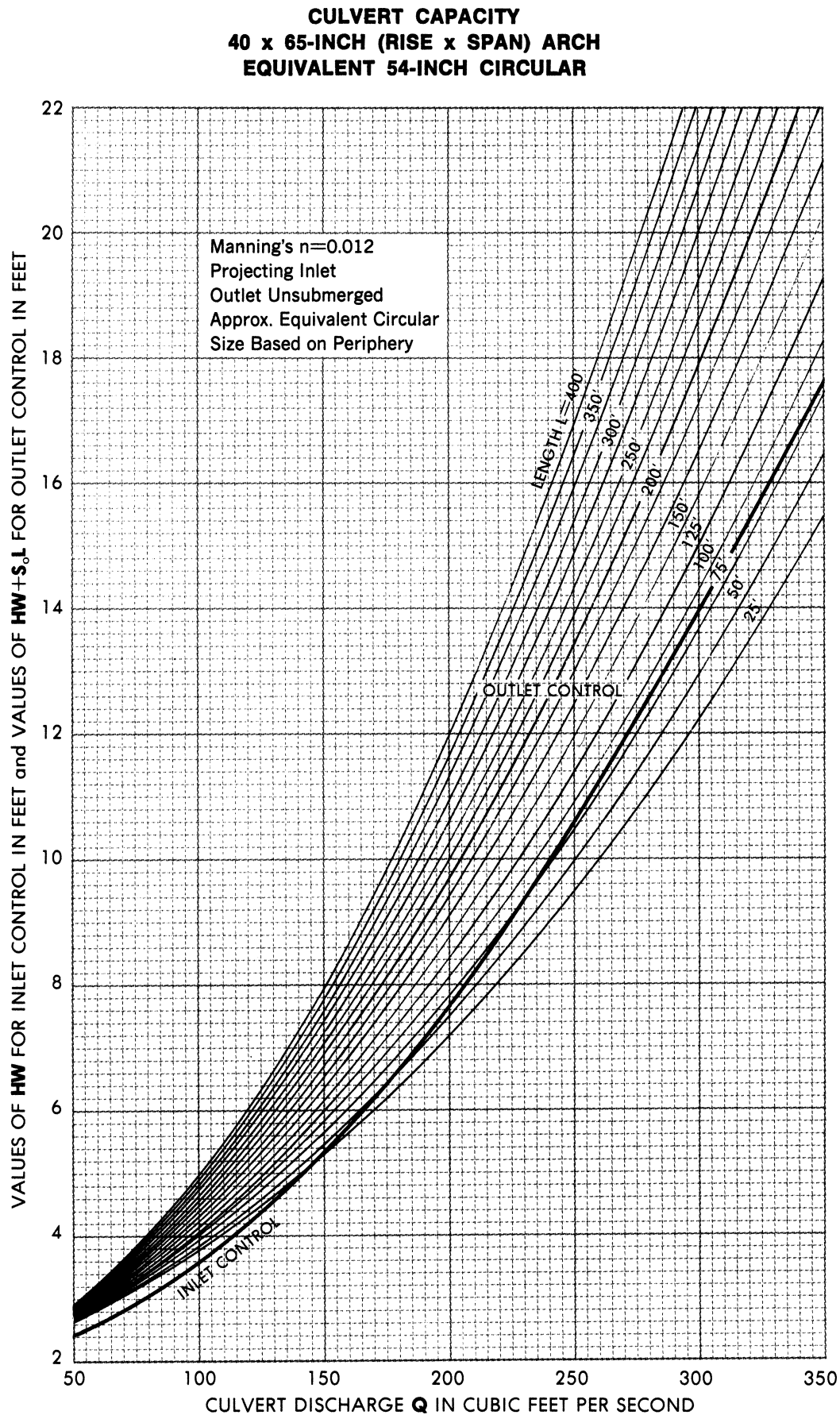


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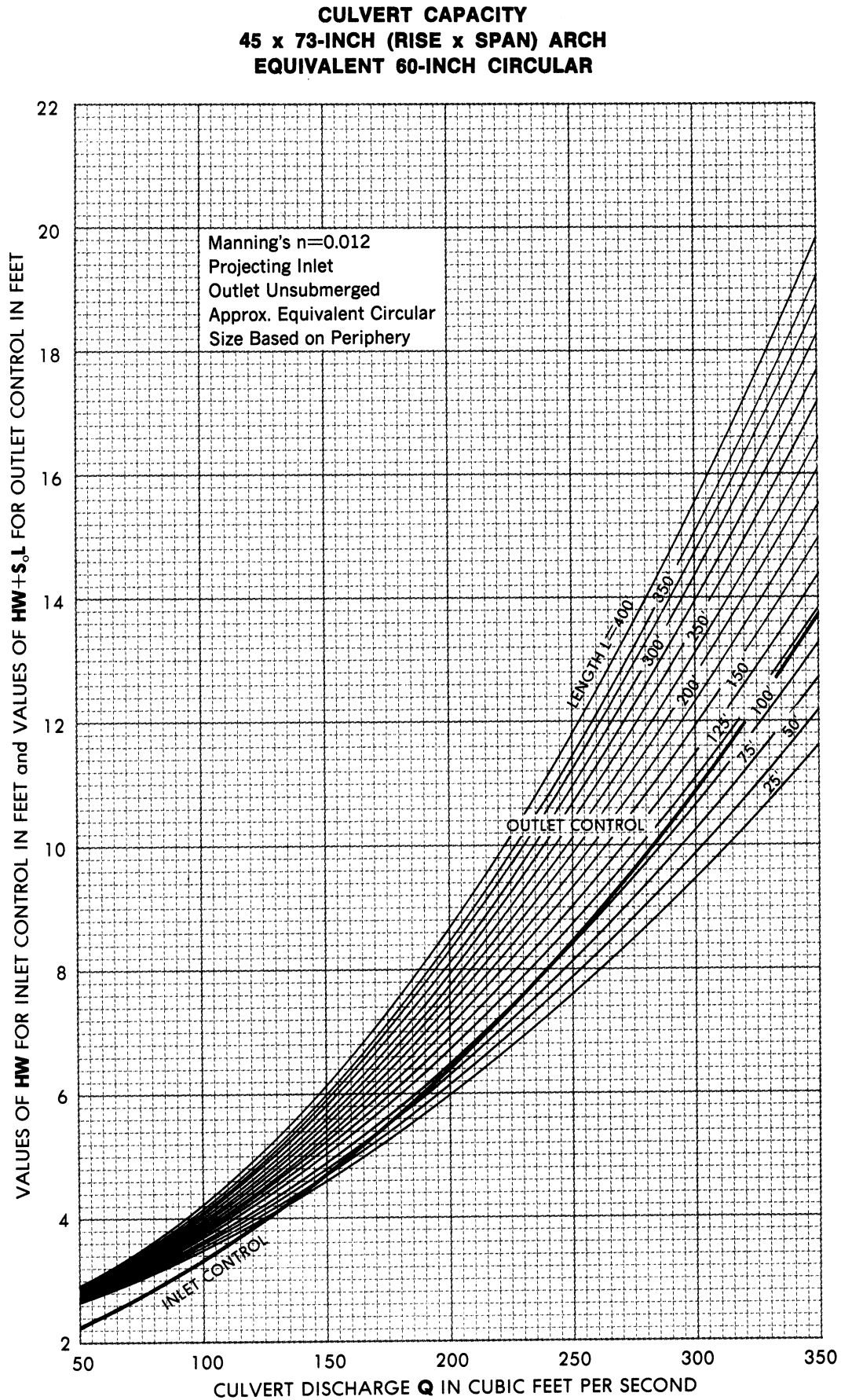


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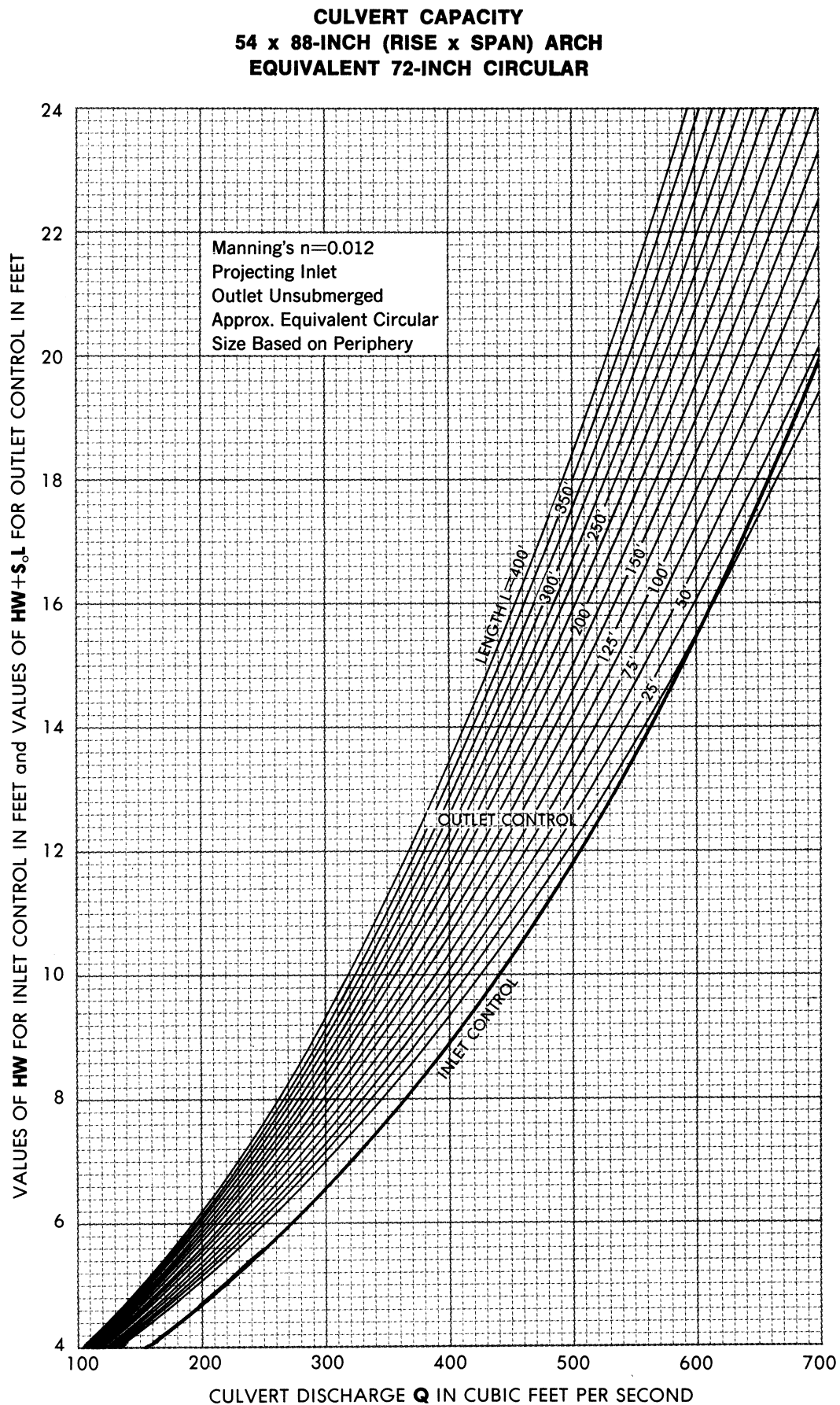


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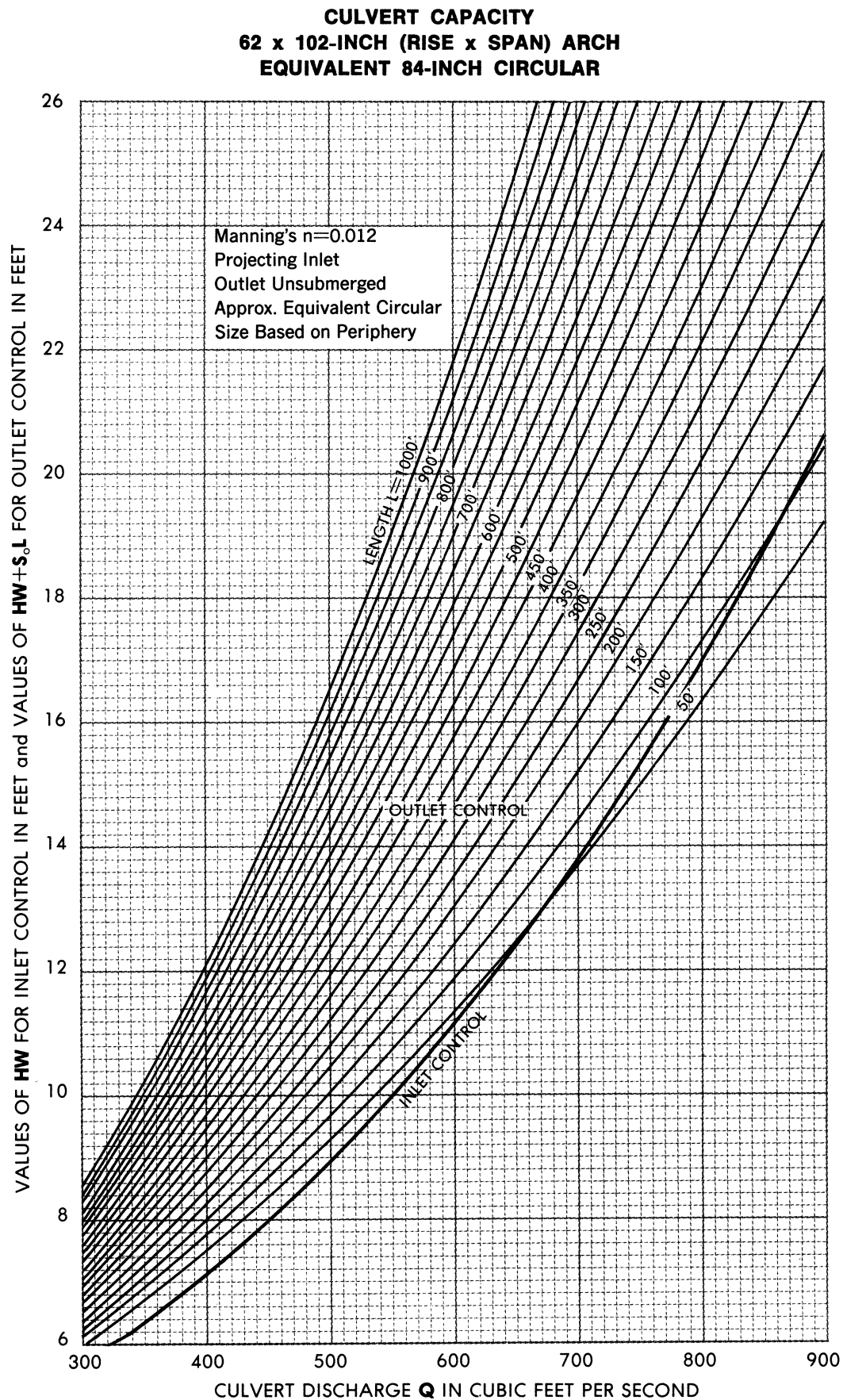


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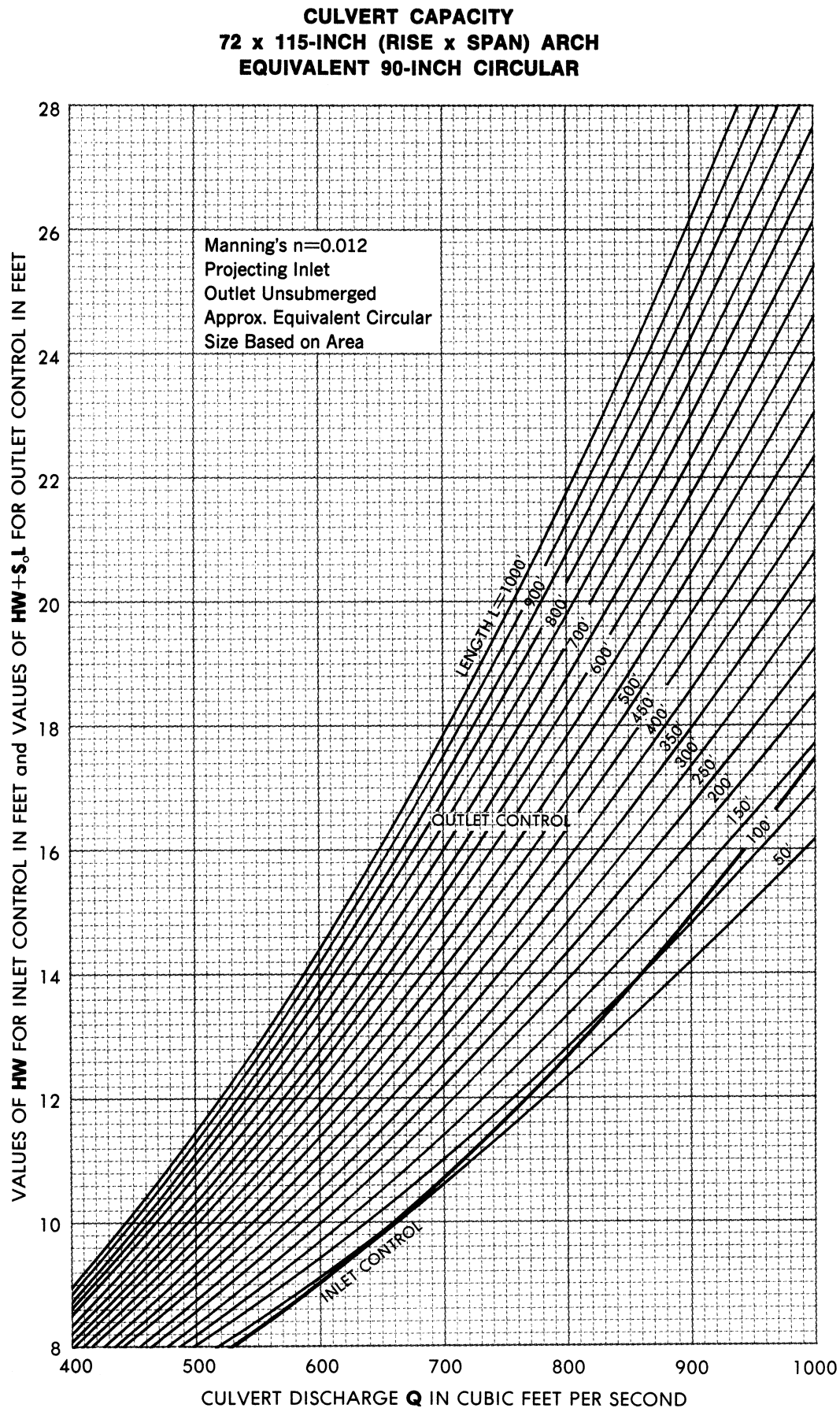


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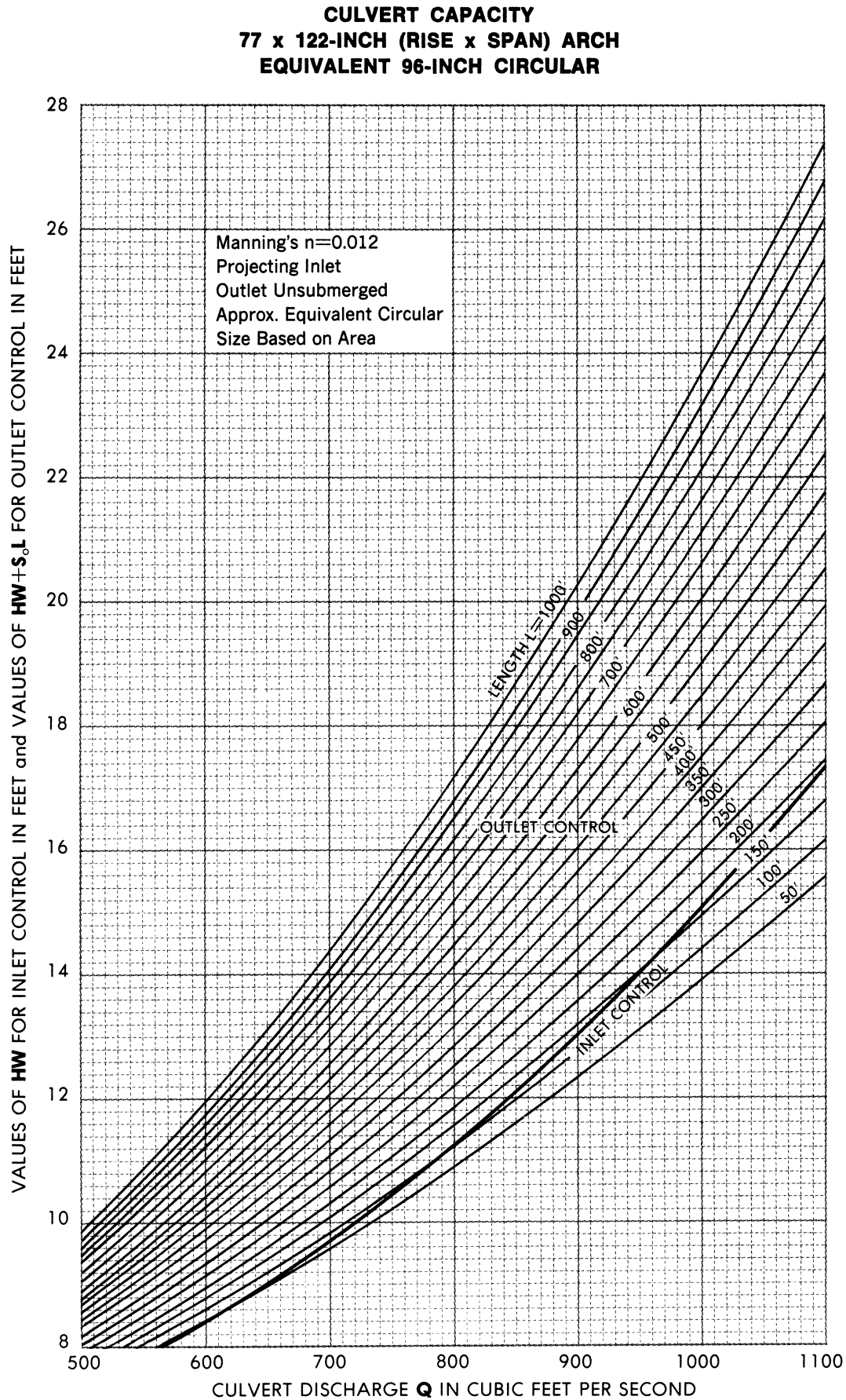


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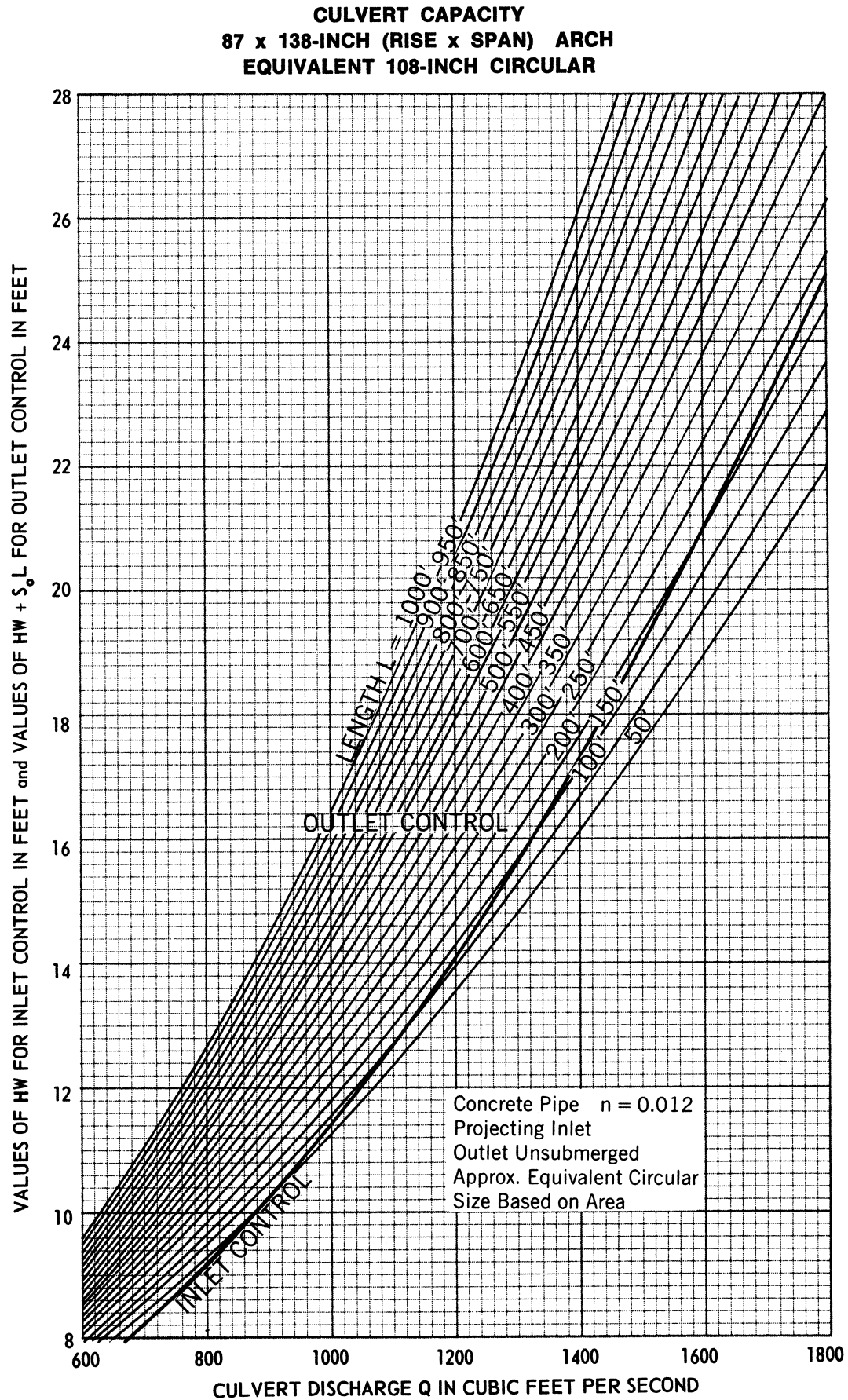


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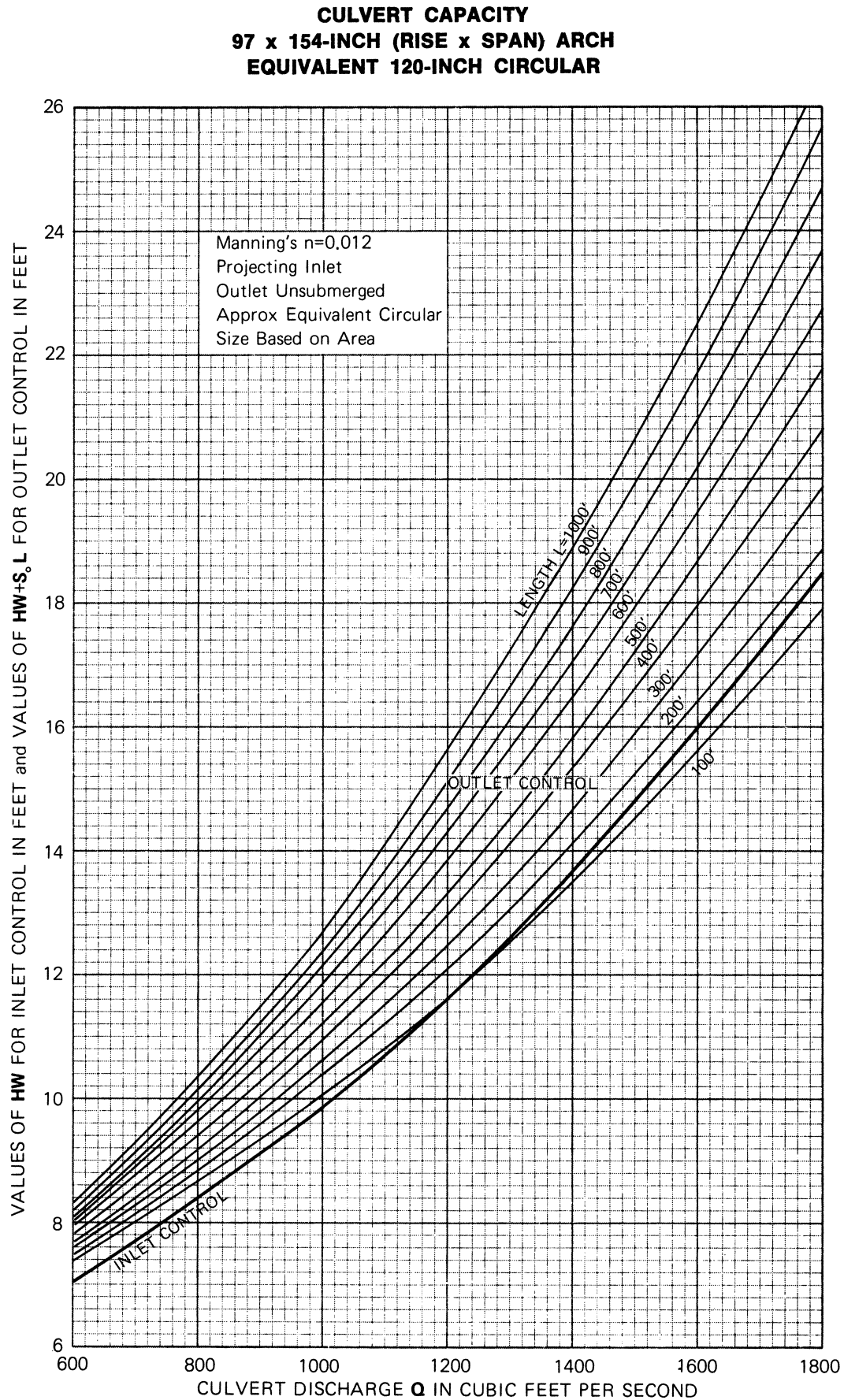


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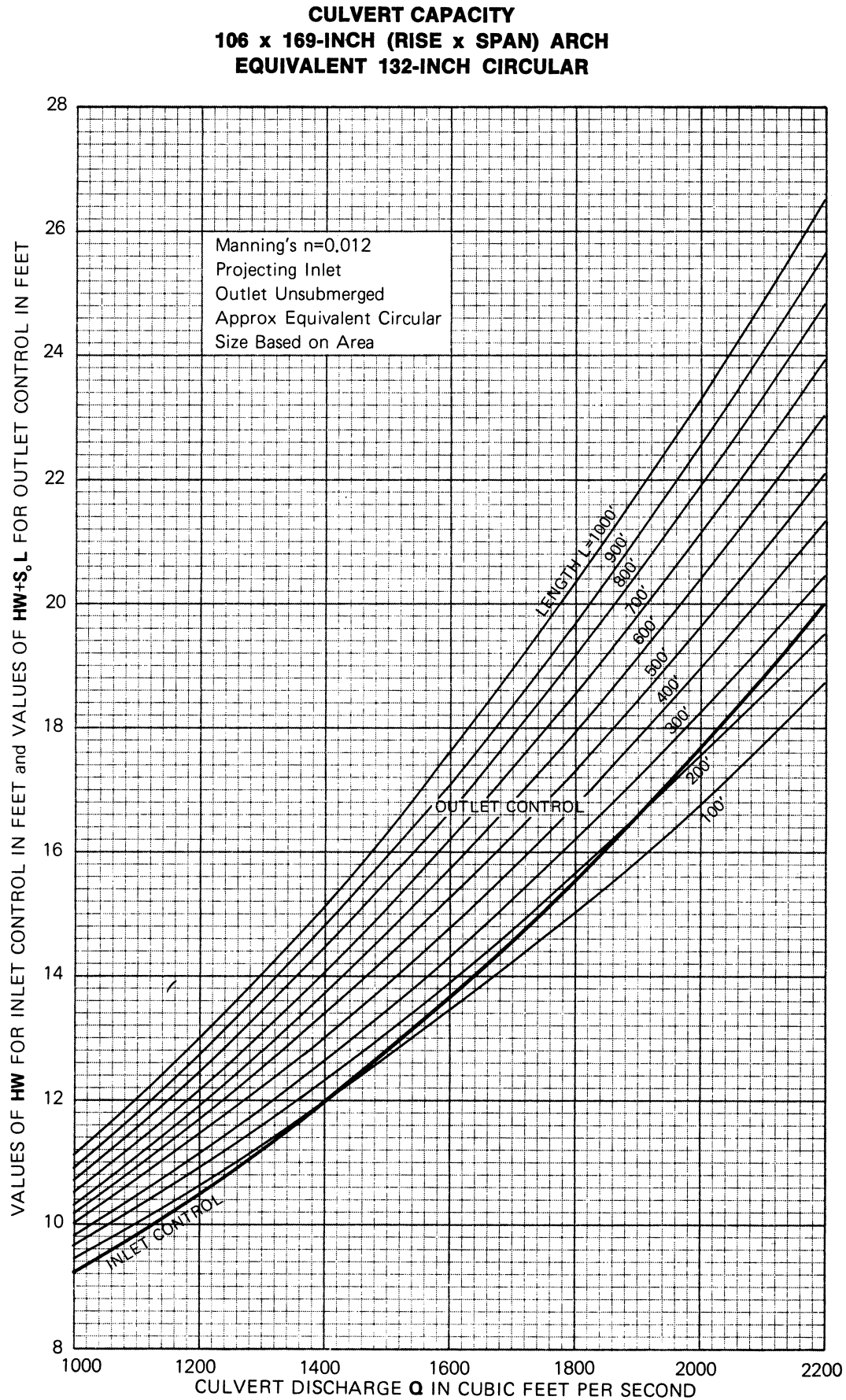


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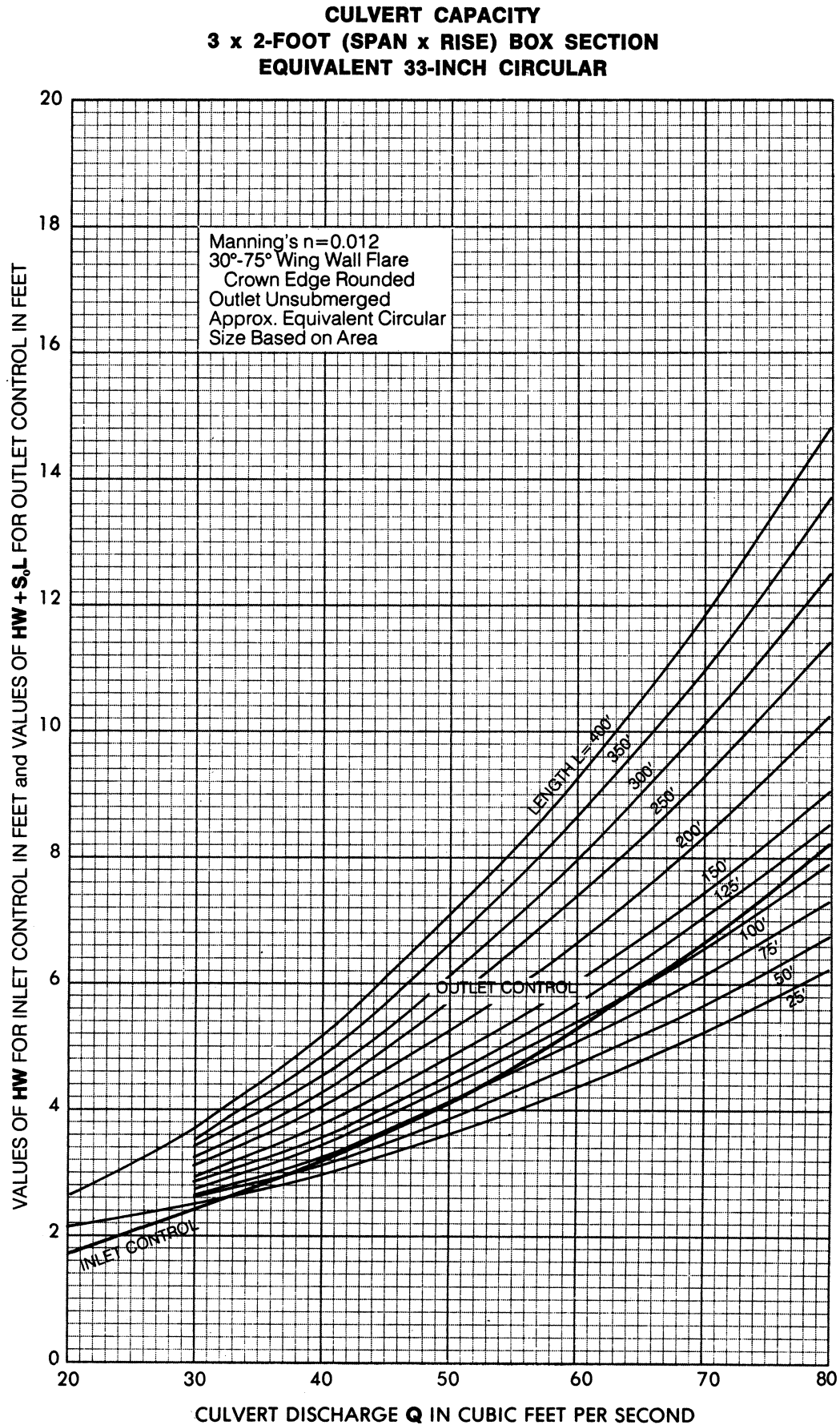


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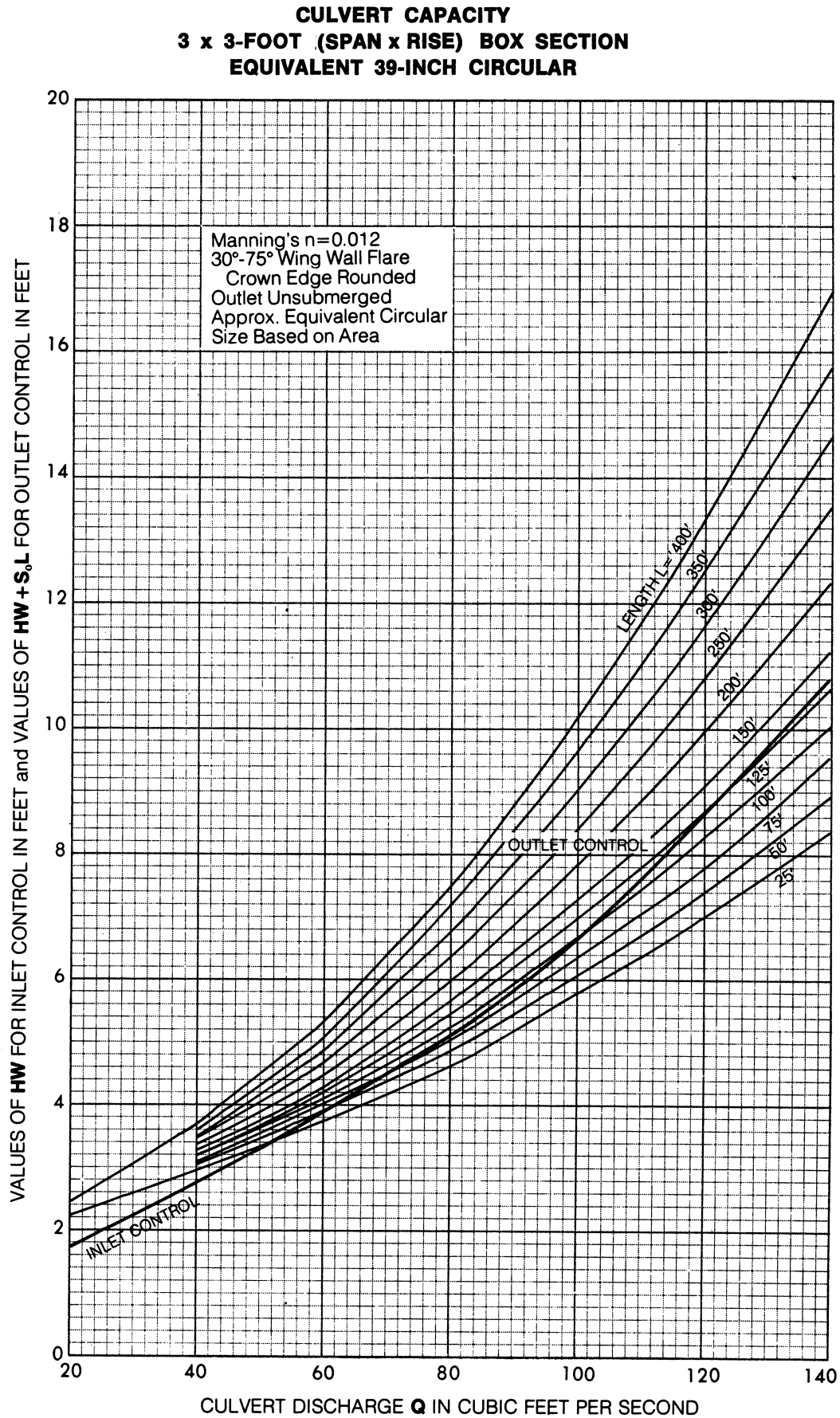


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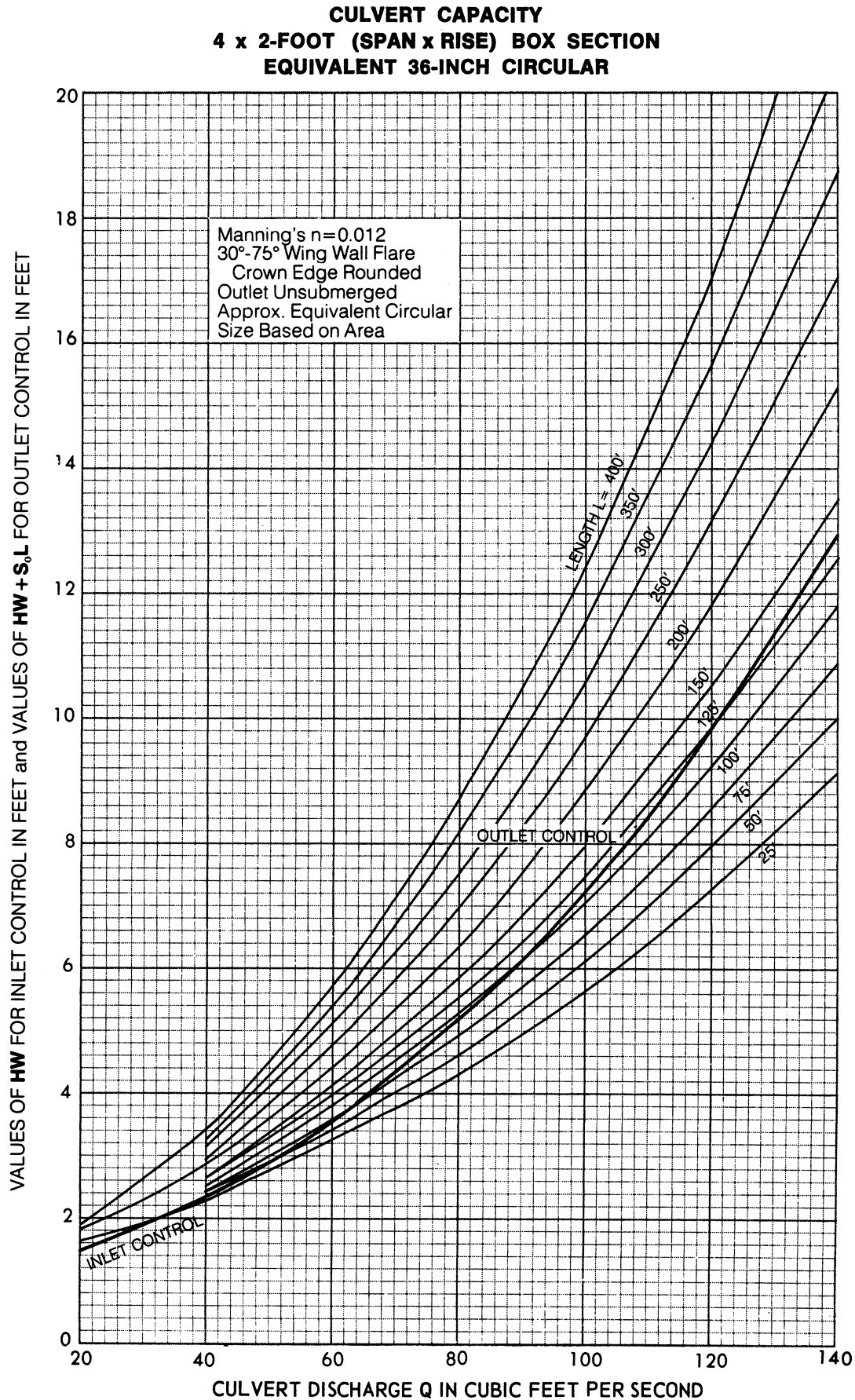


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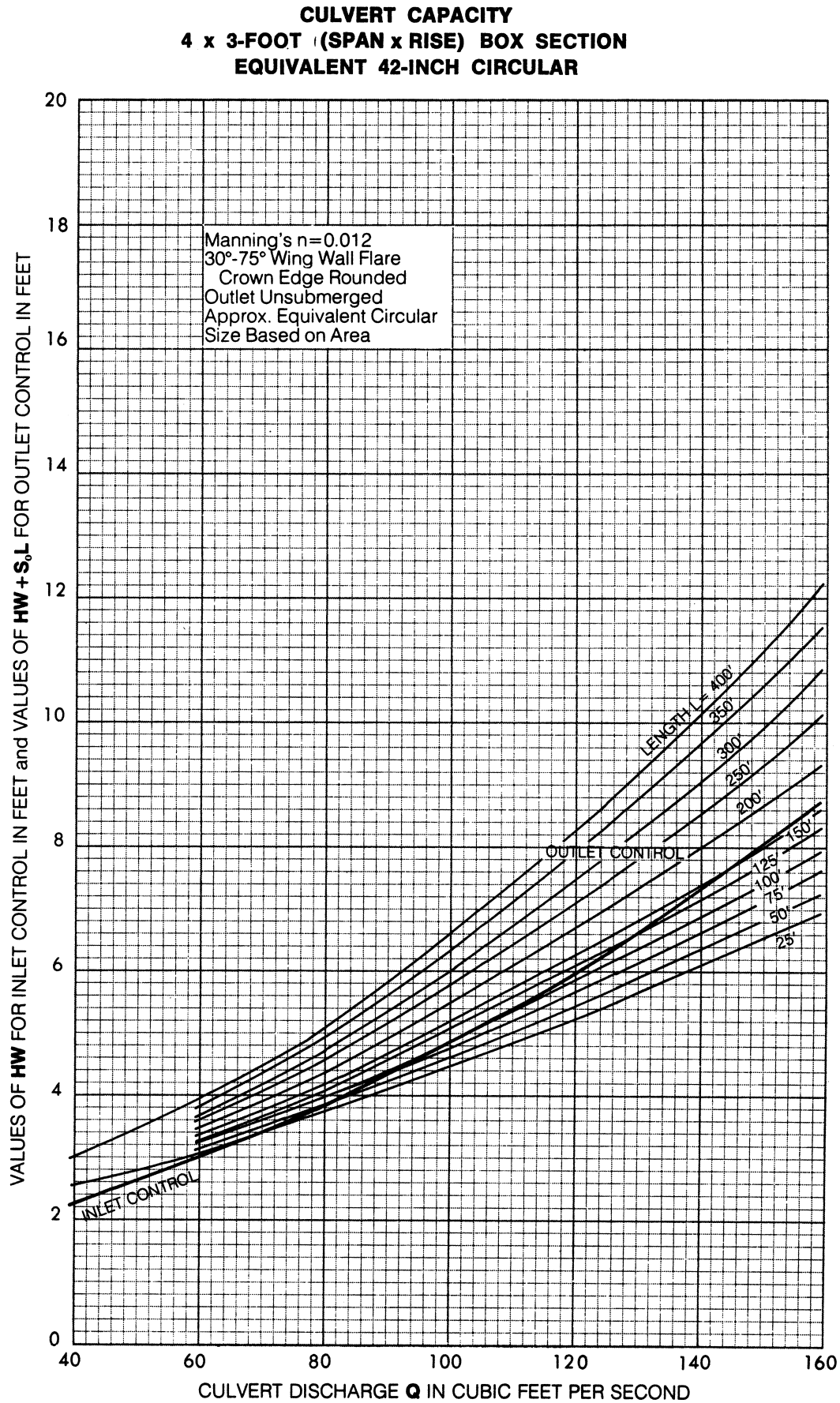


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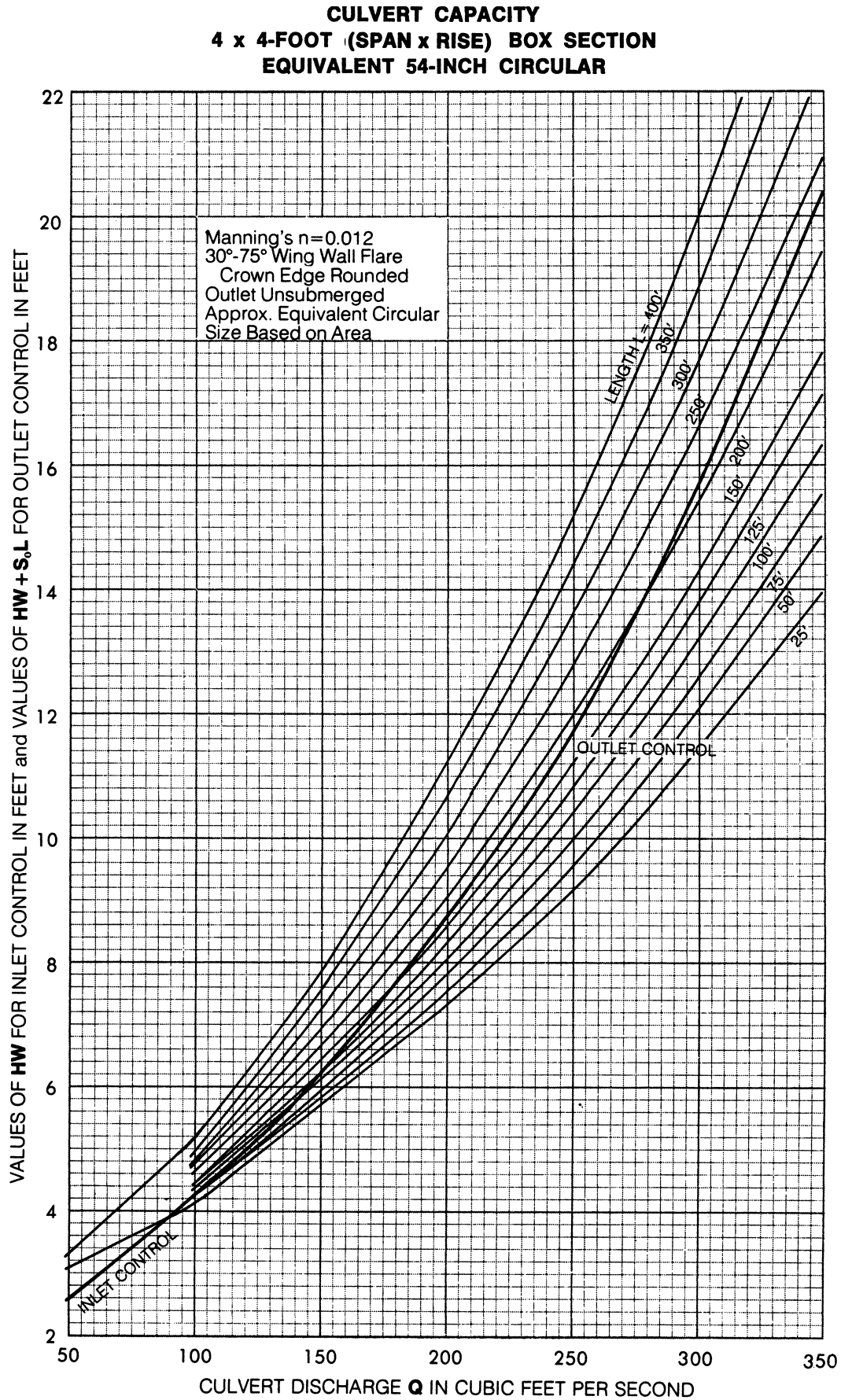


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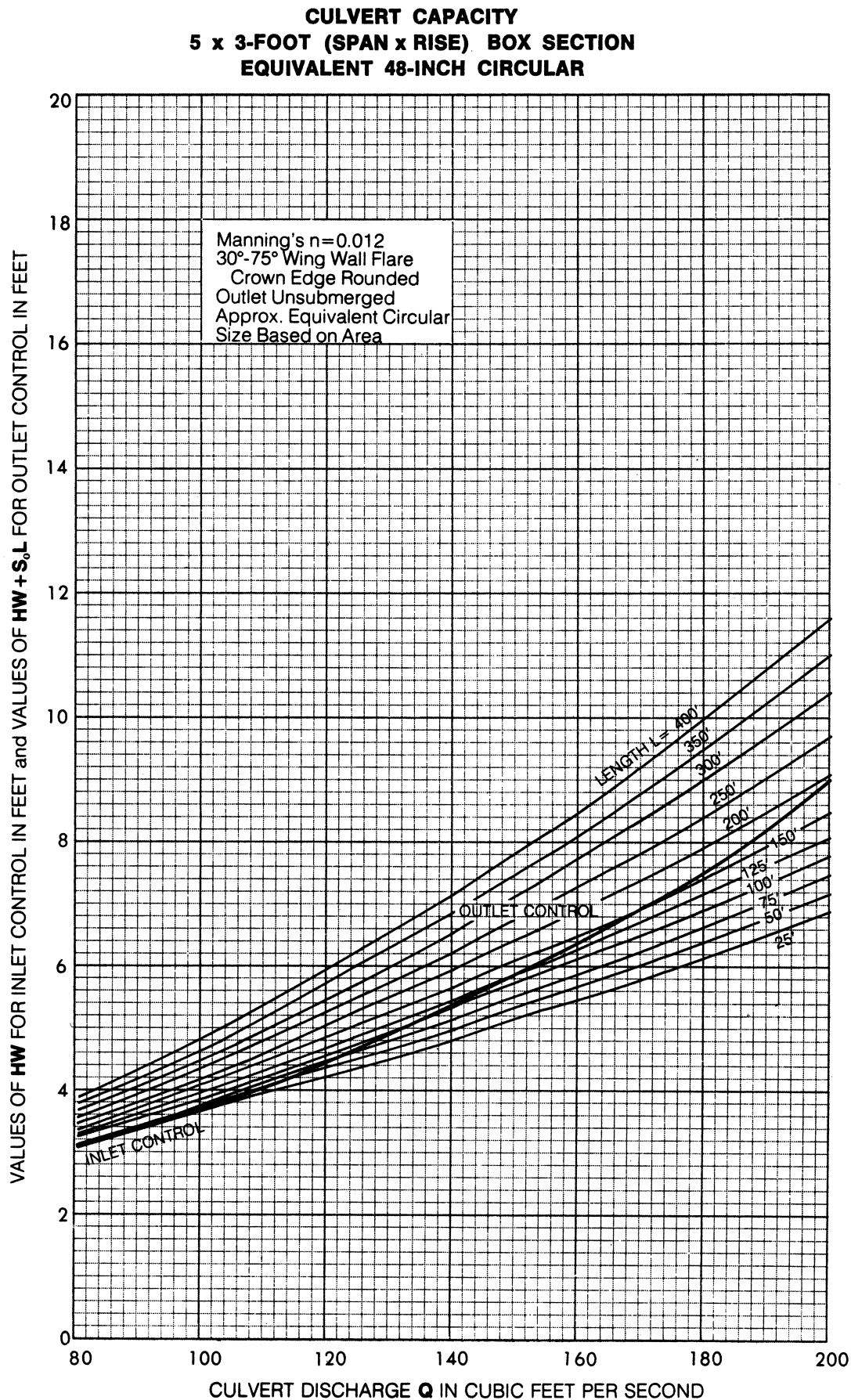


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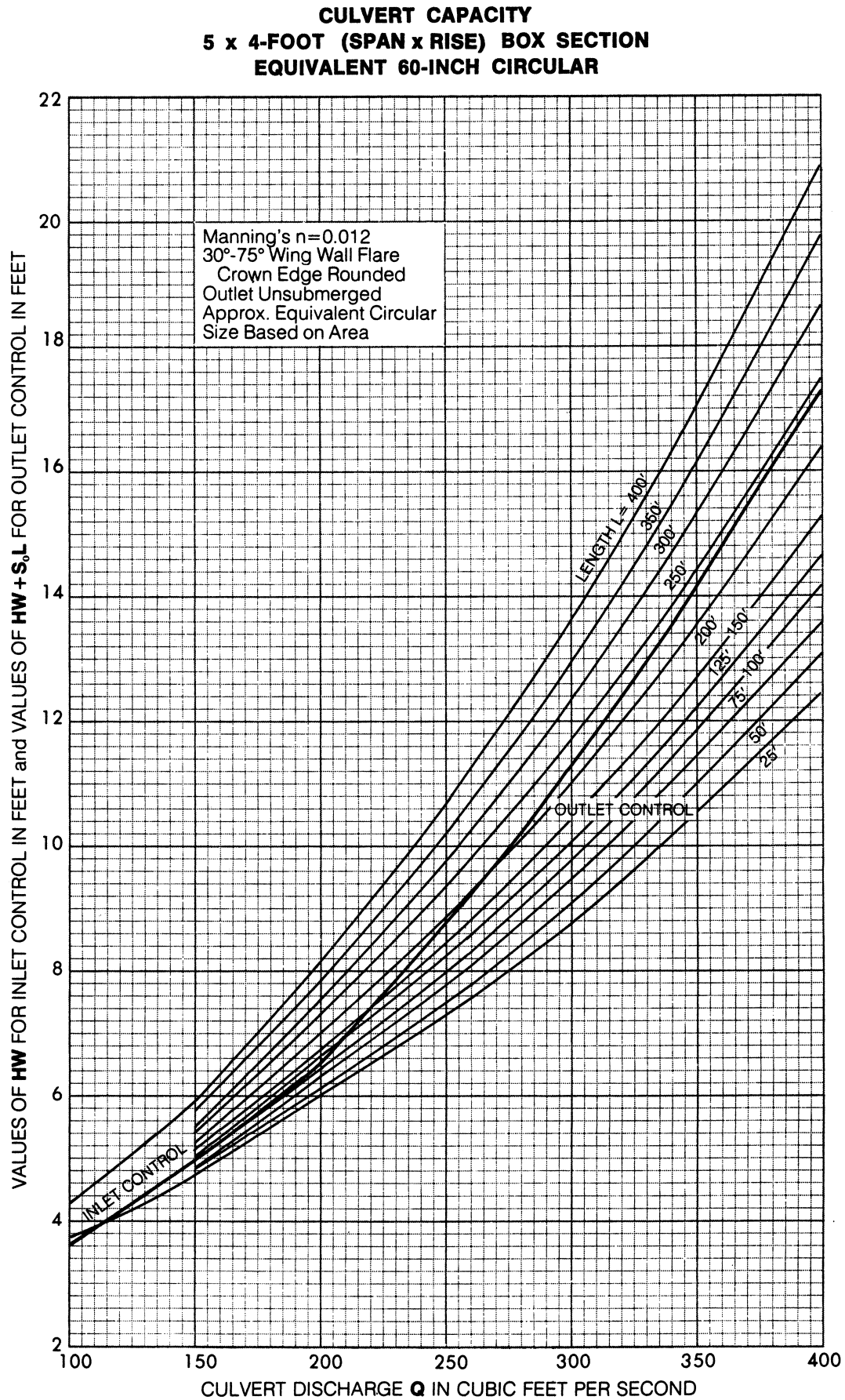


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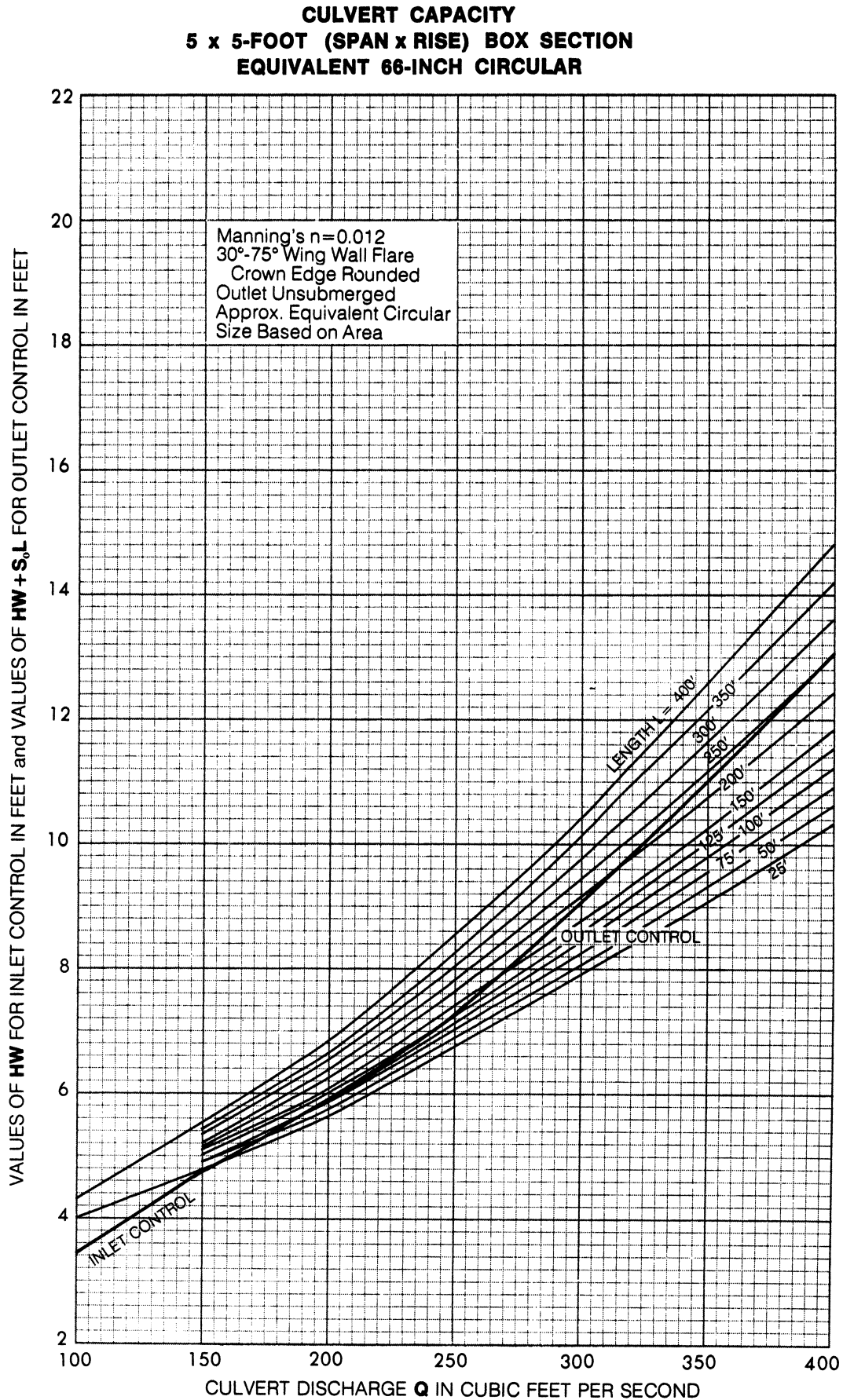


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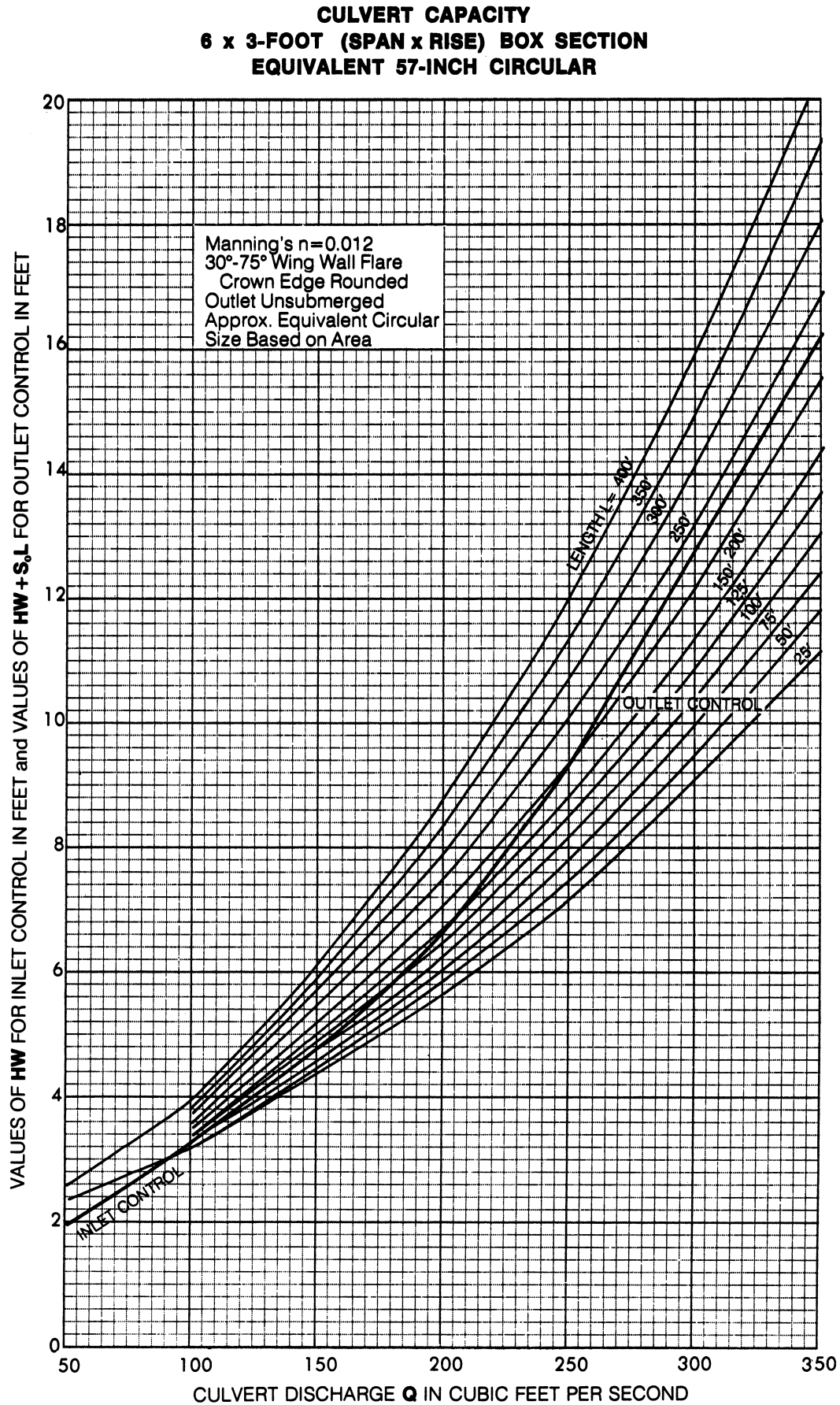


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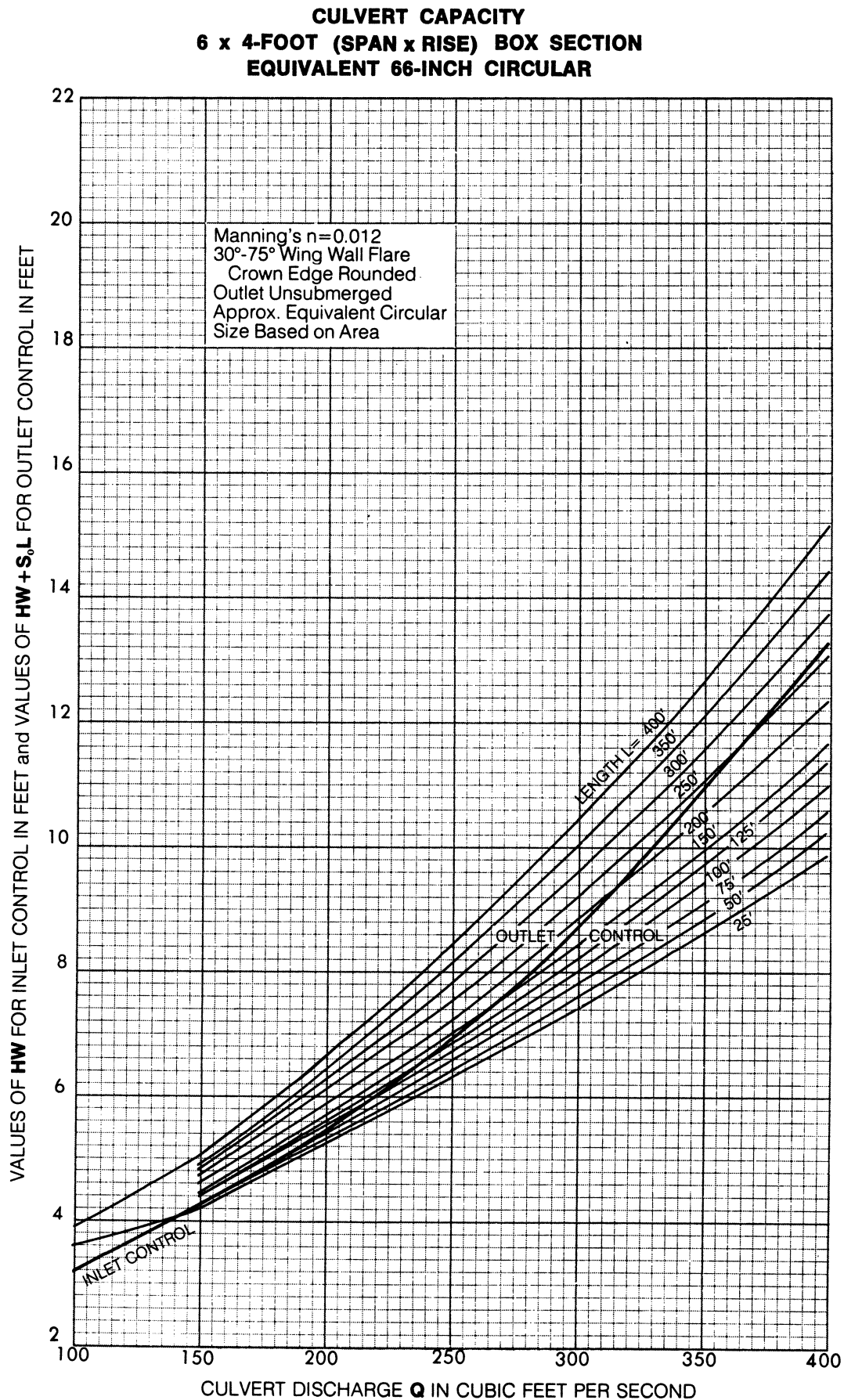


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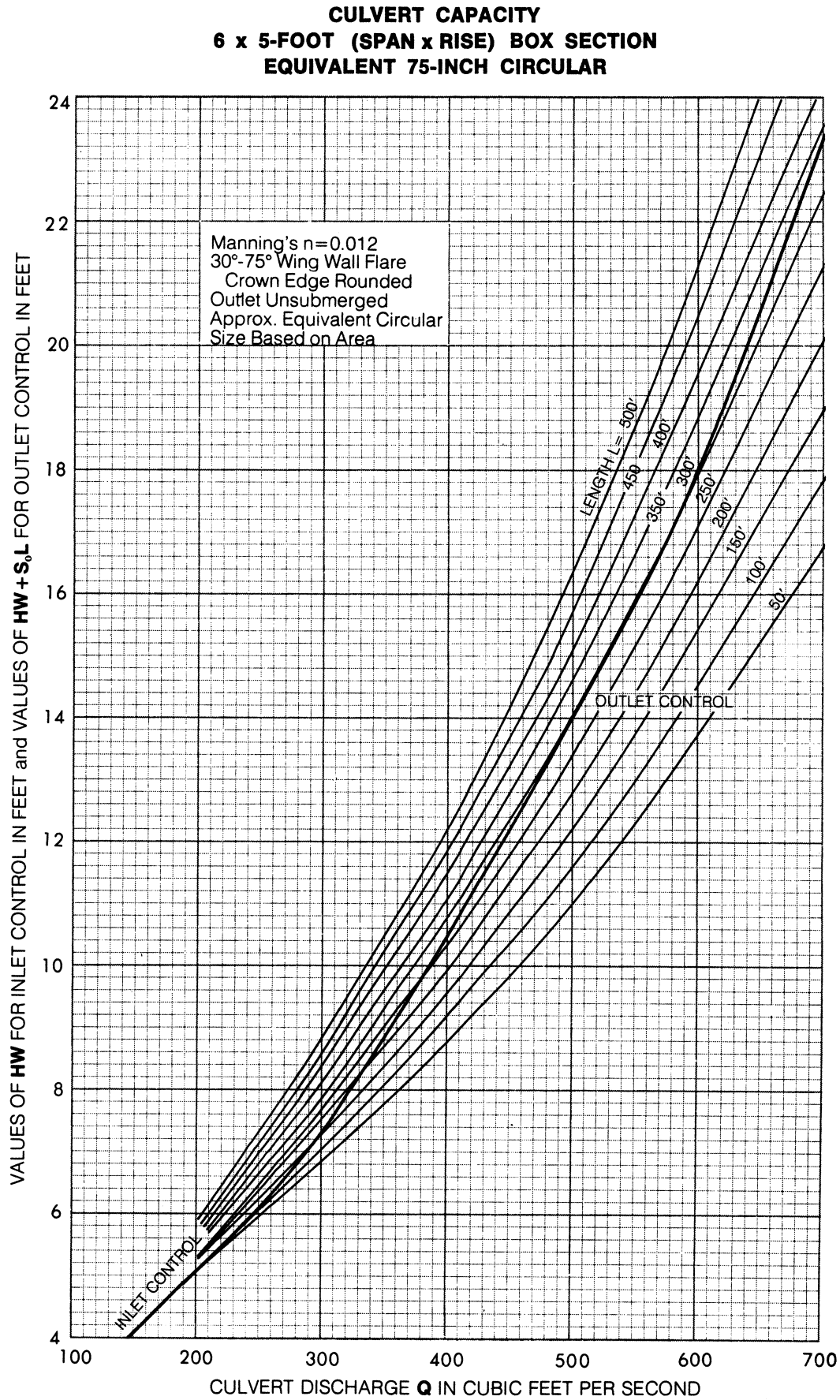


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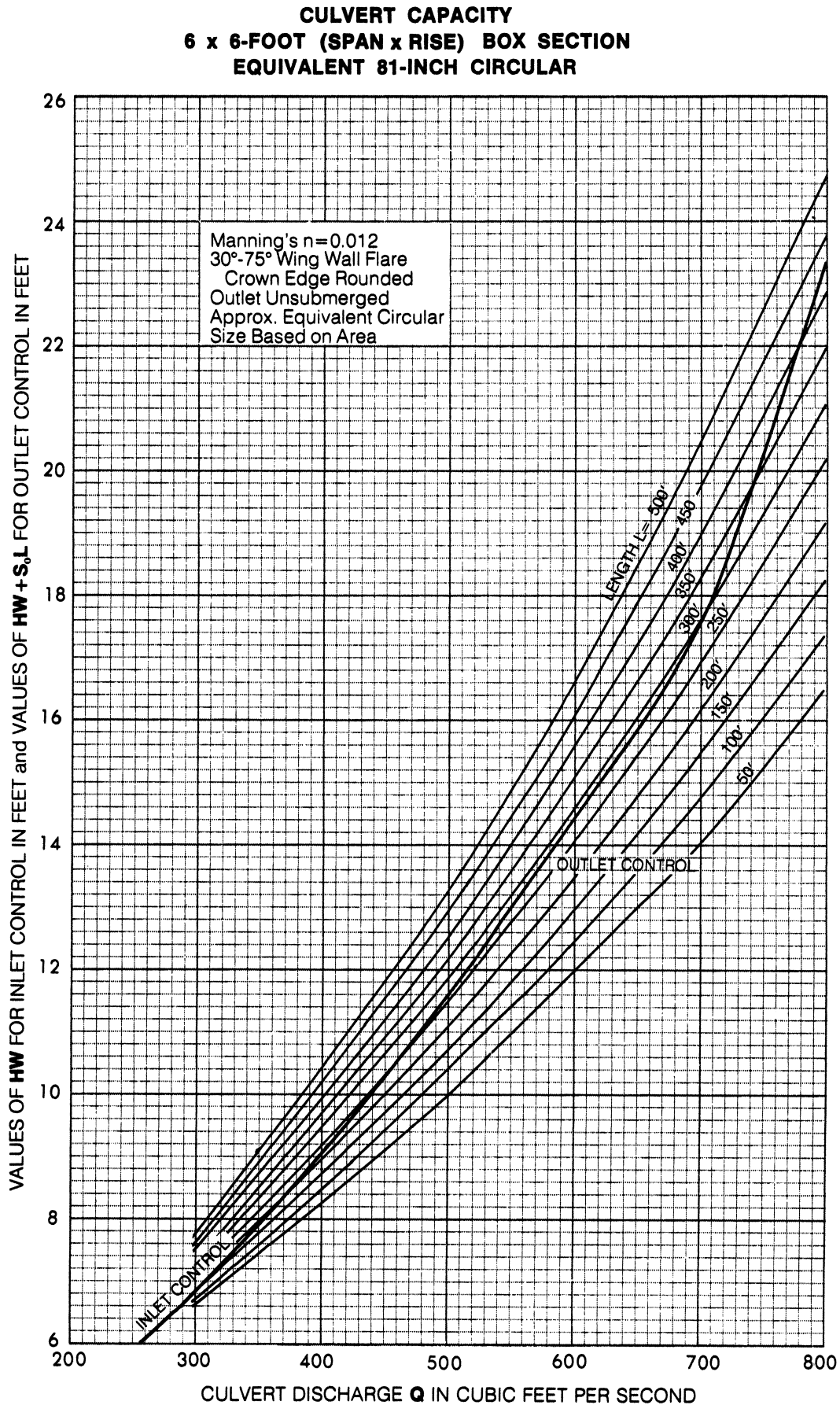


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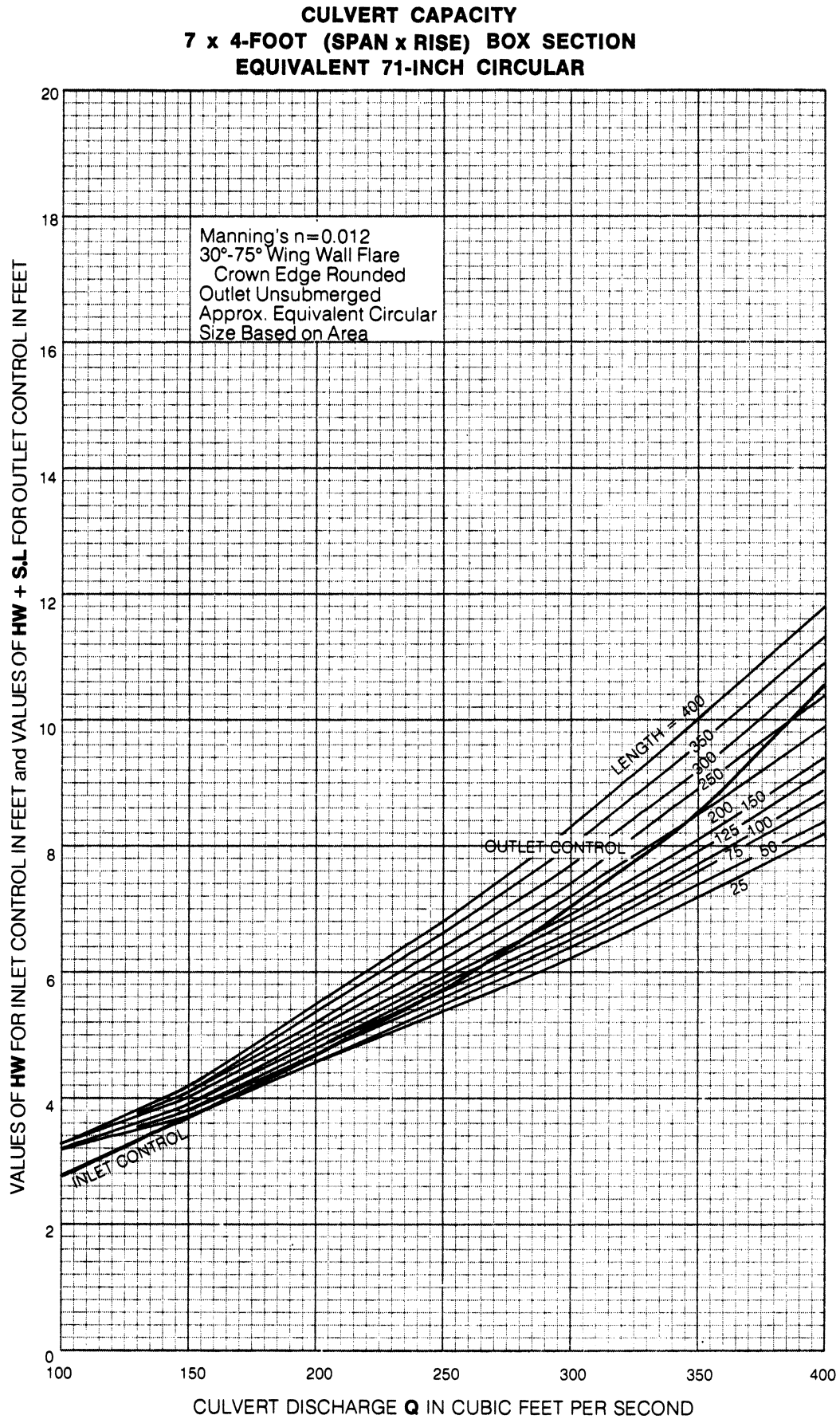


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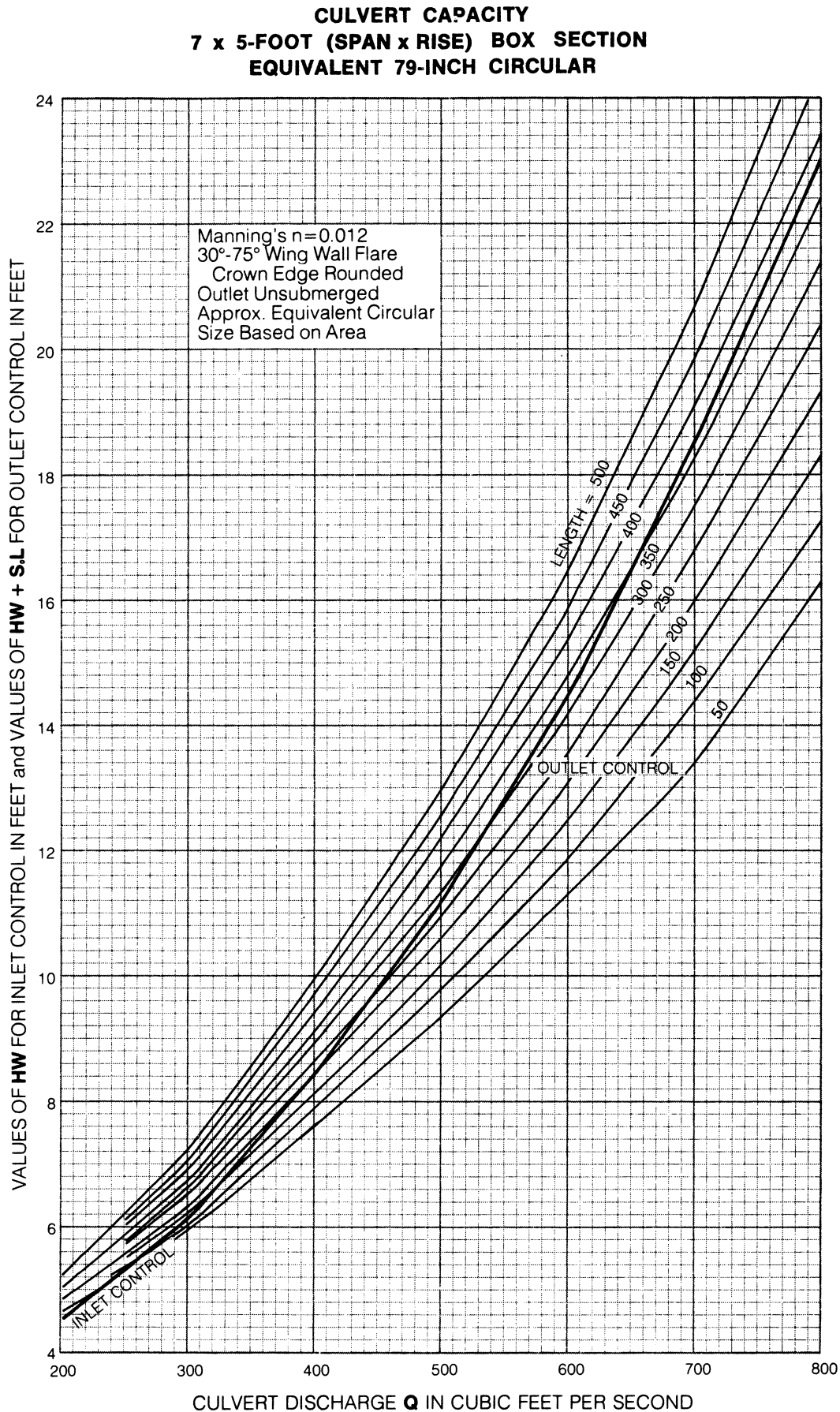


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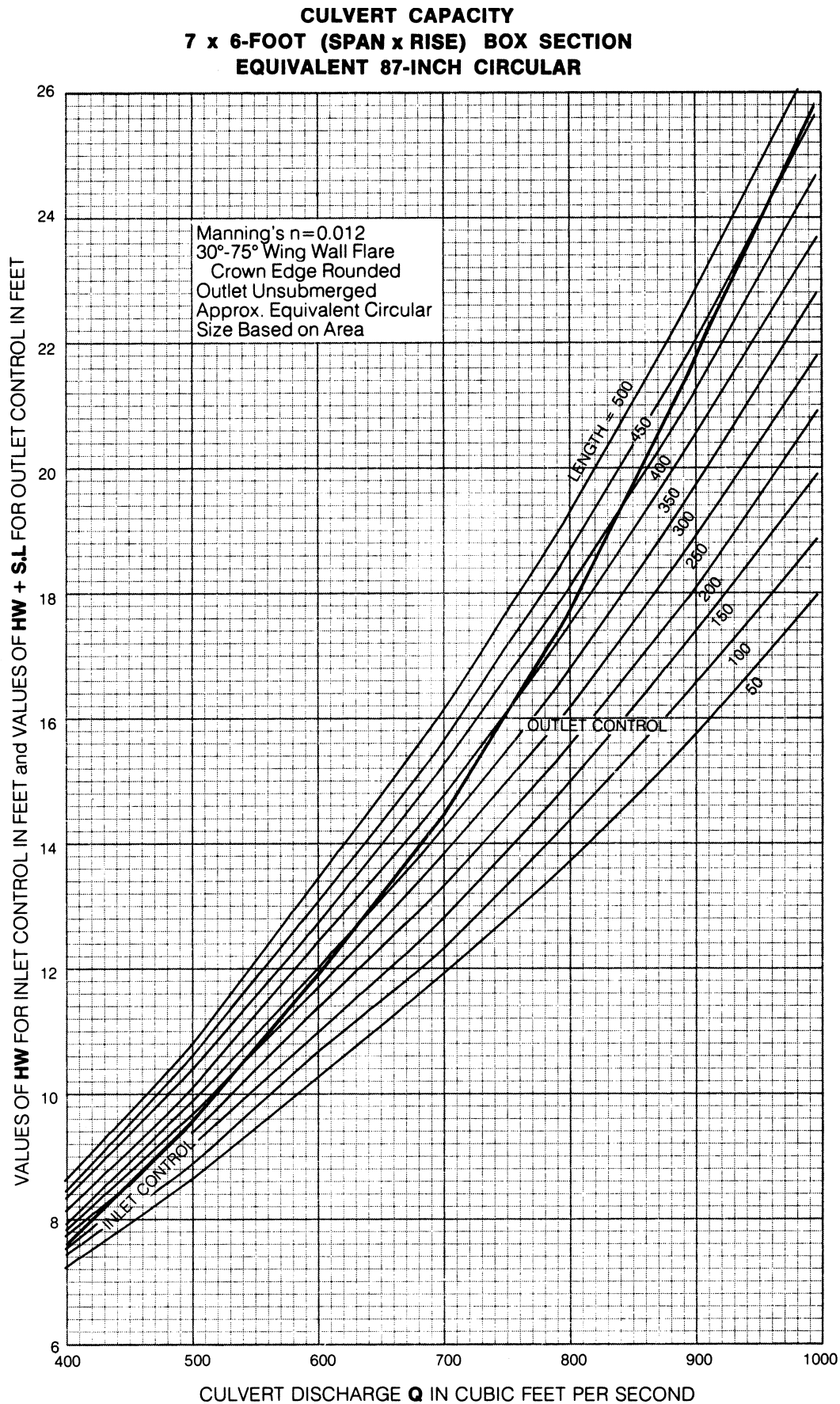


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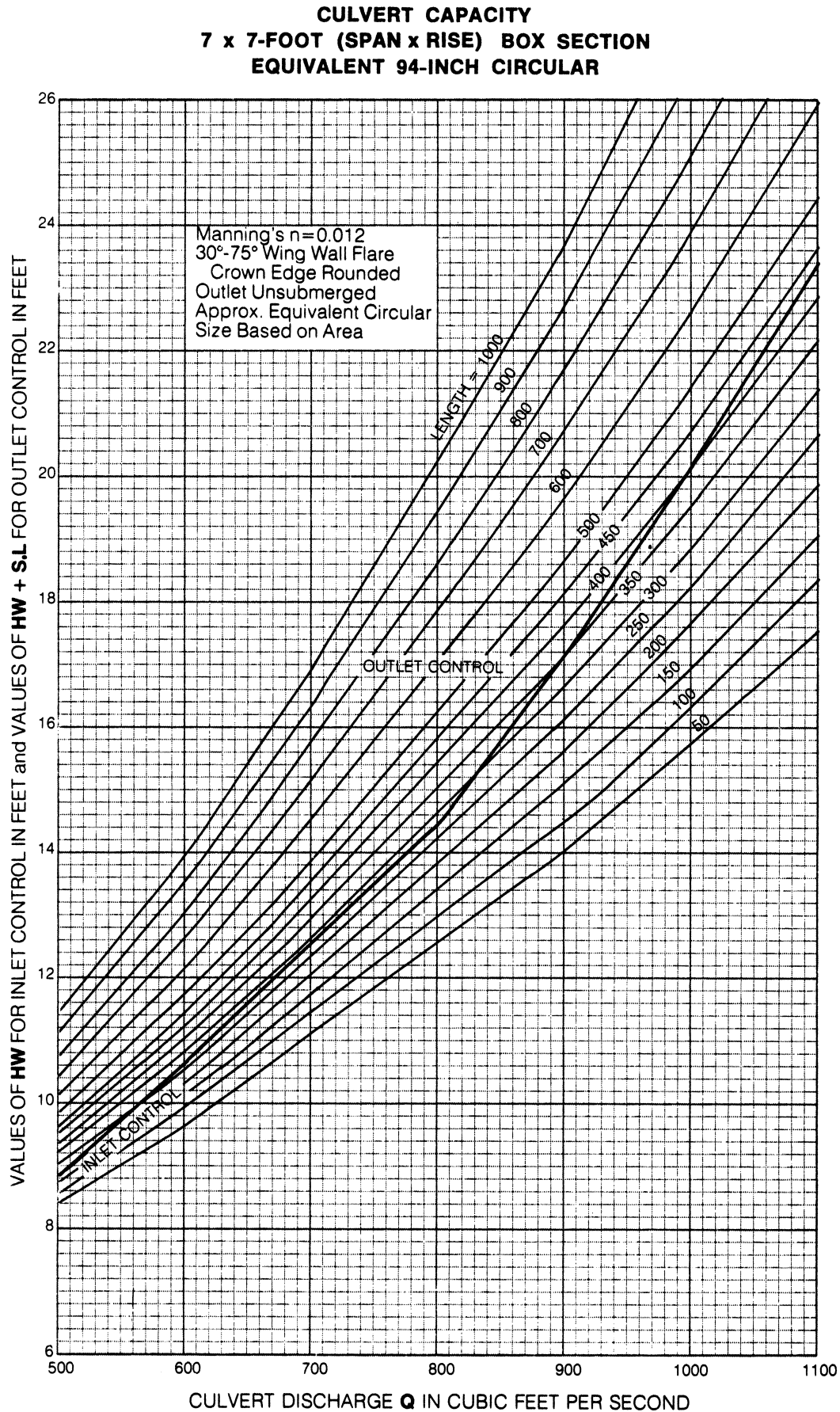


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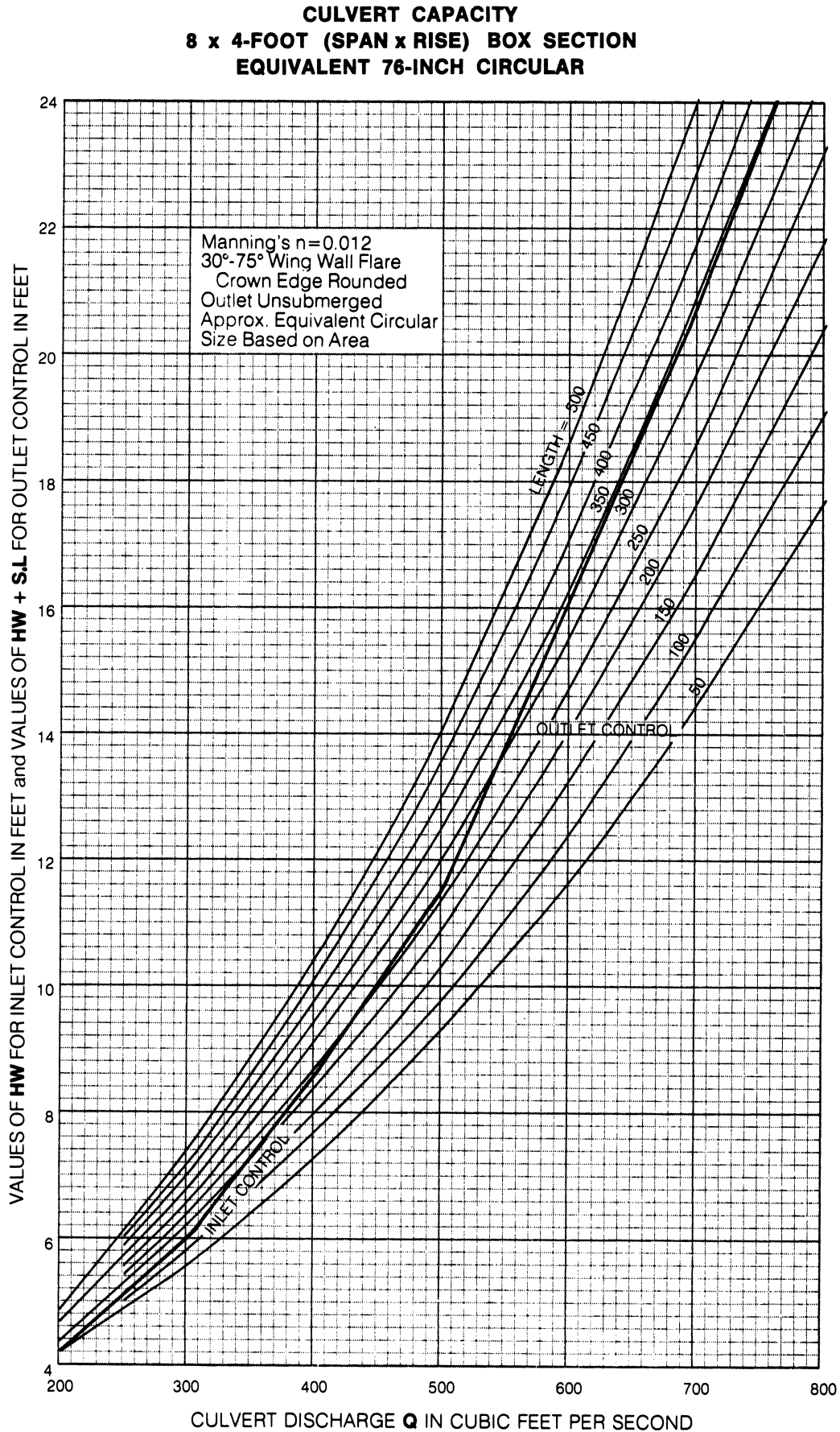


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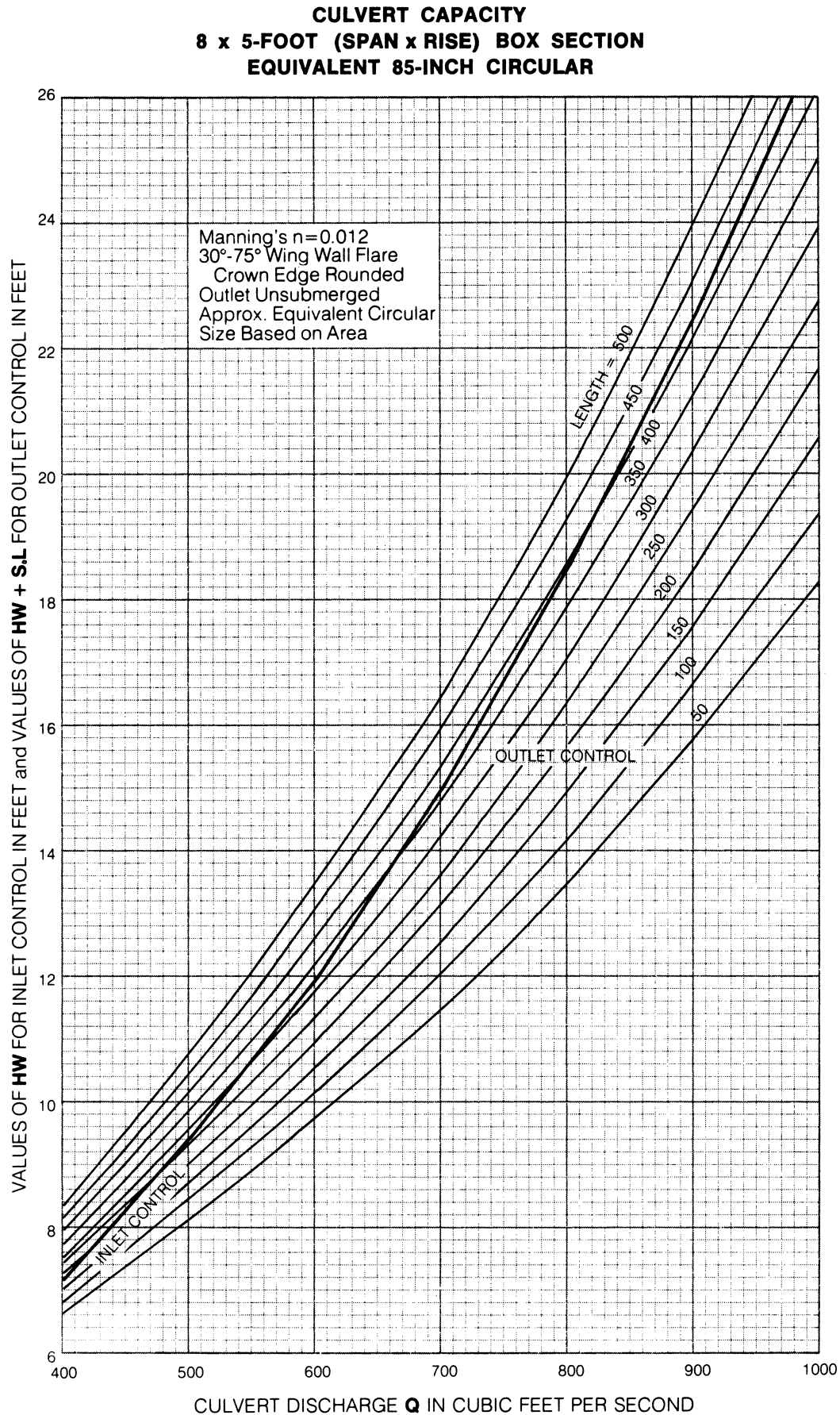


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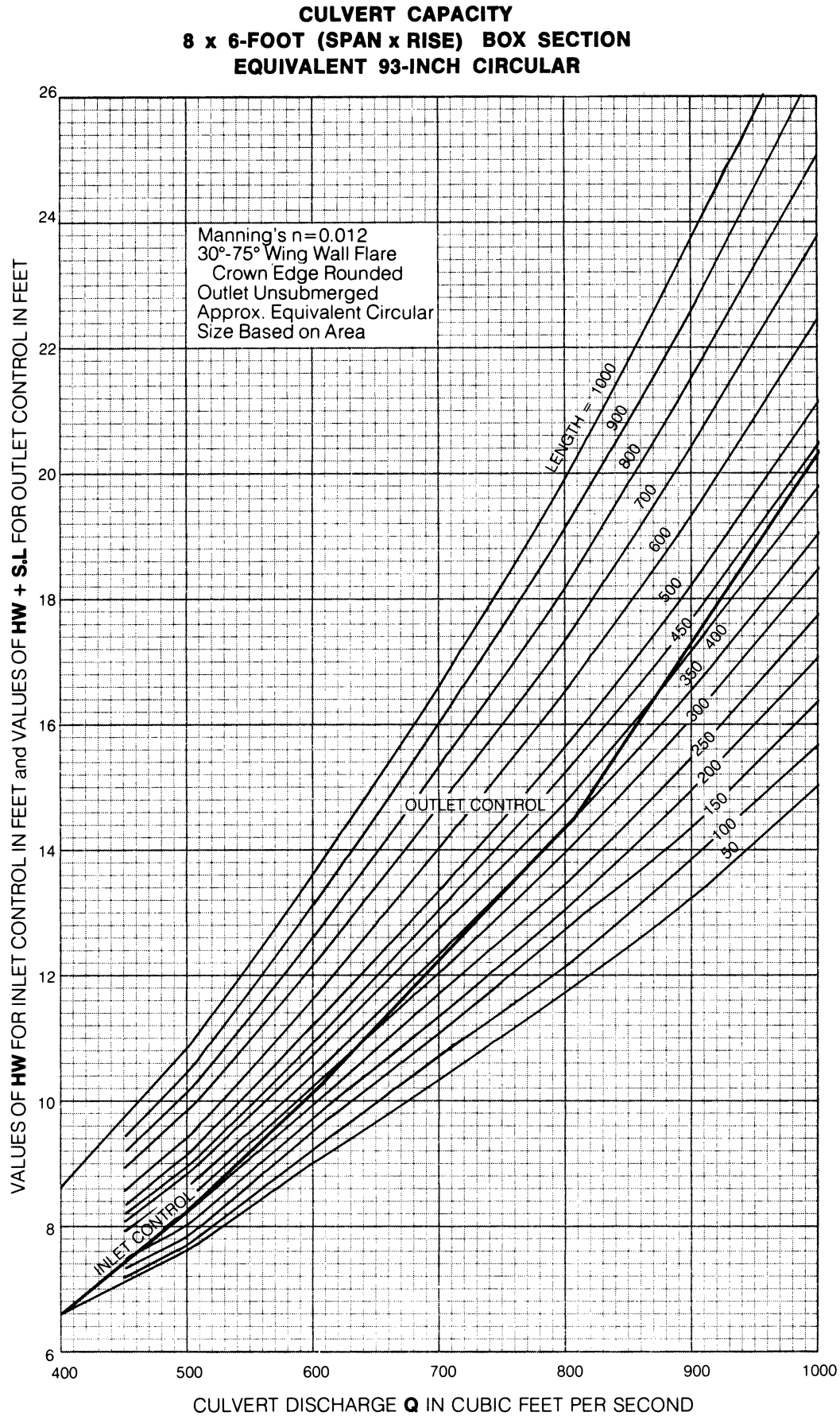


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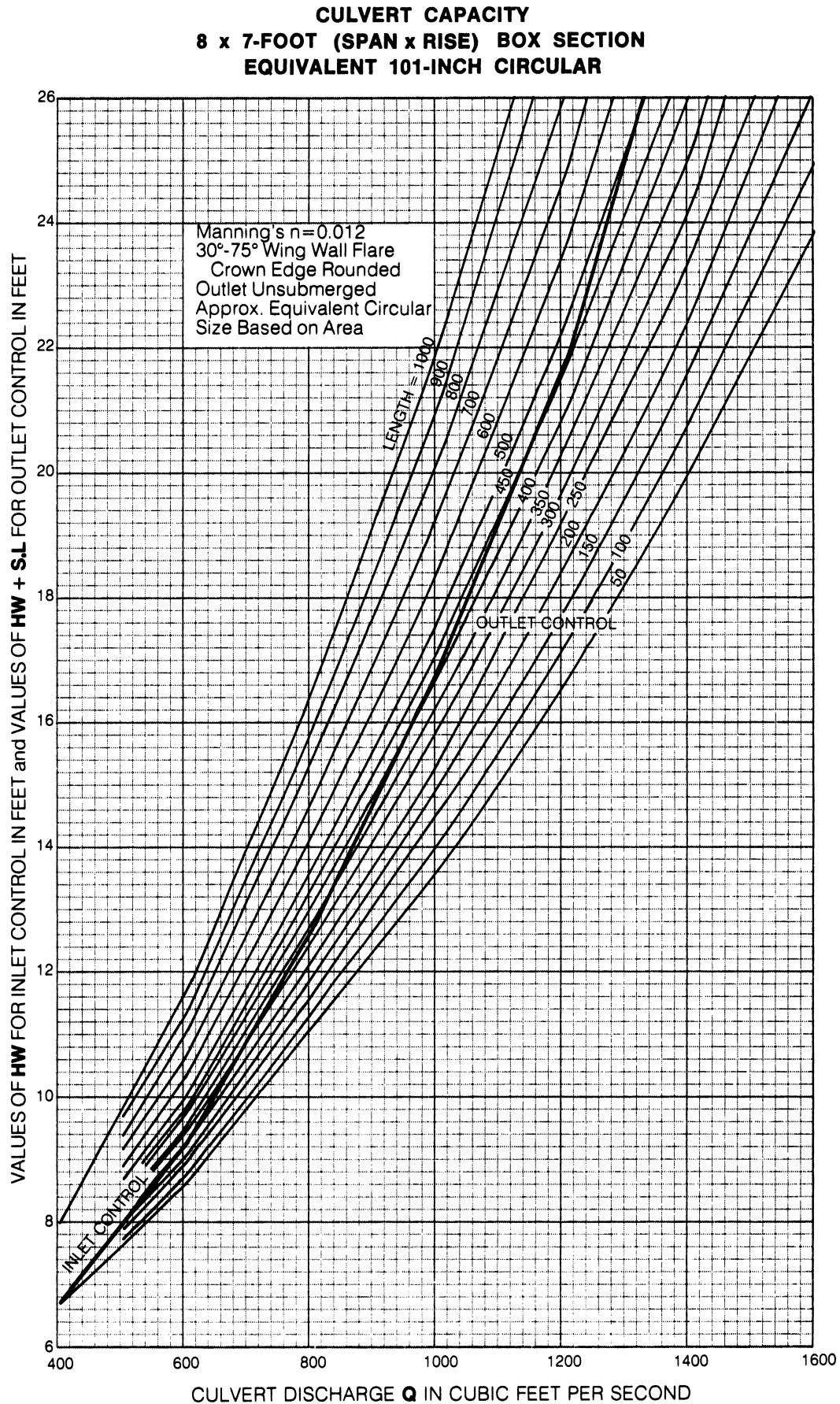


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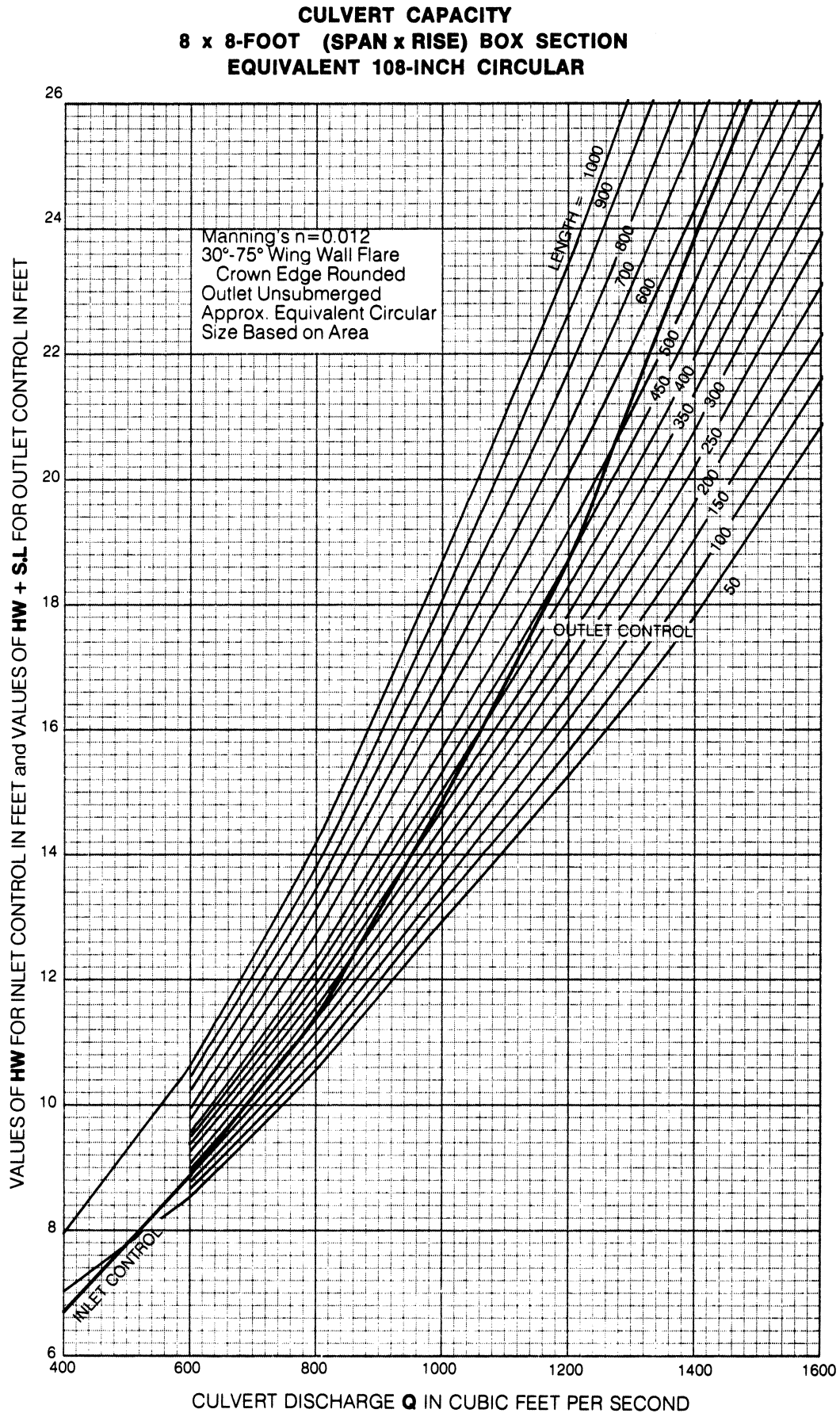


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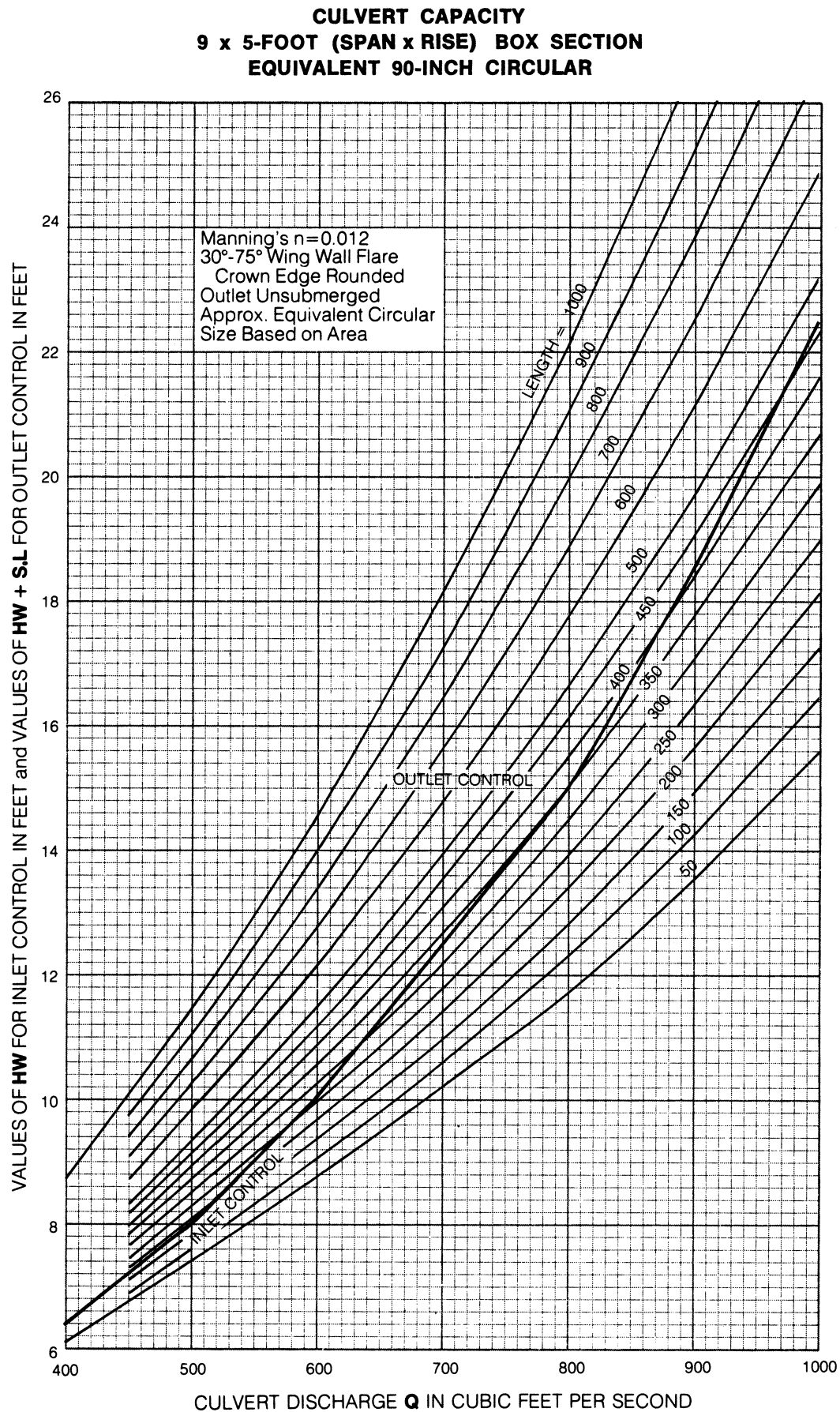


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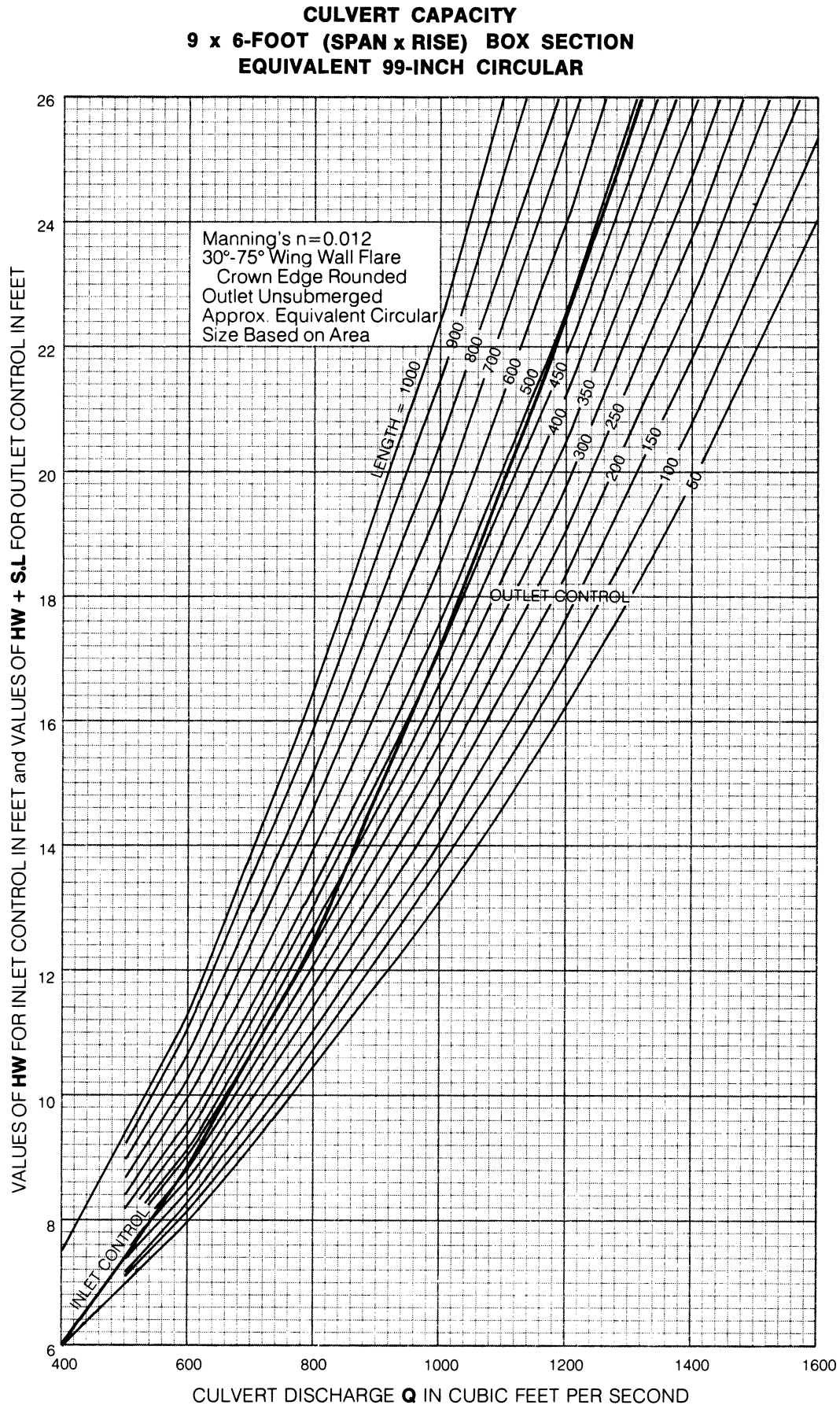


Figure 127

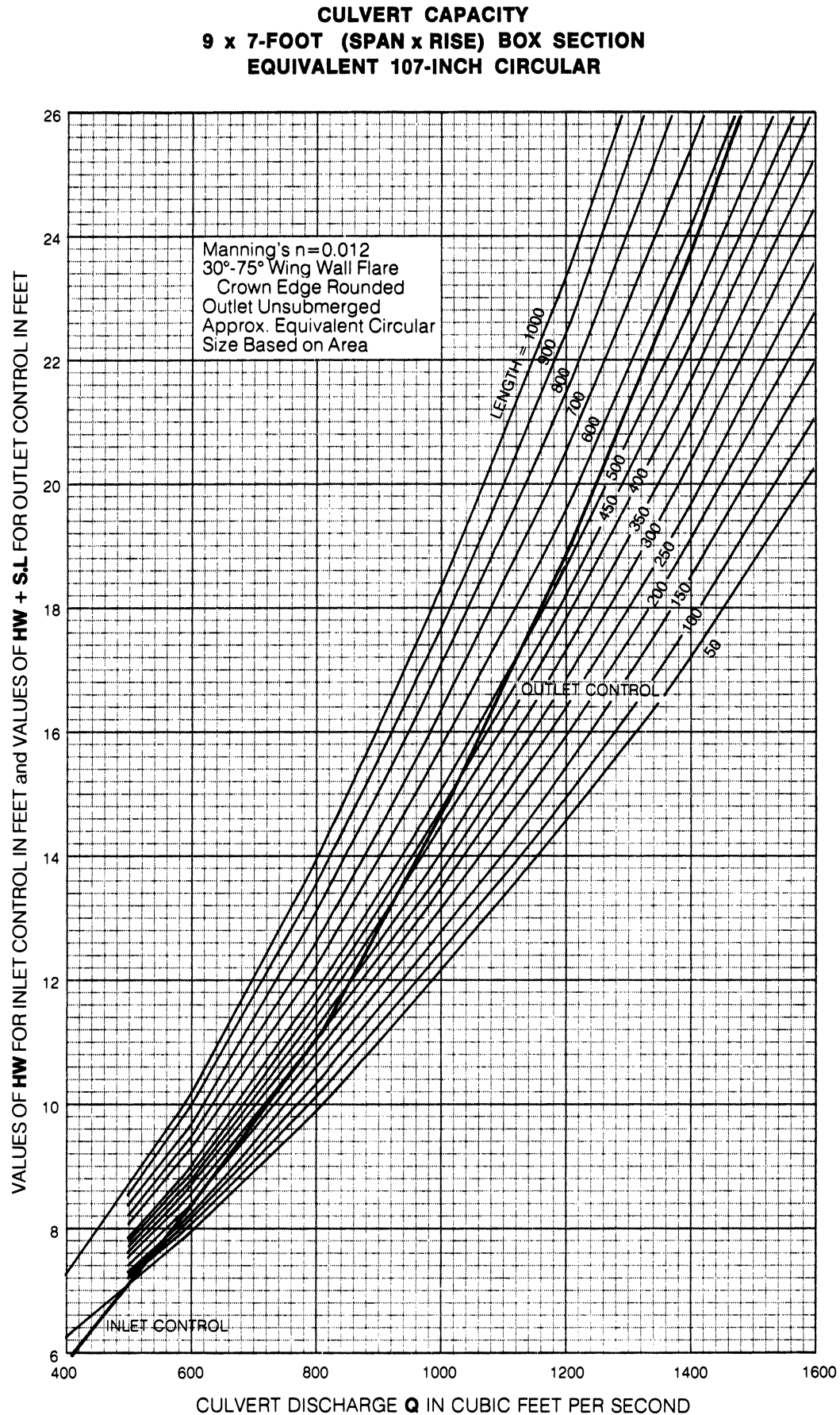


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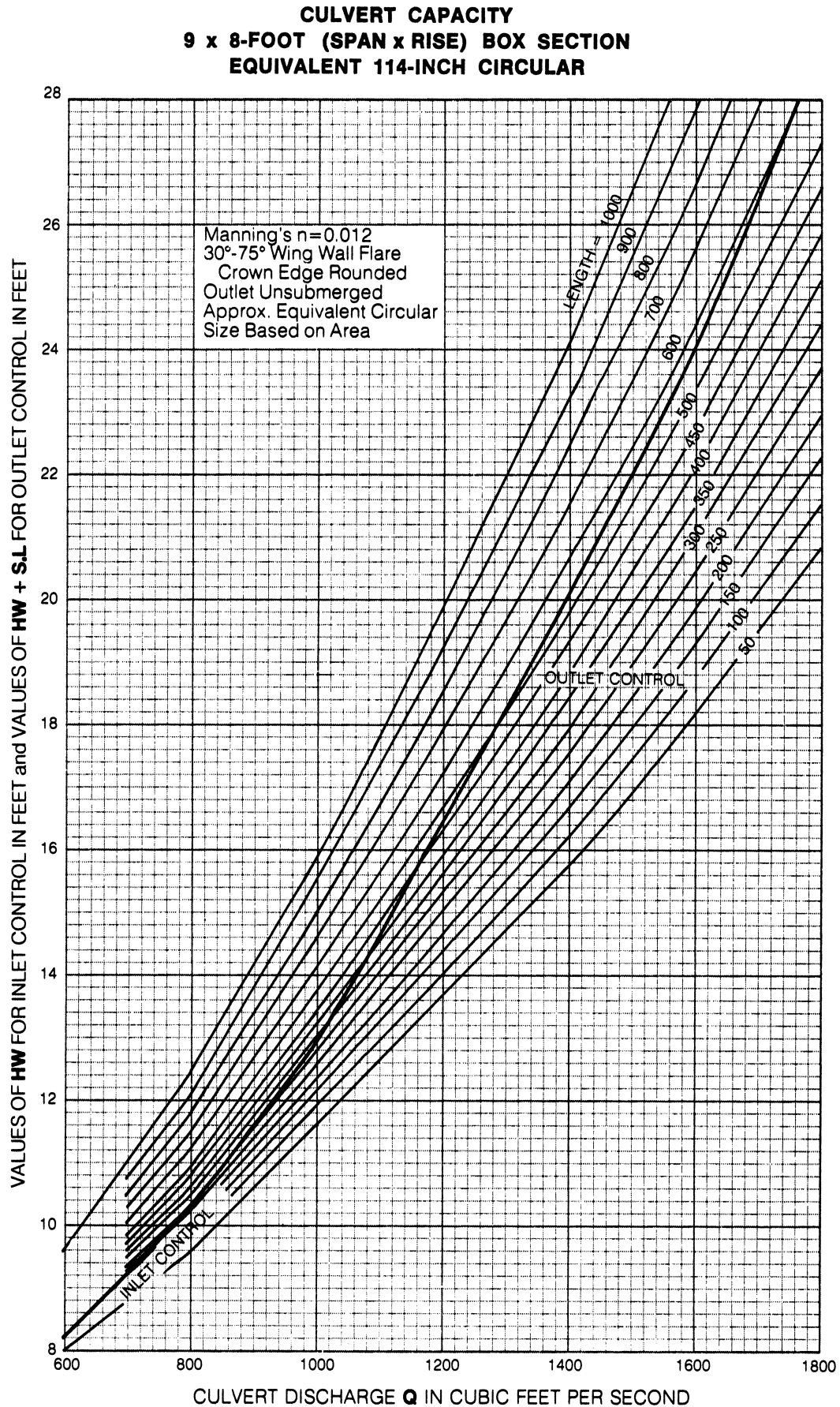


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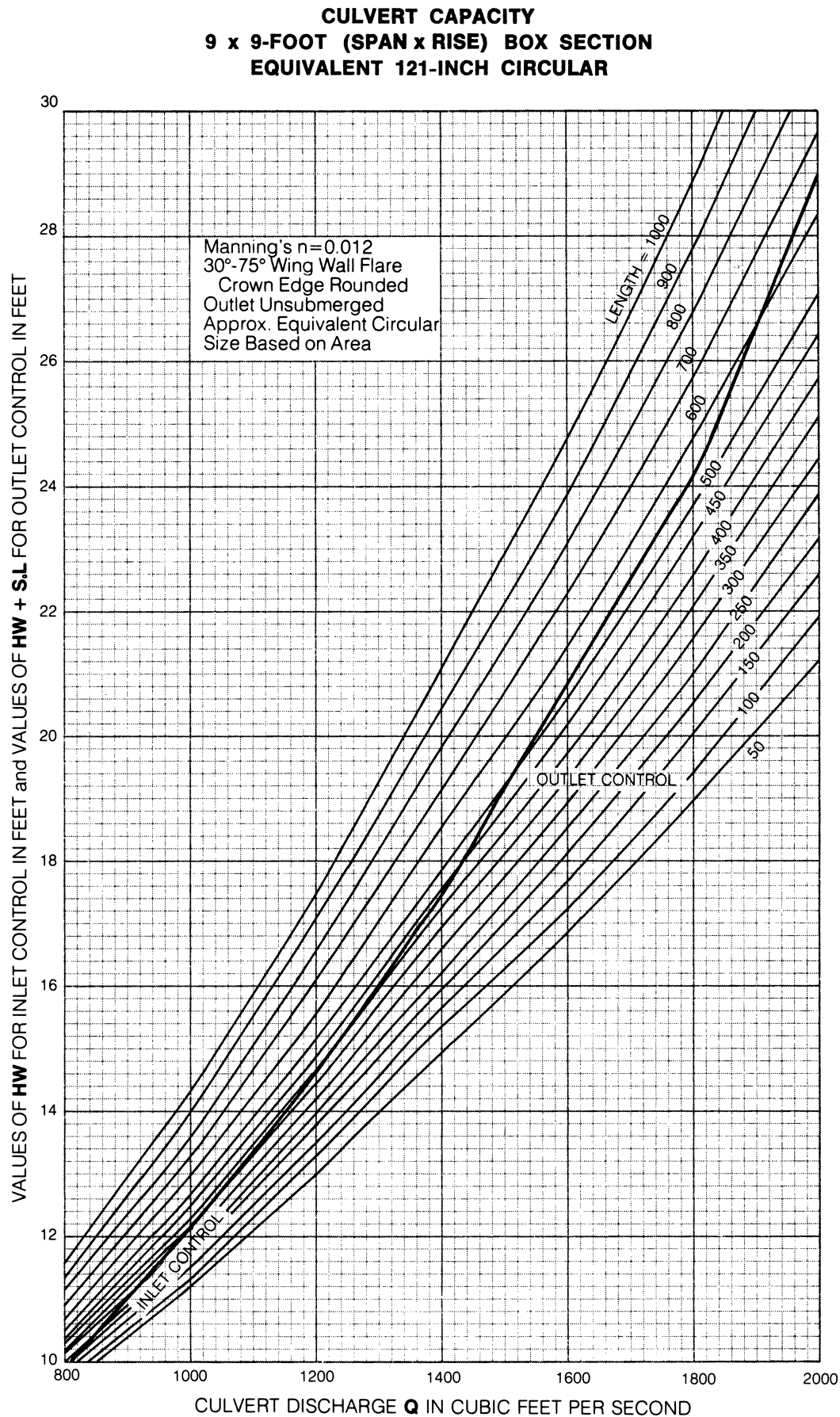


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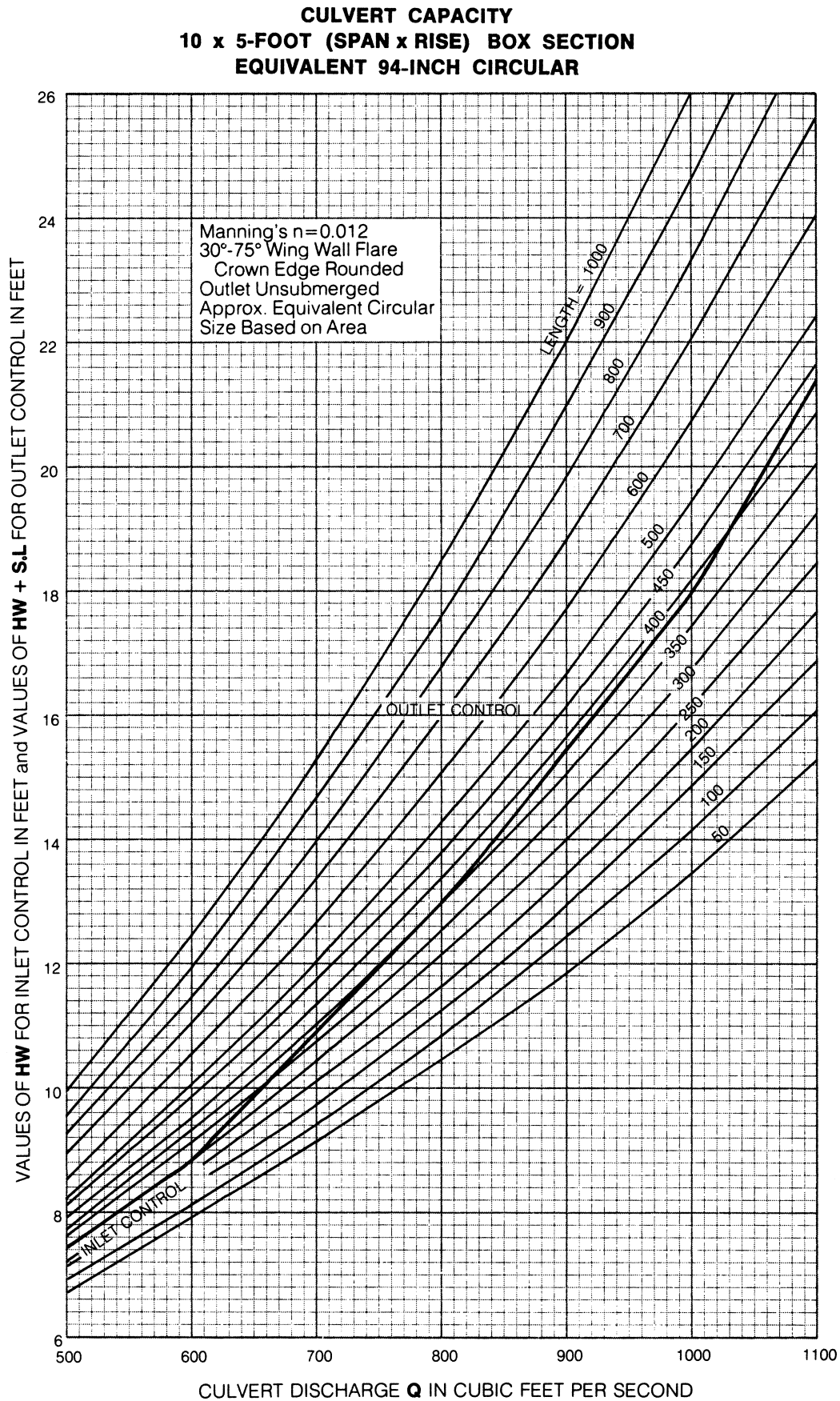


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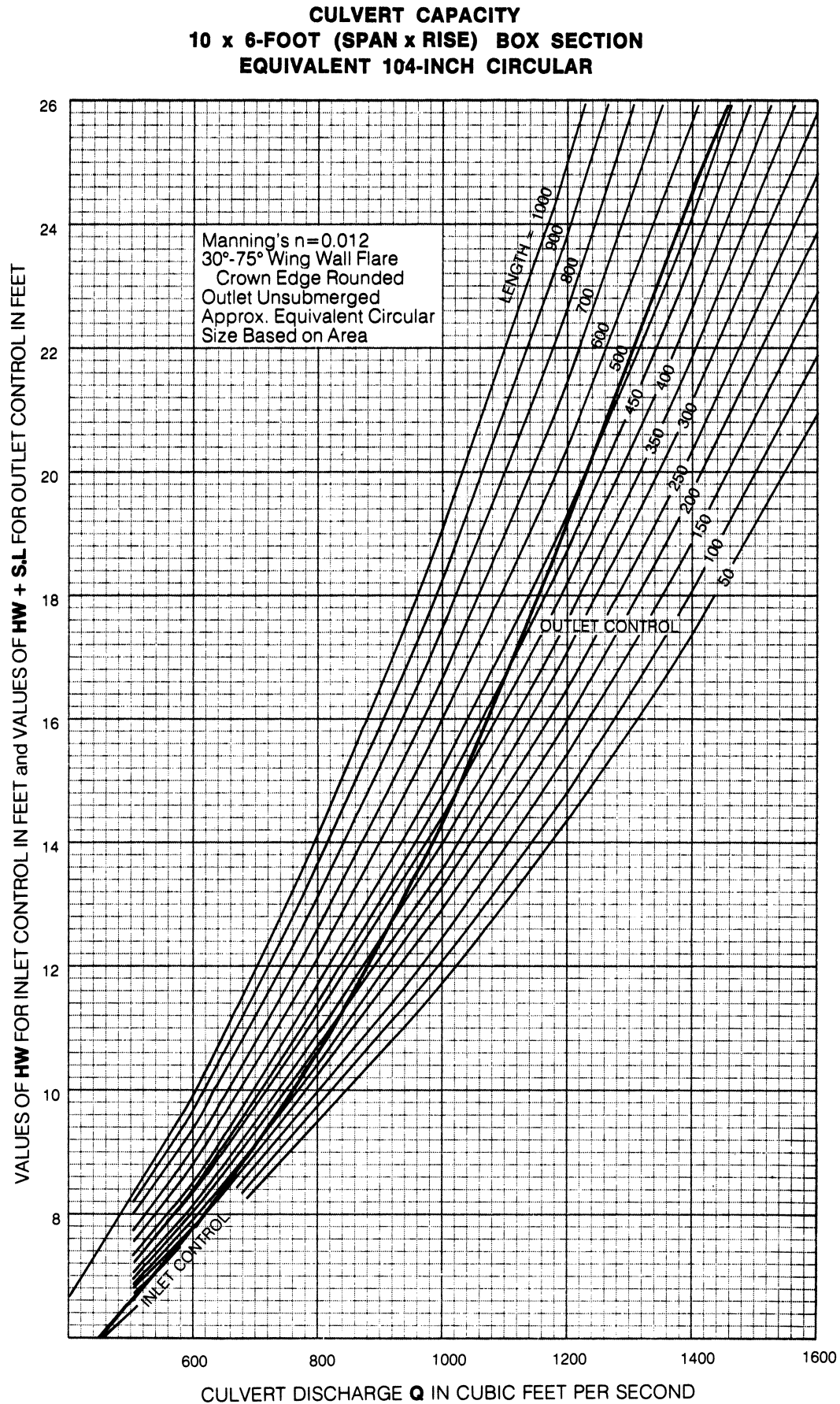


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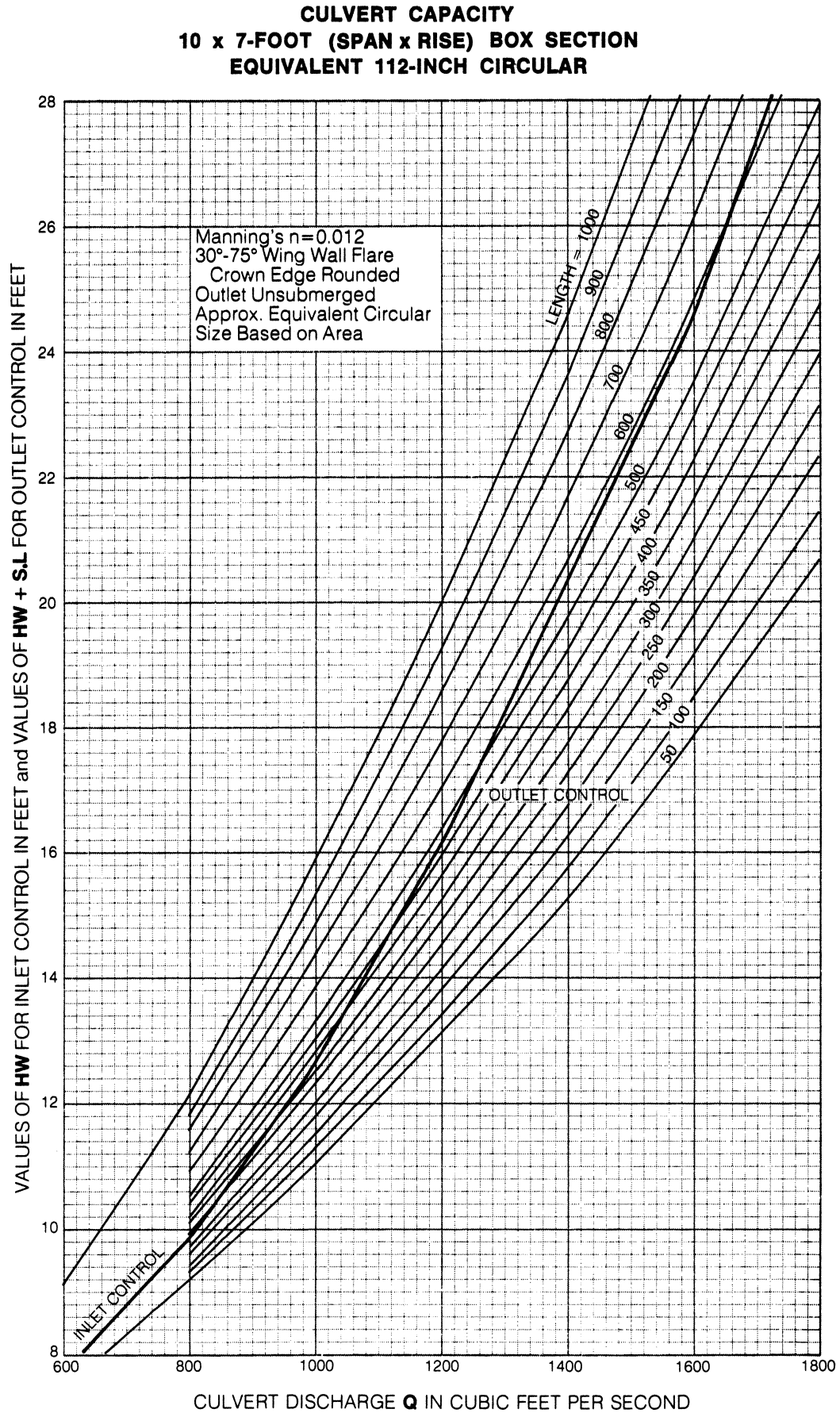


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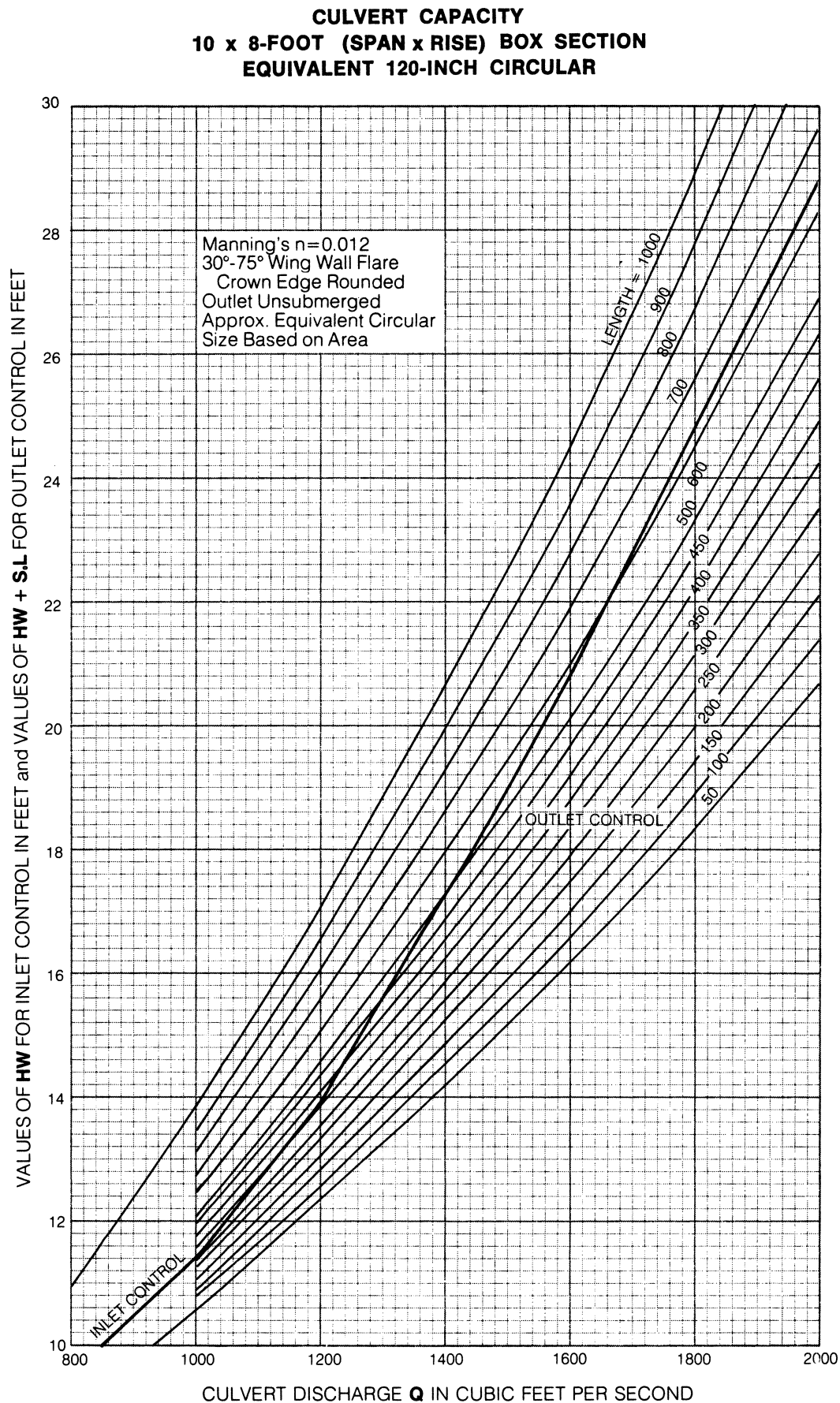


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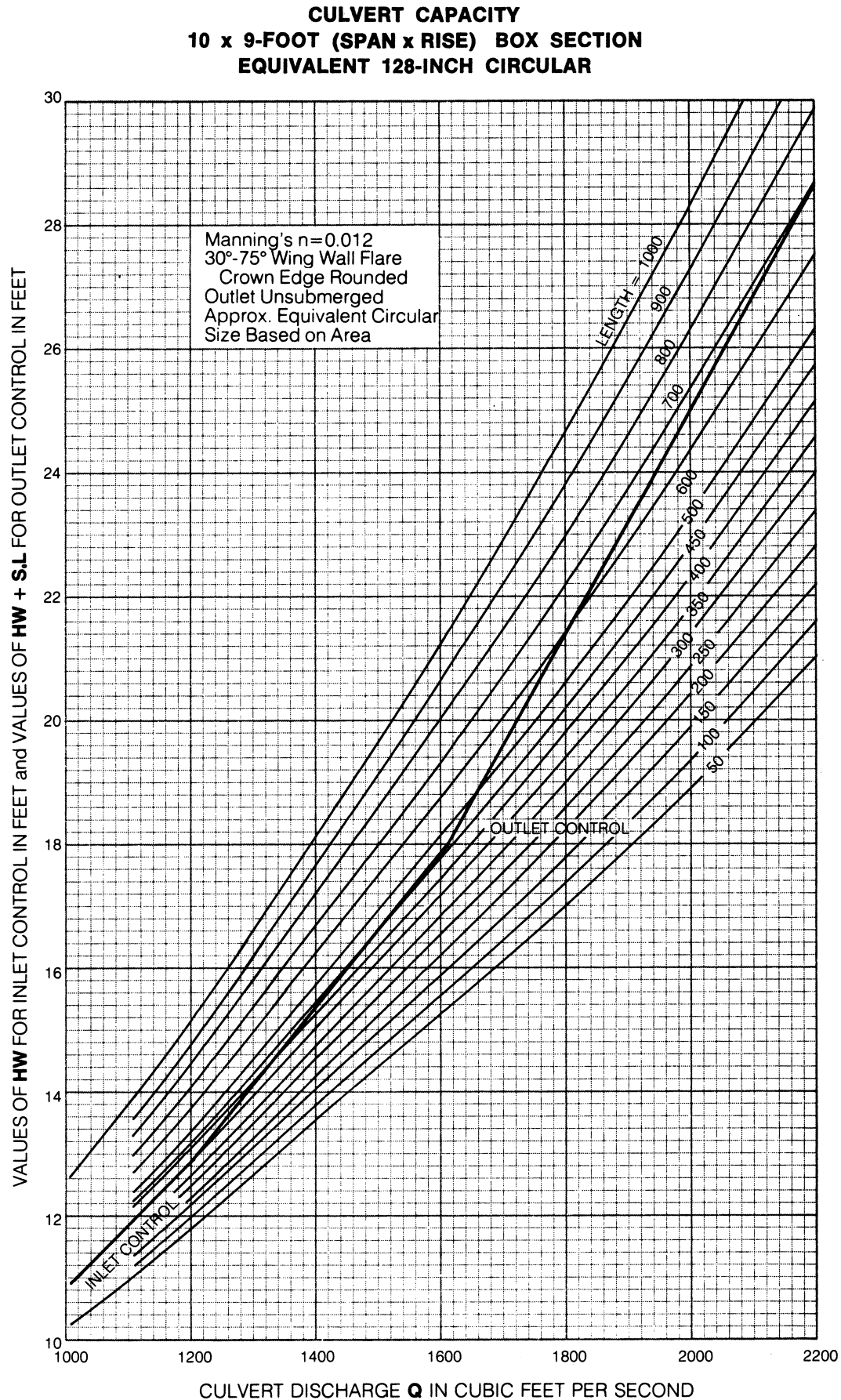


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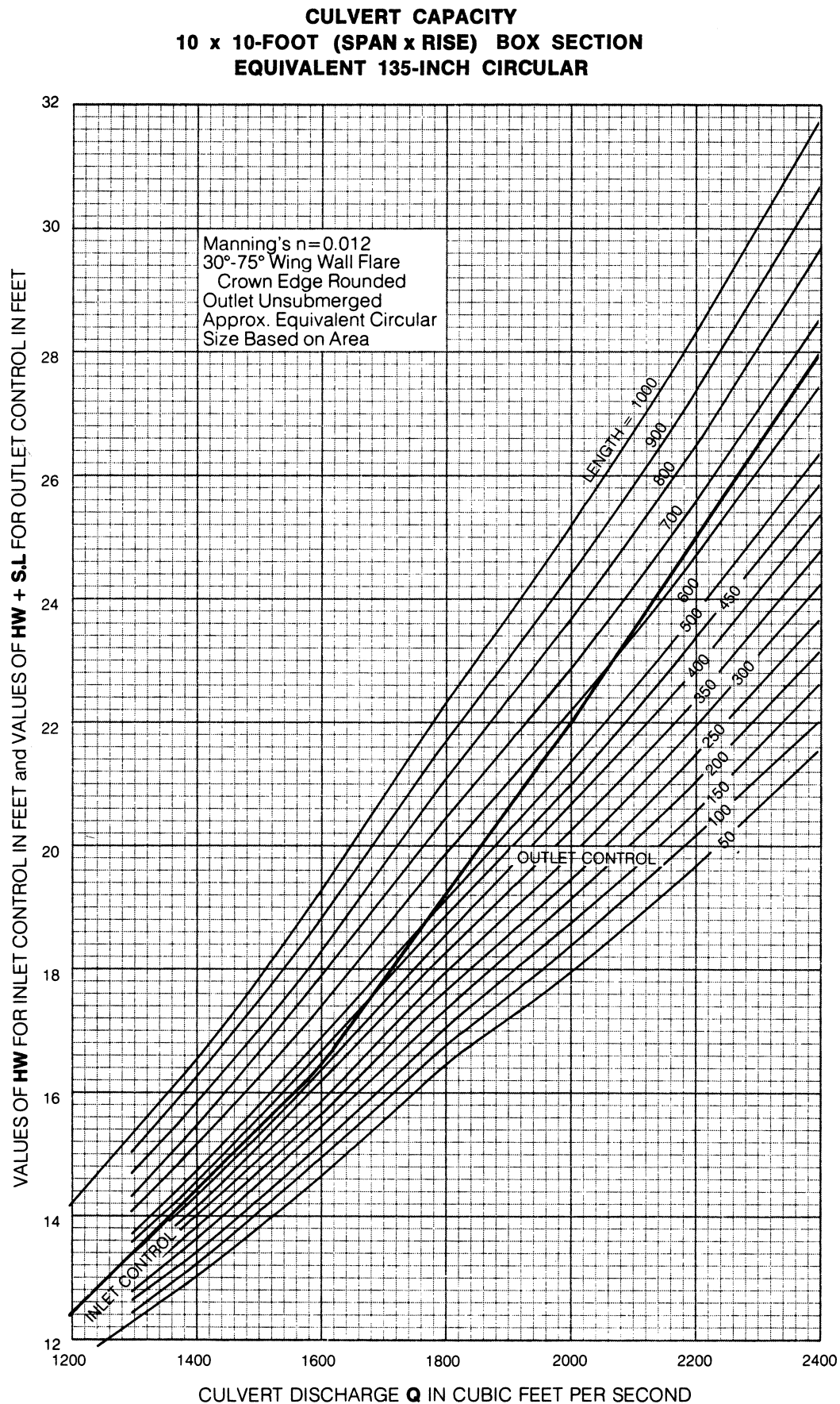


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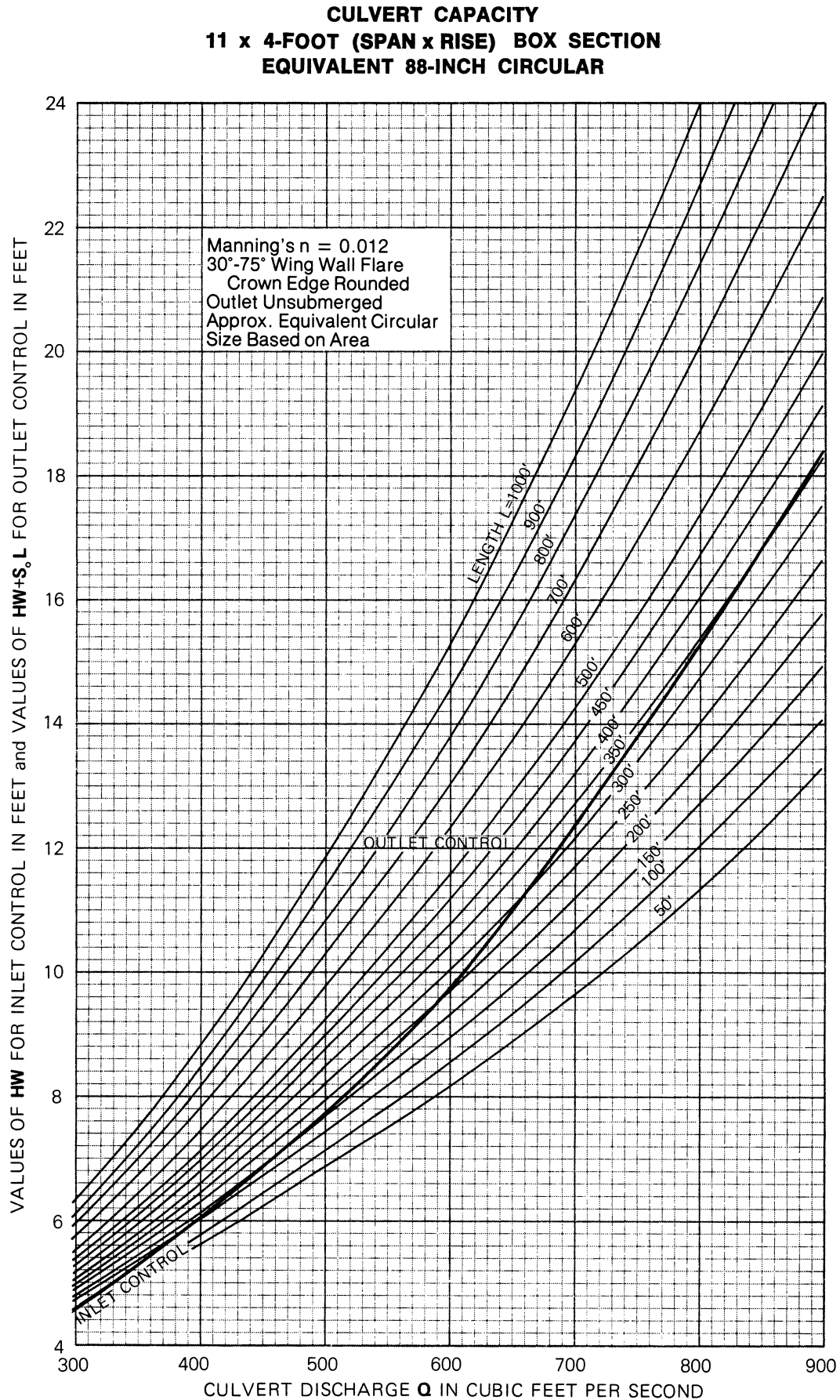


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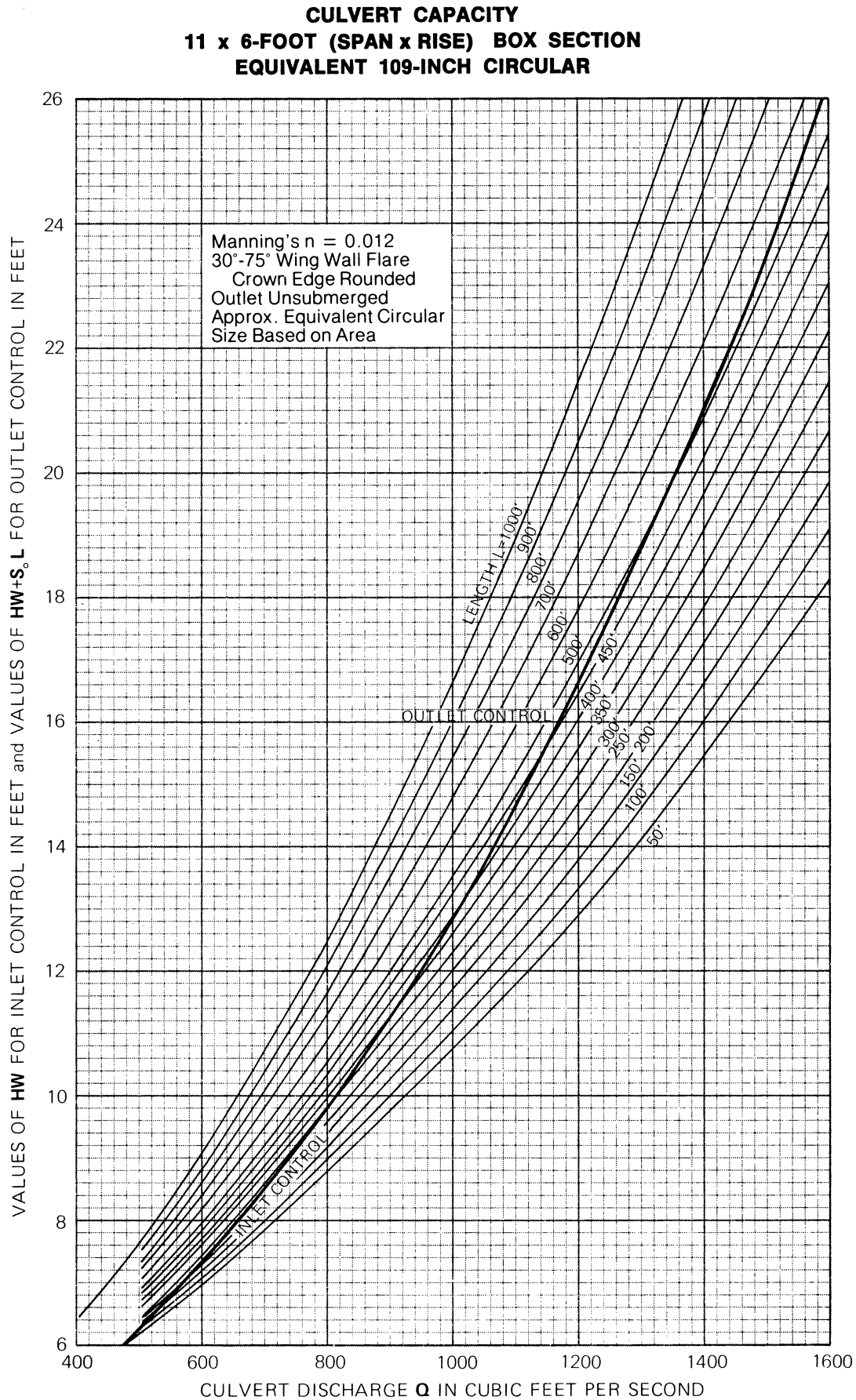


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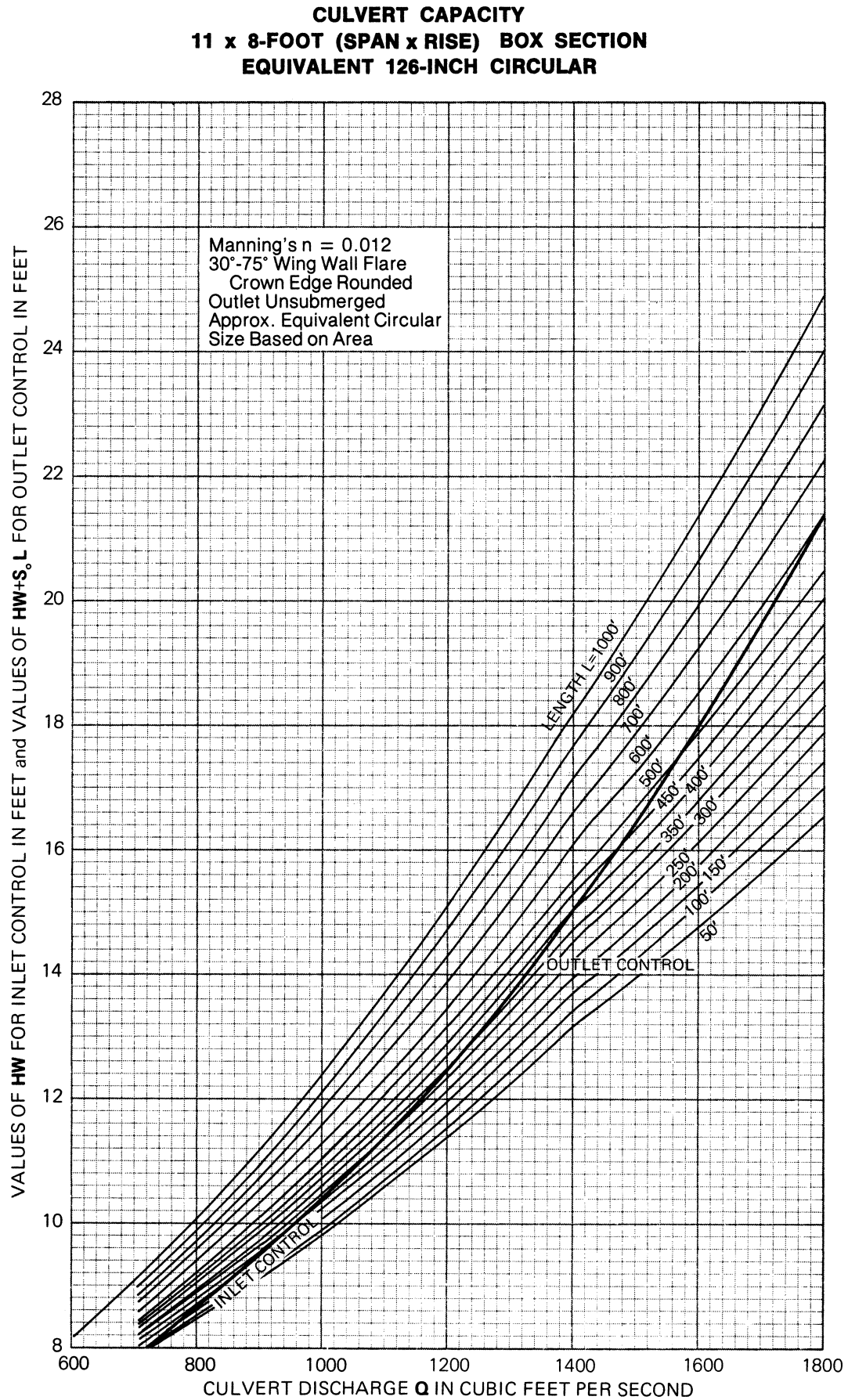


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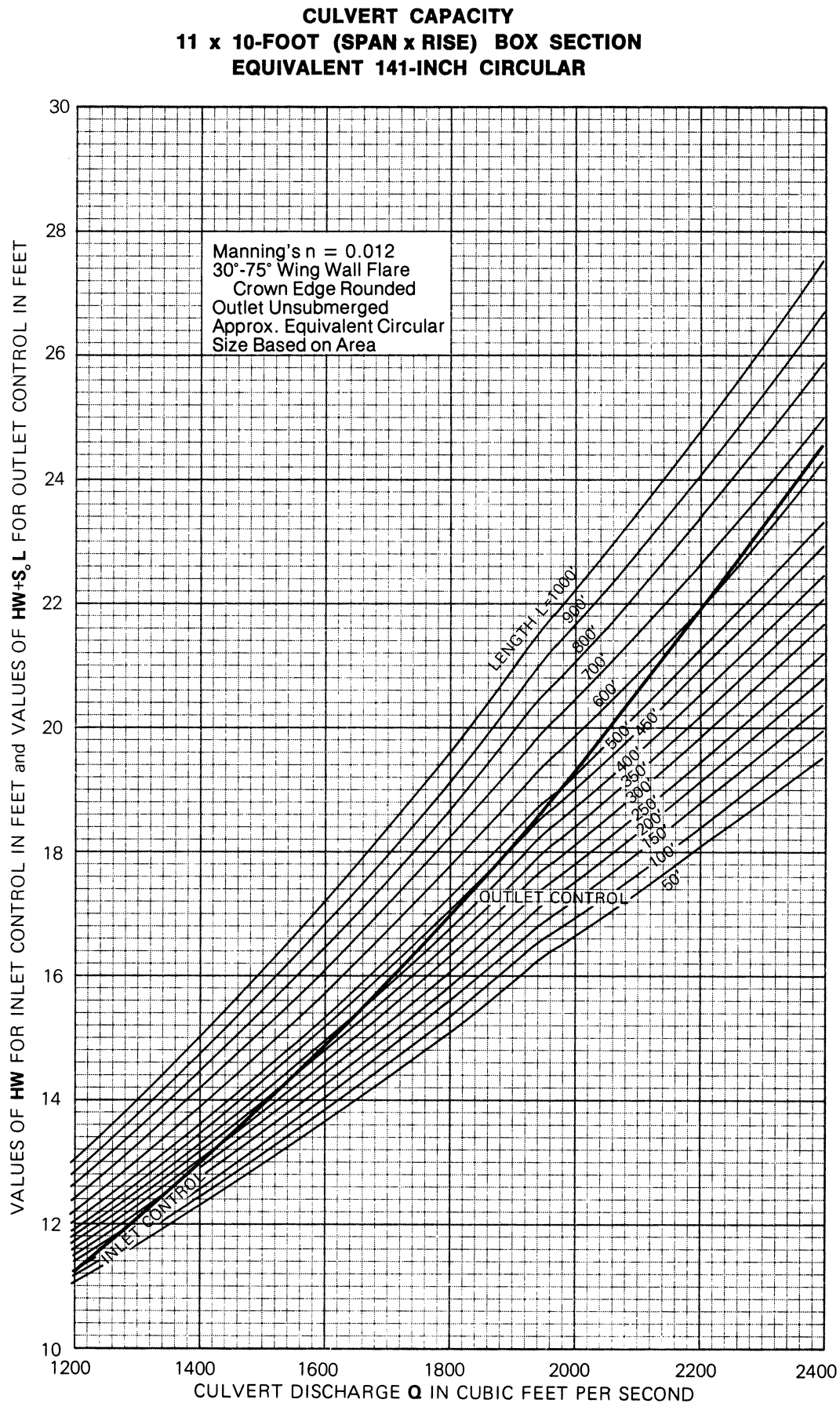


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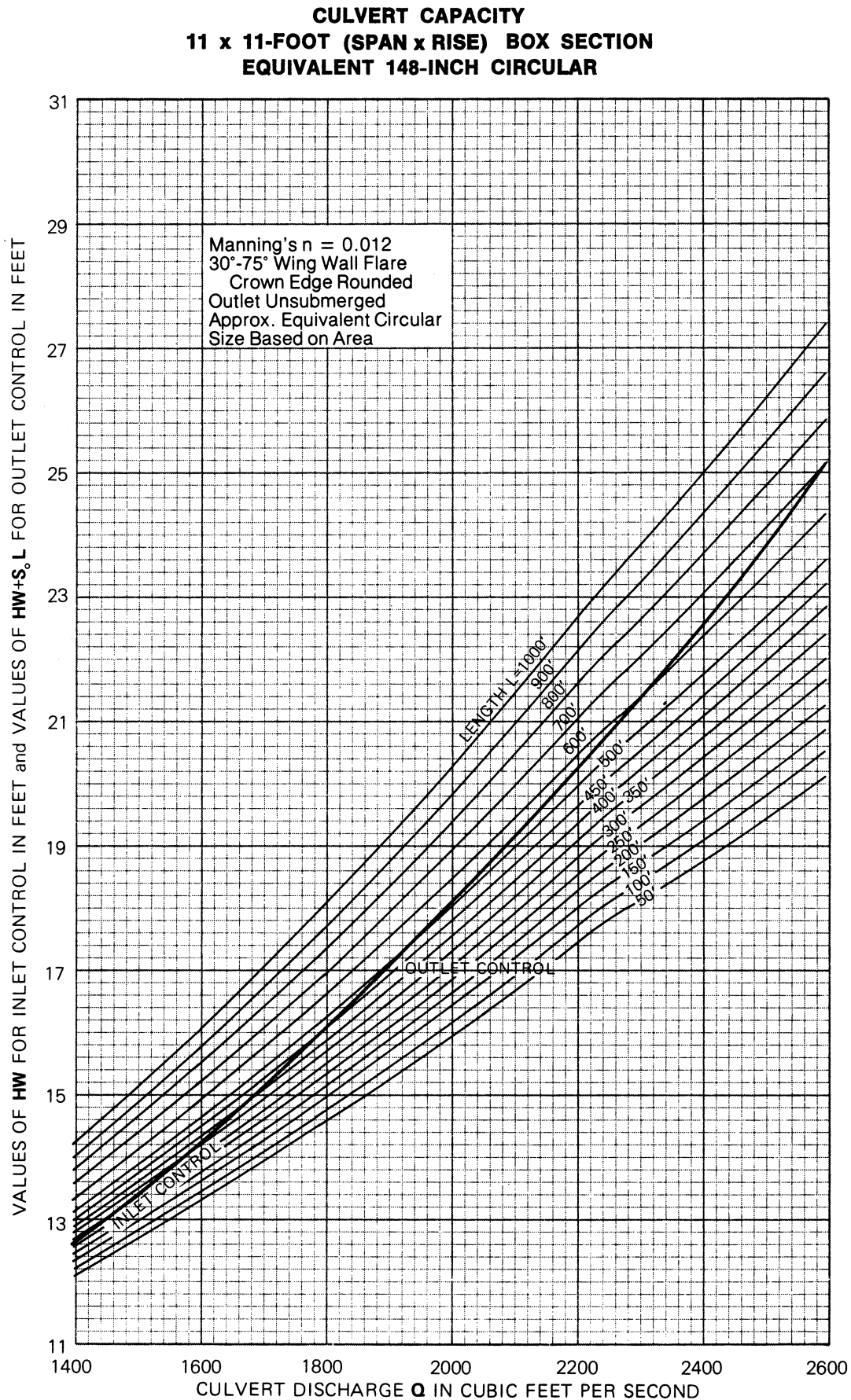


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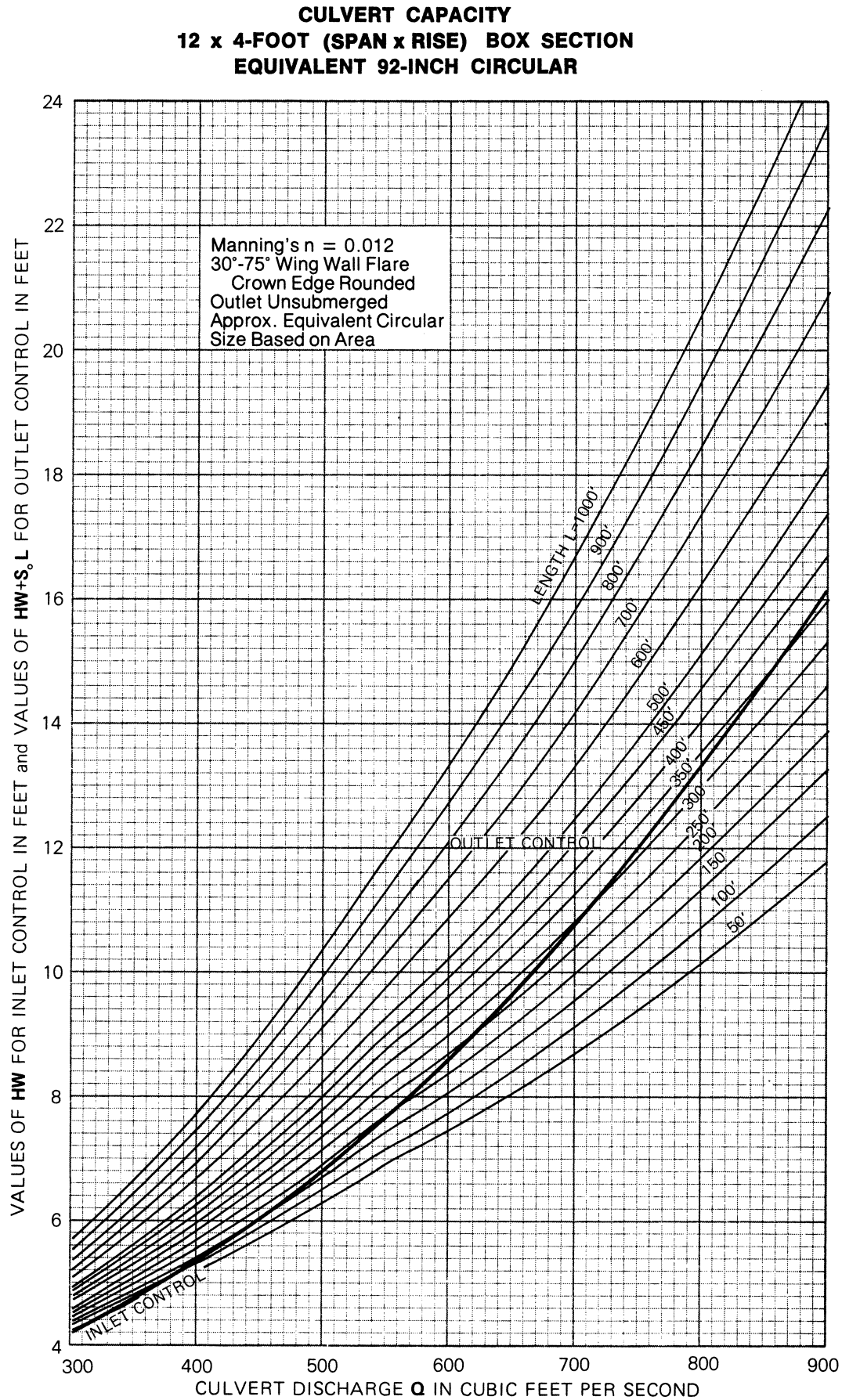


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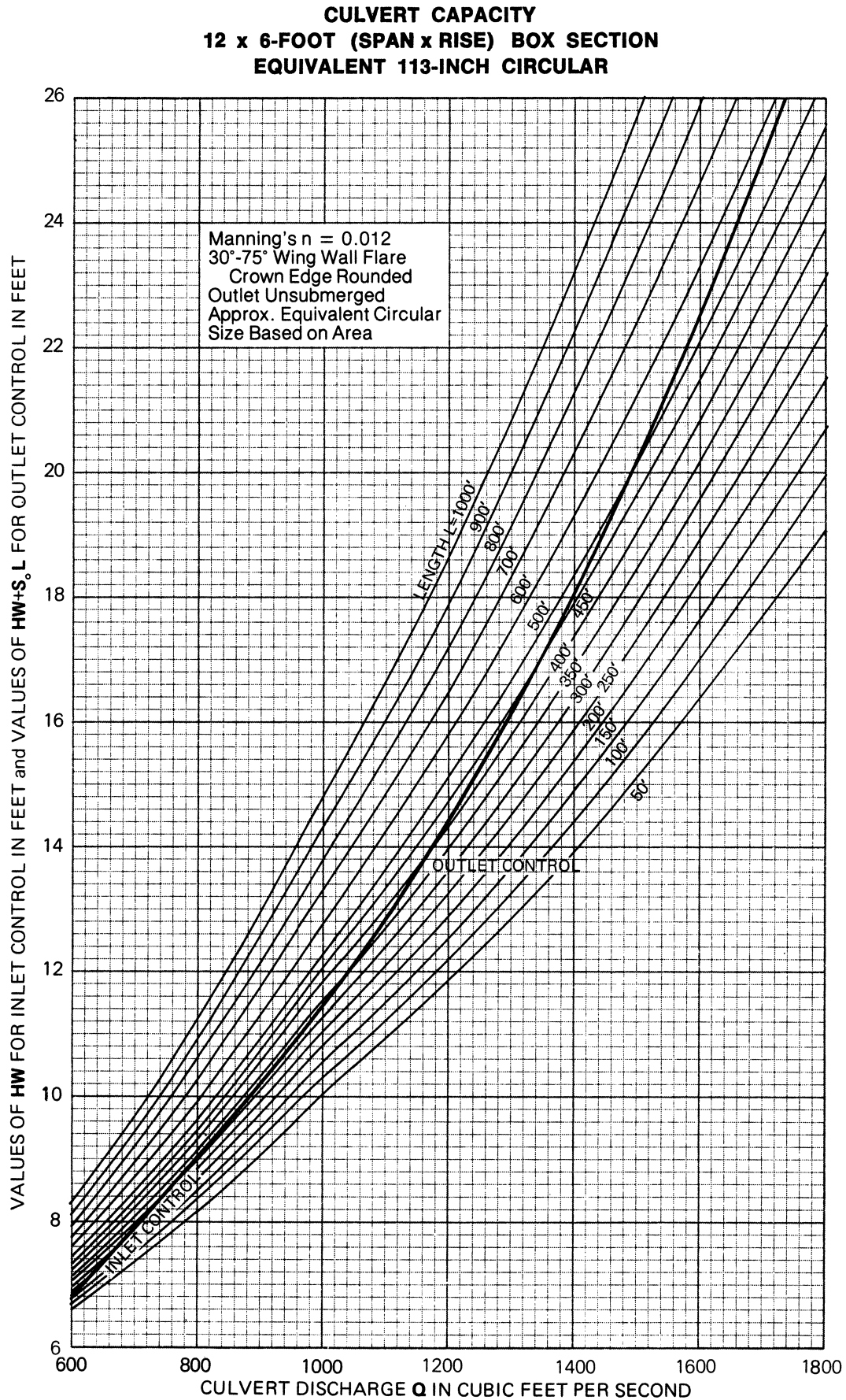


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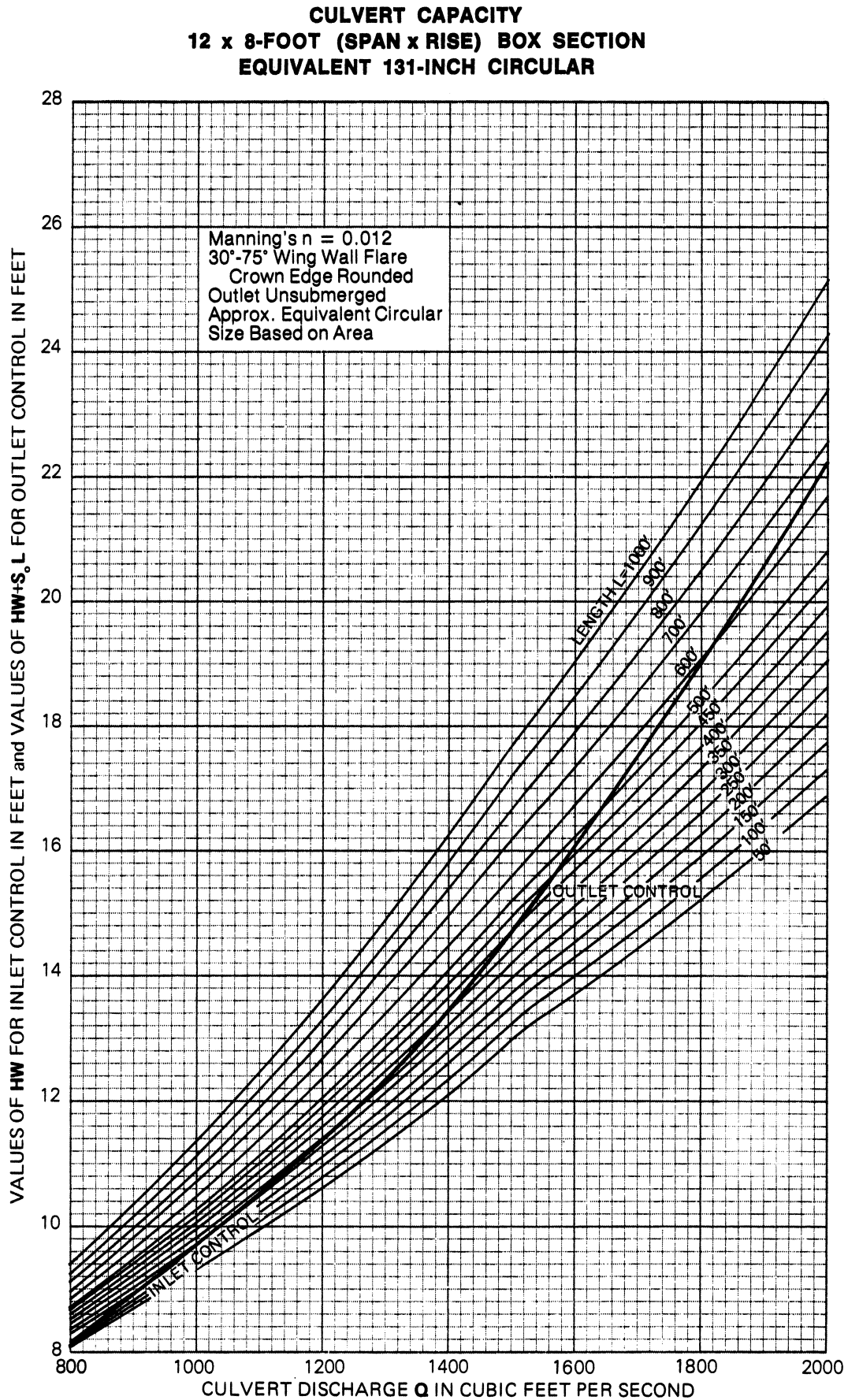


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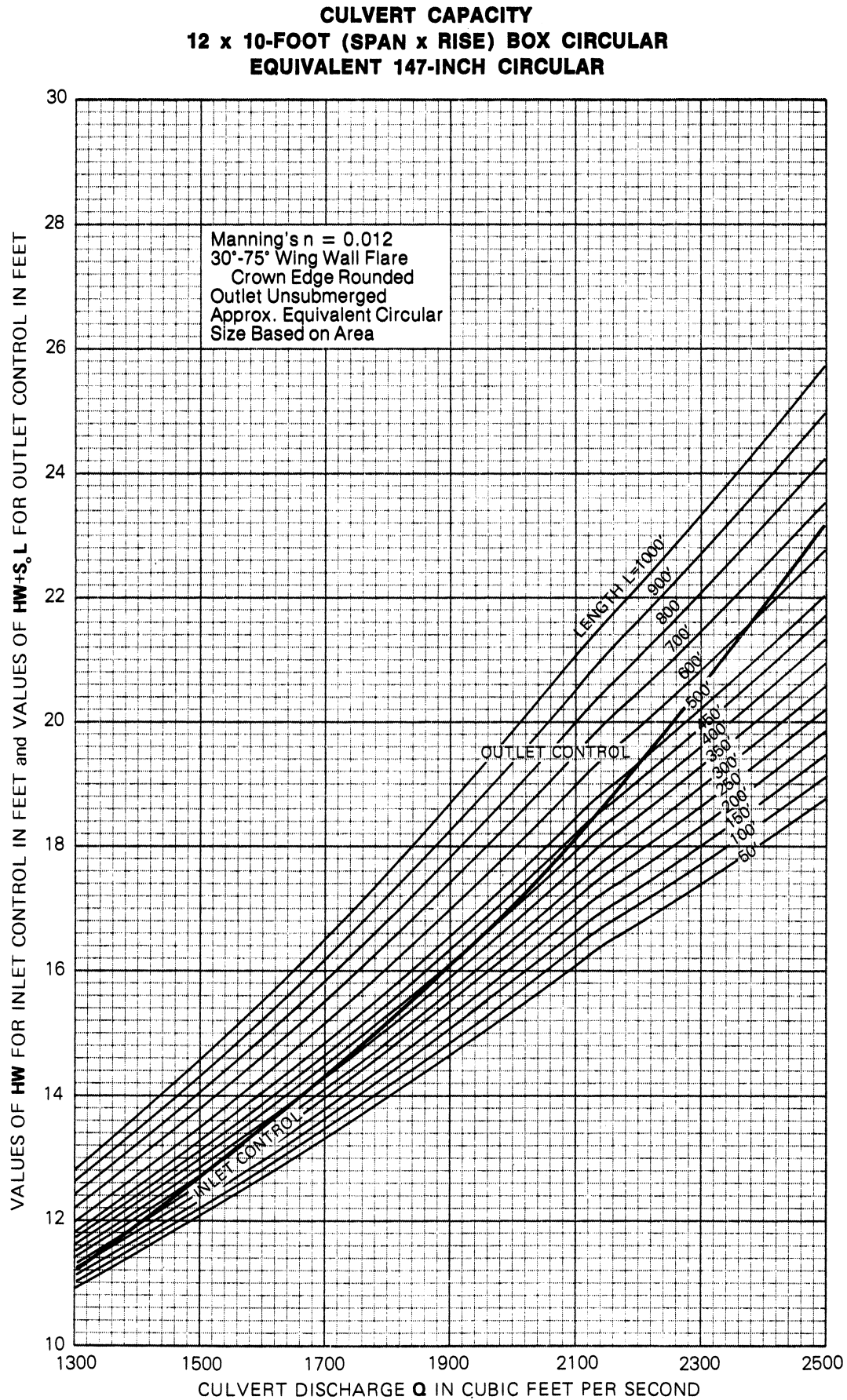


Figure 145

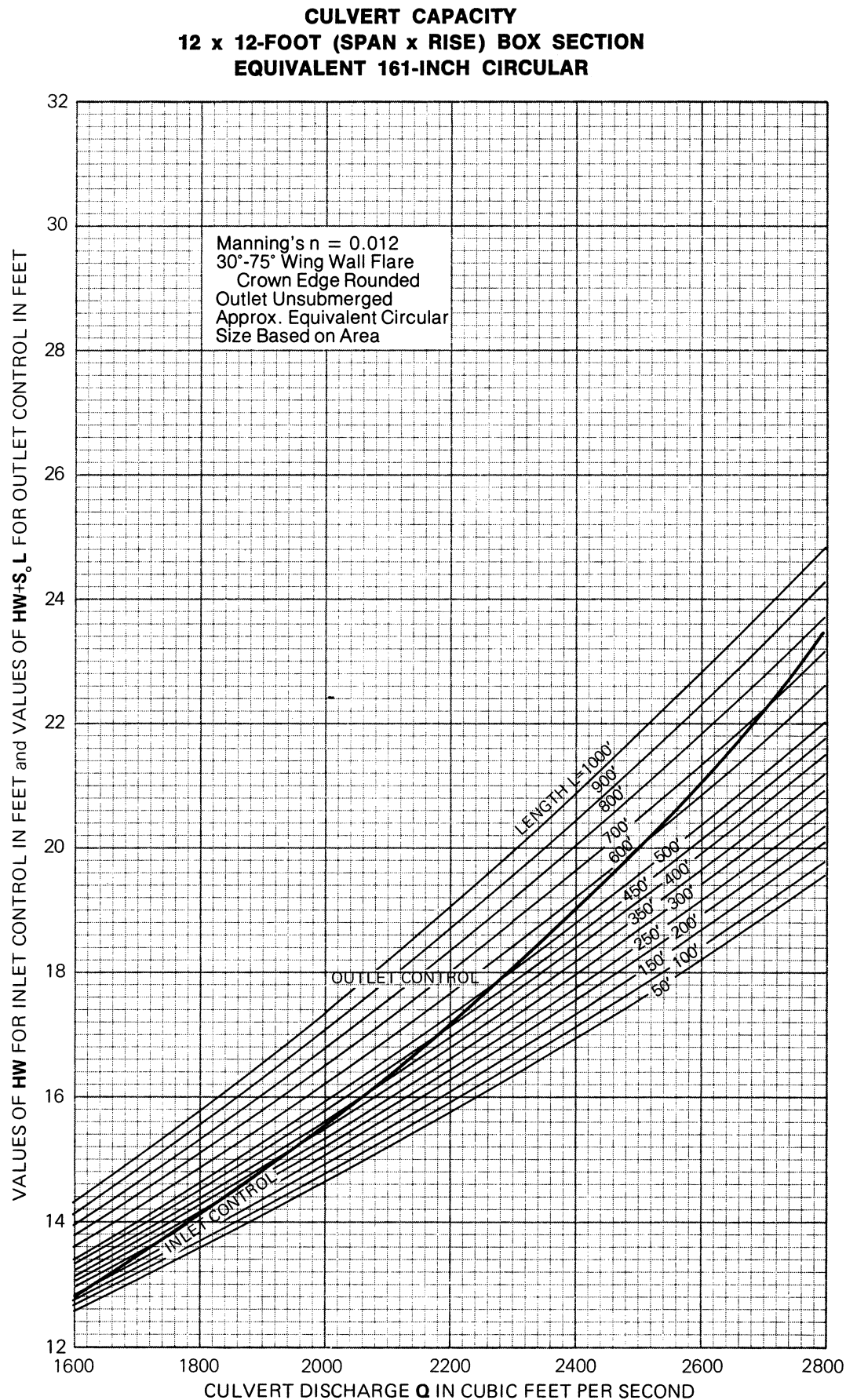


Figure 146

ESSENTIAL FEATURES OF TYPES OF INSTALLATIONS

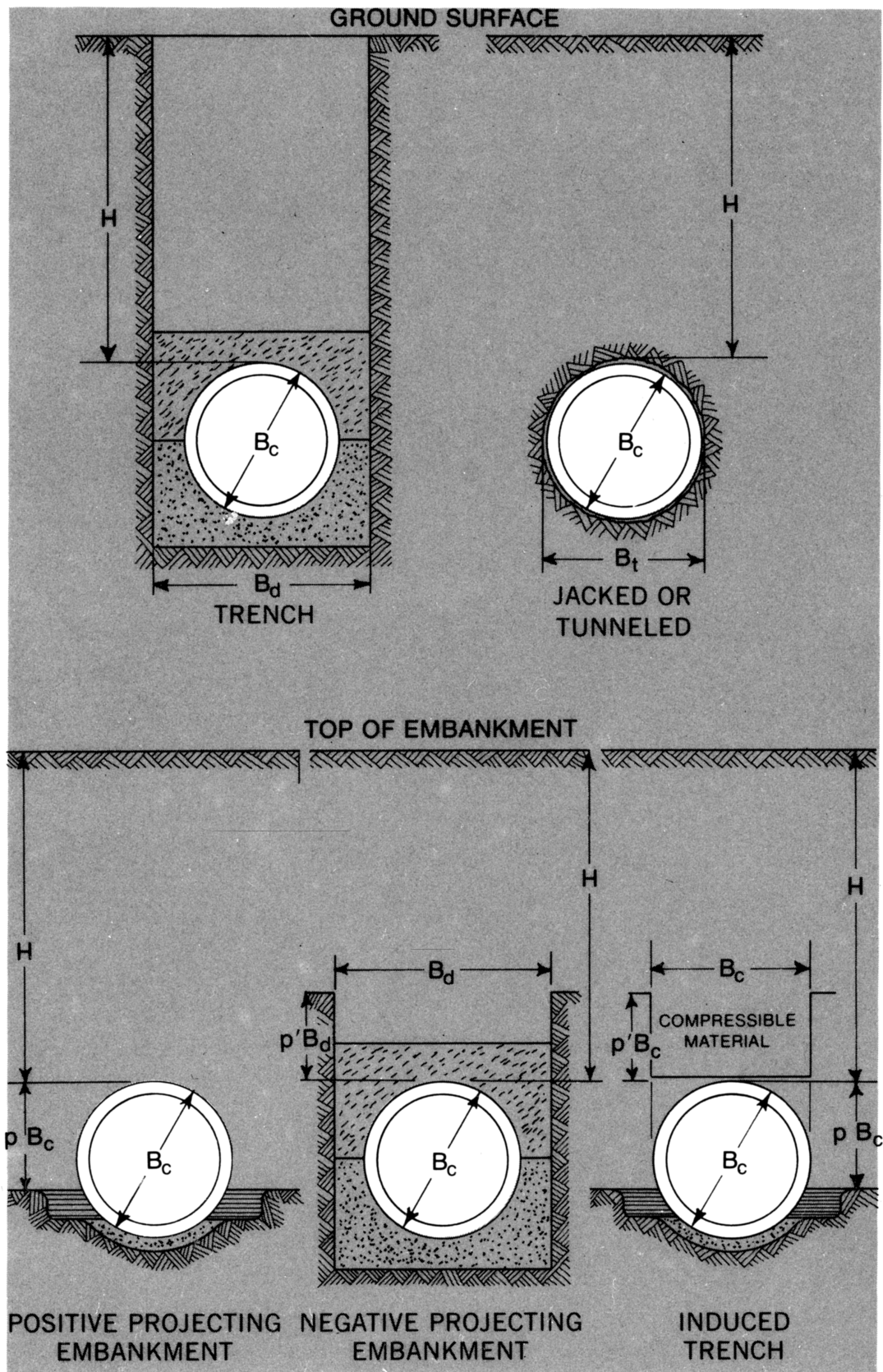


Figure 147

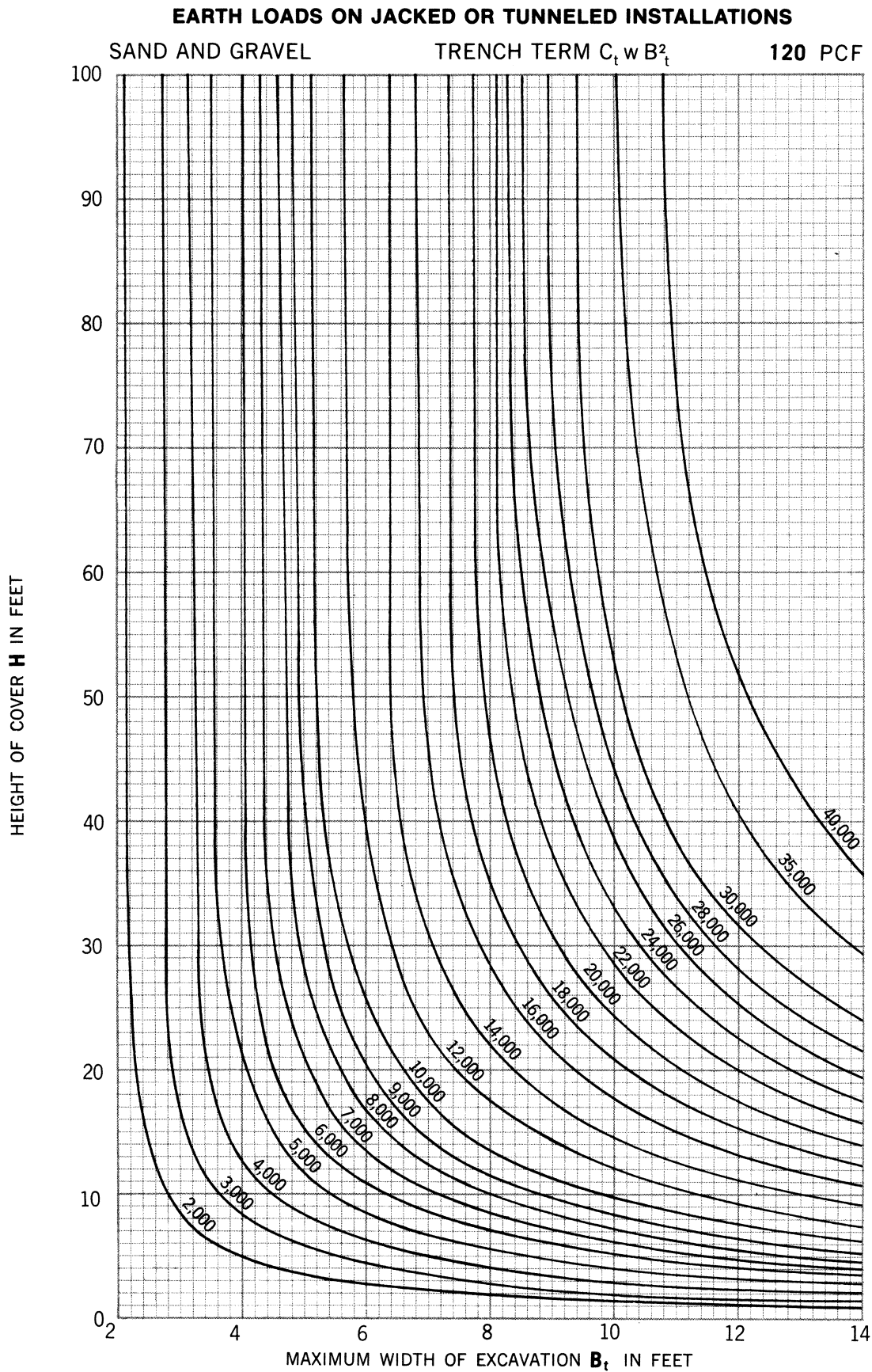


Figure 148

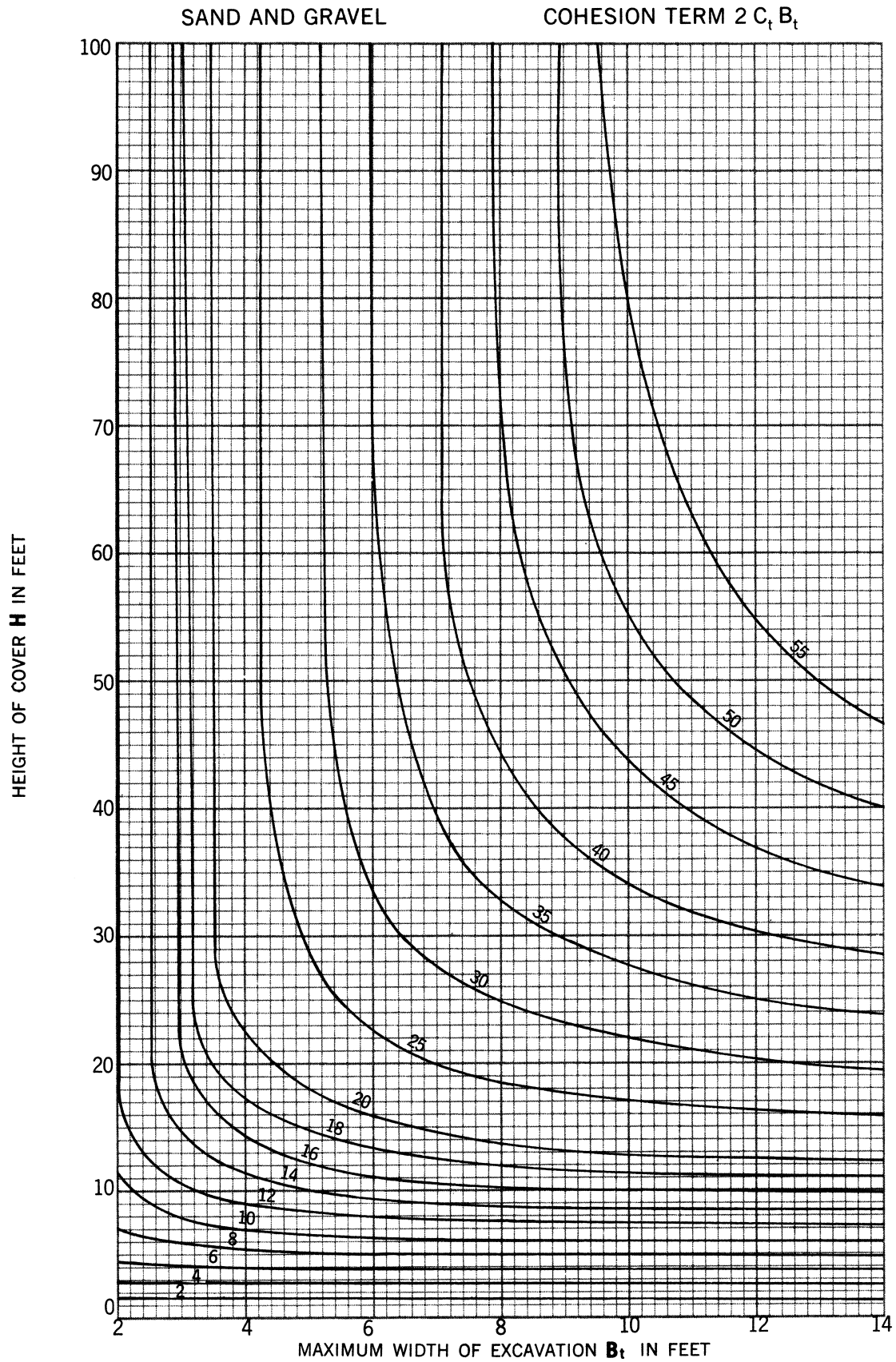
EARTH LOADS ON JACKED OR TUNNELED INSTALLATIONS

Figure 149

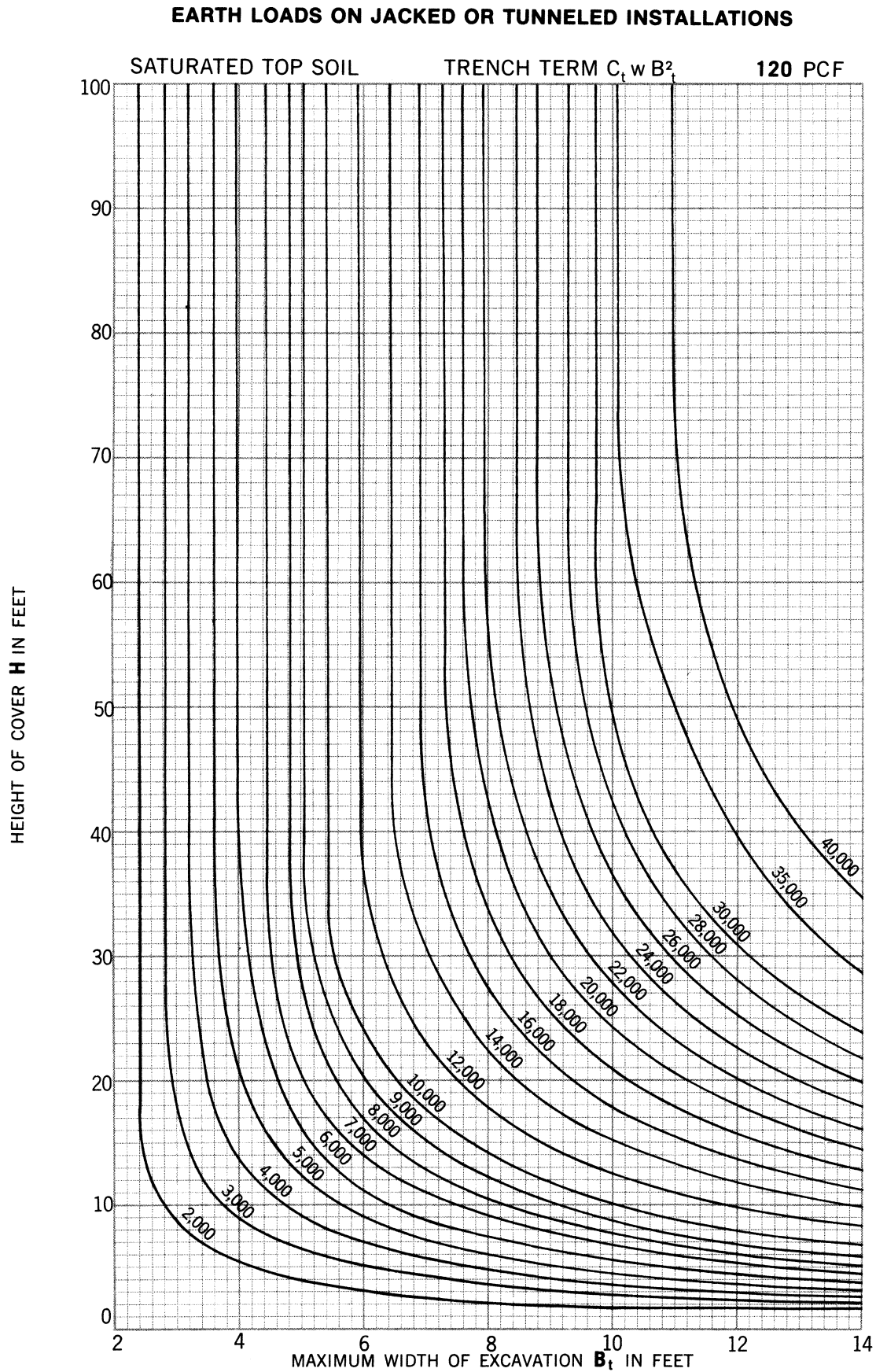


Figure 150

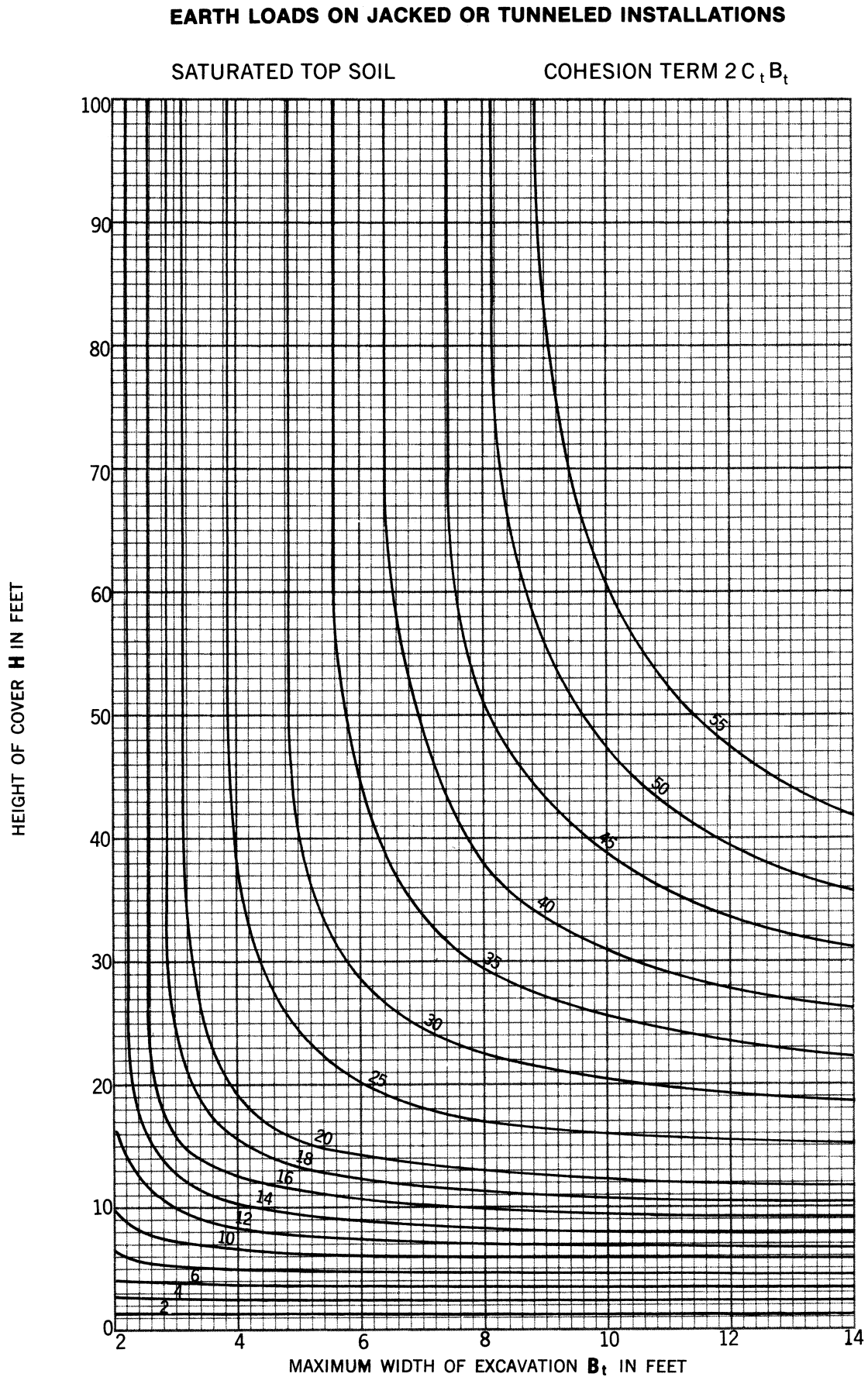


Figure 151

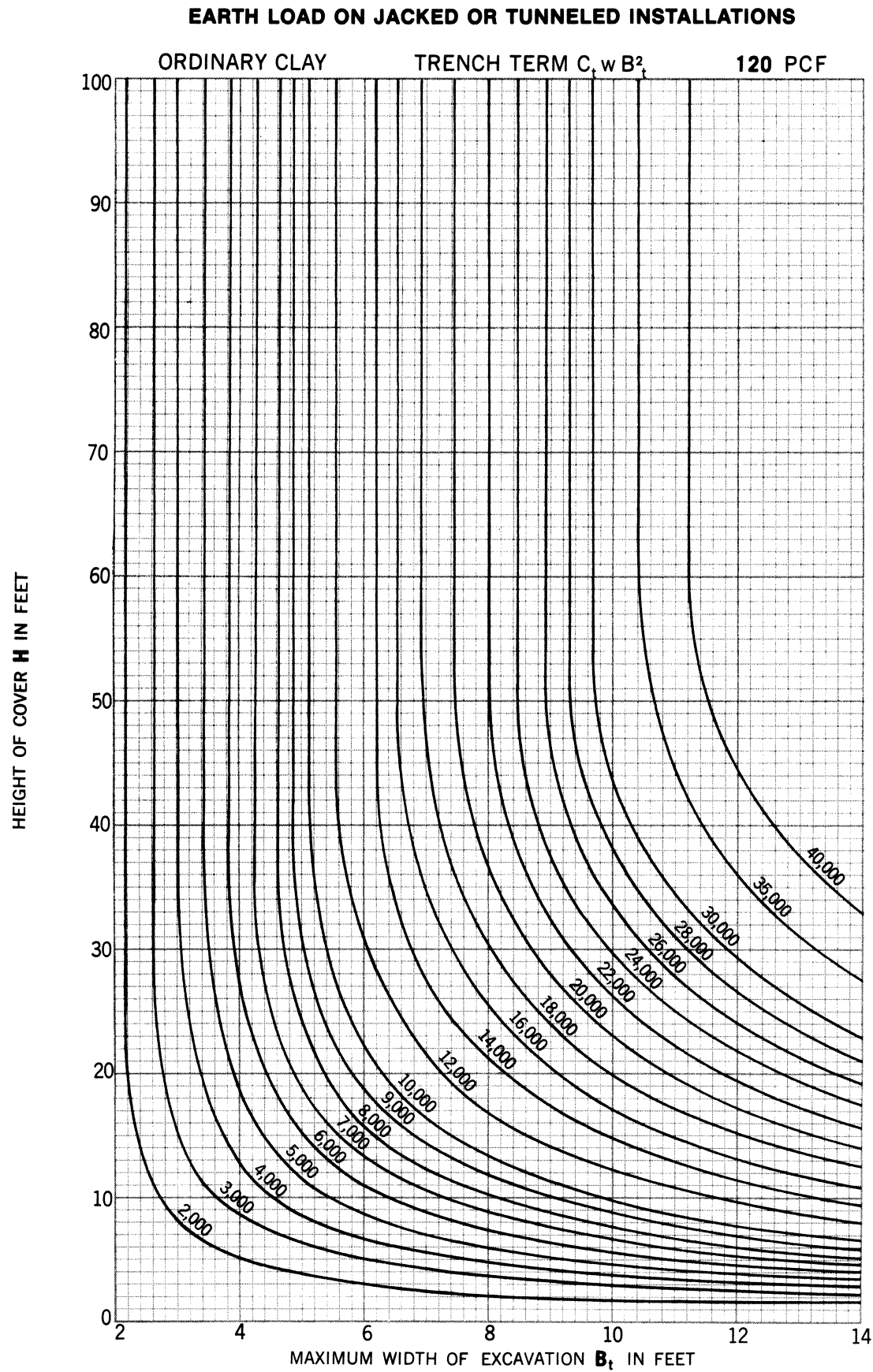


Figure 152

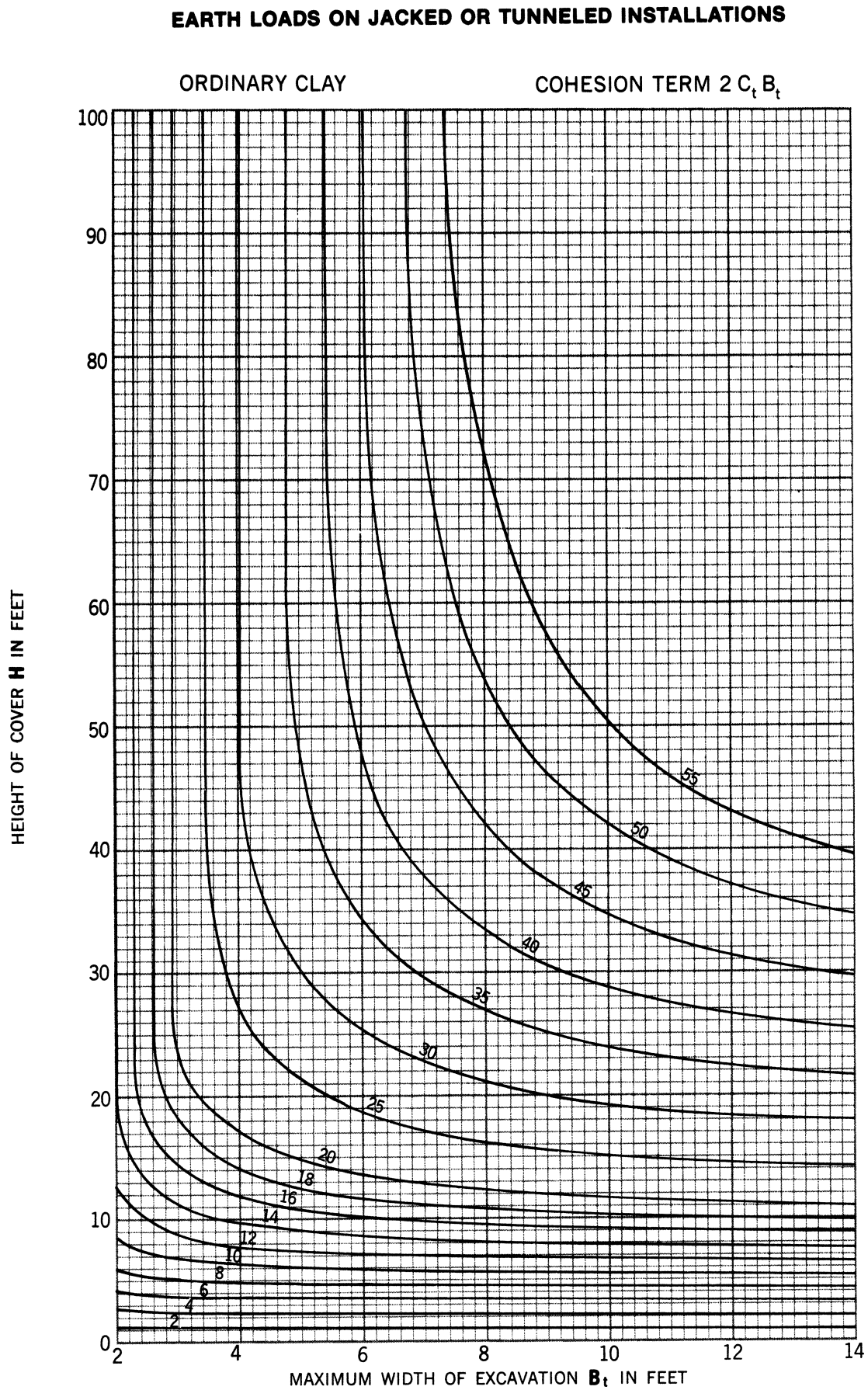
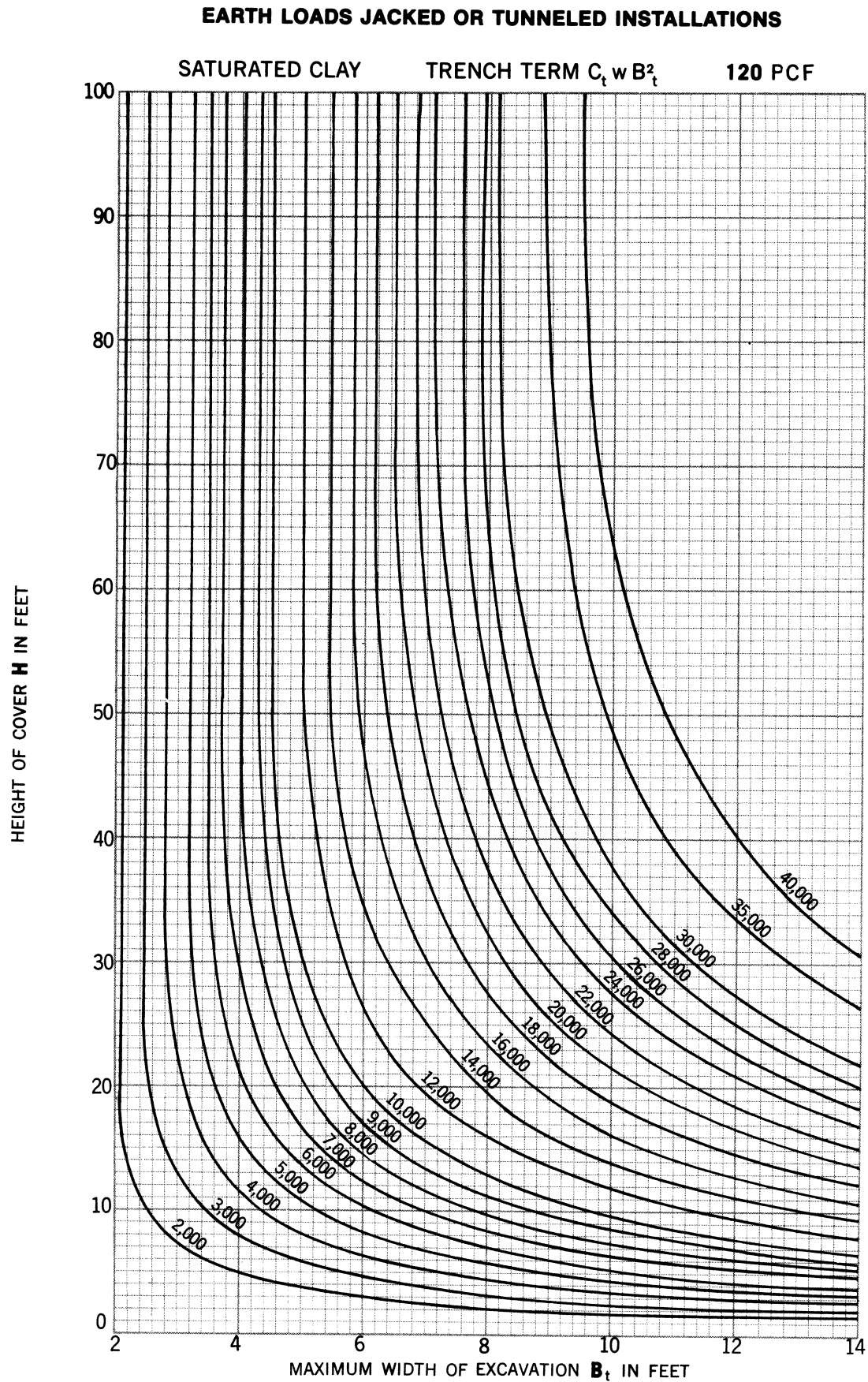


Figure 153



For earth weighing other than 120 pounds per cubic foot, multiply loads by $w/120$.

Figure 154

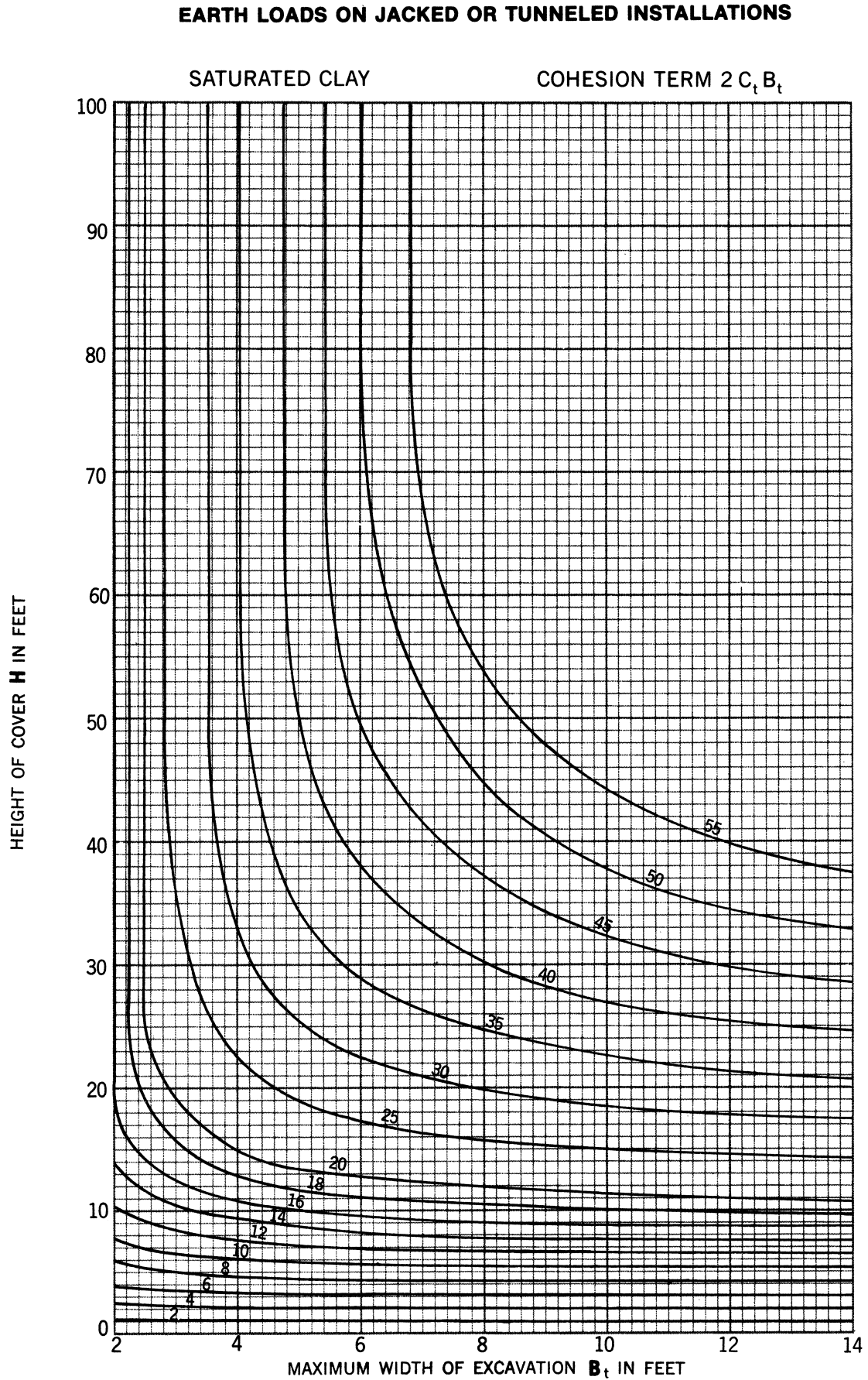
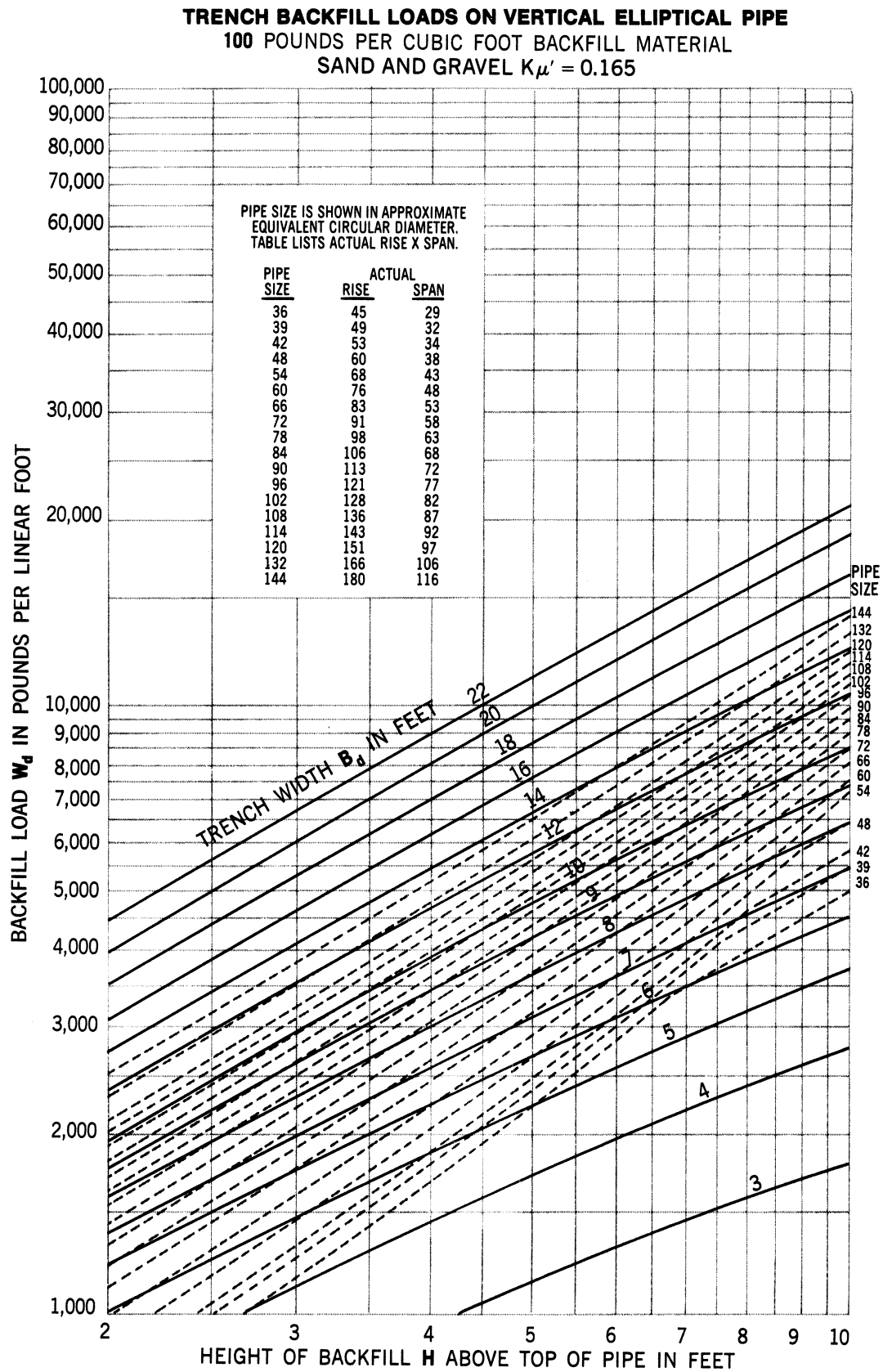


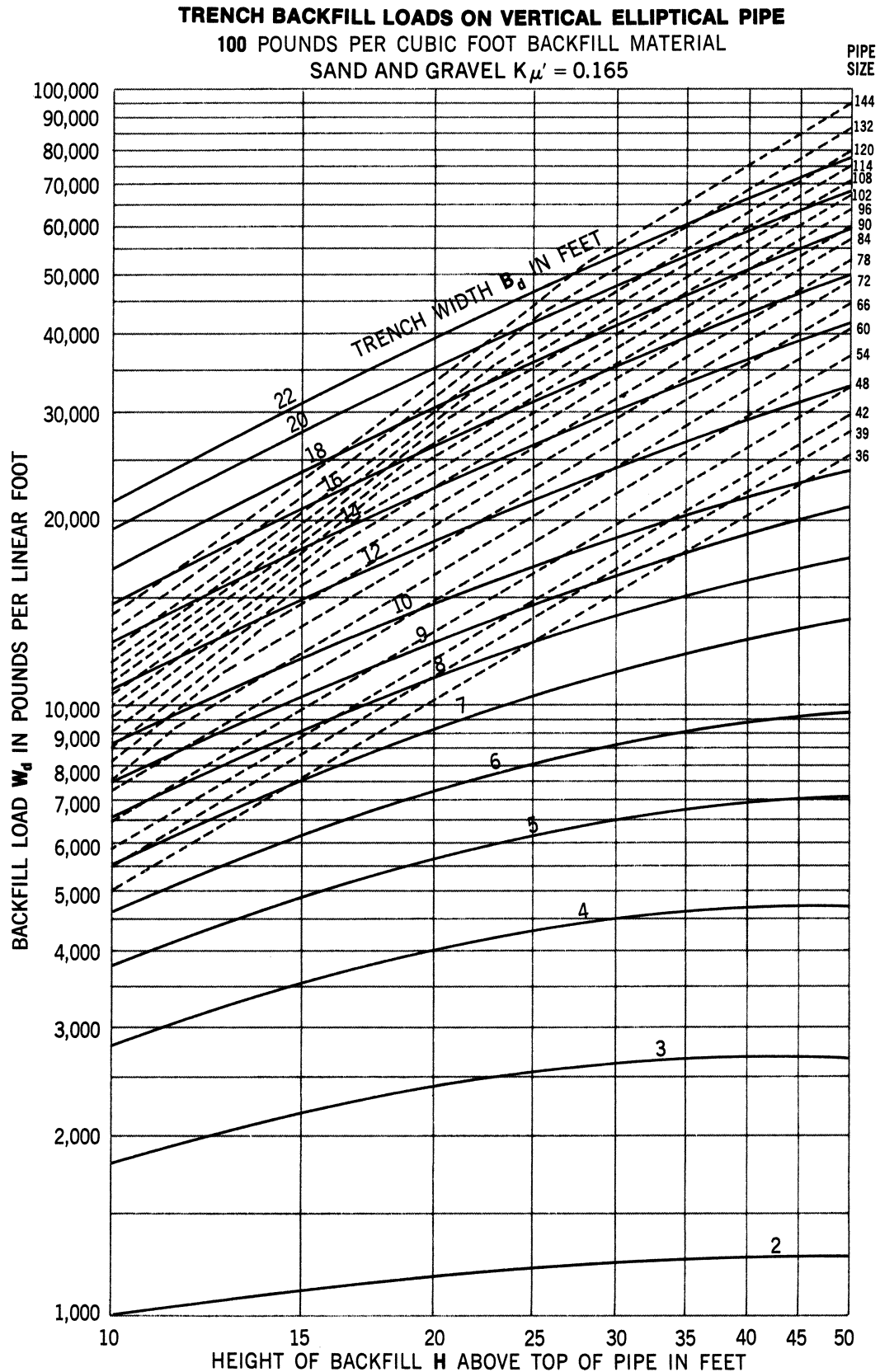
Figure 155



For backfill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds per cubic foot, increase 20%; etc.

Transition loads and widths based on $K\mu = 0.19$, $r_{sd} = 0.7$ and $p = 0.7$ in the embankment equation

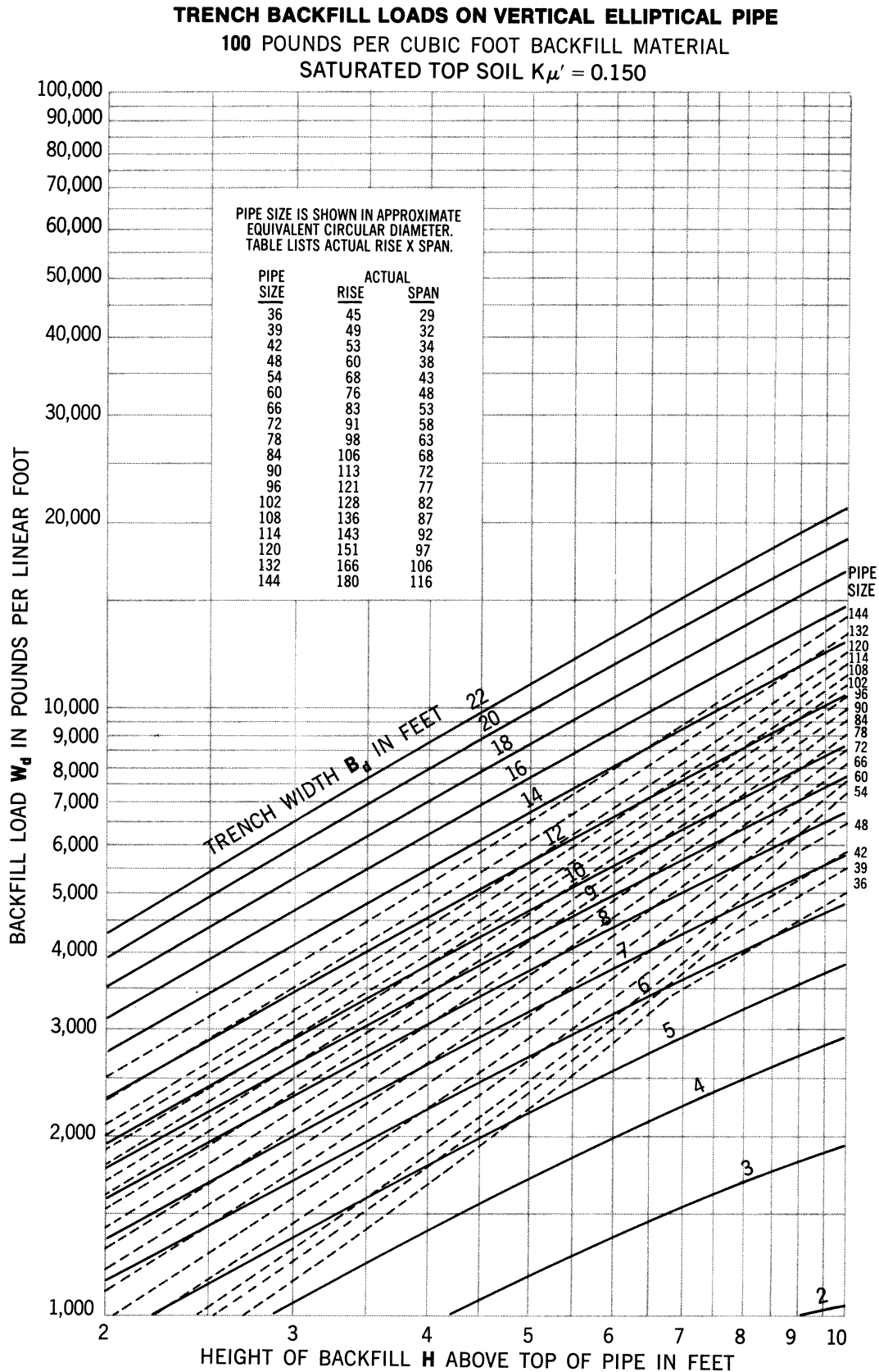
Figure 156



For backfill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds per cubic foot, increase 20%; etc.

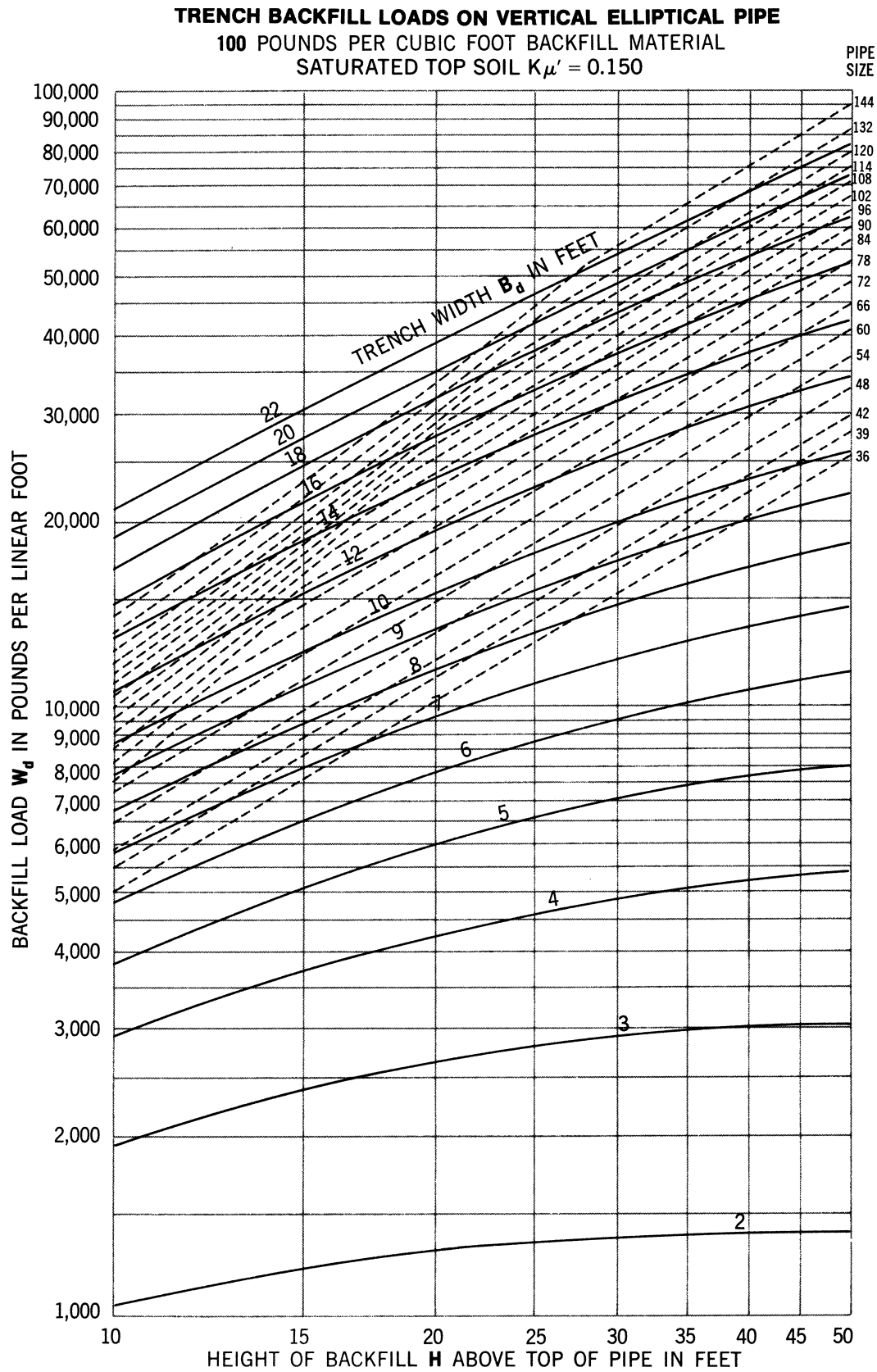
Transition loads and widths based on $K_{\mu} = 0.19$, $r_{sd} = 0.7$ and $p = 0.7$ in the embankment equation

Figure 157



For backfill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds per cubic foot, increase 20%; etc.
 Transition loads and widths based on $K_{\mu} = 0.19$, $r_{sd} = 0.7$ and $p = 0.7$ in the embankment equation

Figure 158

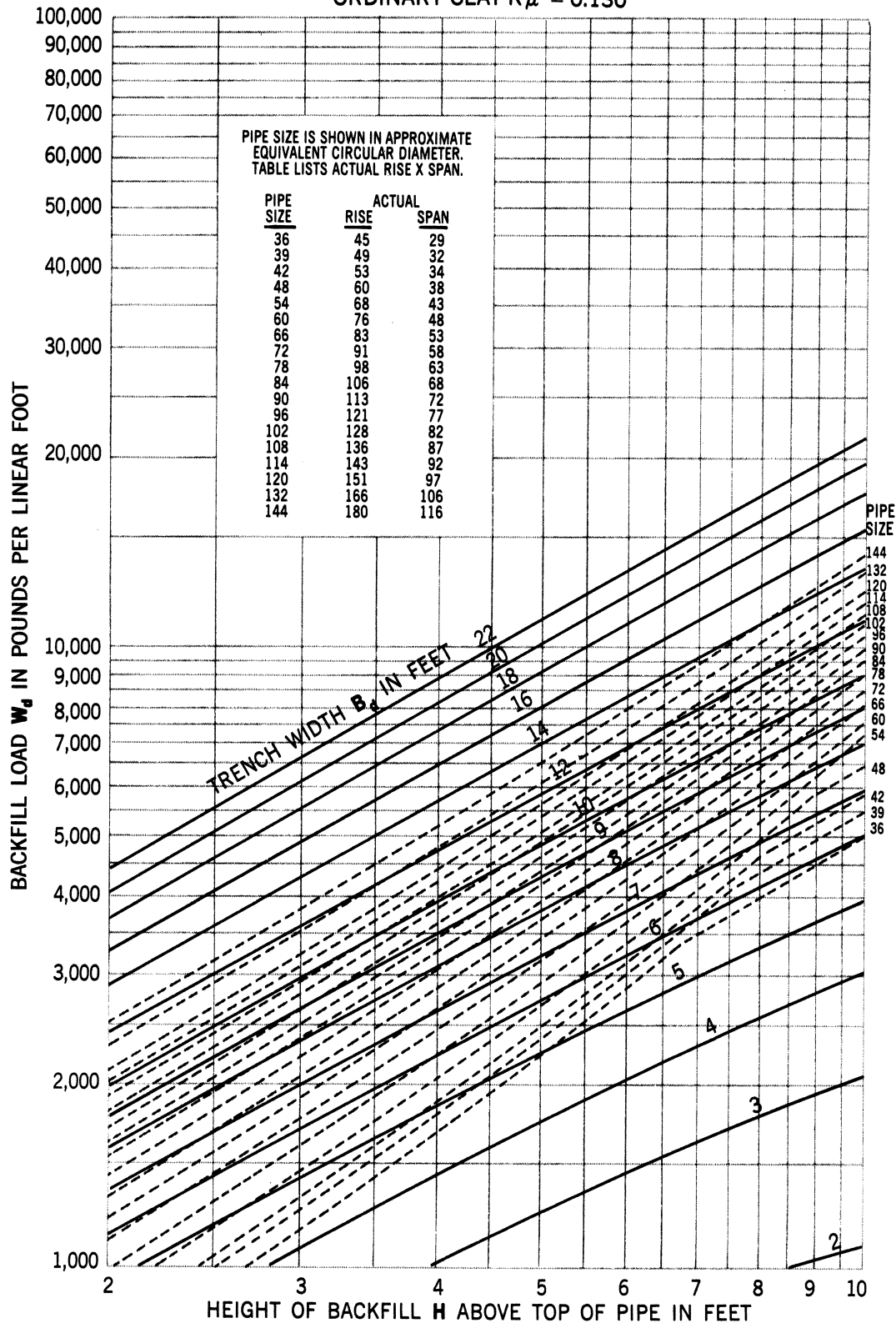


For backfill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds per cubic foot, increase 20%; etc.

Transition loads and widths based on $K_{\mu} = 0.19$, $r_{sd} = 0.7$ and $p = 0.7$ in the embankment equation

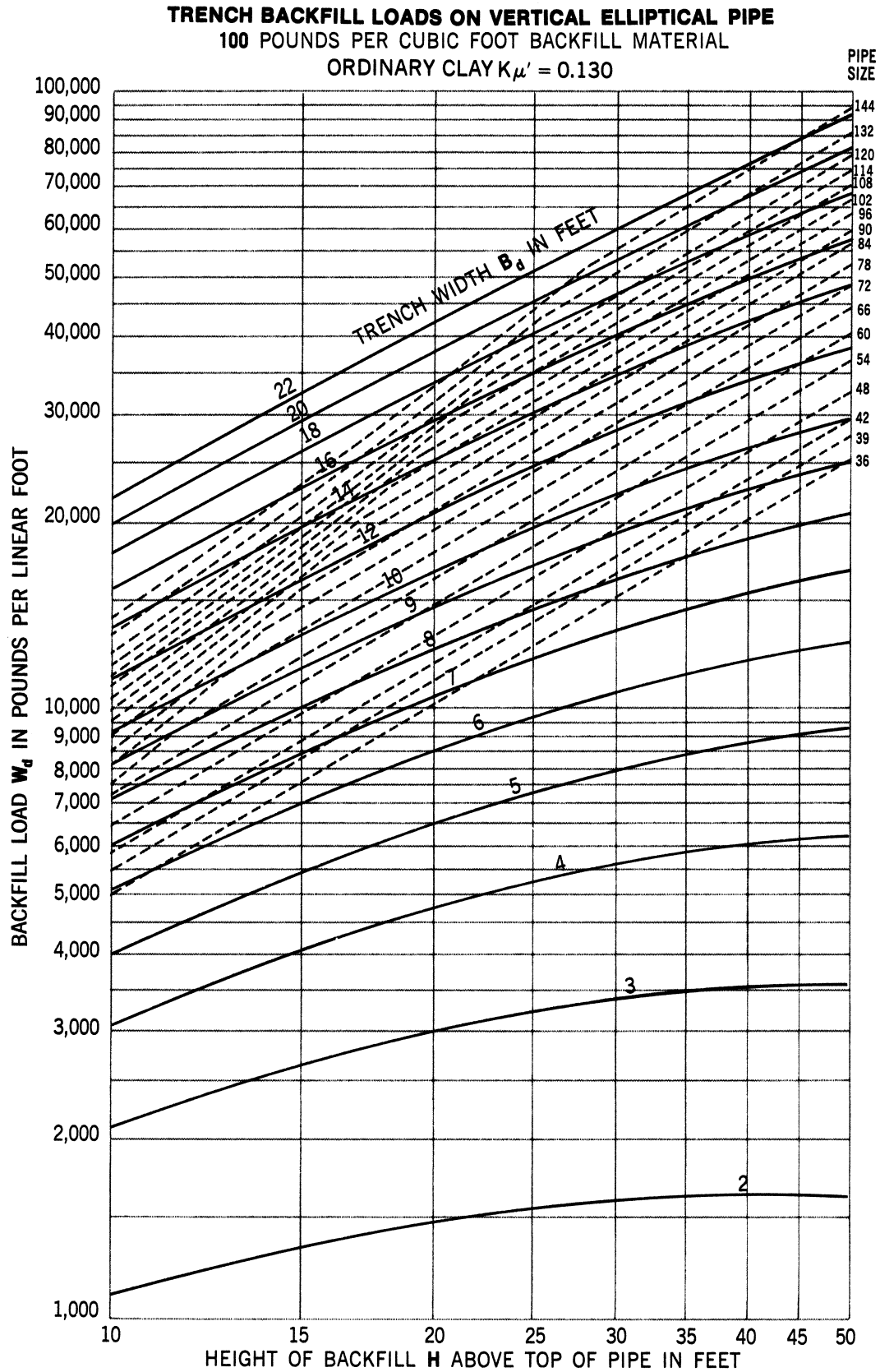
Figure 159

TRENCH BACKFILL LOADS ON VERTICAL ELLIPTICAL PIPE
100 POUNDS PER CUBIC FOOT BACKFILL MATERIAL
ORDINARY CLAY $K\mu' = 0.130$



For backfill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds per cubic foot, increase 20%; etc.
 Transition loads and widths based on $K\mu = 0.19$, $r_{sd} = 0.7$ and $p = 0.7$ in the embankment equation

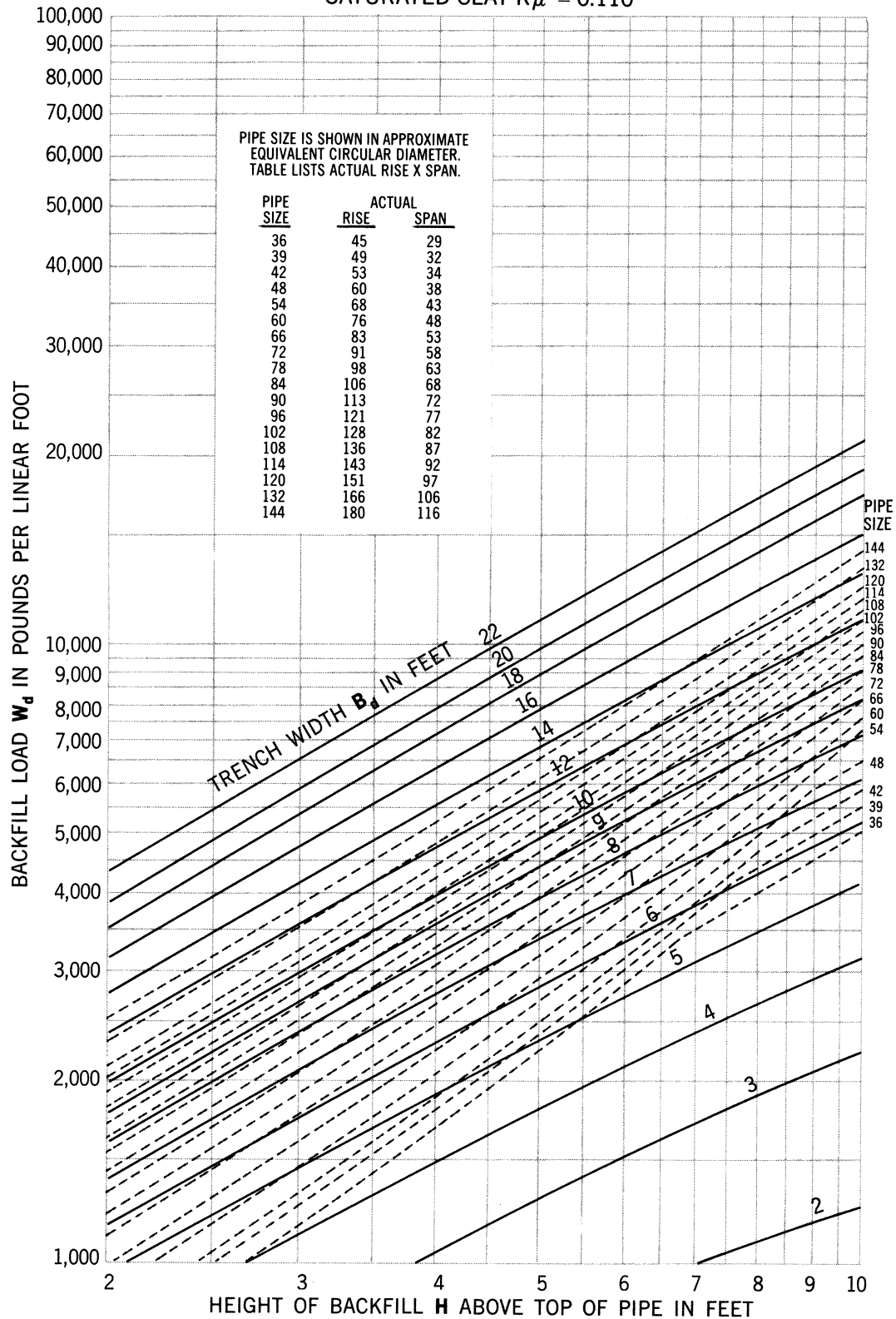
Figure 160



For backfill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds per cubic foot, increase 20%; etc.
 Transition loads and widths based on $K_{\mu} = 0.19$, $r_{sd} = 0.7$ and $p = 0.7$ in the embankment equation

Figure 161

TRENCH BACKFILL LOADS ON VERTICAL ELLIPTICAL PIPE
100 POUNDS PER CUBIC FOOT BACKFILL MATERIAL
SATURATED CLAY $K\mu' = 0.110$



For backfill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds per cubic foot, increase 20%; etc.
 Transition loads and widths based on $K\mu = 0.19$, $r_{sd} = 0.7$ and $p = 0.7$ in the embankment equation

Figure 162

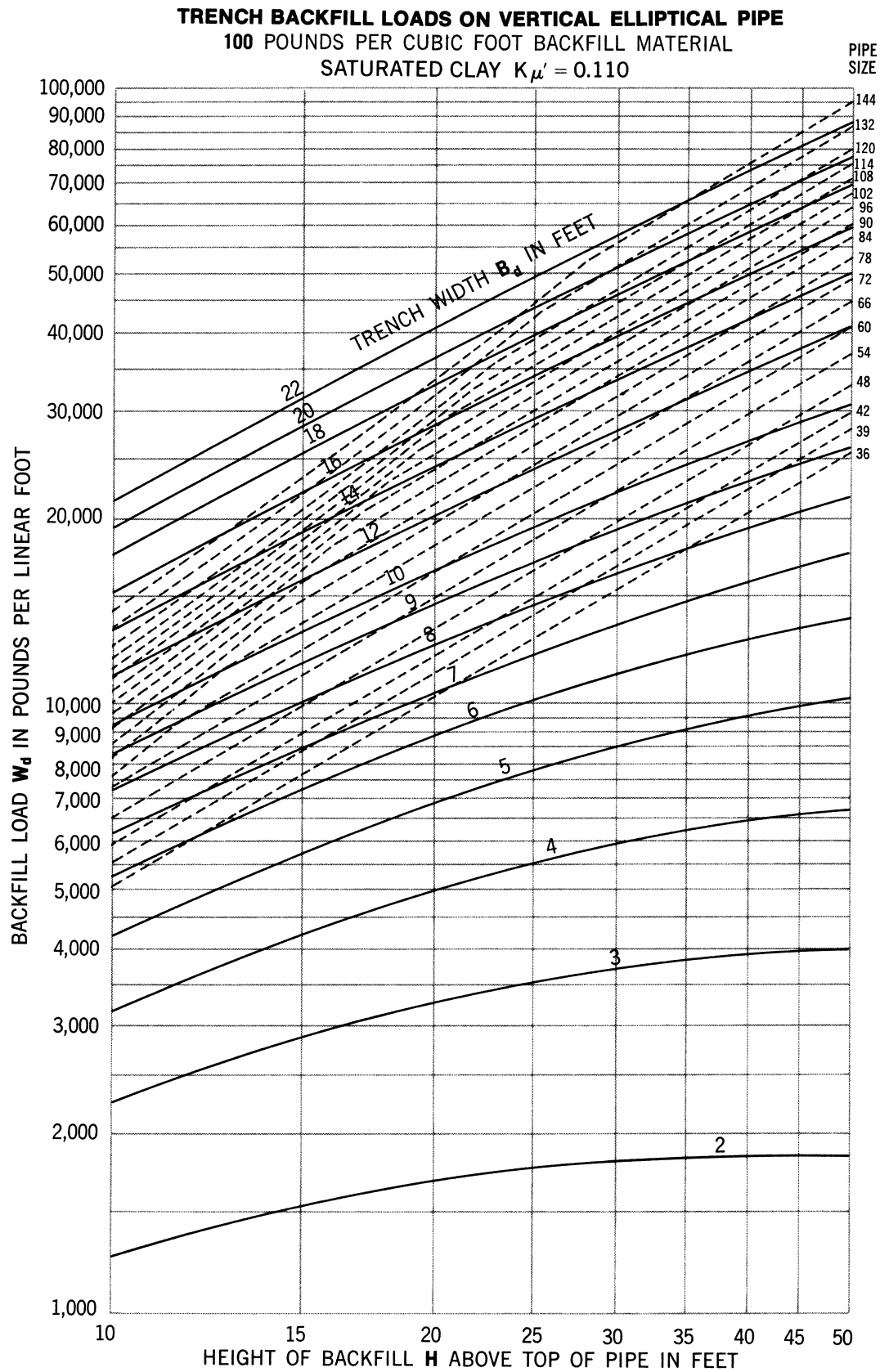
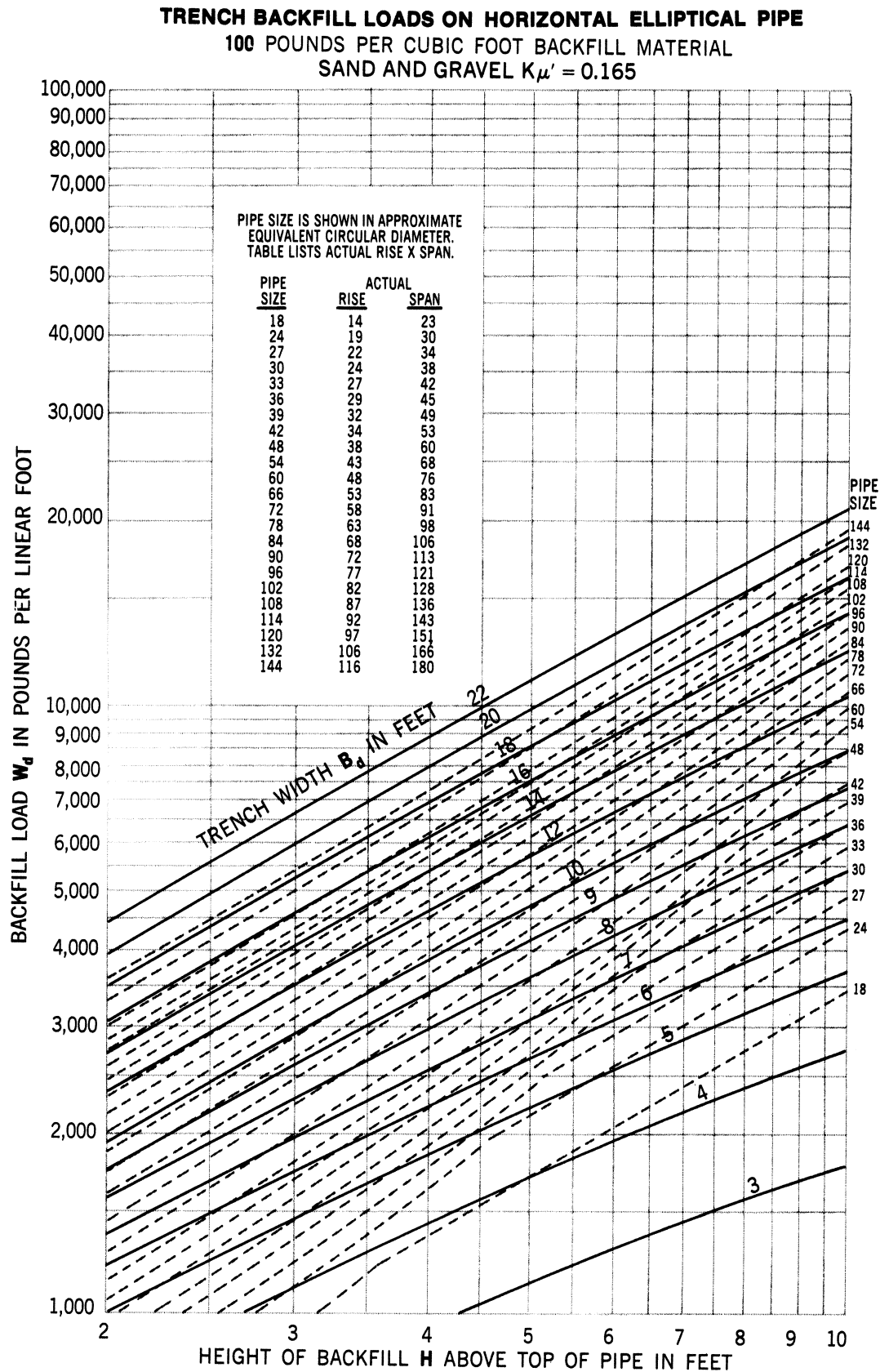


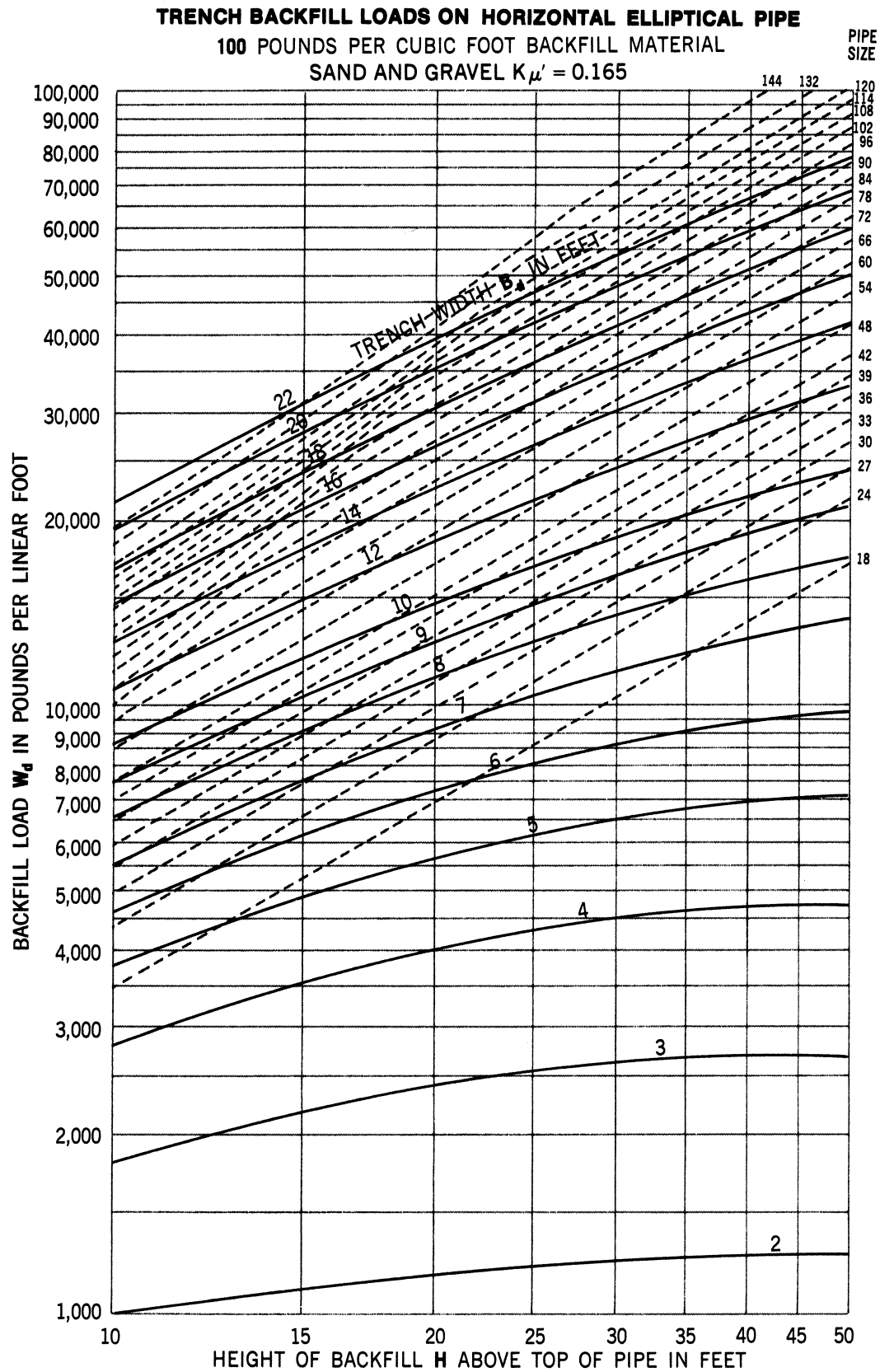
Figure 163



For backfill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds per cubic foot, increase 20%; etc.

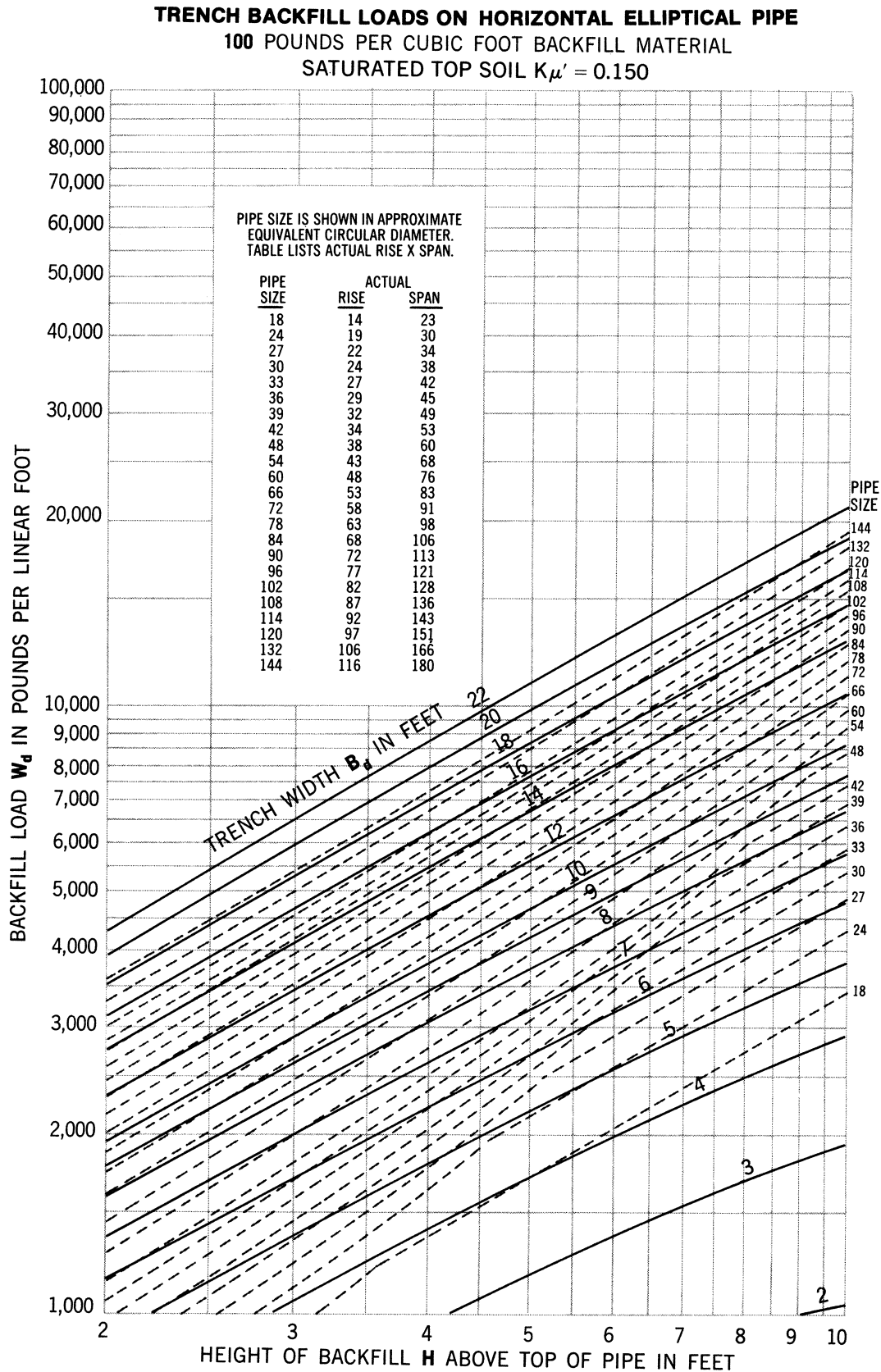
Transition loads and widths based on $K\mu = 0.19$, $r_{sd} = 0.7$ and $p = 0.7$ in the embankment equation

Figure 164



For backfill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds per cubic foot, increase 20%; etc.
 Transition loads and widths based on $K\mu = 0.19$, $r_{sd} = 0.7$ and $p = 0.7$ in the embankment equation

Figure 165



For backfill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds per cubic foot, increase 20%; etc.
 Transition loads and widths based on $K_{\mu} = 0.19$, $r_{sd} = 0.7$ and $p = 0.7$ in the embankment equation

Figure 166

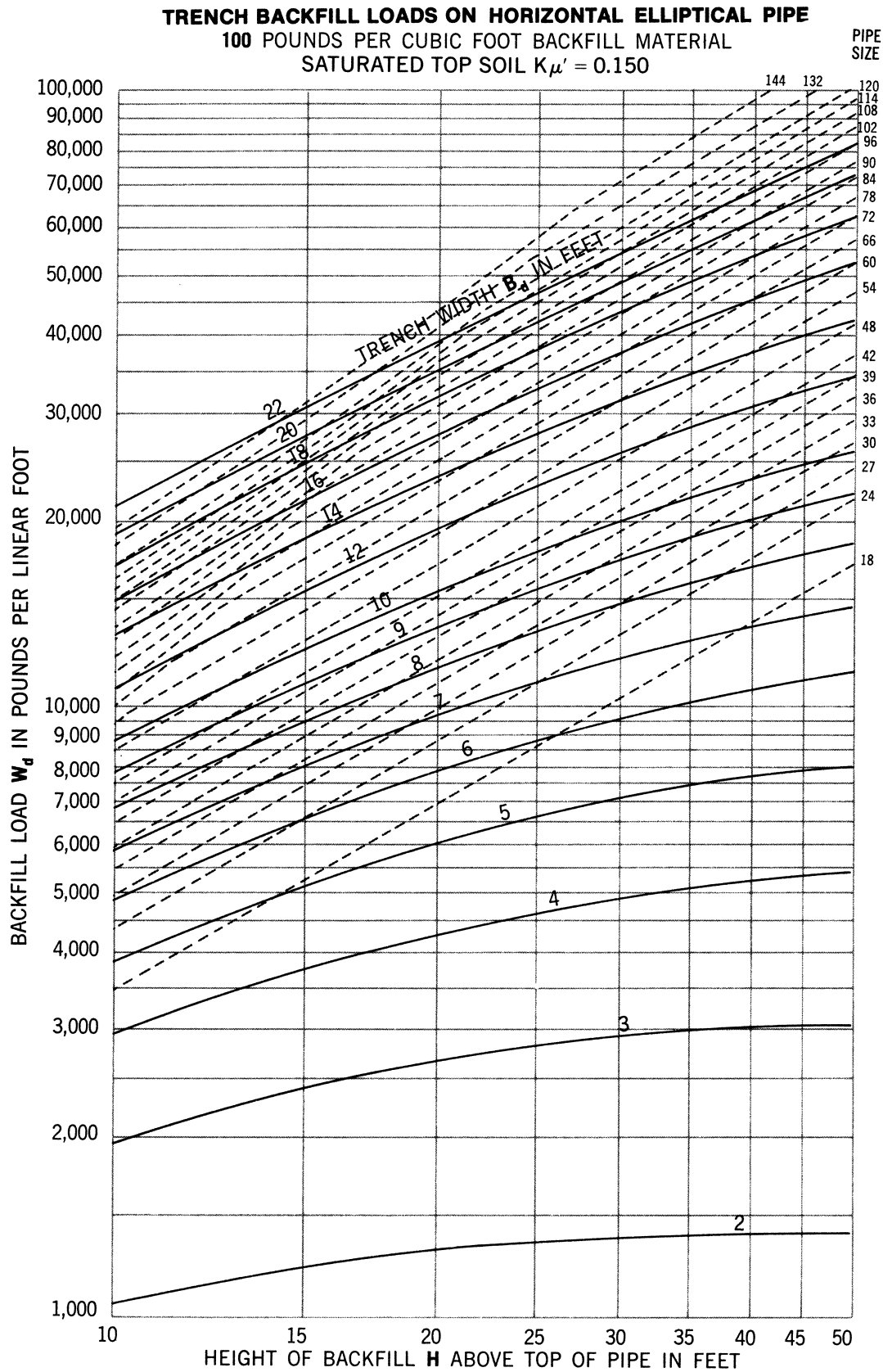
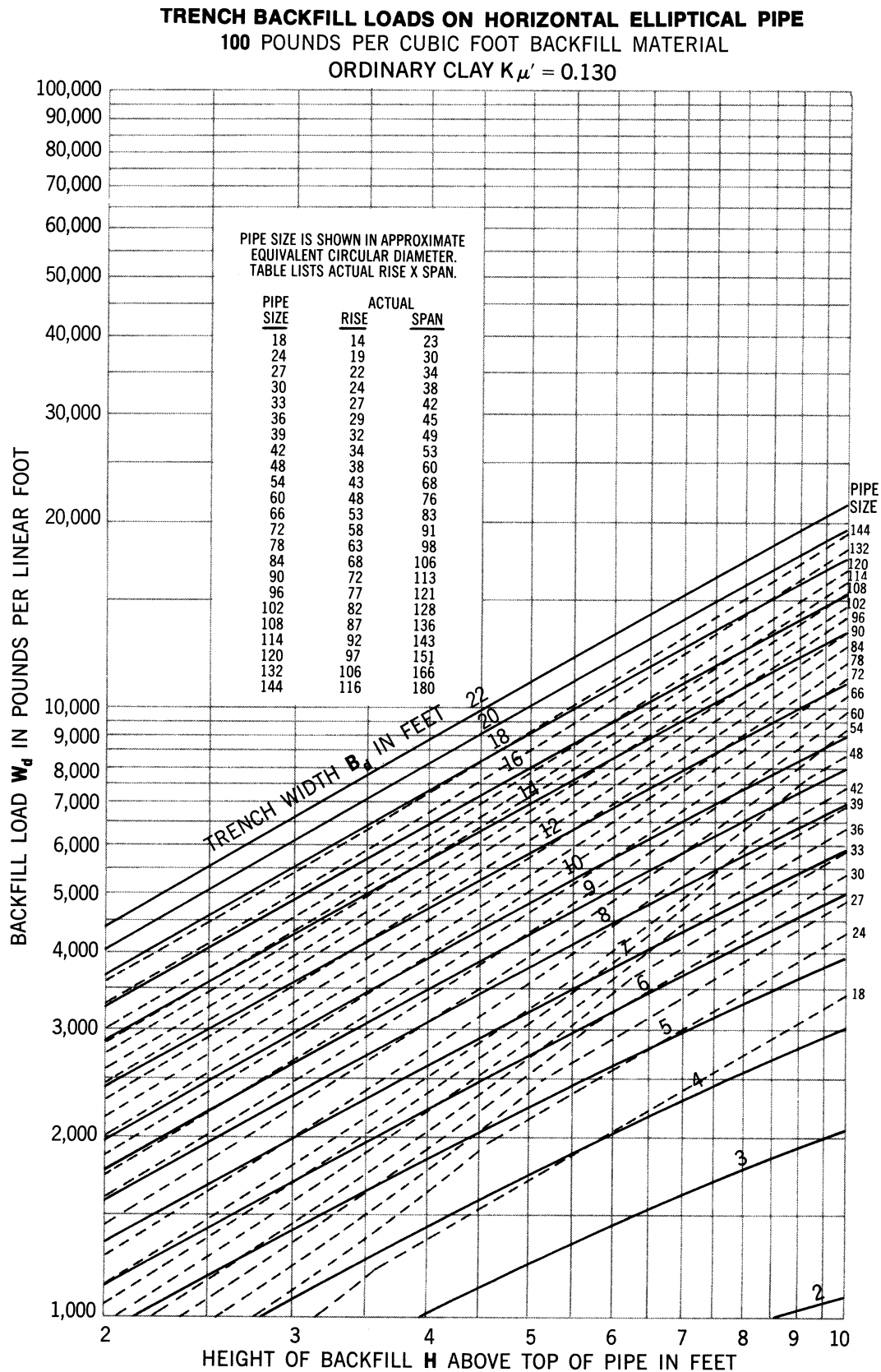


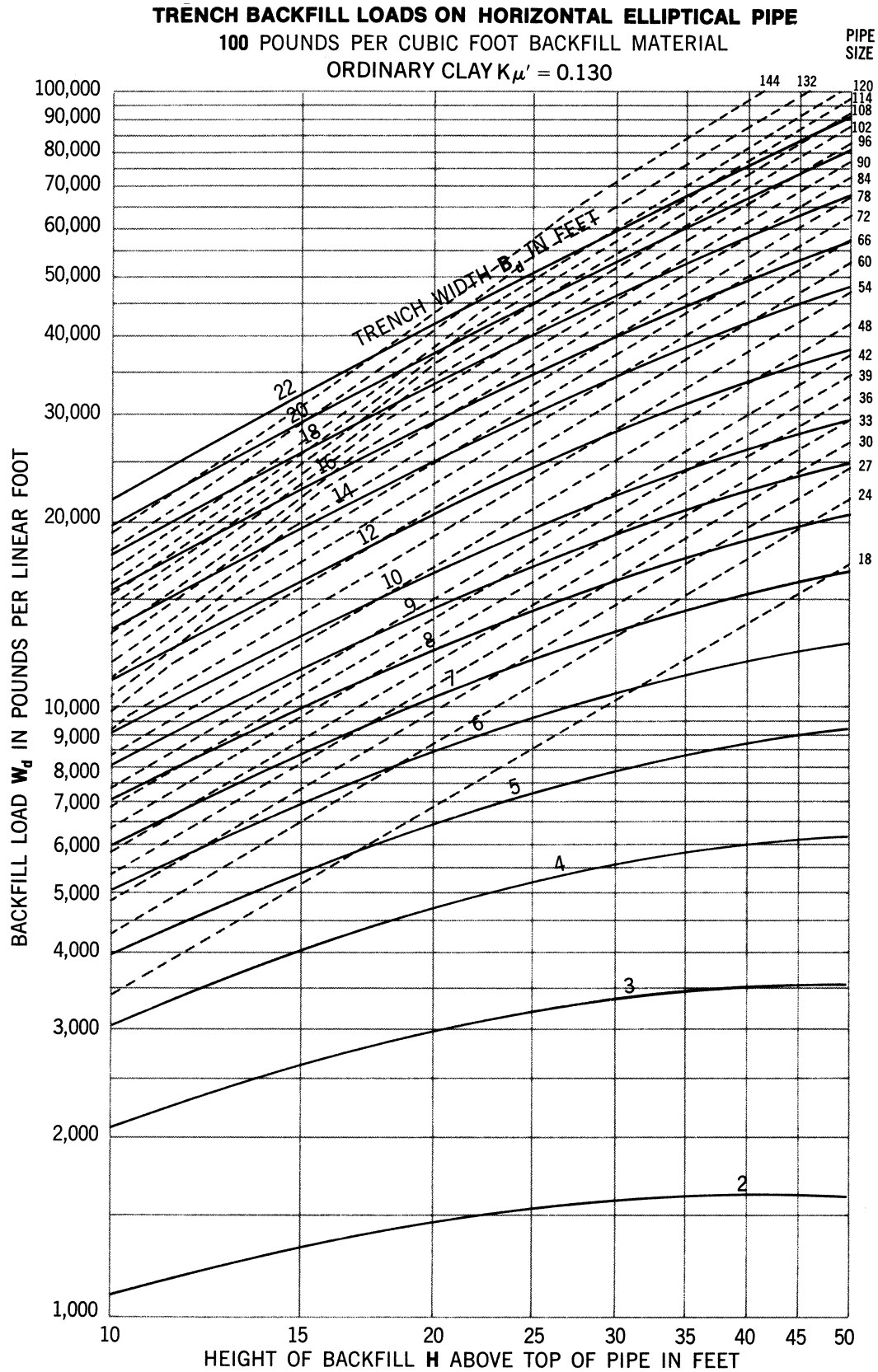
Figure 167



For backfill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds per cubic foot, increase 20%; etc.

Transition loads and widths based on $K\mu = 0.19$, $r_{sd} = 0.7$ and $p = 0.7$ in the embankment equation

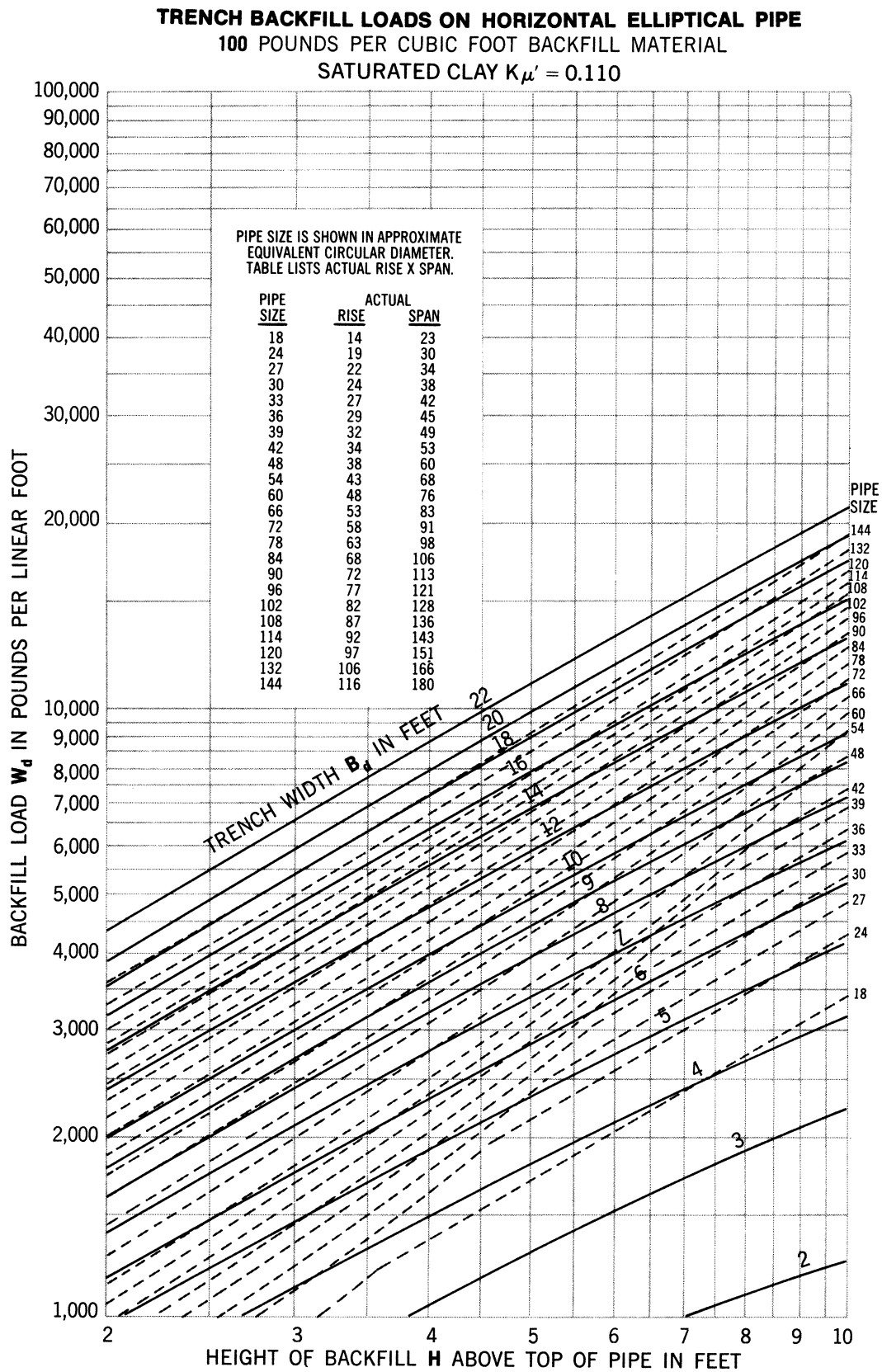
Figure 168



For backfill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds per cubic foot, increase 20%; etc.

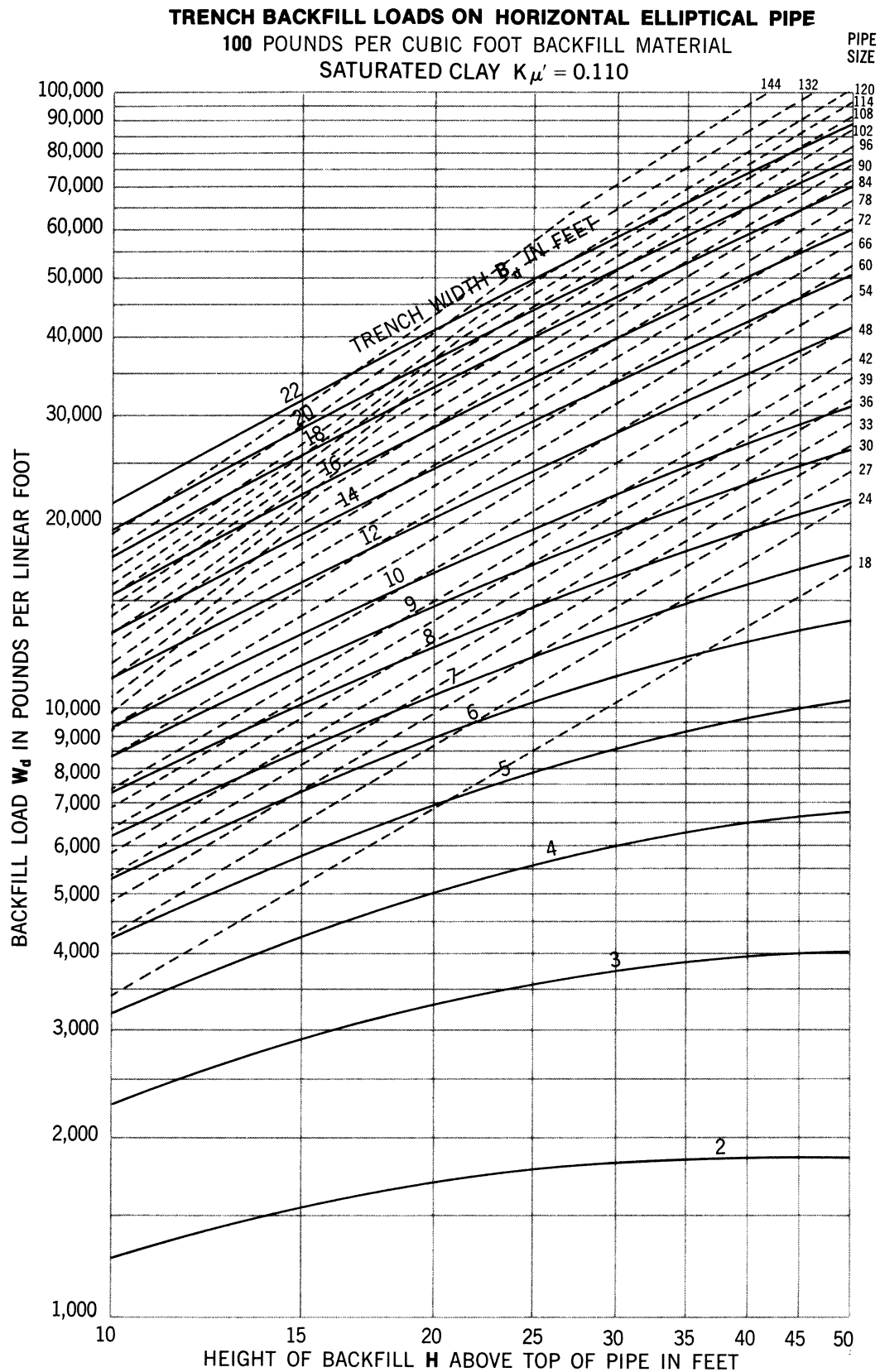
Transition loads and widths based on $K\mu = 0.19$, $r_{sd} = 0.7$ and $p = 0.7$ in the embankment equation

Figure 169



For backfill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds per cubic foot, increase 20%; etc.
 Transition loads and widths based on $K_{\mu} = 0.19$, $r_{sd} = 0.7$ and $p = 0.7$ in the embankment equation

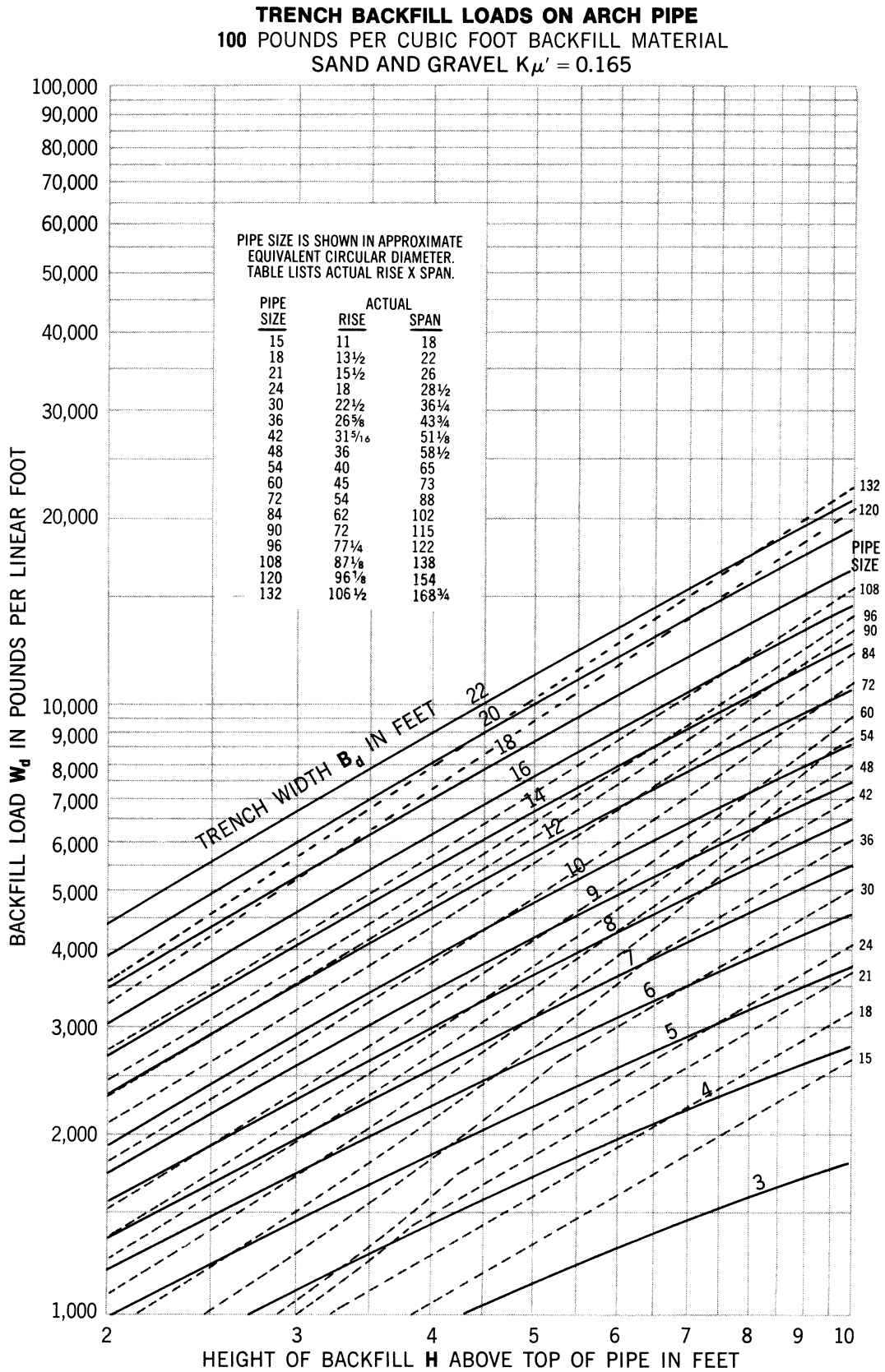
Figure 170



For backfill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds per cubic foot, increase 20%; etc.

Transition loads and widths based on $K_{\mu} = 0.19$, $r_{sd} = 0.7$ and $p = 0.7$ in the embankment equation

Figure 171



For backfill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds per cubic foot, increase 20%; etc.

Transition loads and widths based on $K_{\mu} = 0.19$, $r_{sd} = 0.7$ and $p = 0.7$ in the embankment equation

Figure 172

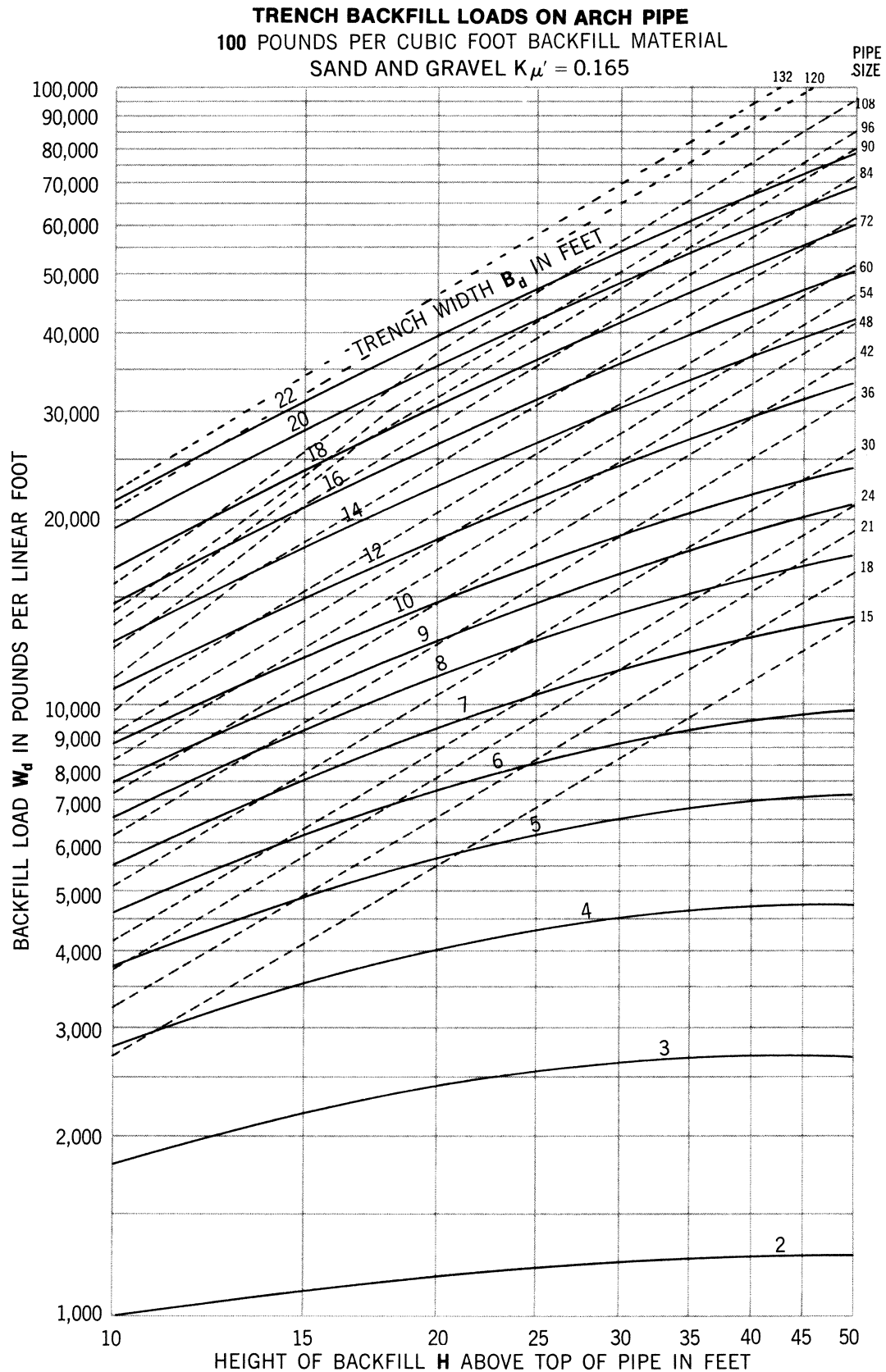
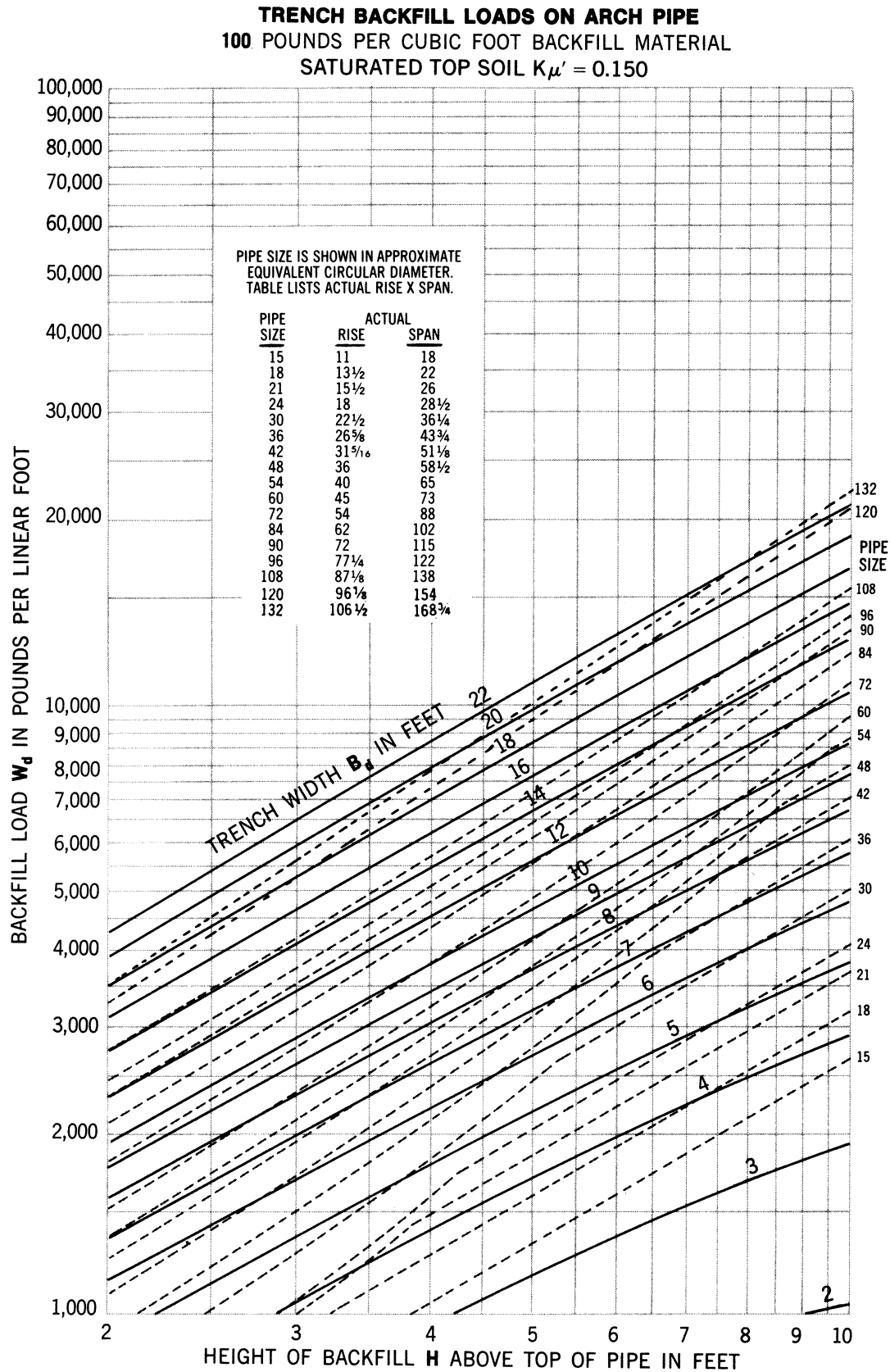
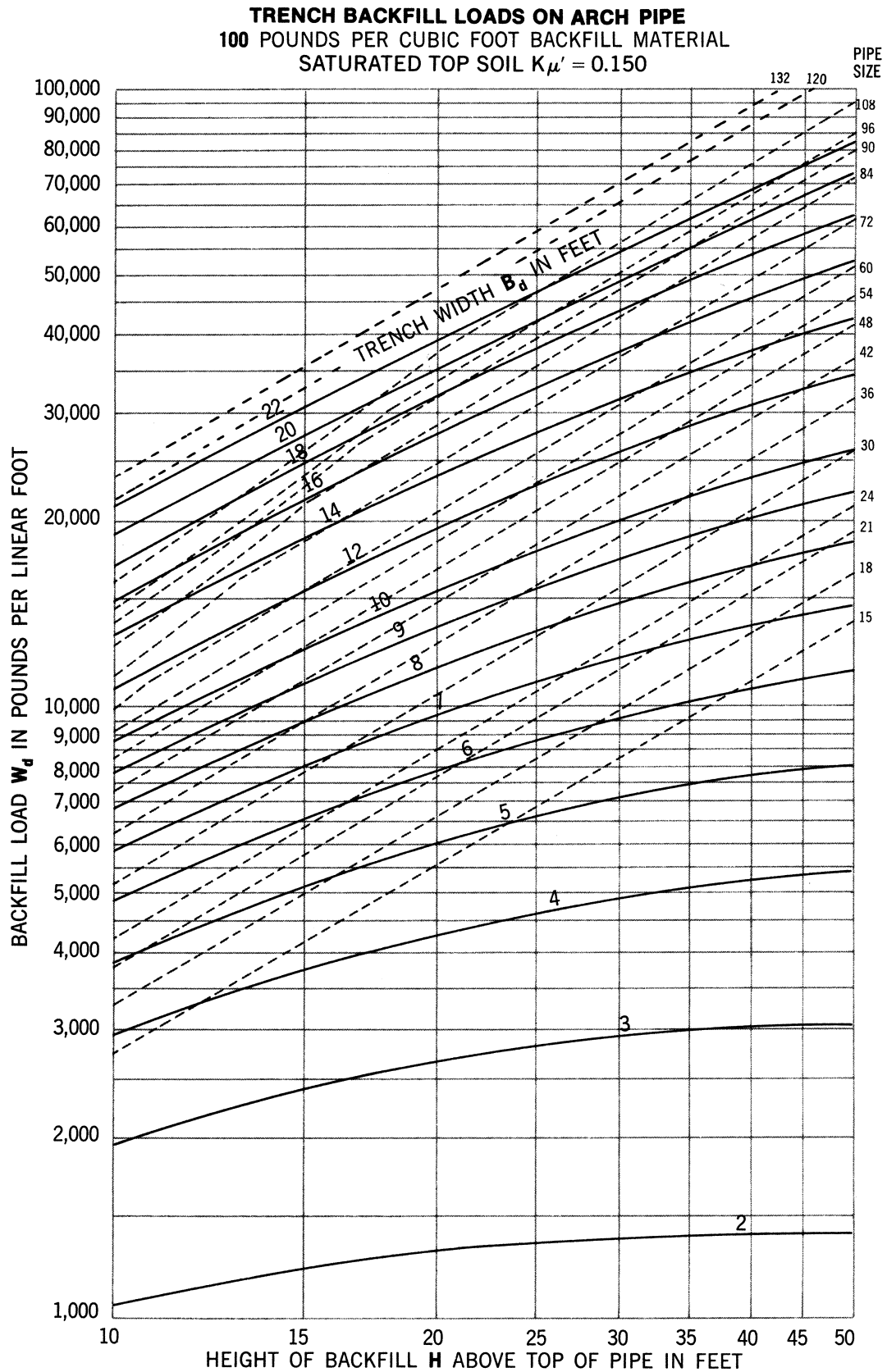


Figure 173



For backfill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds per cubic foot, increase 20%, etc.
 Transition loads and widths based on $K_{\mu} = 0.19$, $r_{sd} = 0.7$ and $p = 0.7$ in the embankment equation

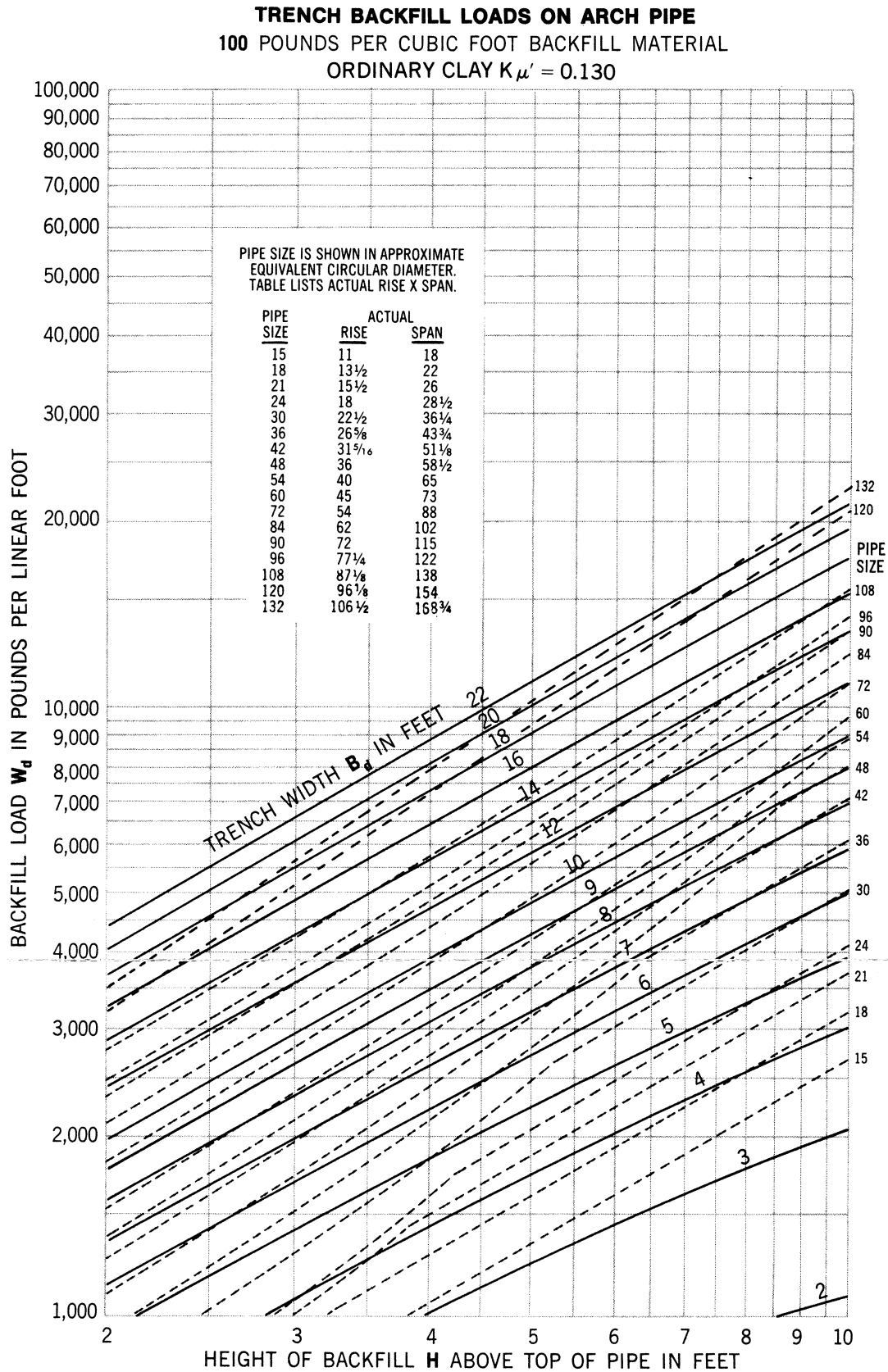
Figure 174



For backfill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds per cubic foot, increase 20%; etc.

Transition loads and widths based on $K_{\mu} = 0.19$, $r_{sd} = 0.7$ and $p = 0.7$ in the embankment equation

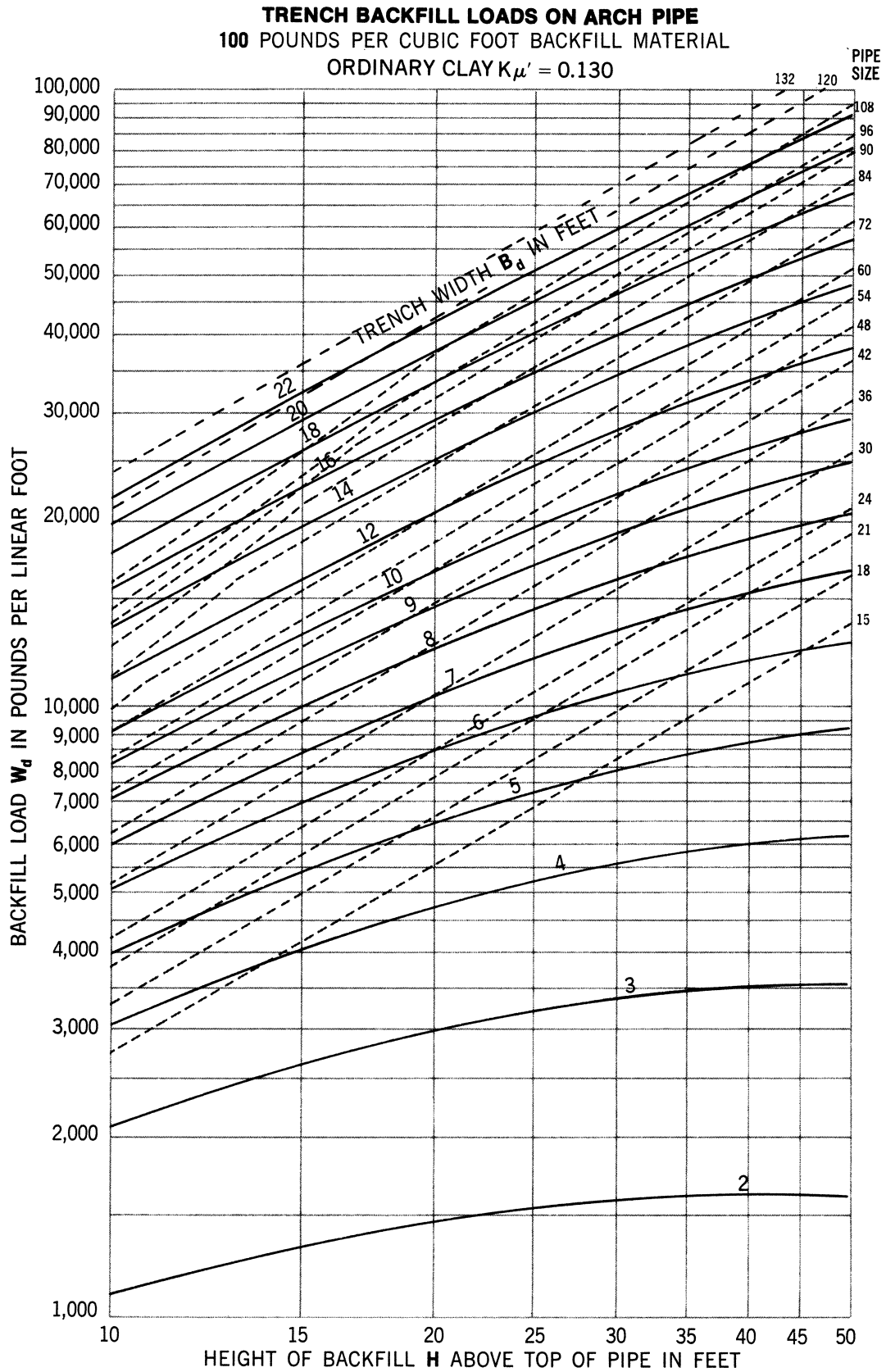
Figure 175



For backfill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds per cubic foot, increase 20%; etc.

Transition loads and widths based on $K_{\mu} = 0.19$, $r_{sd} = 0.7$ and $p = 0.7$ in the embankment equation

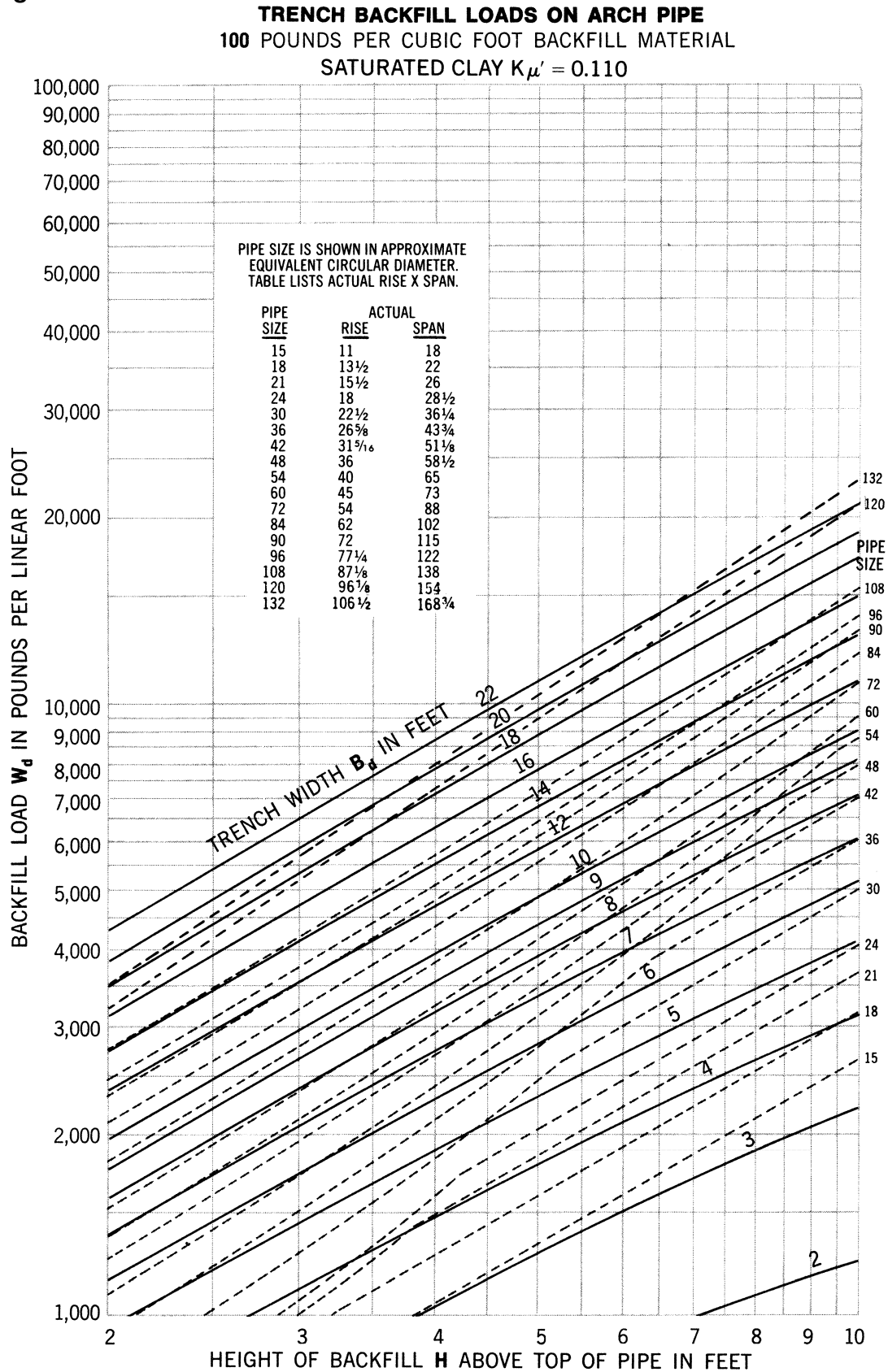
Figure 176



For backfill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds per cubic foot, increase 20%; etc.

Transition loads and widths based on $K_{\mu} = 0.19$, $r_{sd} = 0.7$ and $p = 0.7$ in the embankment equation

Figure 177



For backfill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds per cubic foot, increase 20%; etc.

Transition loads and widths based on $K_{\mu} = 0.19$, $r_{sd} = 0.7$ and $p = 0.7$ in the embankment equation

Figure 178

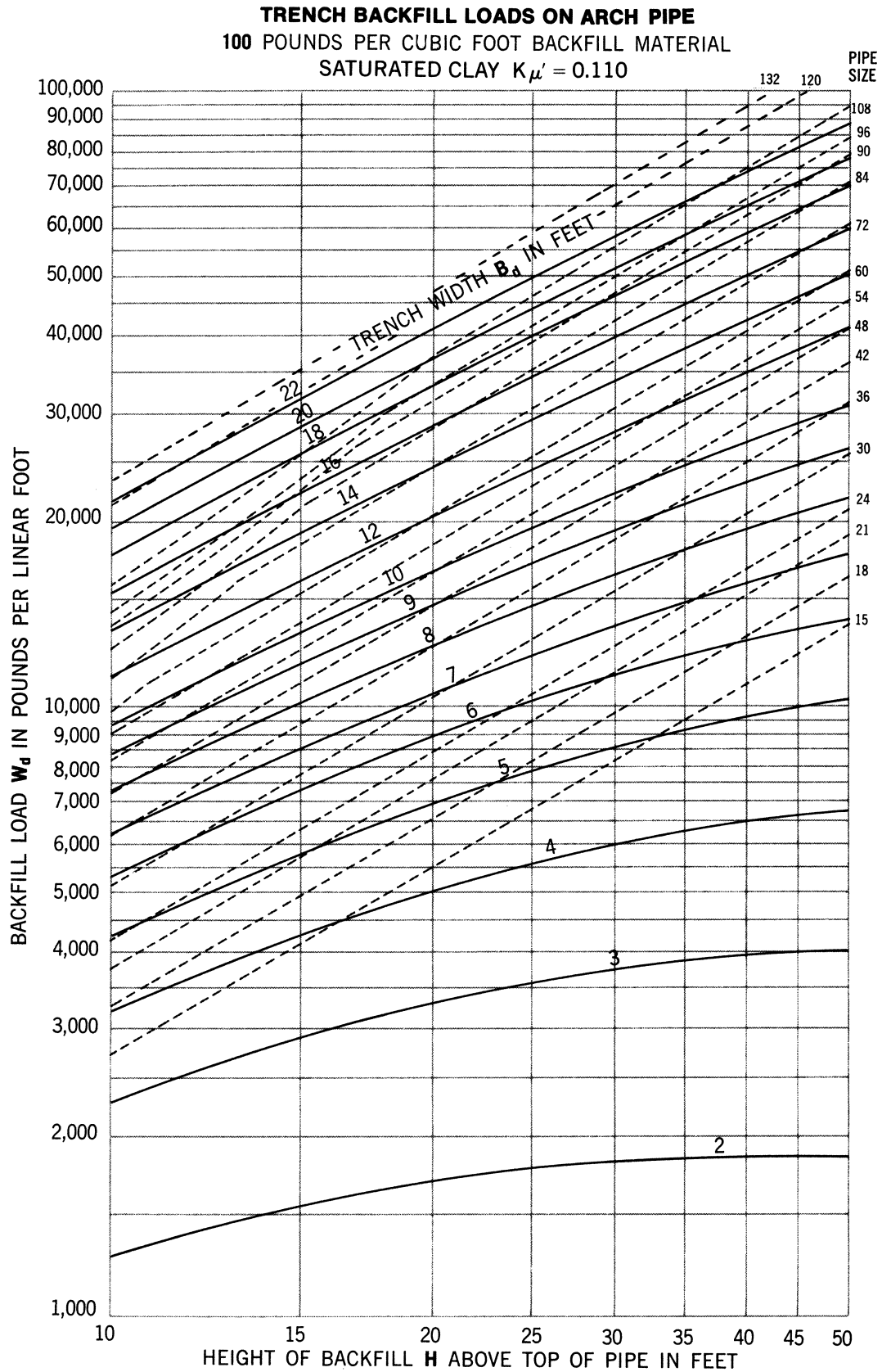
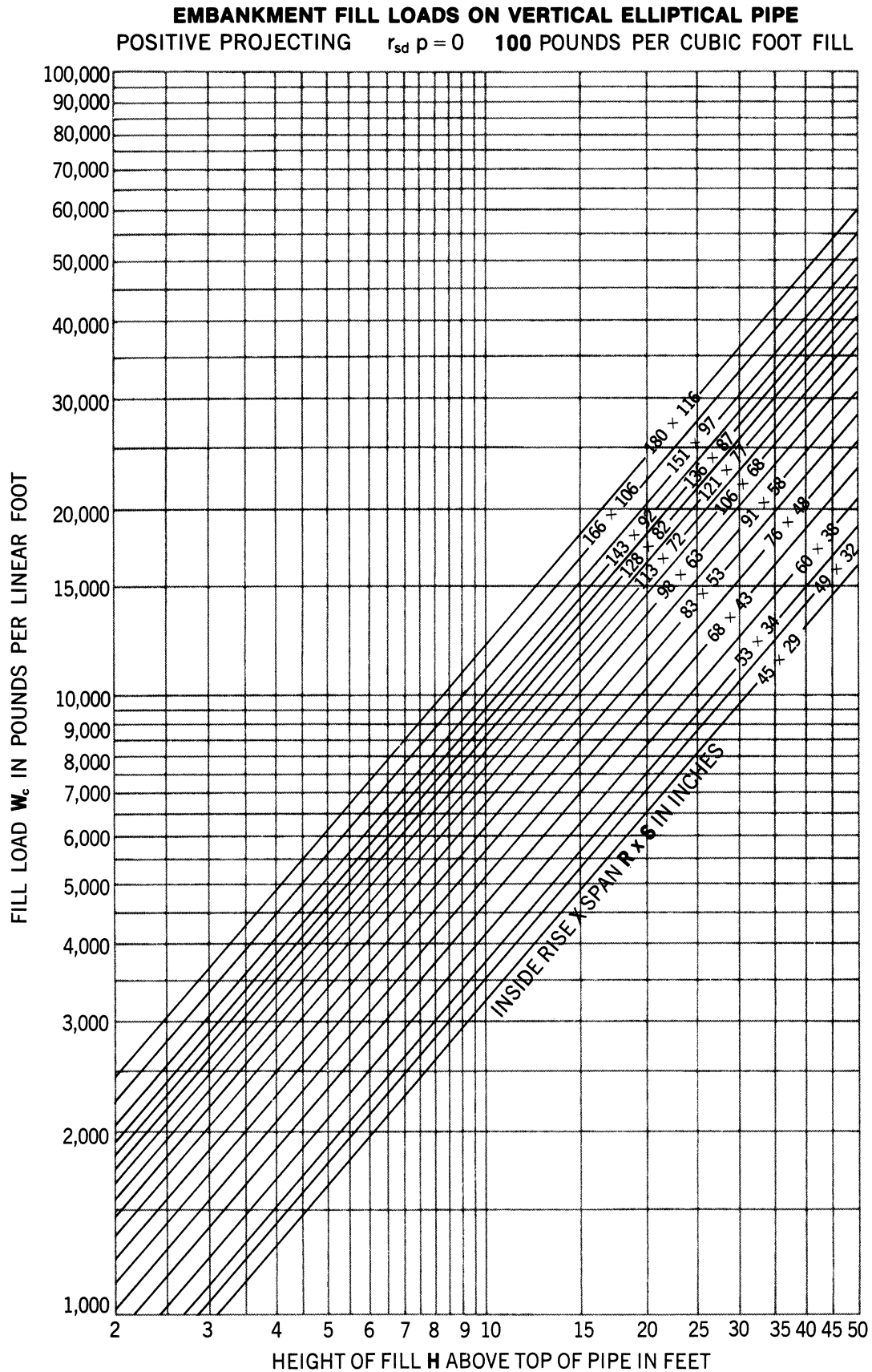
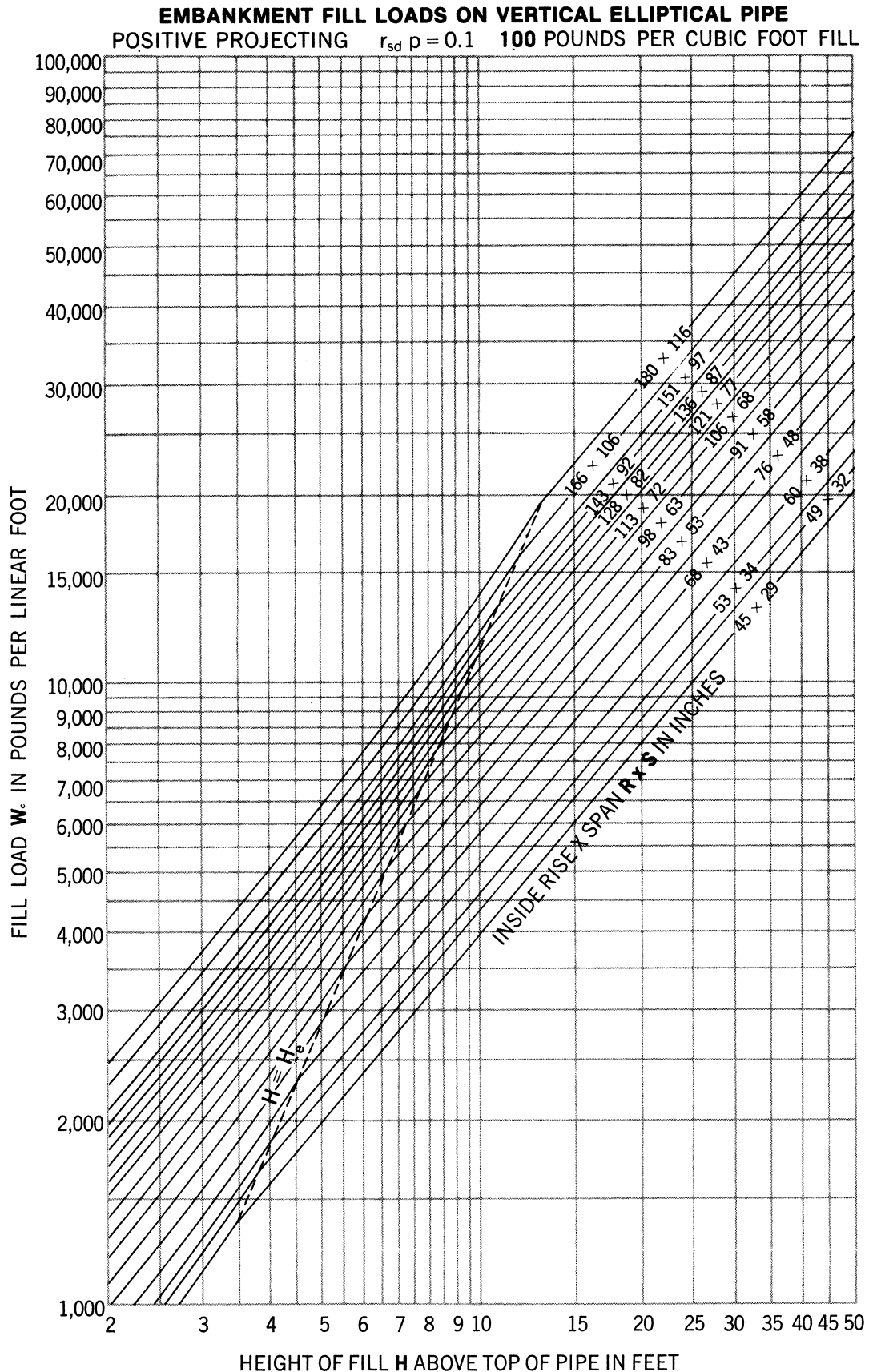


Figure 179



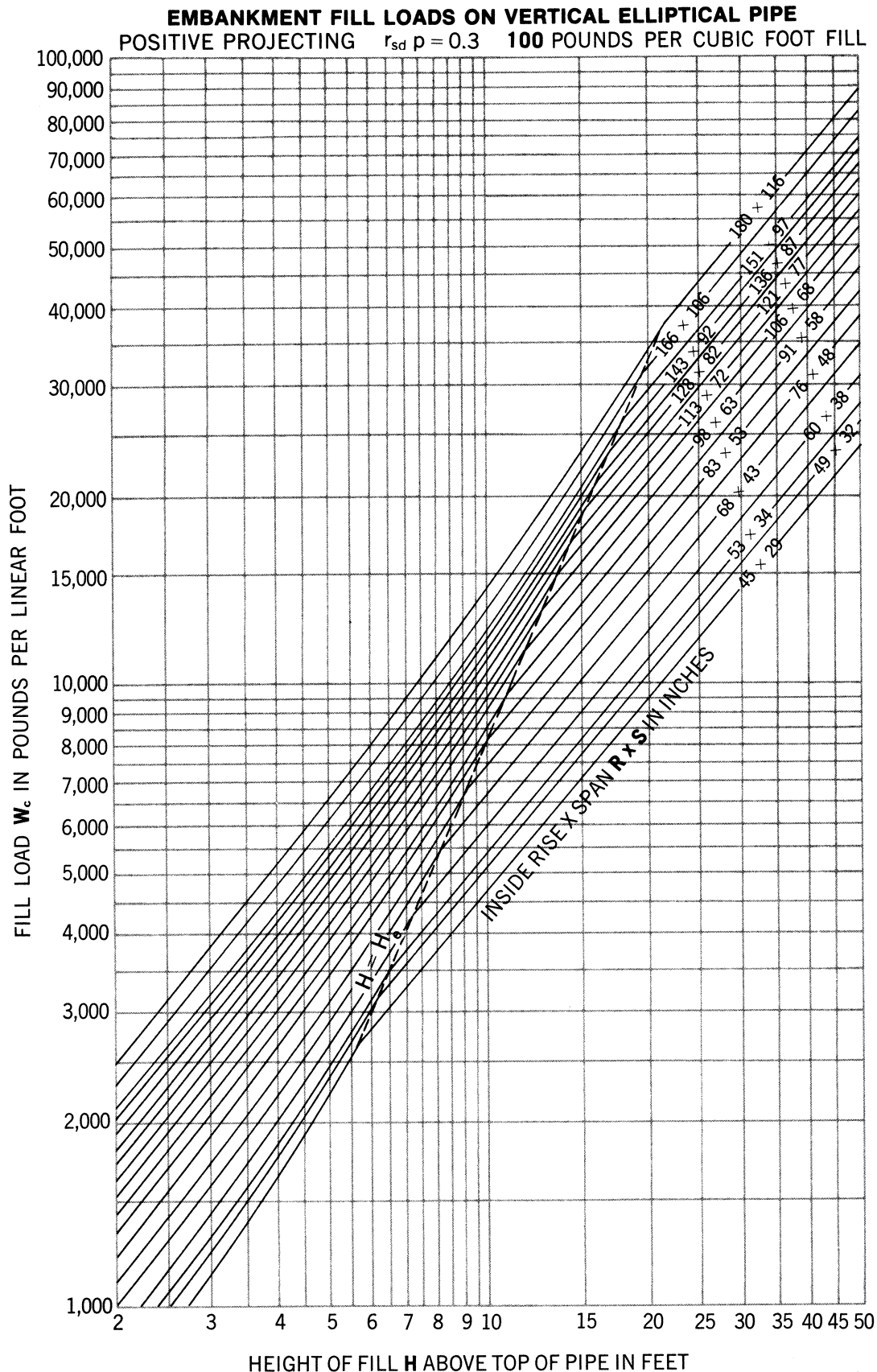
*For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate pipe sizes.*

Figure 180



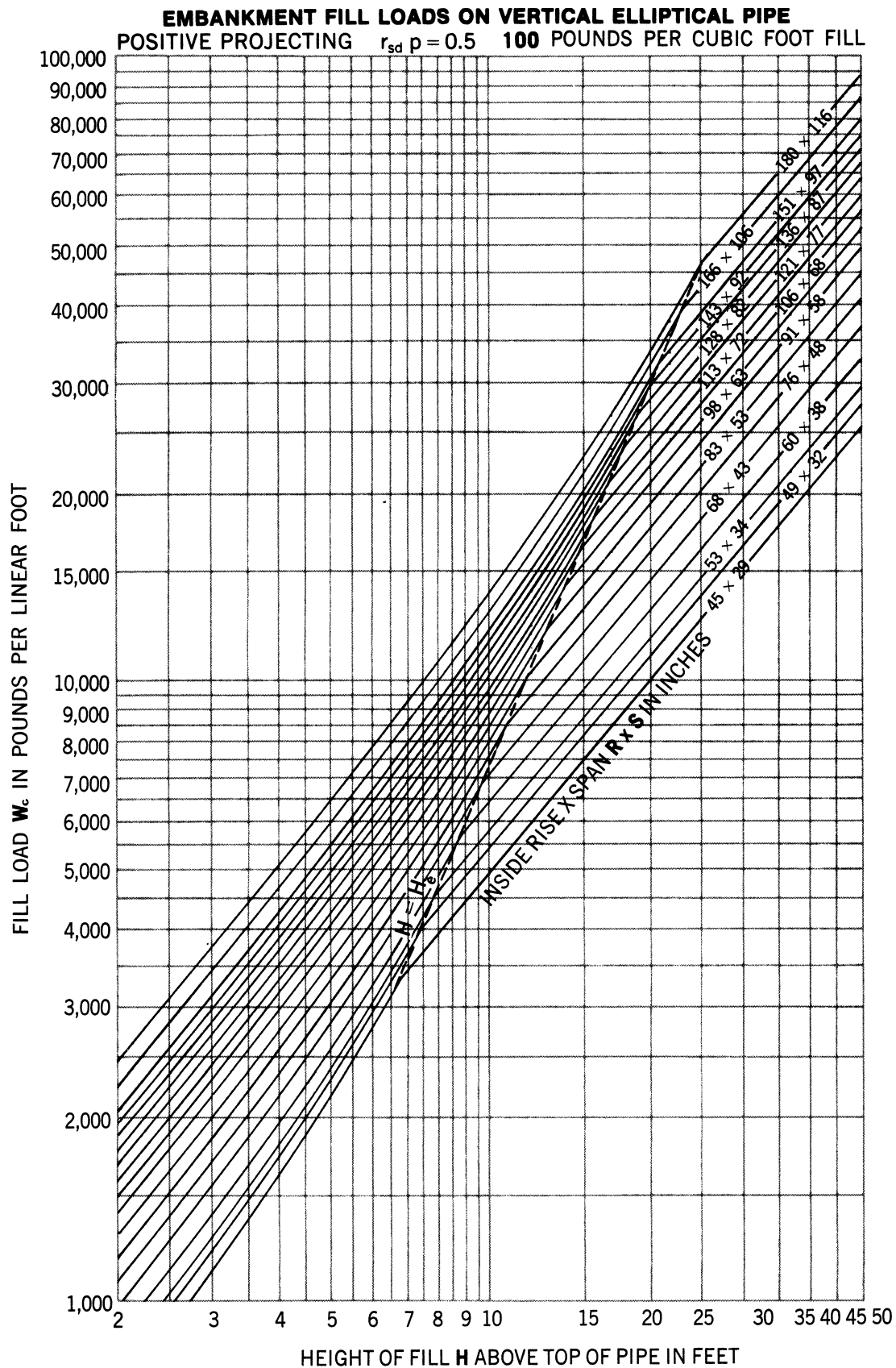
For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate pipe sizes.

Figure 181



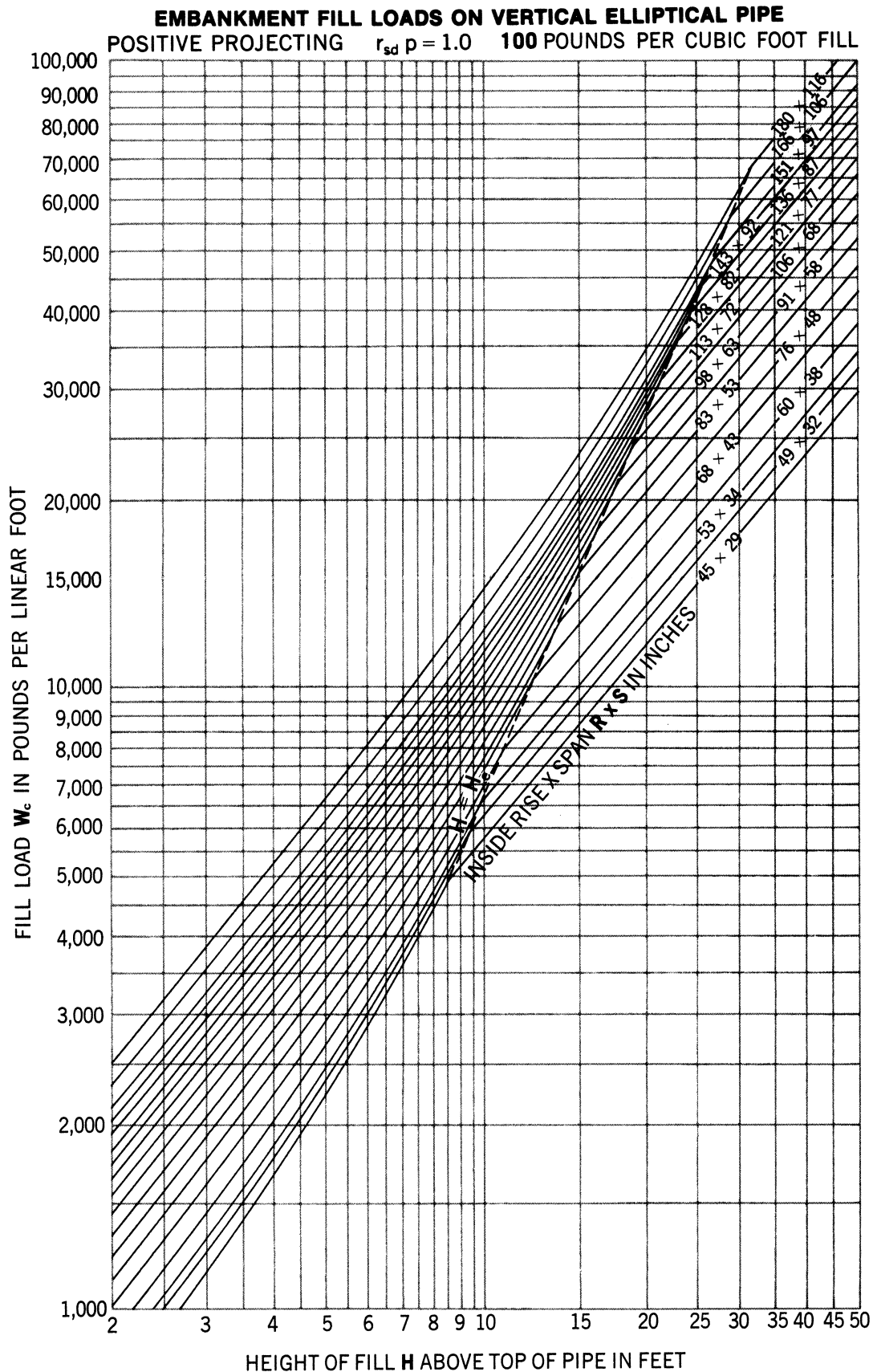
For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate pipe sizes.

Figure 182



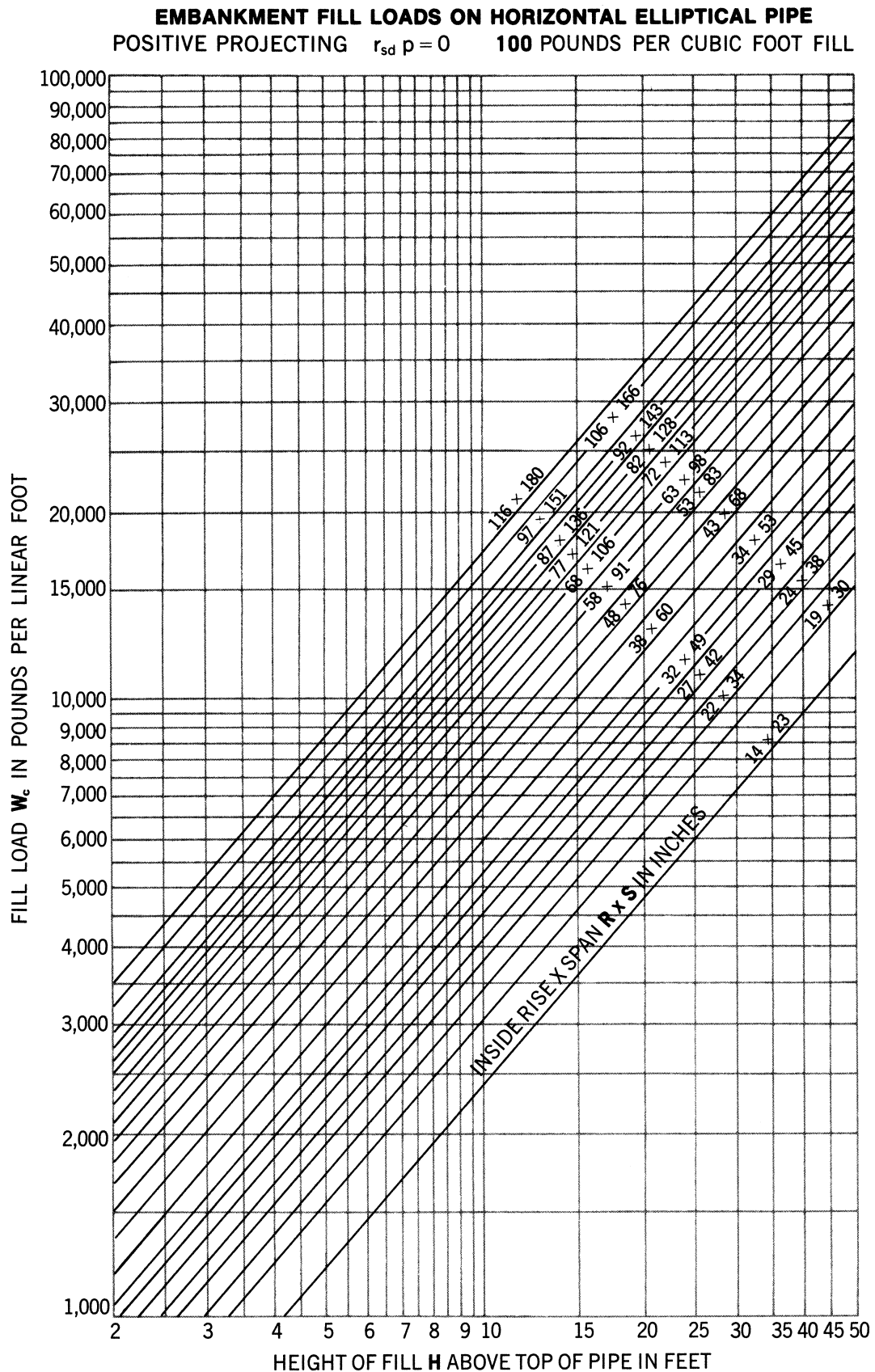
*For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate pipe sizes.*

Figure 183



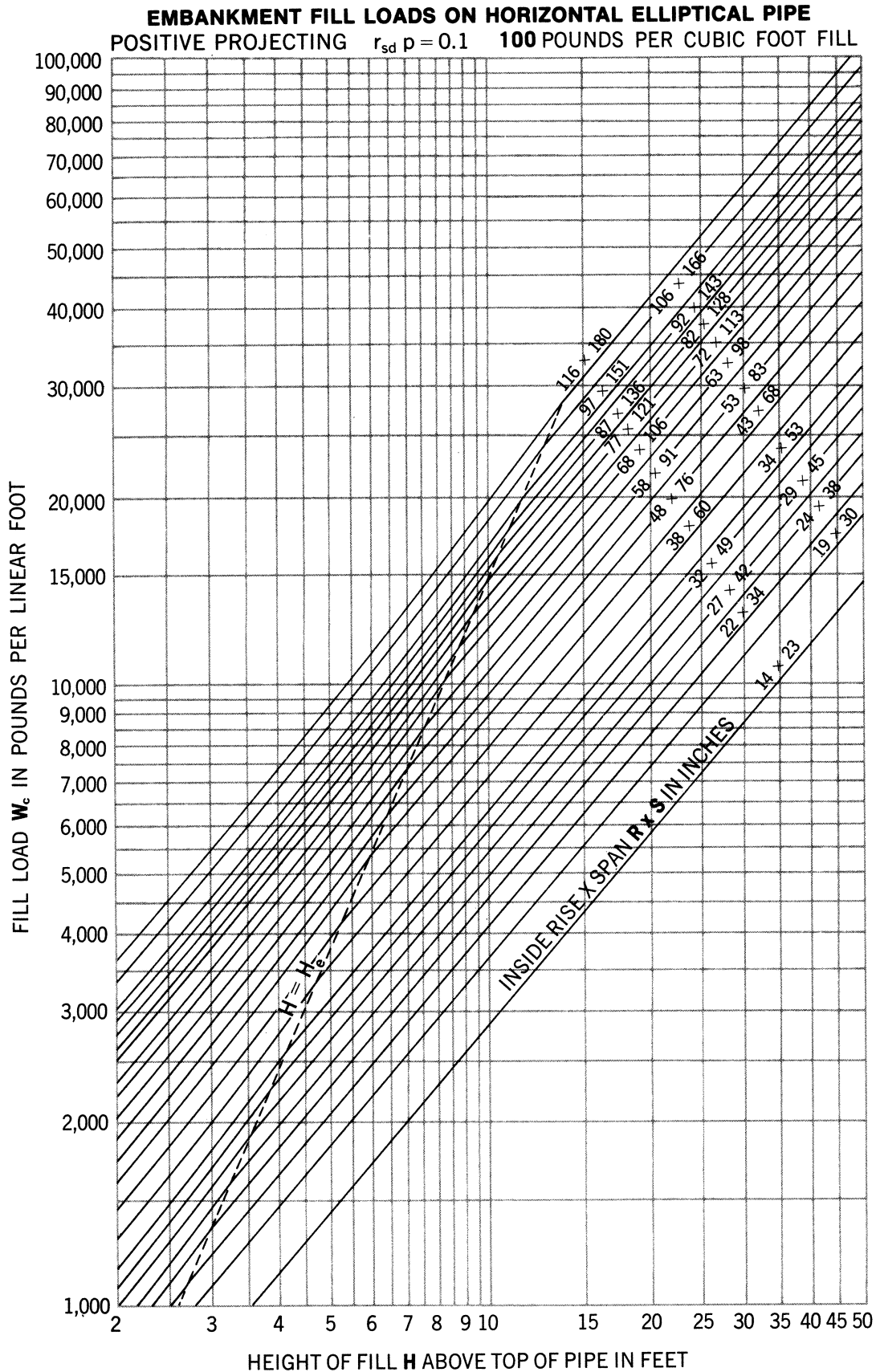
For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase
 Interpolate for intermediate pipe sizes.

Figure 184



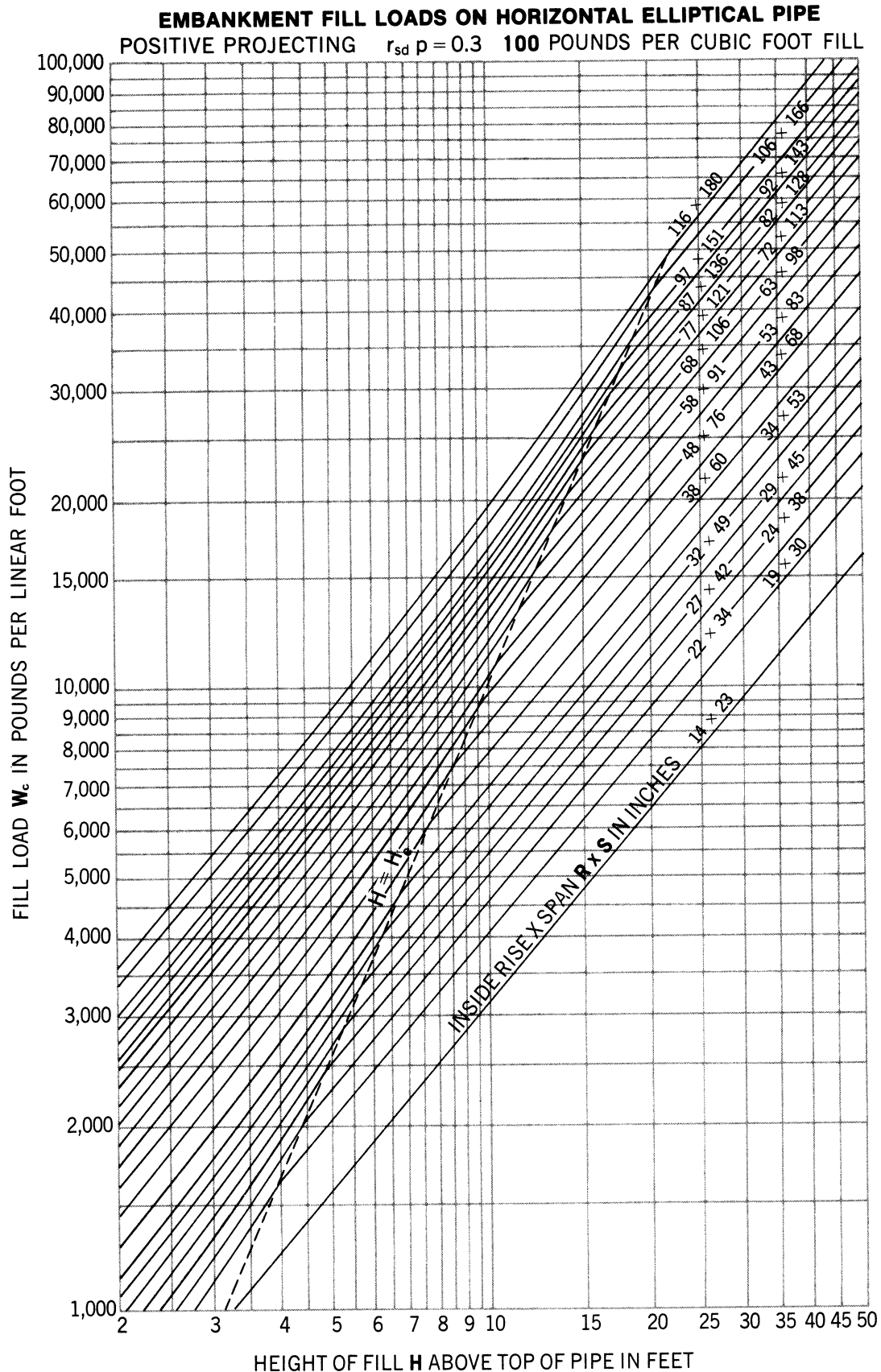
*For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate pipe sizes.*

Figure 185



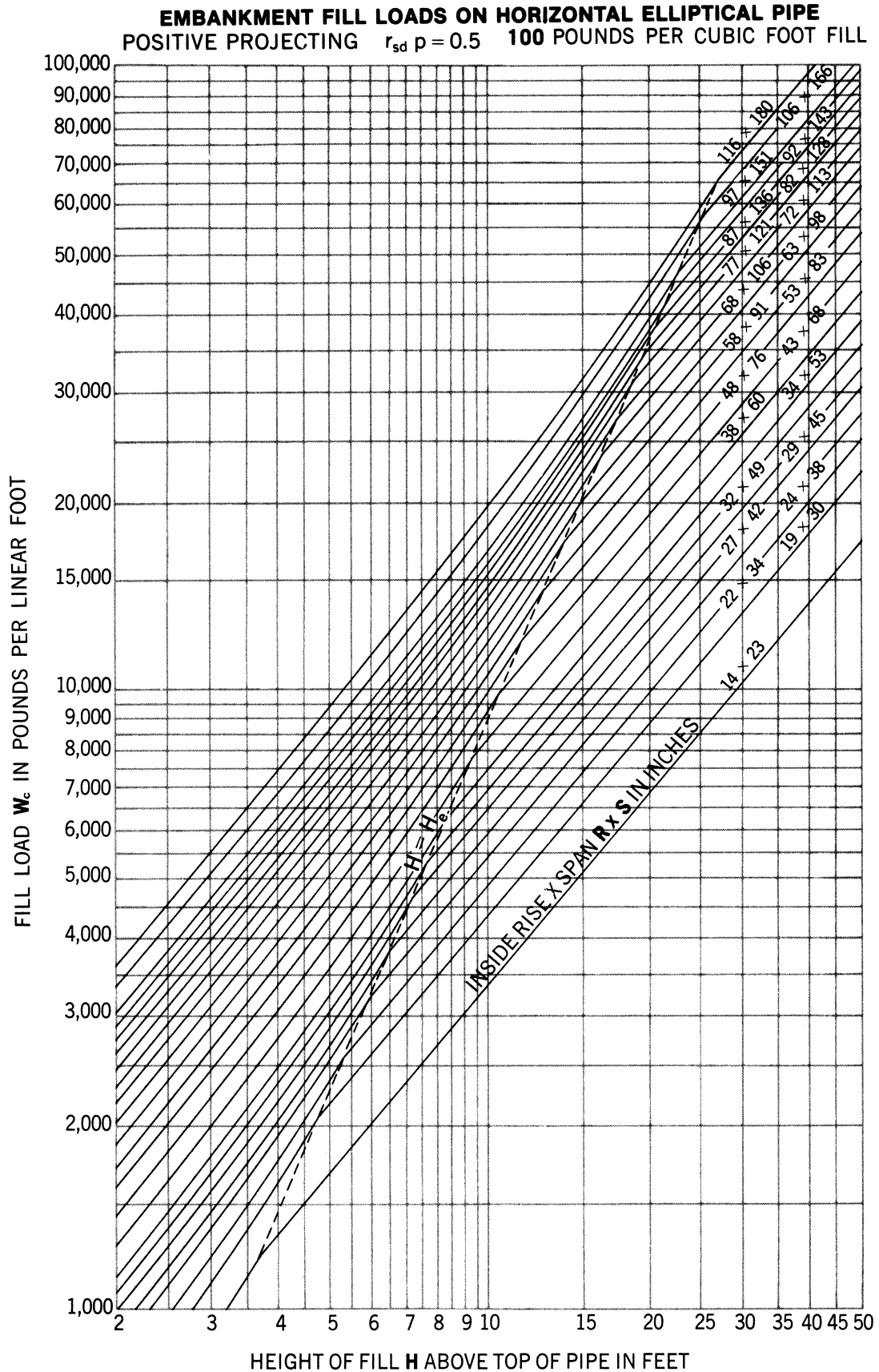
For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate pipe sizes.

Figure 186



For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate pipe sizes.

Figure 187



For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate pipe sizes.

Figure 188

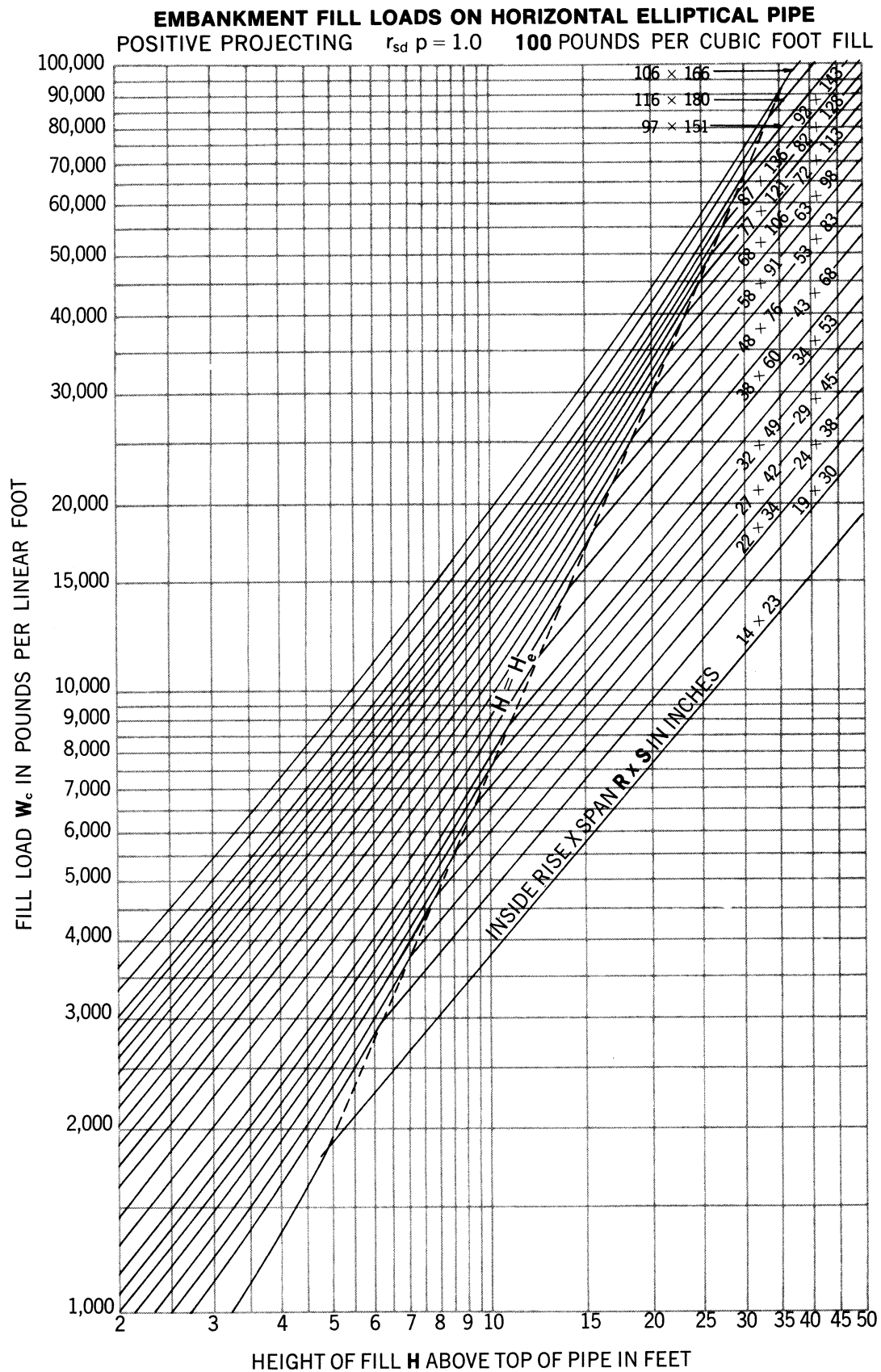
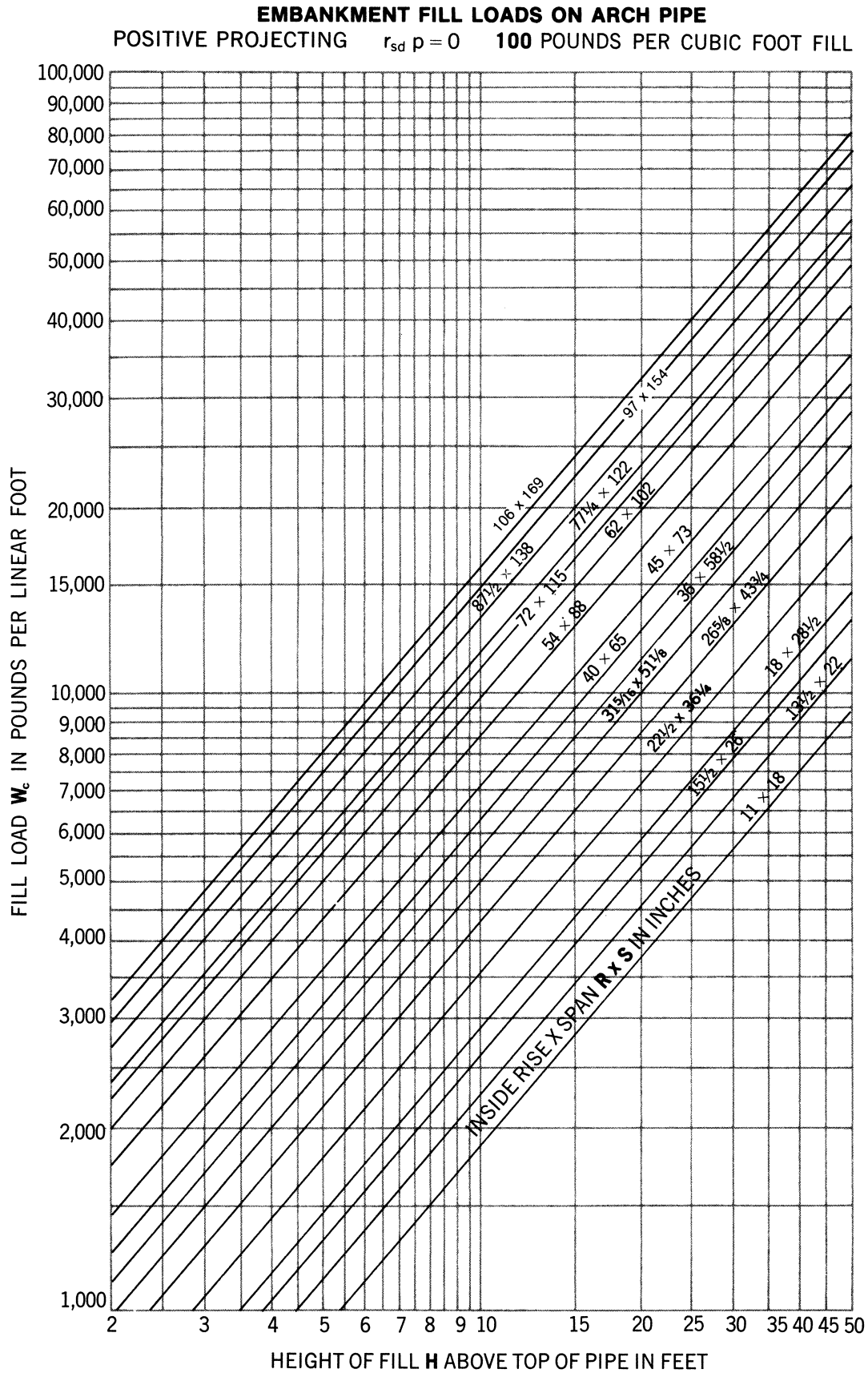
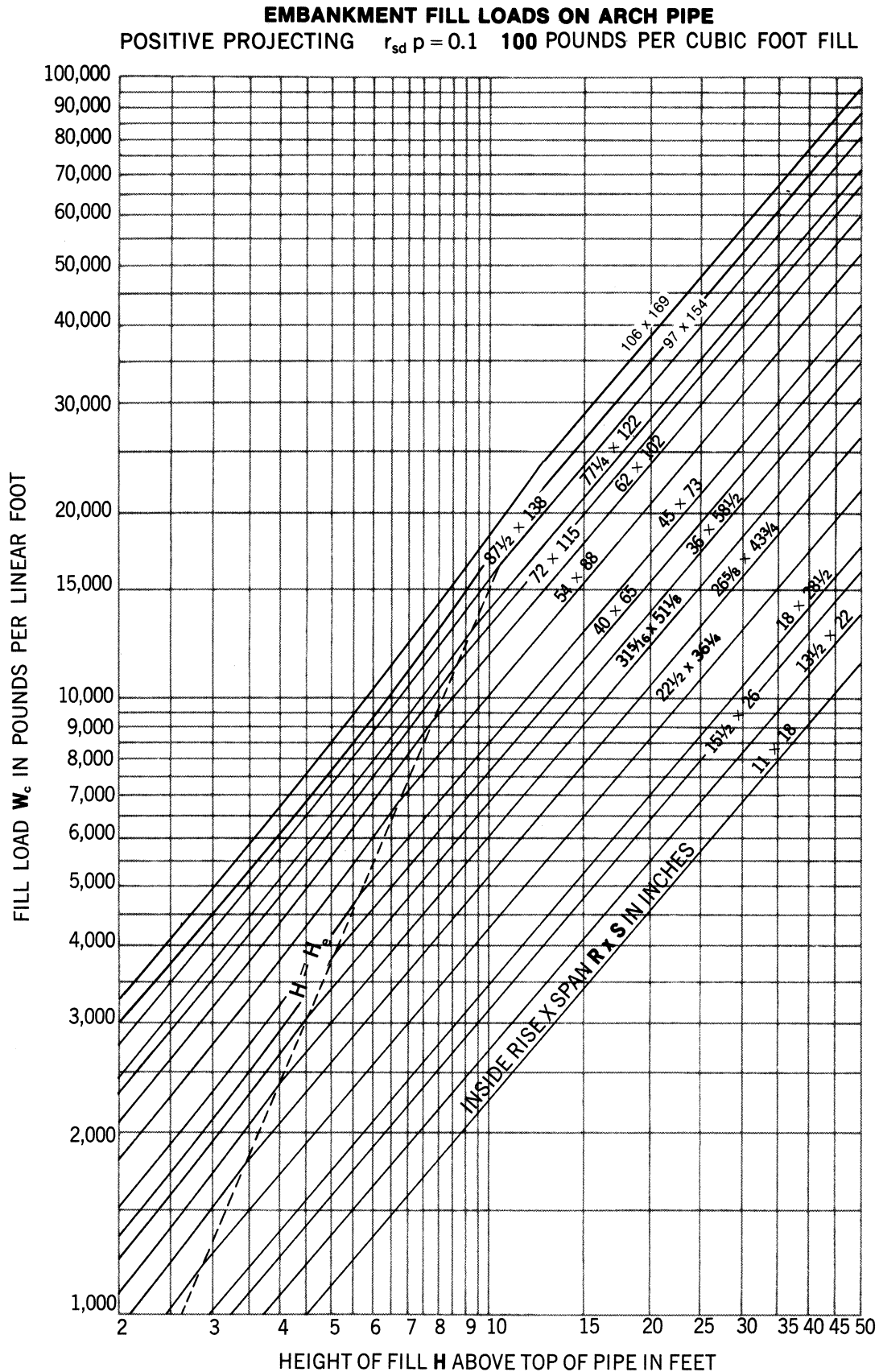


Figure 189



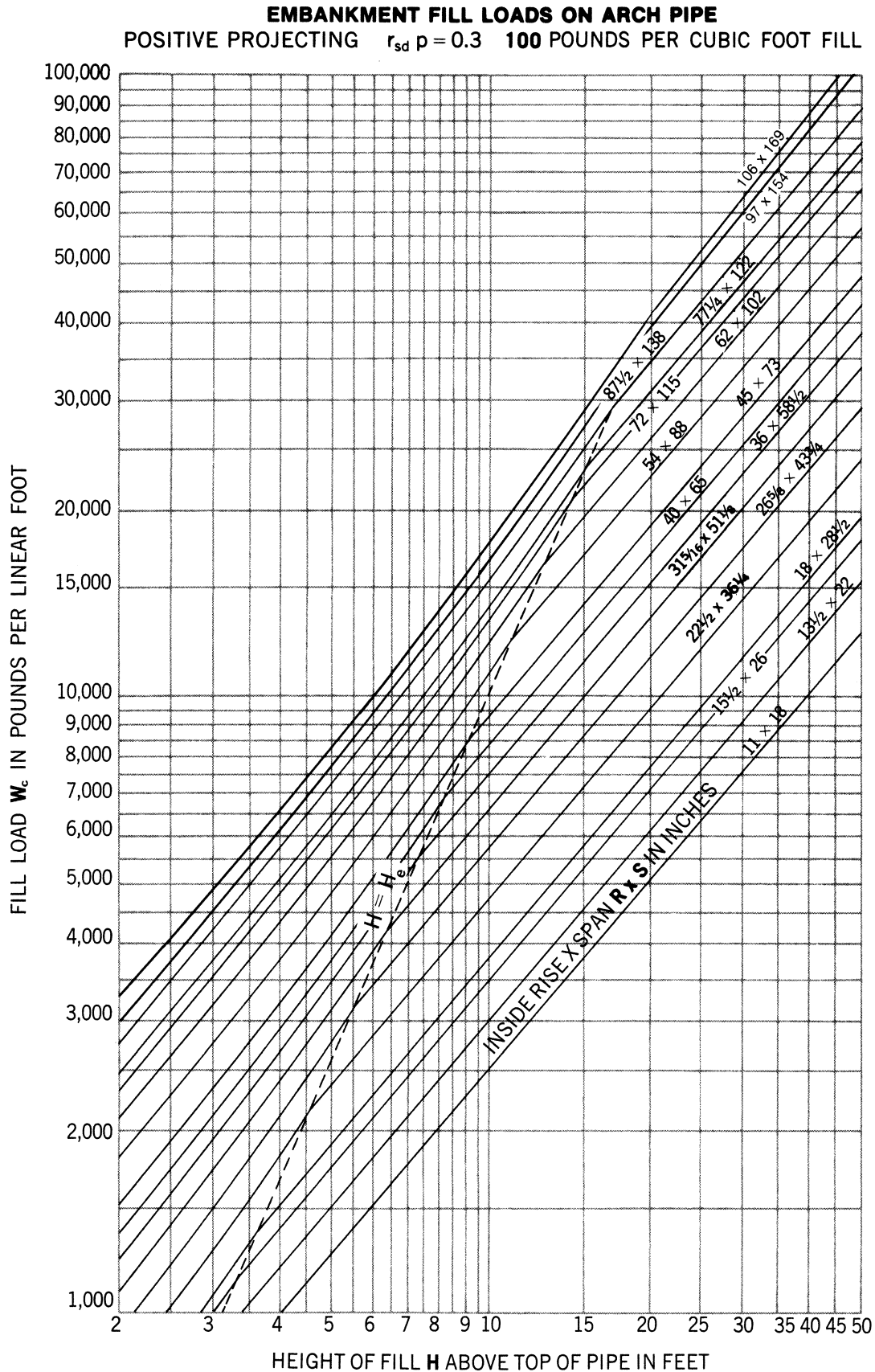
For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate pipe sizes.

Figure 190



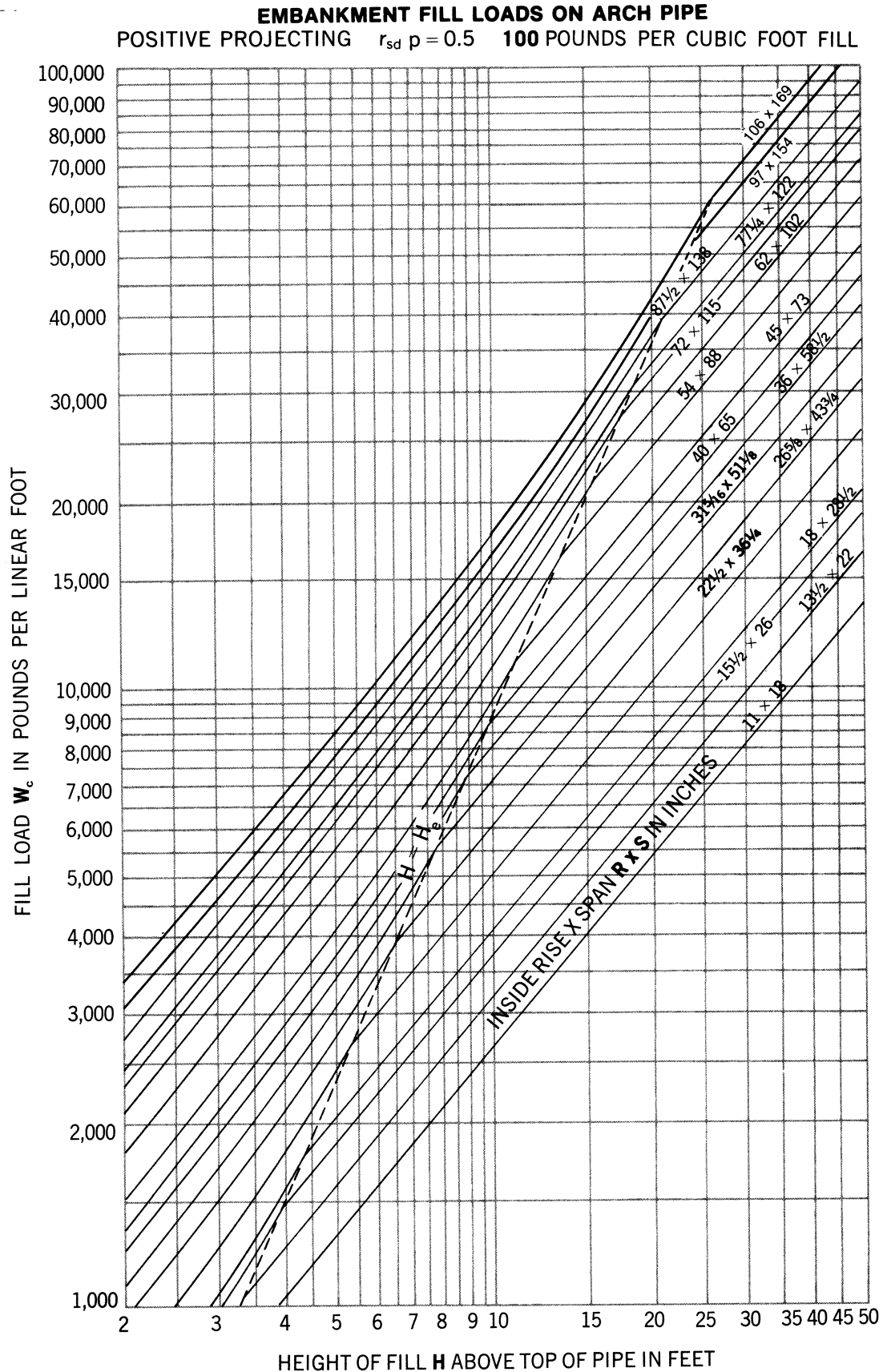
For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate pipe sizes.

Figure 191



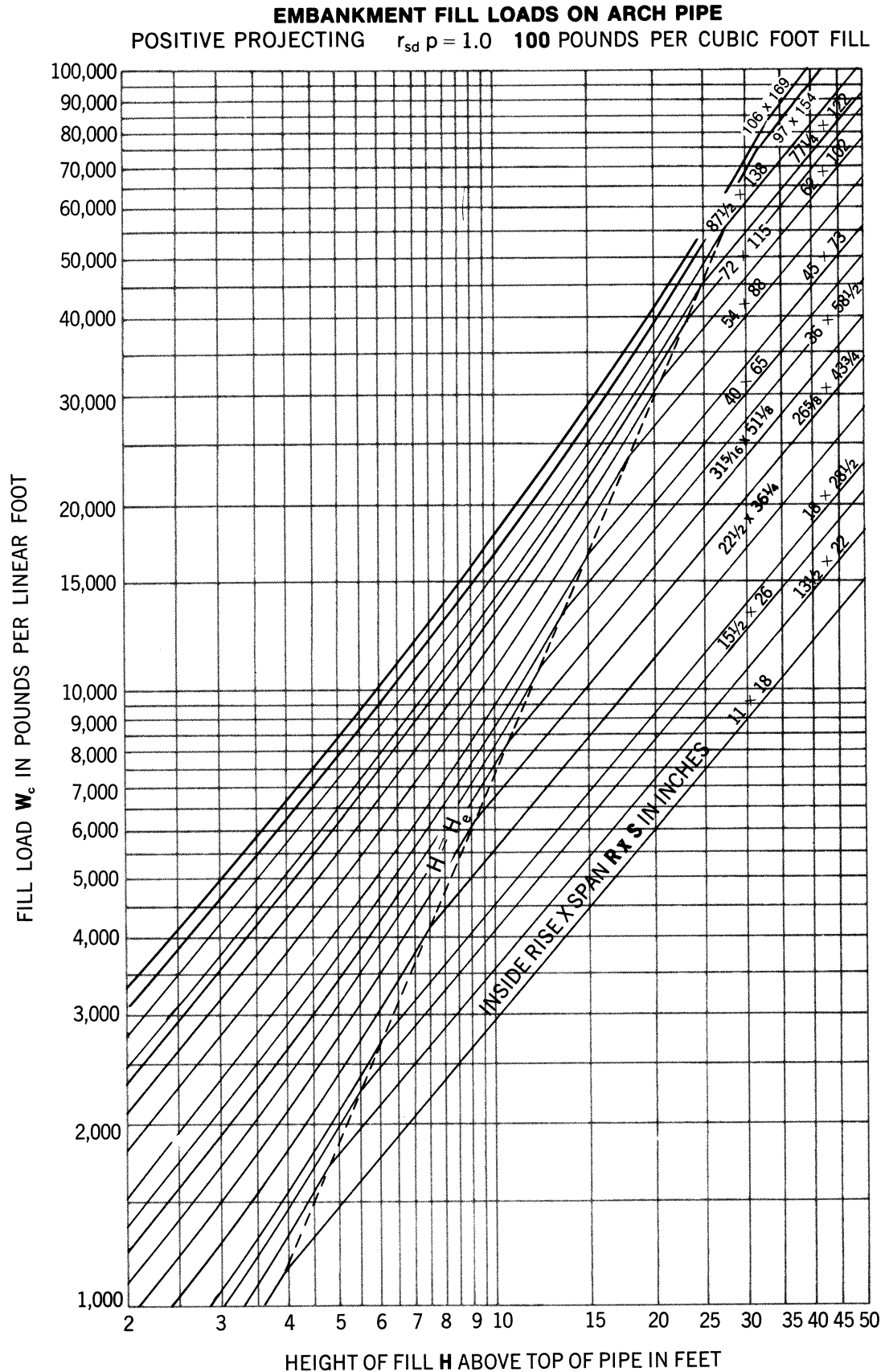
For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate pipe sizes.

Figure 192



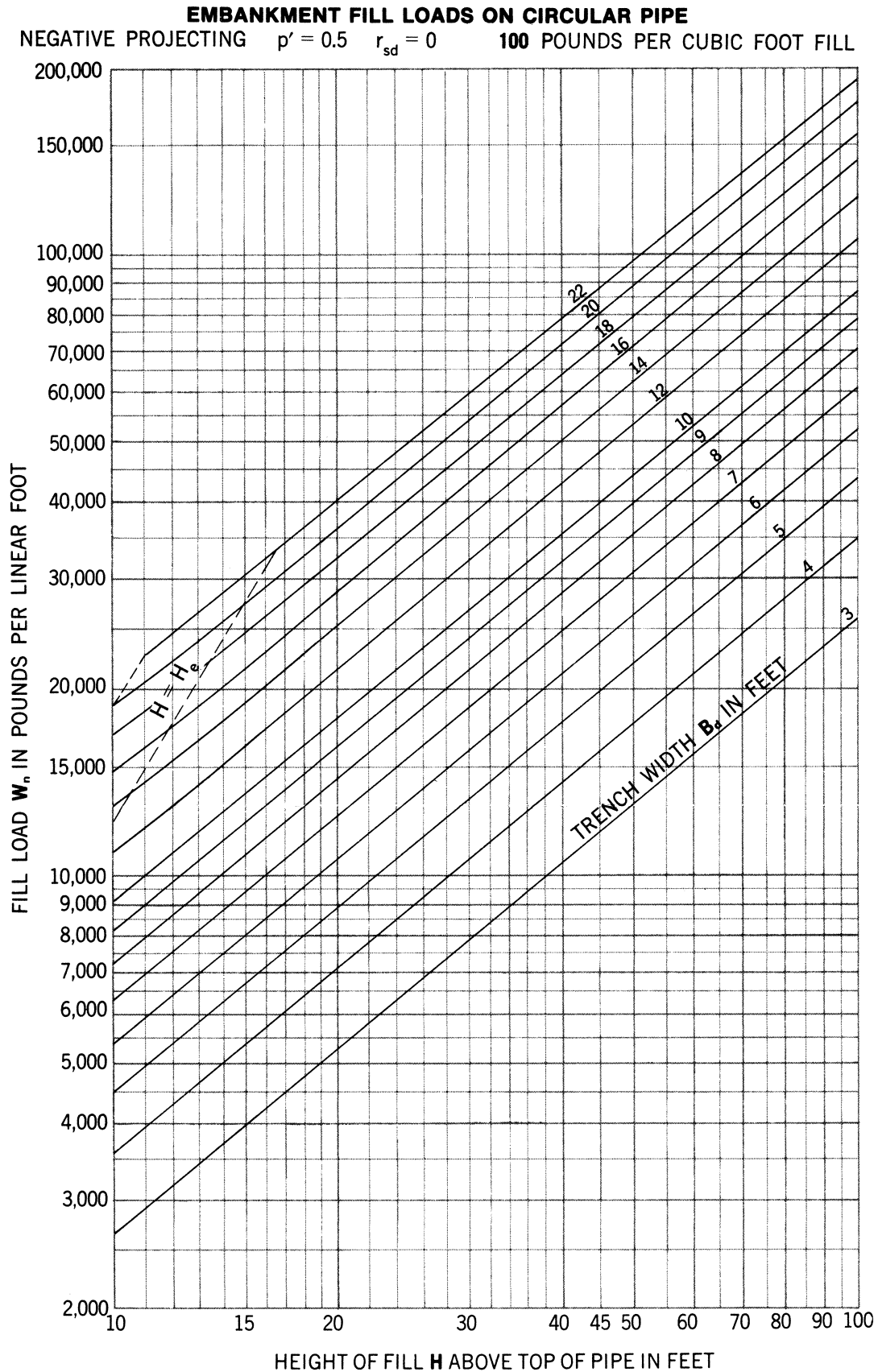
*For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate pipe sizes.*

Figure 193



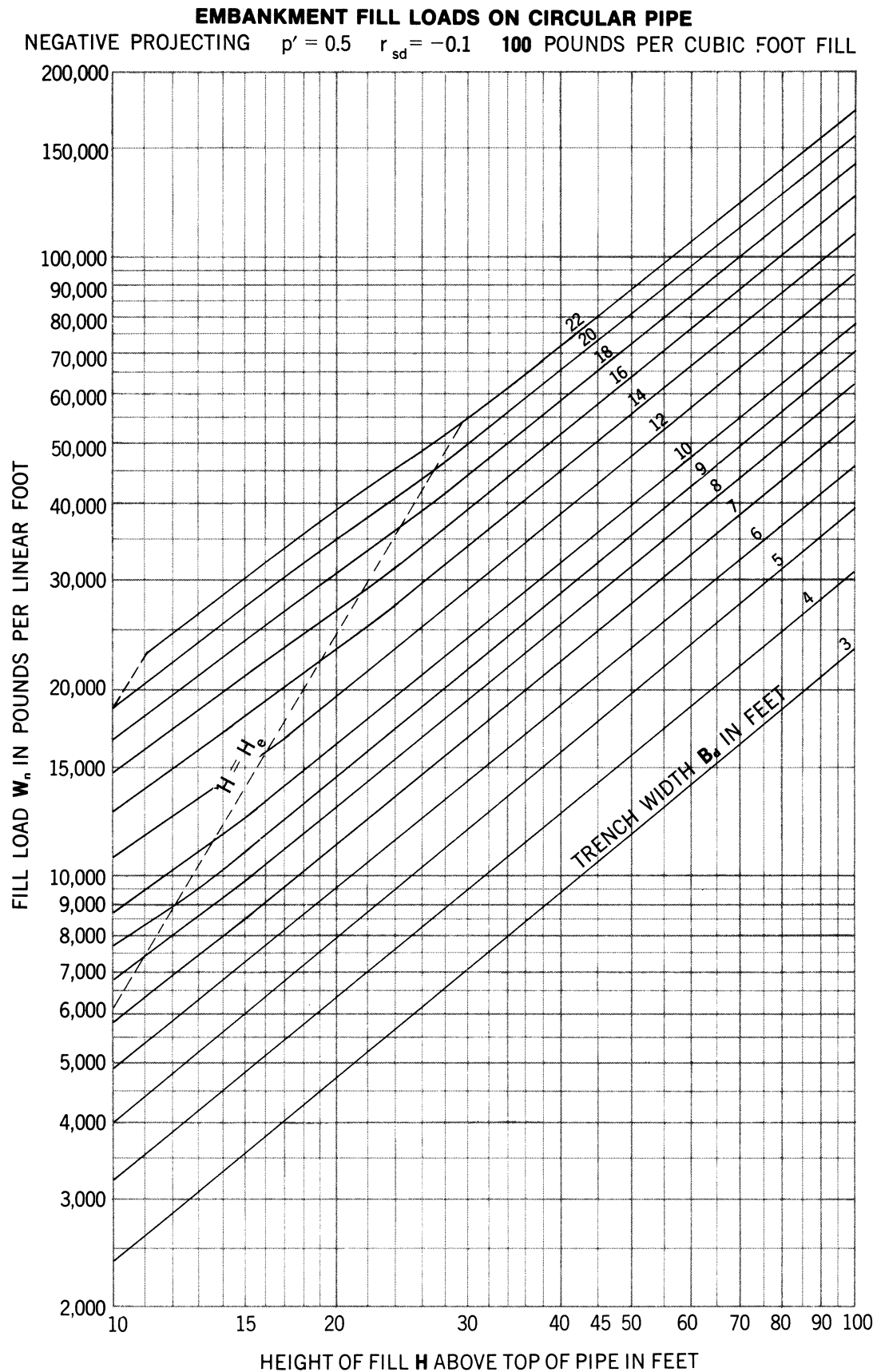
For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate pipe sizes.

Figure 194



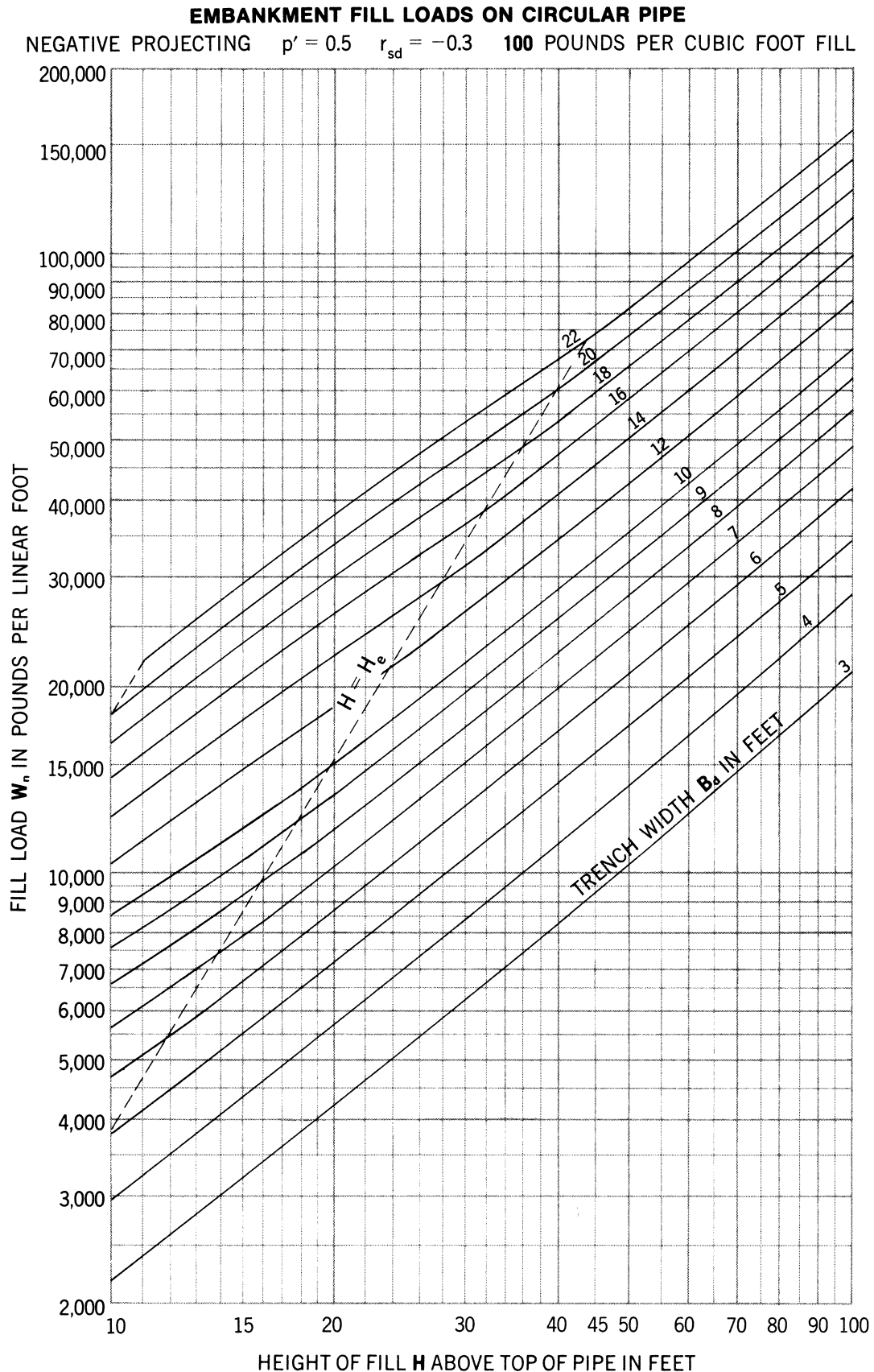
For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate trench widths.

Figure 195



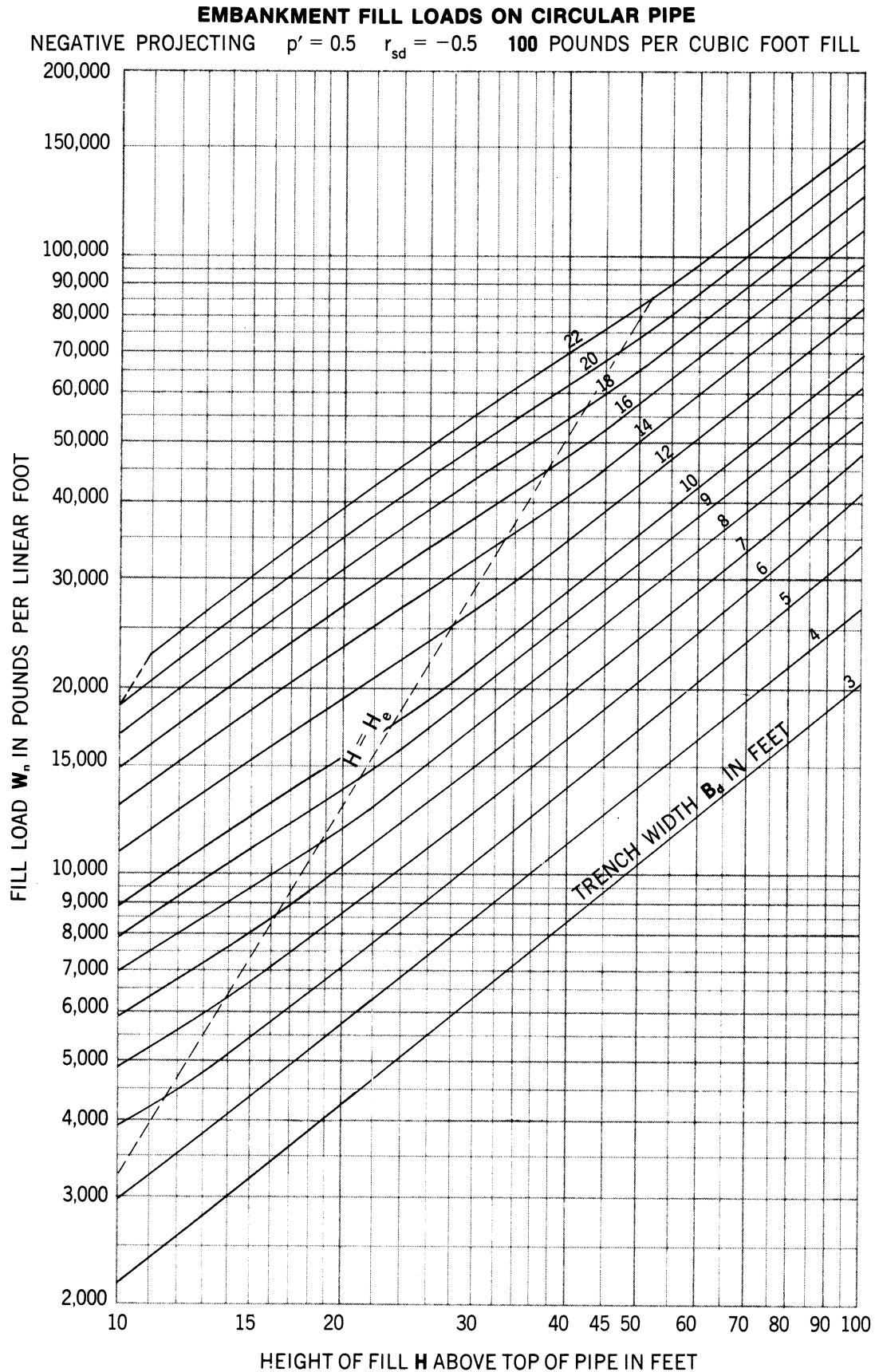
For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate trench widths.

Figure 196



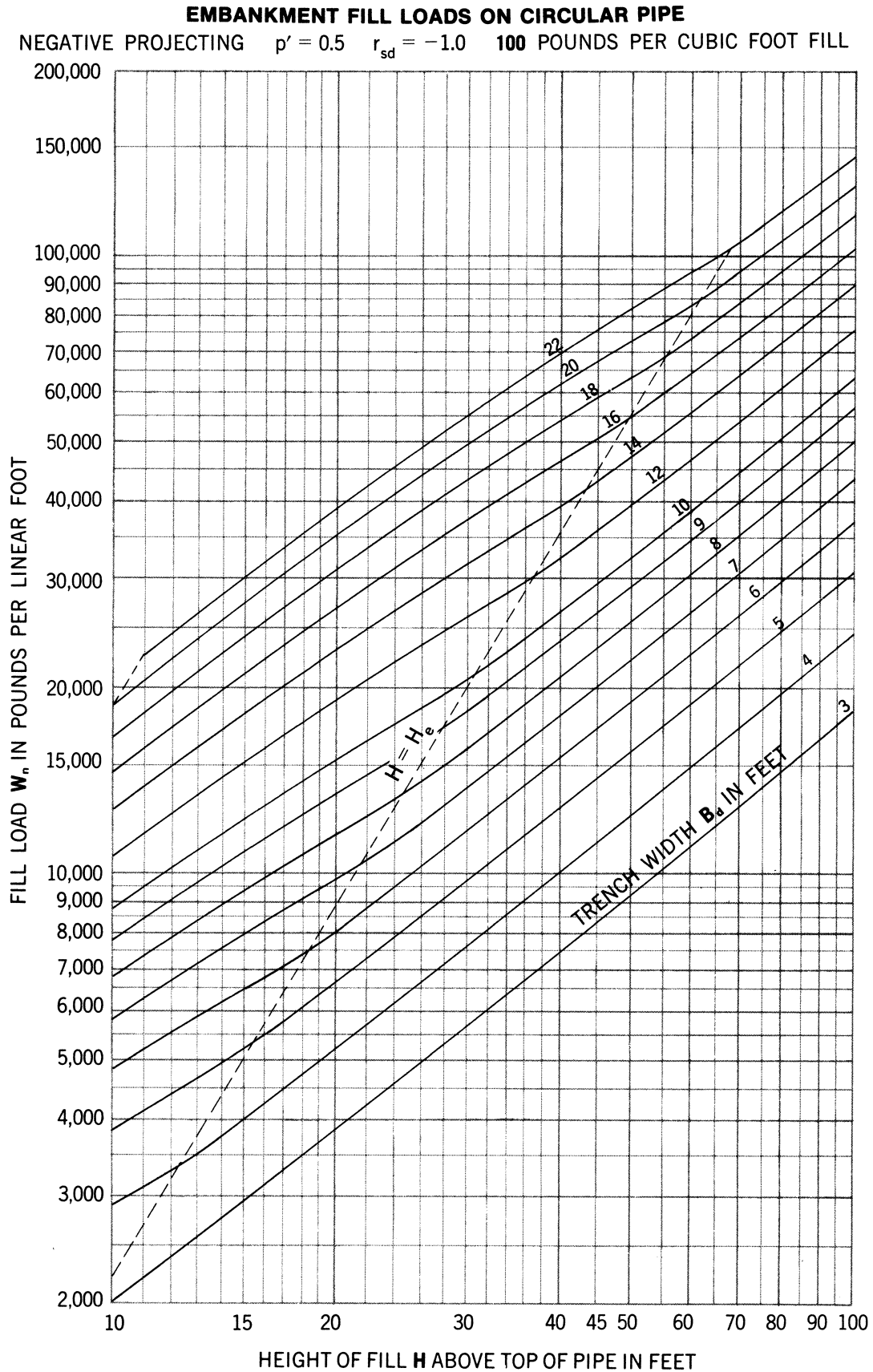
For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate trench widths.

Figure 197



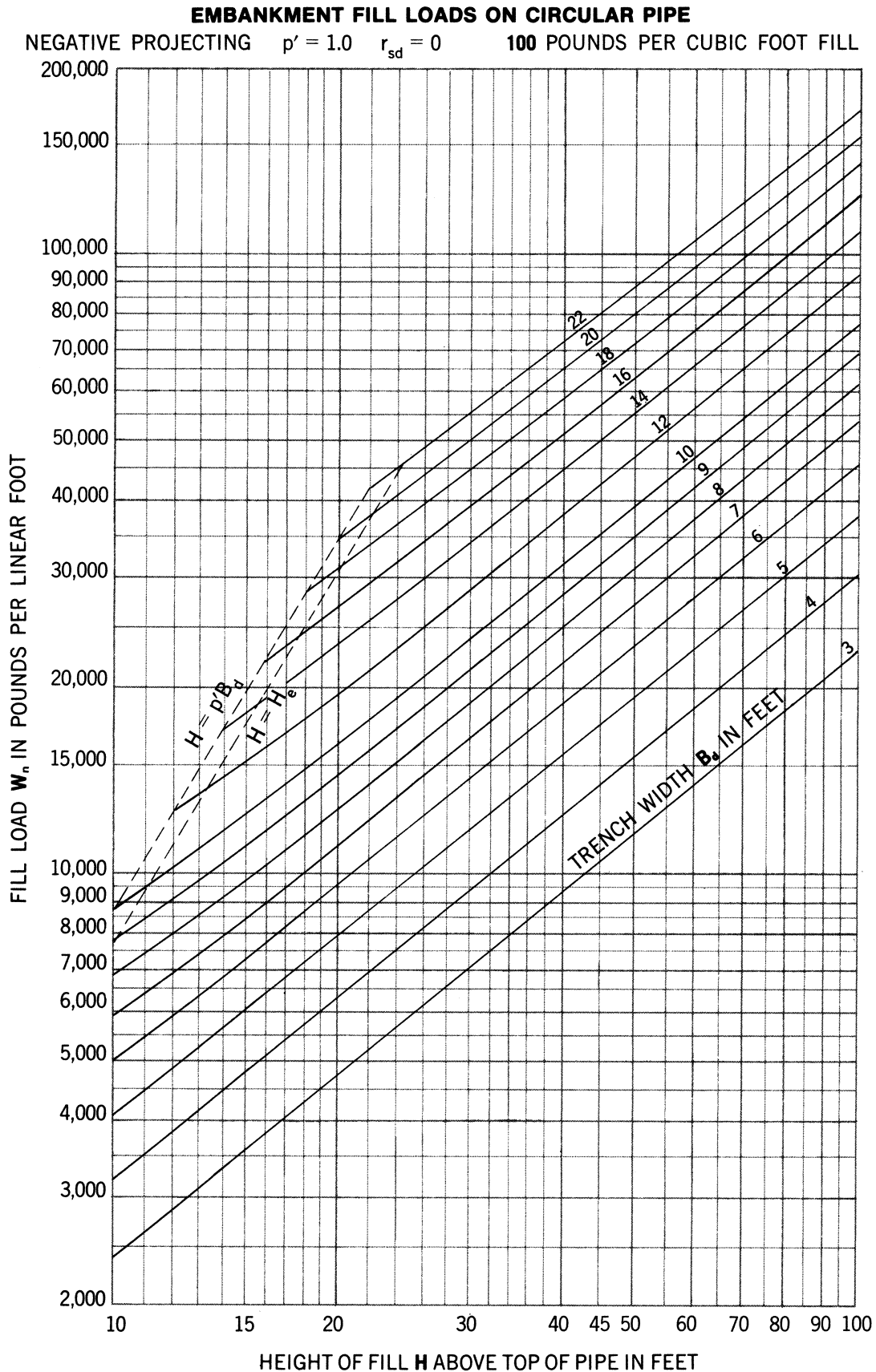
For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate trench widths.

Figure 198



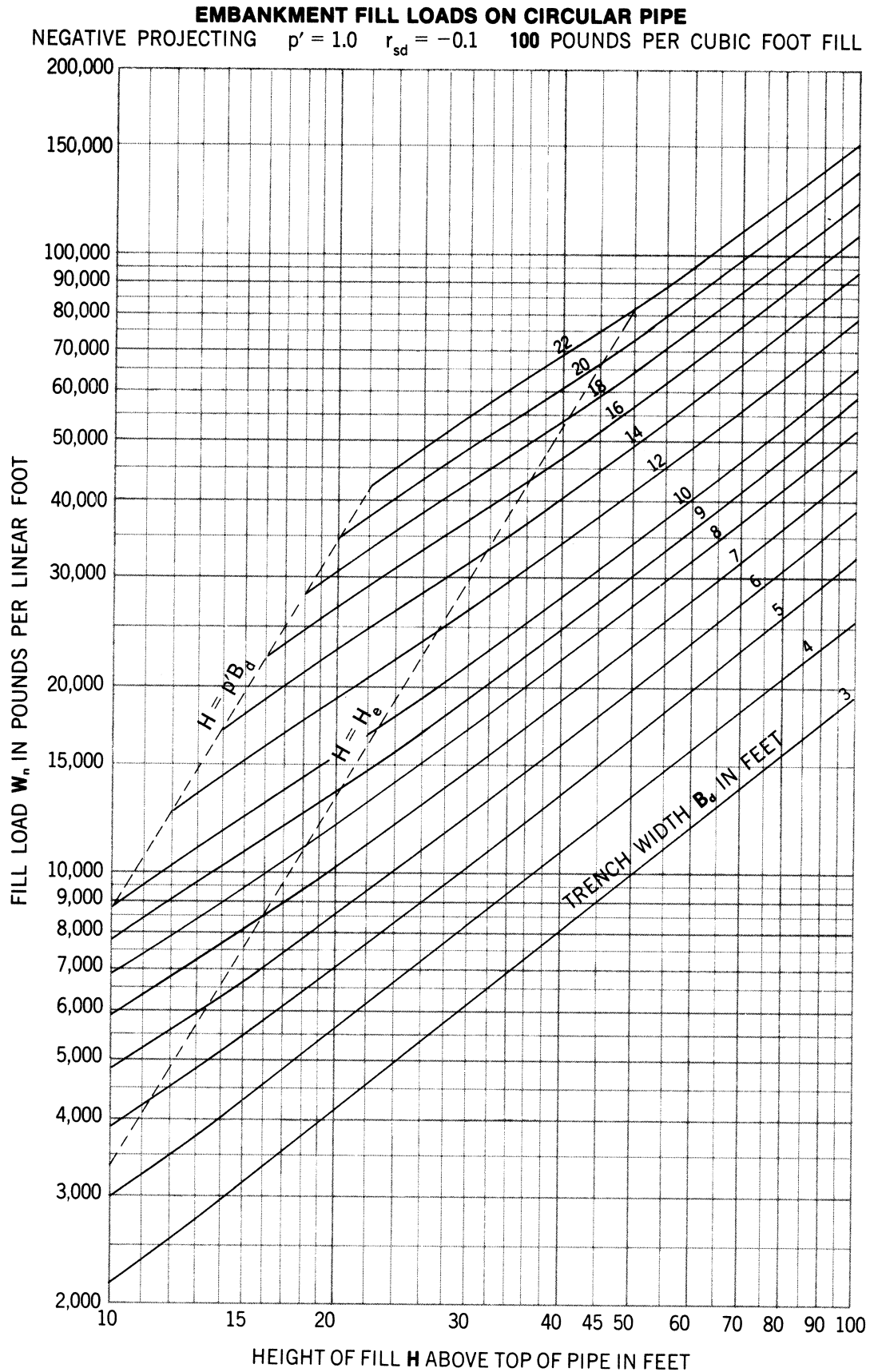
For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate trench widths.

Figure 199



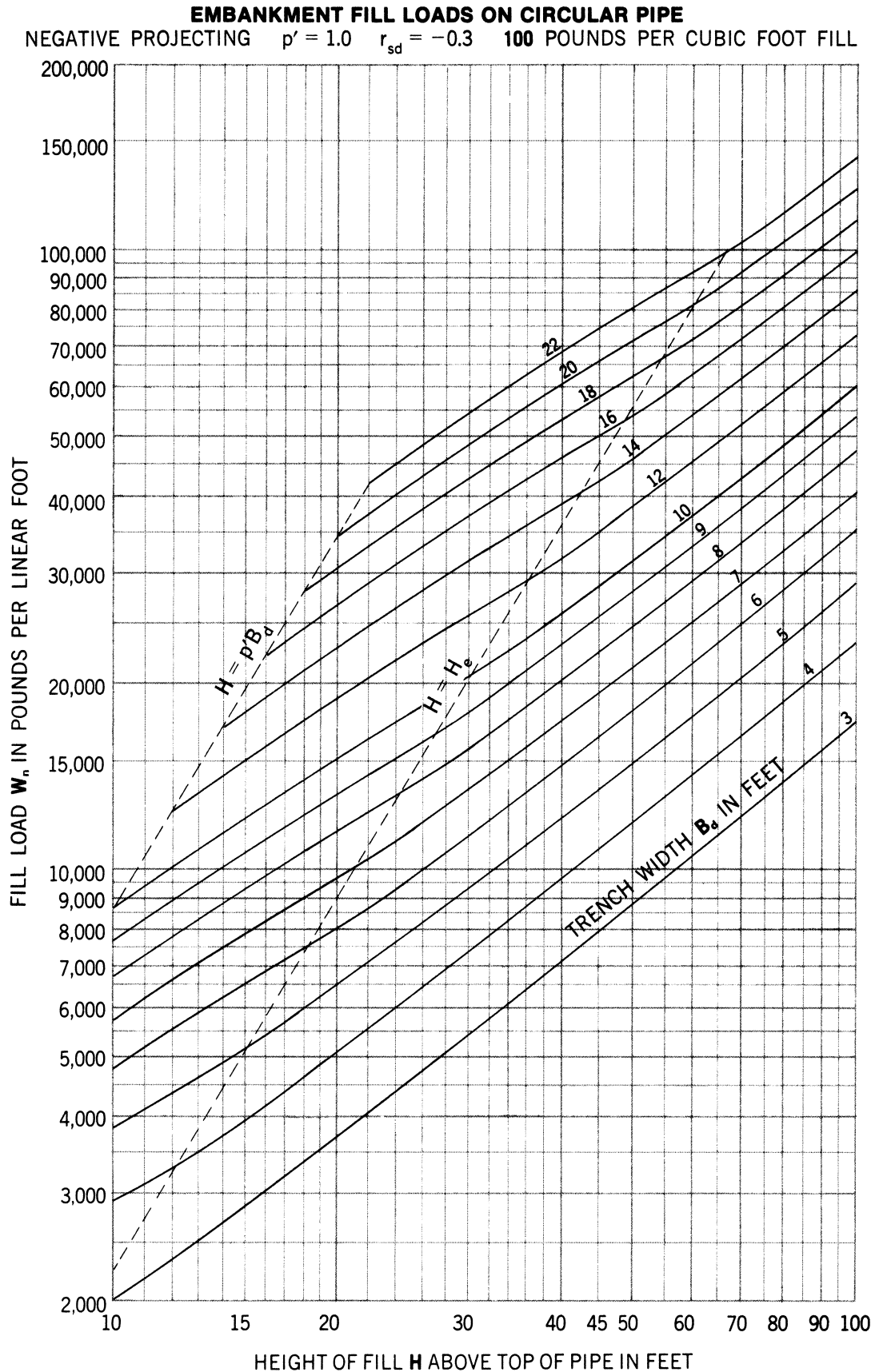
For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate trench widths.

Figure 200



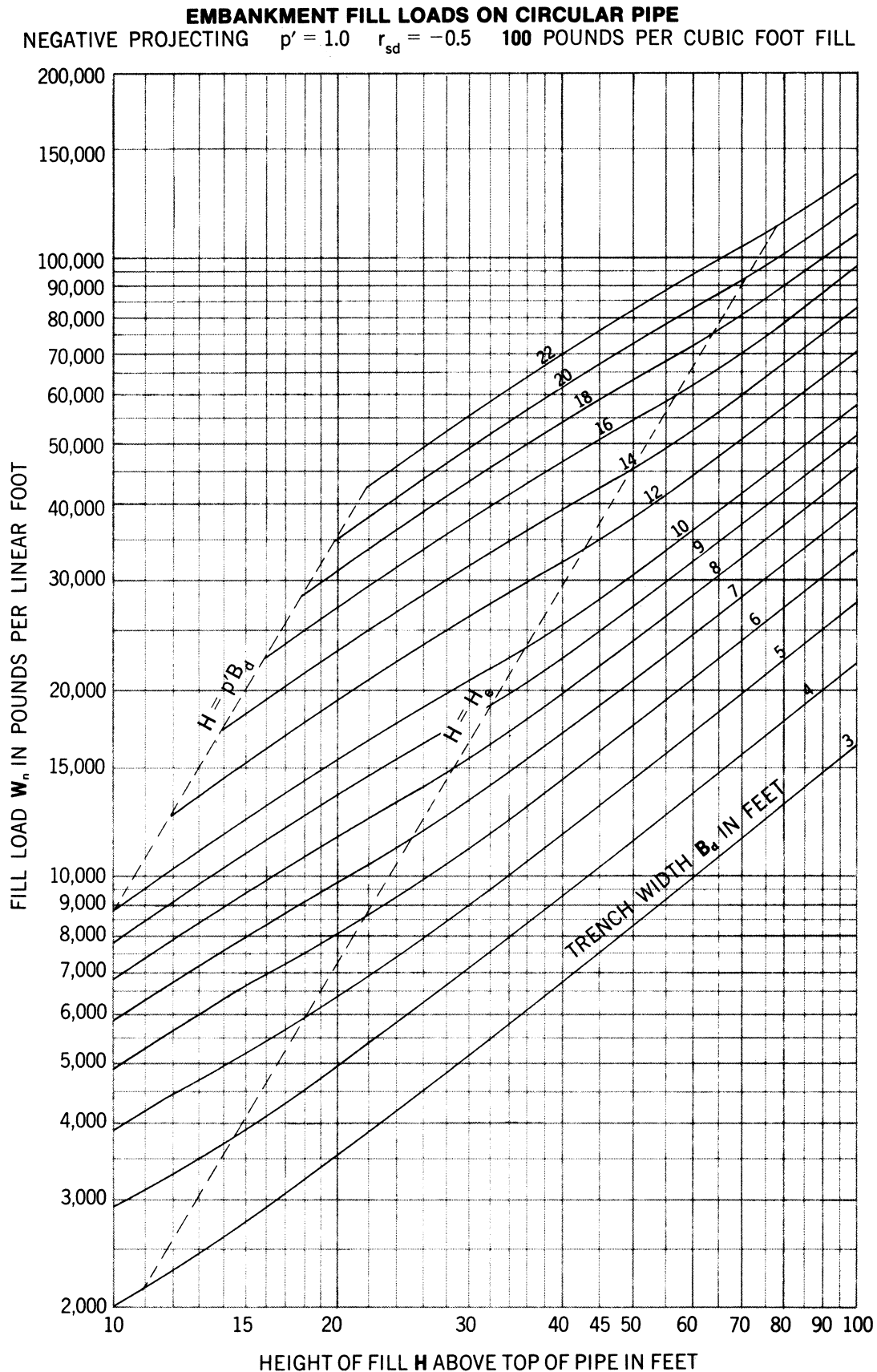
*For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate trench widths.*

Figure 201



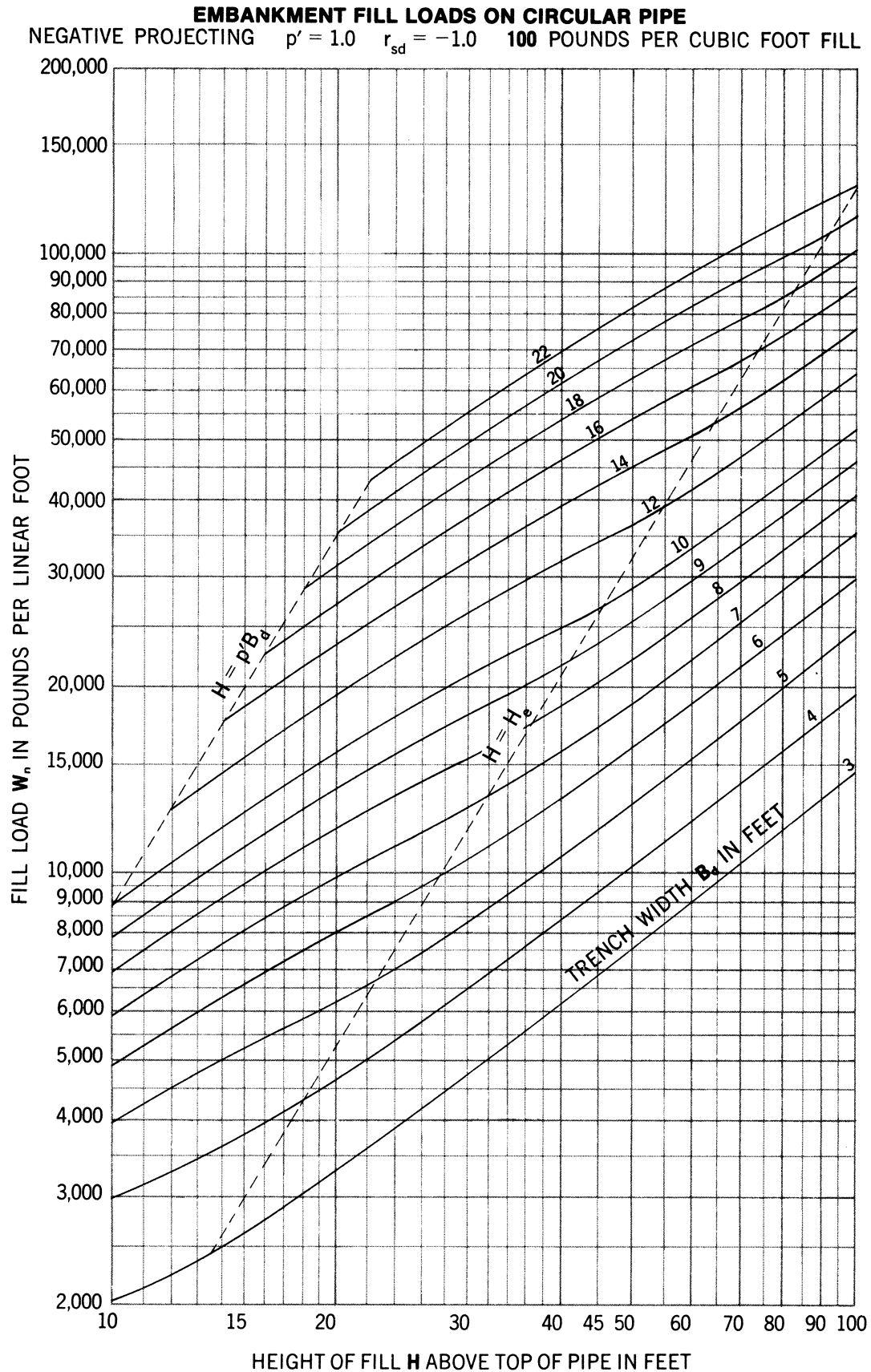
*For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate trench widths.*

Figure 202



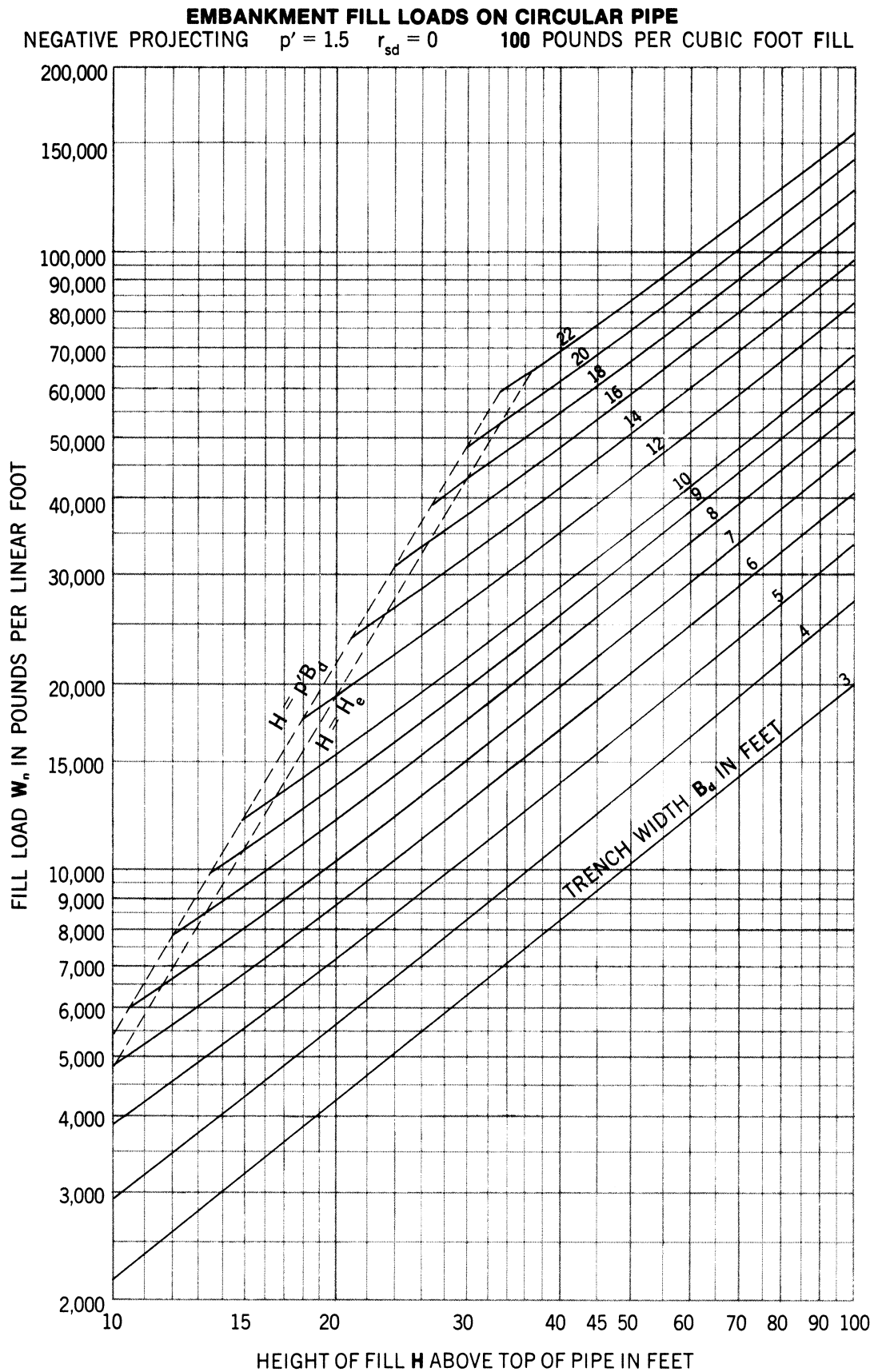
For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate trench widths.

Figure 203



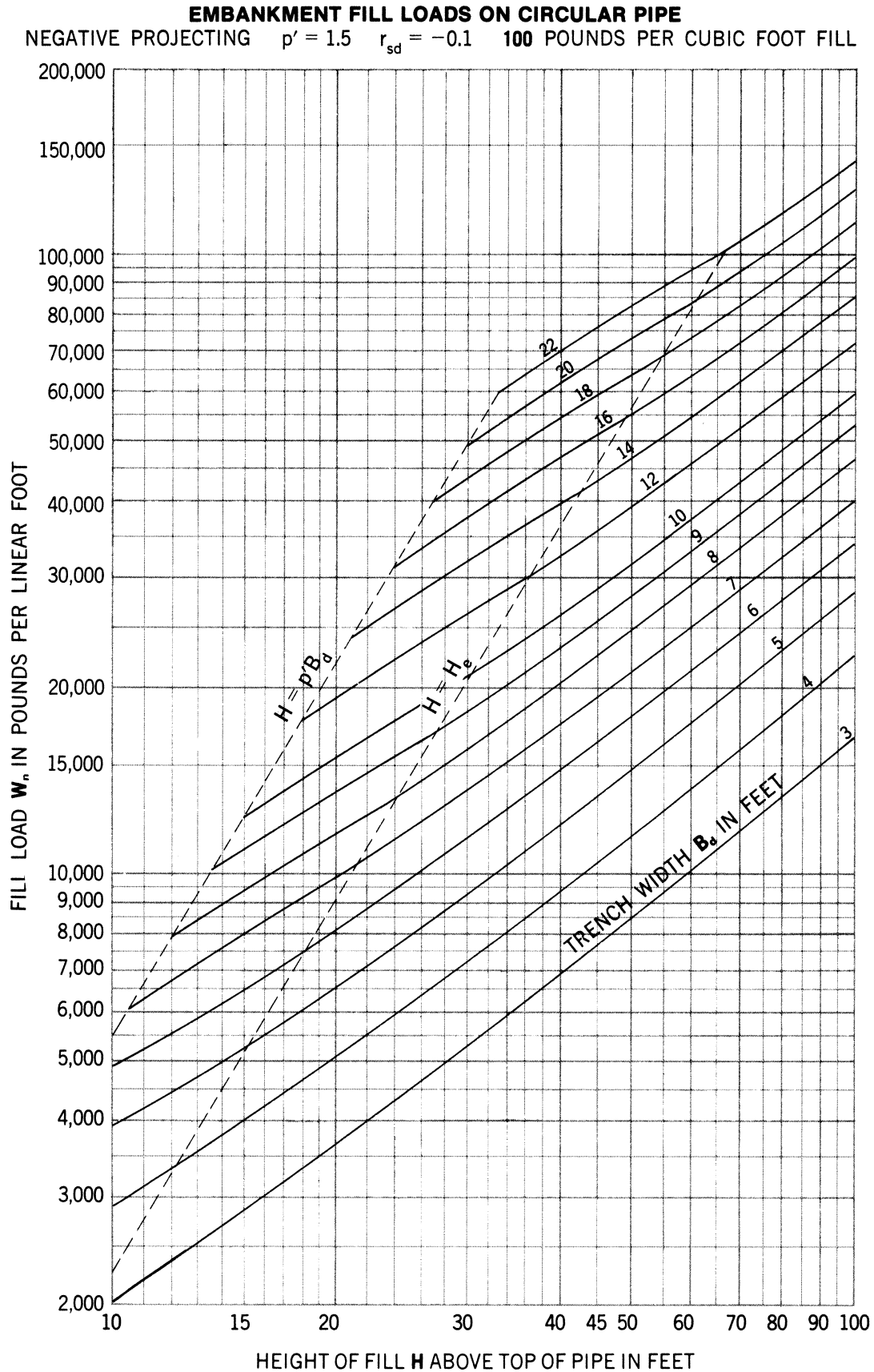
*For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate trench widths.*

Figure 204



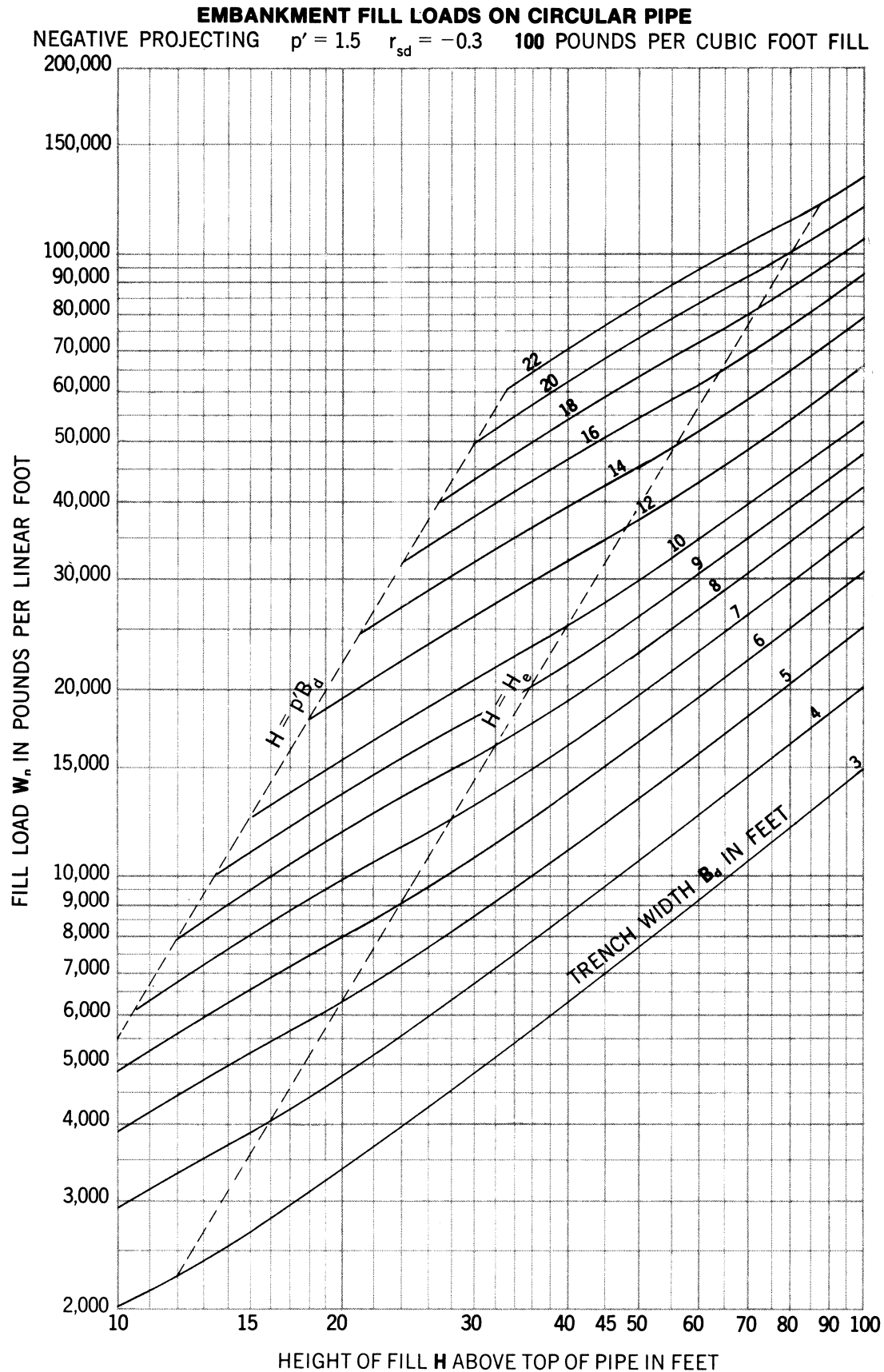
*For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate trench widths.*

Figure 205



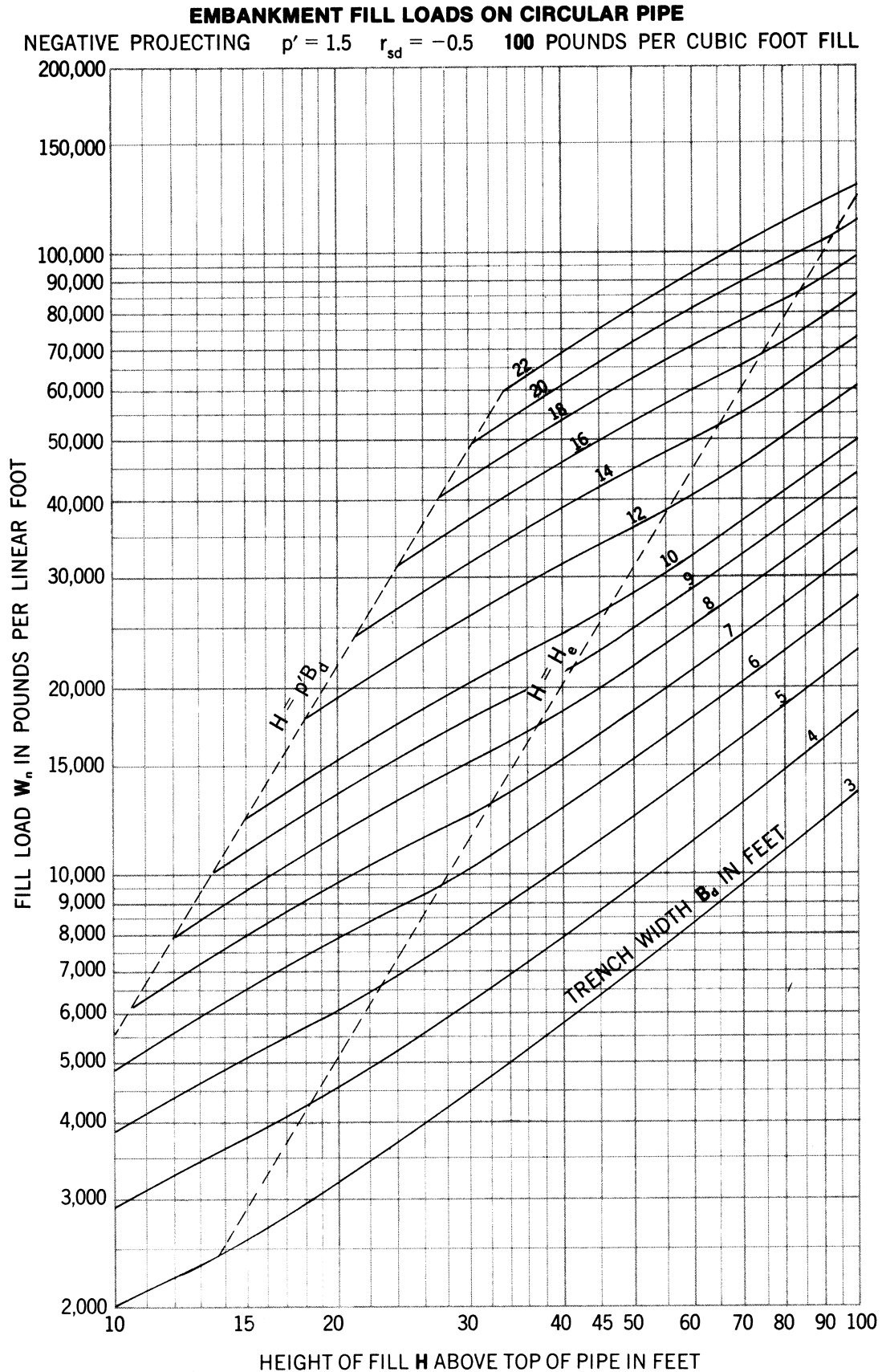
*For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate trench widths.*

Figure 206



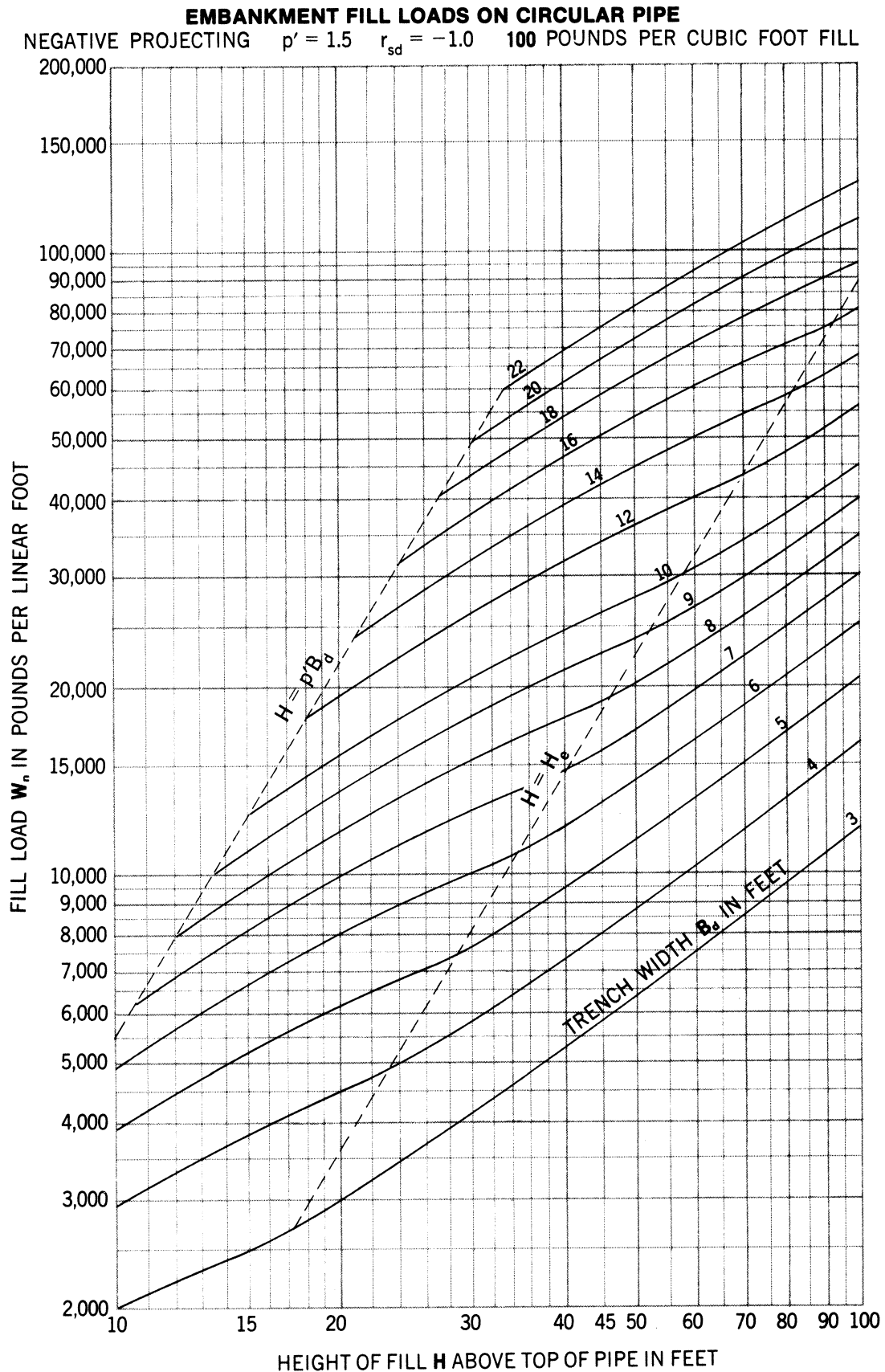
*For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate trench widths.*

Figure 207



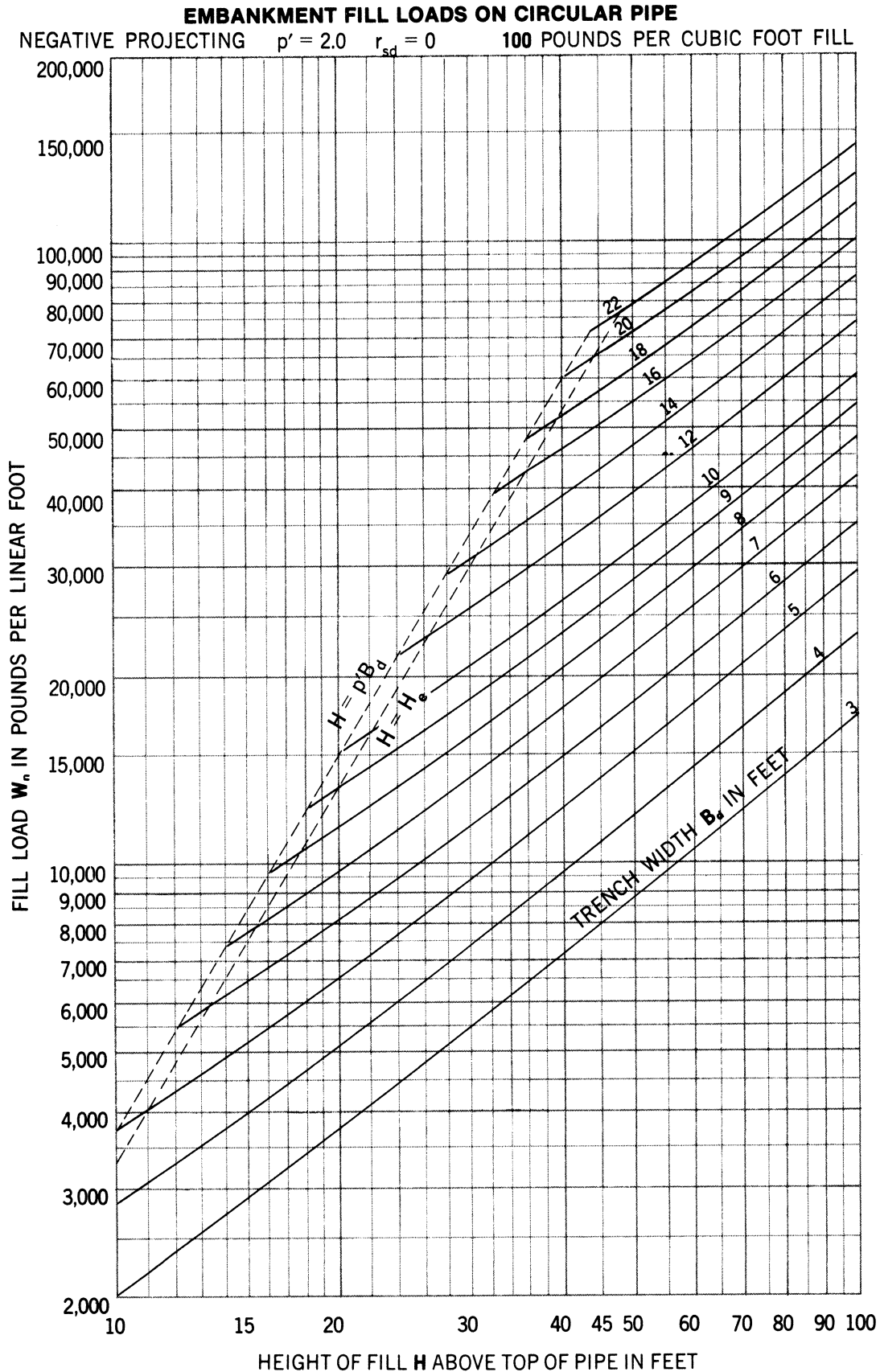
*For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate trench widths.*

Figure 208



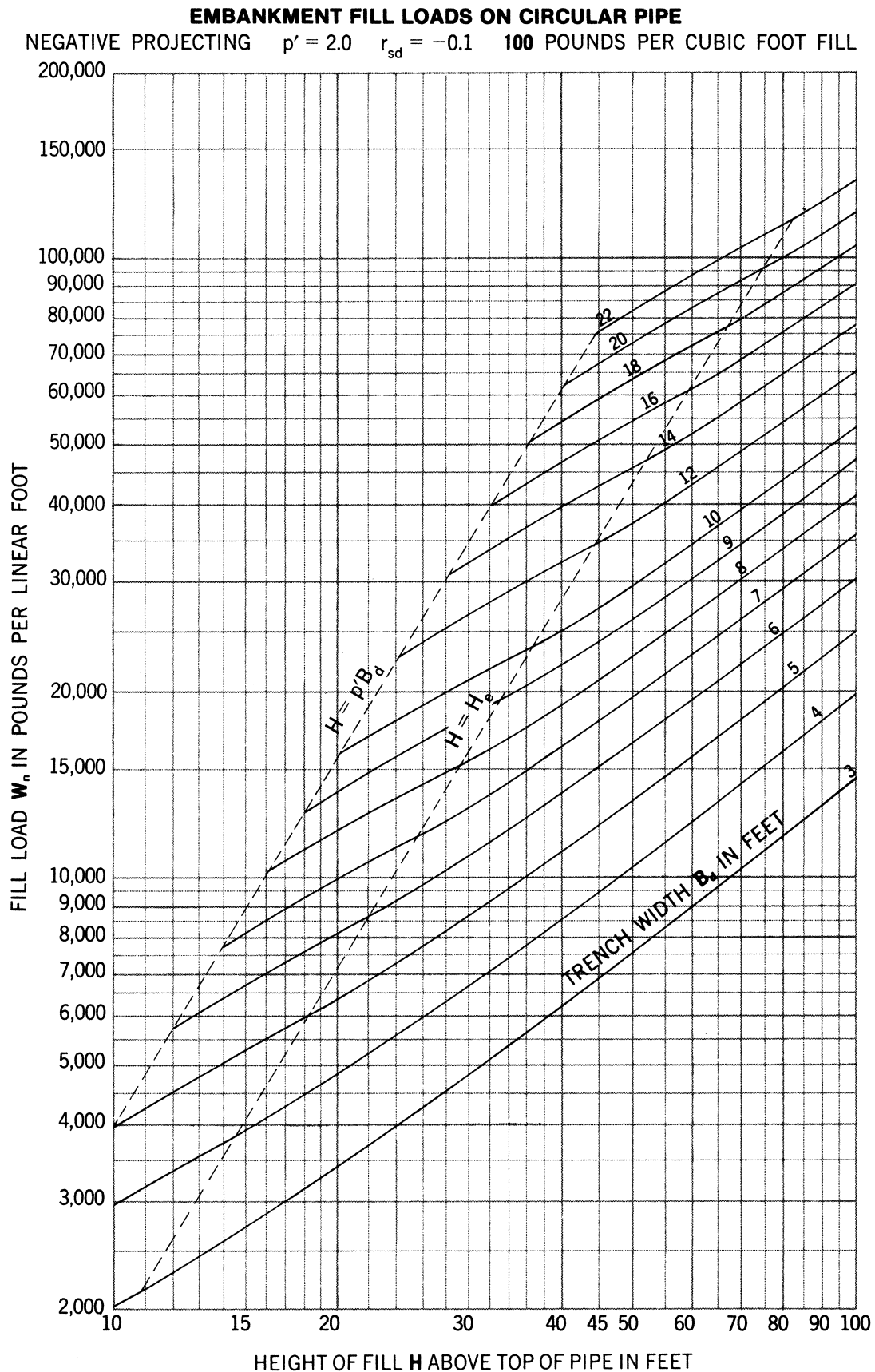
For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate trench widths.

Figure 209



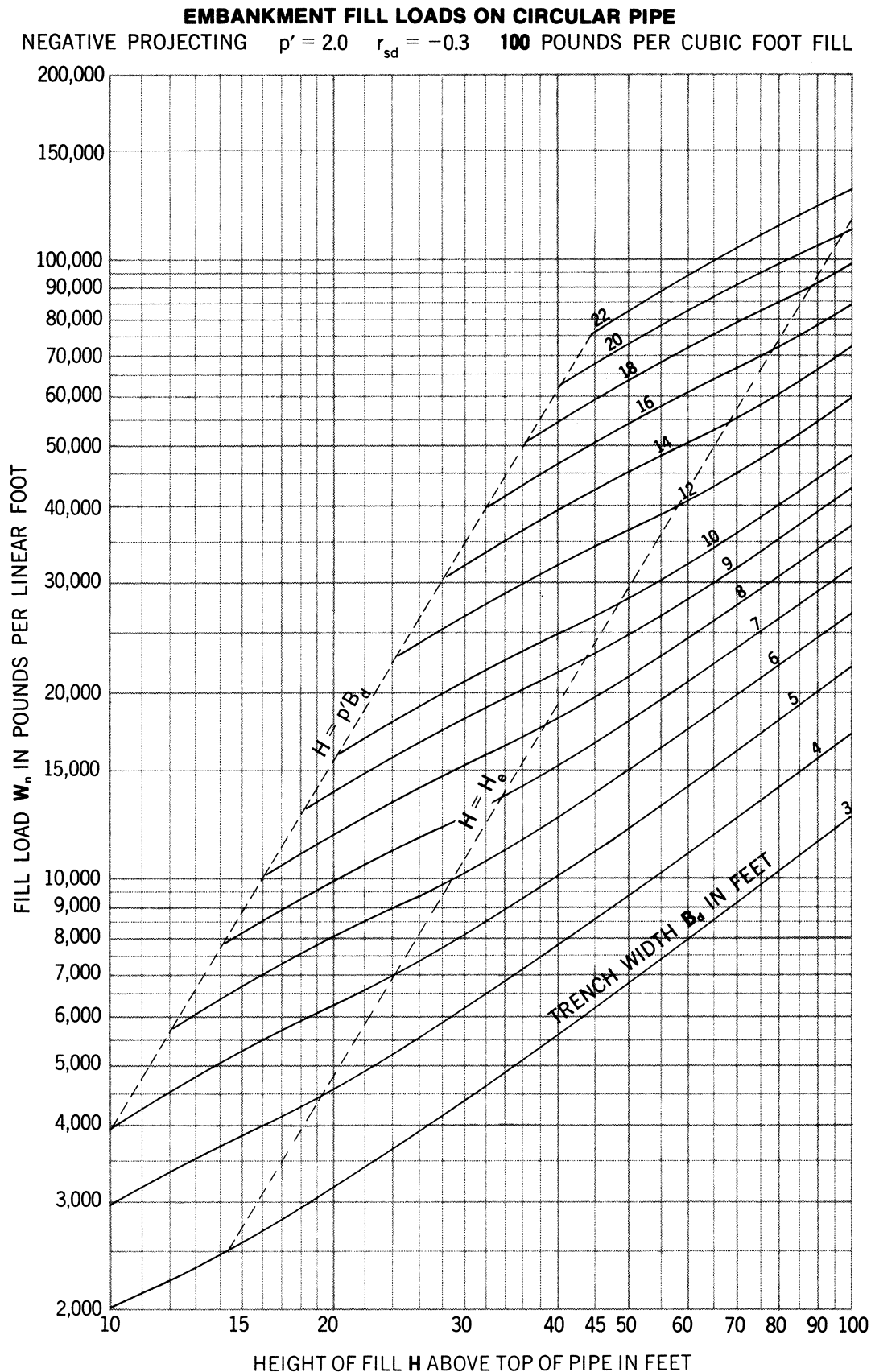
*For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate trench widths.*

Figure 210



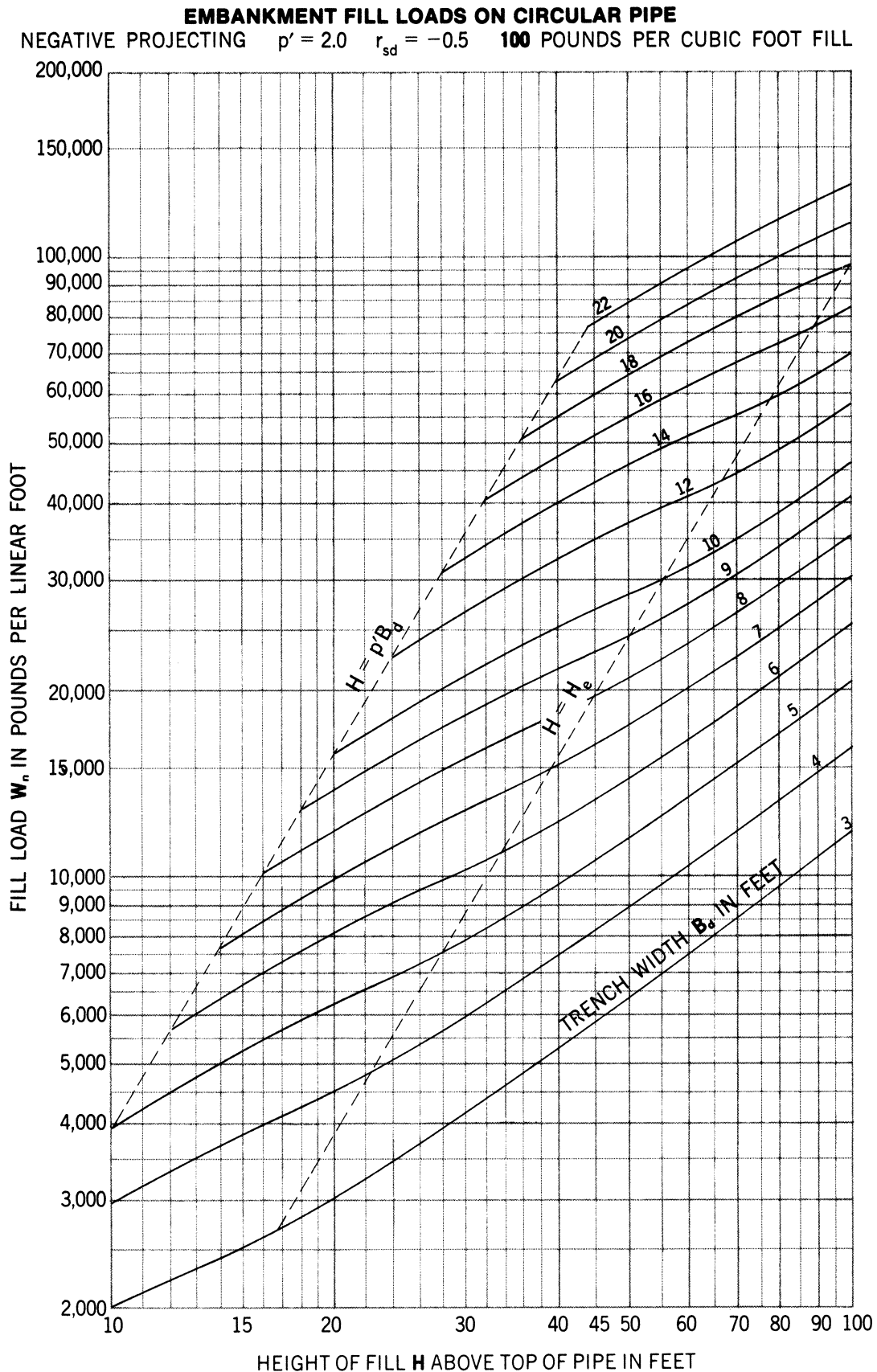
For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate trench widths.

Figure 211



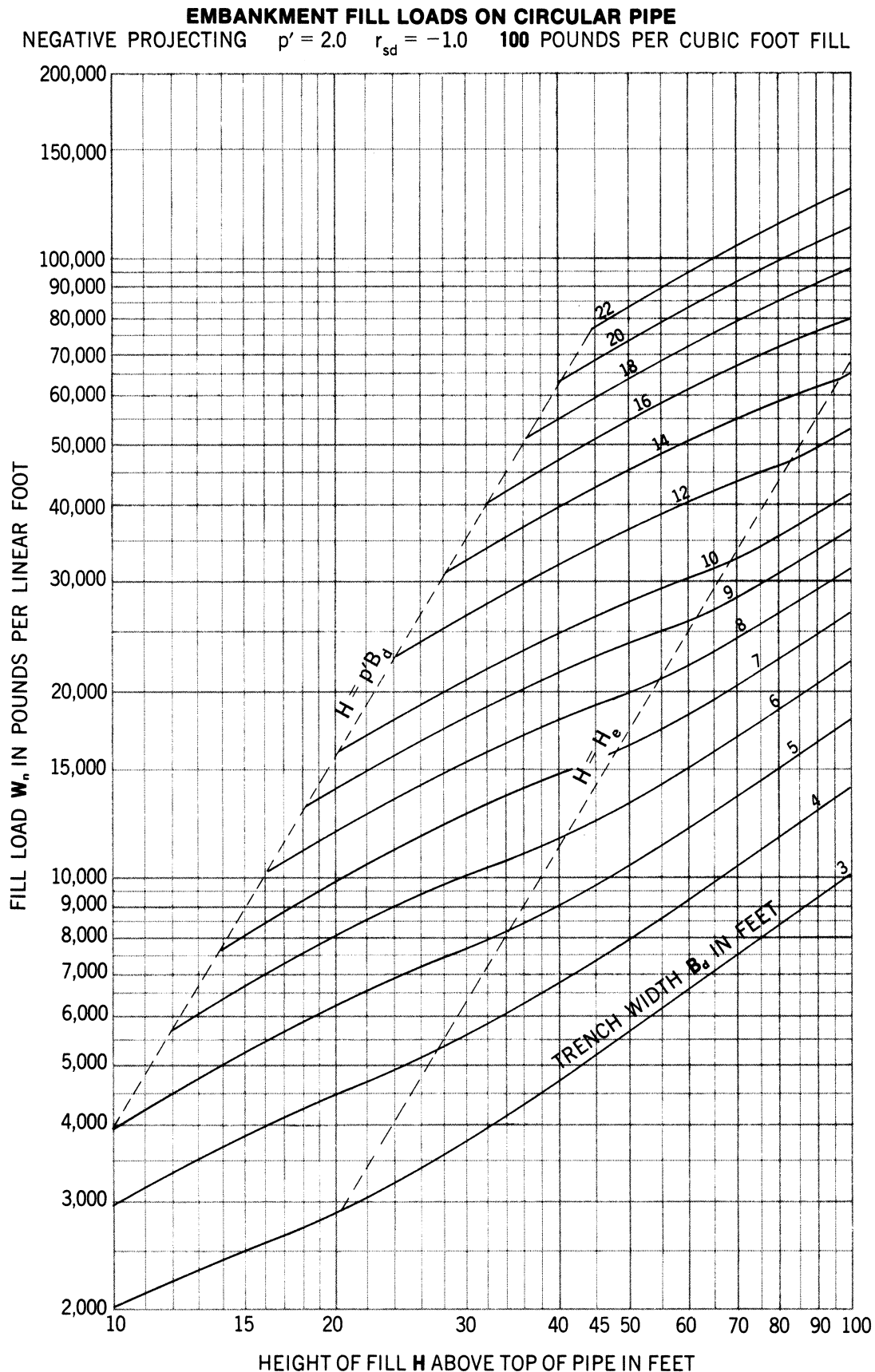
*For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate trench widths.*

Figure 212



For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc. Interpolate for intermediate trench widths.

Figure 213



For fill weighing 110 pounds per cubic foot, increase loads 10%; for 120 pounds increase 20%, etc.
 Interpolate for intermediate trench widths

Figure 214

LOAD COEFFICIENT DIAGRAM FOR TRENCH INSTALLATIONS

